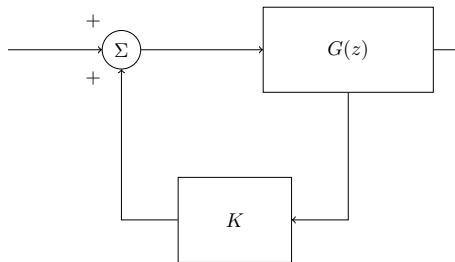


- 35) The system $\frac{900}{s(s+1)(s+9)}$ is to be compensated such that its gain-crossover frequency becomes same as its uncompensated phase-crossover frequency and provides a 45° phase margin. To achieve this, one may use
- a) A lag compensator that provides an attenuation of $20dB$ and a phase lag of 45° at the frequency of $3\sqrt{3}rad/s$ b) A lead compensator that provides an amplification of $20dB$ and a phase lead of 45° at the frequency of $3rad/s$
- c) A lag-lead compensator that provides an amplification of $20dB$ and a phase lag of 45° at the frequency of $\sqrt{3}rad/s$ d) A lag-lead compensator that provides an attenuation of $20dB$ and a phase lead of 45° at the frequency of $3rad/s$
- 36) Consider the discrete-time system shown in the figure where the impulse response of $(G(z))$ is $g(0) = 0, g(1) = g(2) = 1, g(3) = g(4) = \dots = 0$. This system is stable for the range of values of K



- a) $\left[-1, \frac{1}{2}\right]$ b) $[-1, 1]$
- c) $\left[-\frac{1}{2}, 1\right]$ d) $\left[-\frac{1}{2}, 2\right]$
- 37) A signal $x(t)$ is given by

$$x(t) = \begin{cases} 1, & -\frac{T}{4} < t \leq \frac{3T}{4} \\ -1, & \frac{3T}{4} < t \leq \frac{7T}{4} \\ -x(t+T) \end{cases}$$

Which among the following gives the fundamental Fourier term of $x(t)$?

a) $\frac{4}{\pi} \cos\left(\frac{\pi t}{T} - \frac{\pi}{4}\right)$

b) $\frac{\pi}{4} \cos\left(\frac{\pi t}{2T} + \frac{\pi}{4}\right)$

c) $\frac{4}{\pi} \sin\left(\frac{\pi t}{T} - \frac{\pi}{4}\right)$

d) $\frac{\pi}{4} \sin\left(\frac{\pi t}{2T} + \frac{\pi}{4}\right)$

38) If the loop gain K of a negative feedback system having a loop transfer function $\left[K \frac{(s+3)}{(s+8)^2}\right]$ is to be adjusted to induce a sustained oscillation then

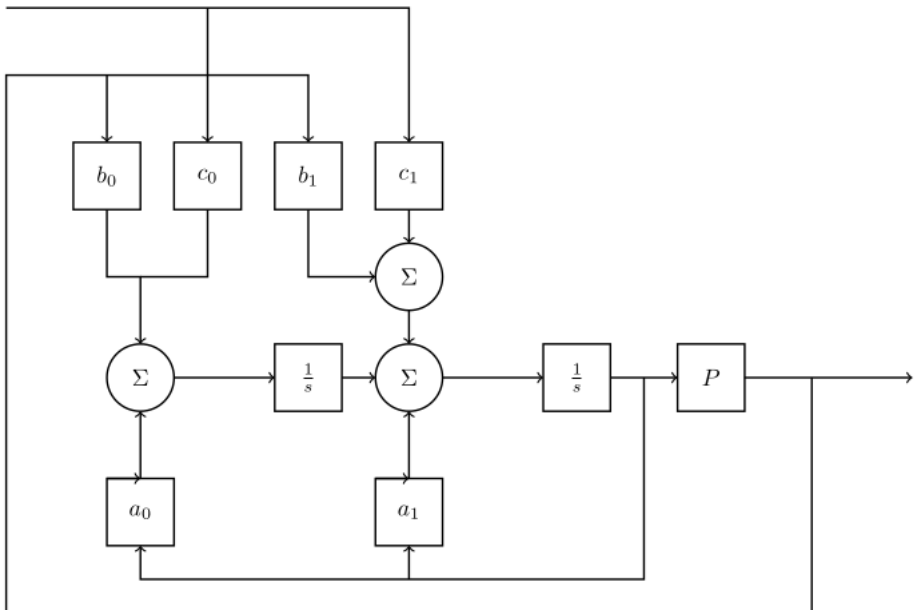
a) The frequency of this oscillation must be $\frac{4}{\sqrt{3}} \text{ rad/s}$

b) The frequency of this oscillation must be 4 rad/s

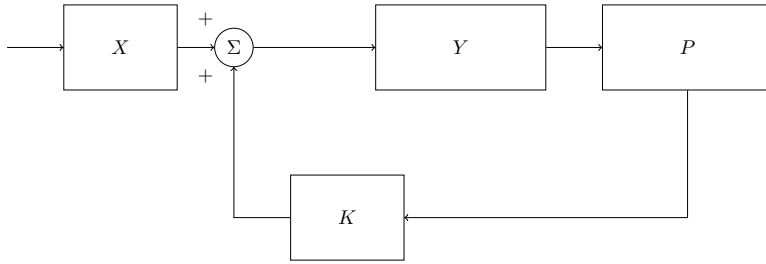
c) The frequency of this oscillation must be 4 or $\frac{4}{\sqrt{3}} \text{ rad/s}$

d) such a K does not exist

39) The system shown in the figure below,



can be reduced to the form,



a)

$$\begin{aligned}
 X &= c_0 s + c_1 \\
 Y &= \frac{1}{(s^2 + a_0 s + a_1)} \\
 Z &= b_0 s + b_1
 \end{aligned}$$

b)

$$\begin{aligned}
 X &= 1 \\
 Y &= \frac{(c_0 s + c_1)}{(s^2 + a_0 s + a_1)} \\
 Z &= b_0 s + b_1
 \end{aligned}$$

c)

$$\begin{aligned}
 X &= c_0 s + c_1 \\
 Y &= \frac{(b_1 s + b_0)}{(s^2 + a_1 s + a_0)} \\
 Z &= 1
 \end{aligned}$$

d)

$$\begin{aligned}
 X &= c_0 s + c_1 \\
 Y &= \frac{1}{(s^2 + a_1 s + a_0)} \\
 Z &= b_1 s + b_0
 \end{aligned}$$

40) The value of $\oint_C \frac{dz}{(1+z^2)}$, where C is the contour $|z - \frac{i}{2}| = 1$ is

a) $2\pi i$

b) π

c) $\tan^{-1} z$

d) $\pi.i.\tan^{-1} z$

41) A single-phase voltage source inverter is controlled in a single pulse-width modulated mode with a pulse width of 150° in each half cycle. Total harmonic distortion is defined as $\text{THD} = \frac{\sqrt{V_{rms}^2 - V_1^2}}{V_1} \times 100$, where V_1 is the rms value of the fundamental component of the output voltage. The THD of output ac voltage waveform is

a) 65.65%

b) 48.42%

c) 31.83%

d) 30.49%

42) A voltage source inverter is used to control the speed of a three-phase, 50Hz, squirrel cage induction motor. Its slip for rated torque is 4%. The flux is maintained at the

c) $\frac{1}{2}(t-1)u(t-1)$

d) None of the above