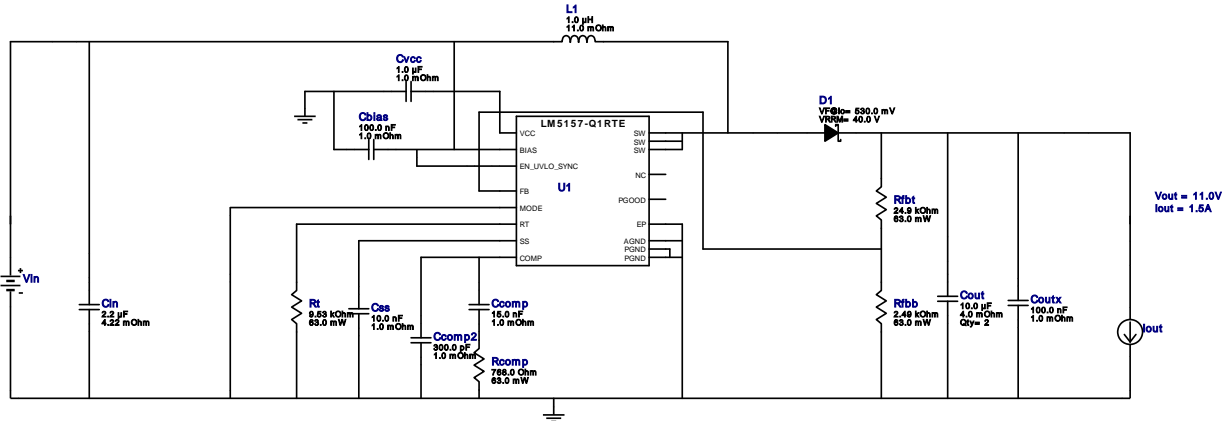


WEBENCH® Design Report

Design : 2 XLM5157QRTERQ1
XLM5157QRTERQ1 4.5V-5.5V to 11.00V @ 1.5A










Design Alerts

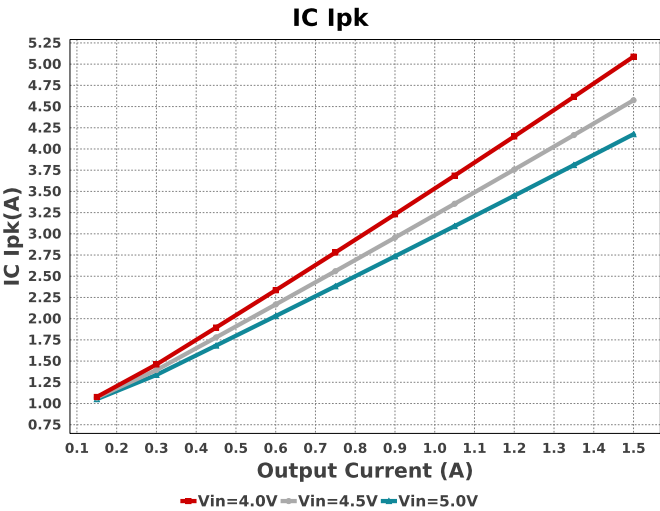
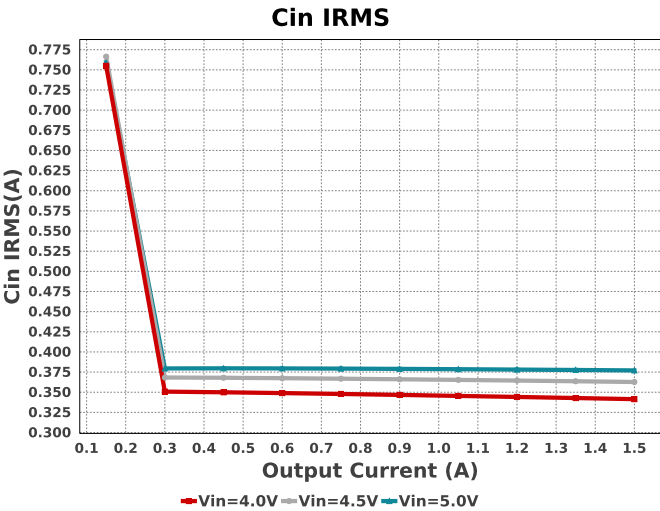
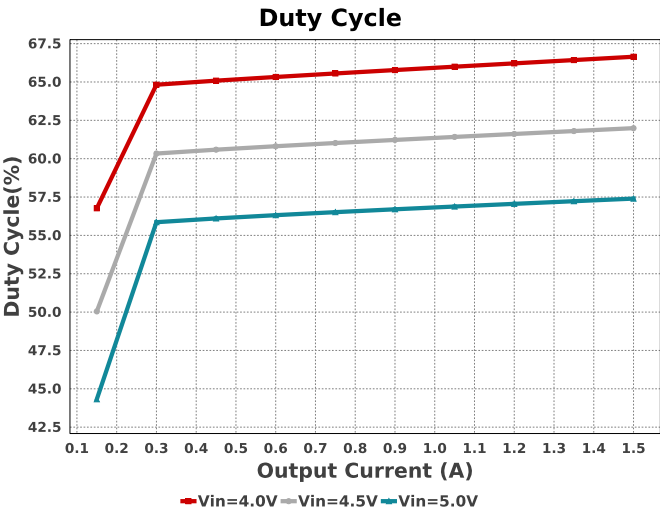
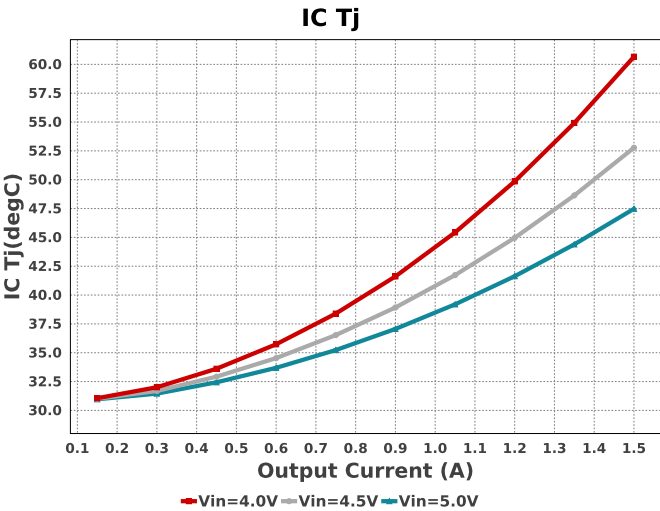
Component Selection Information

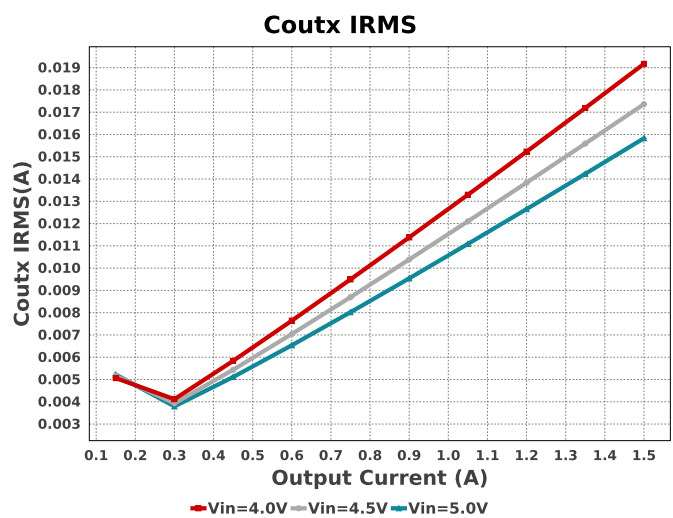
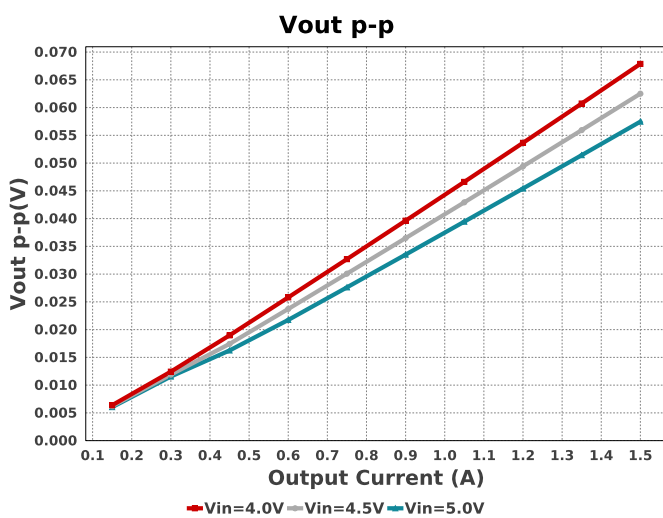
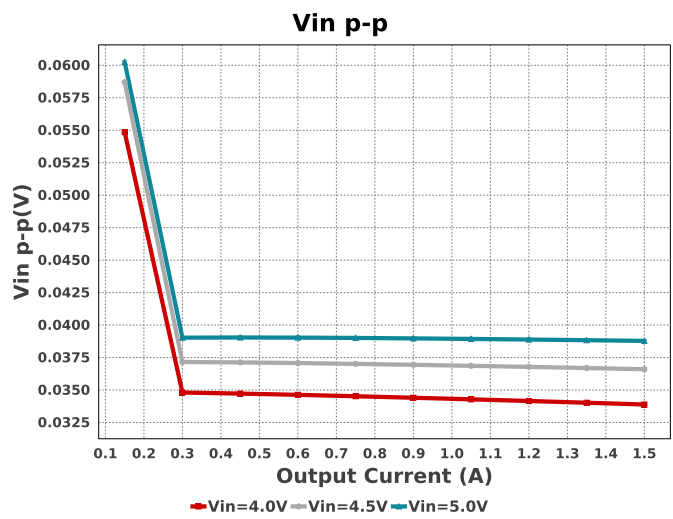
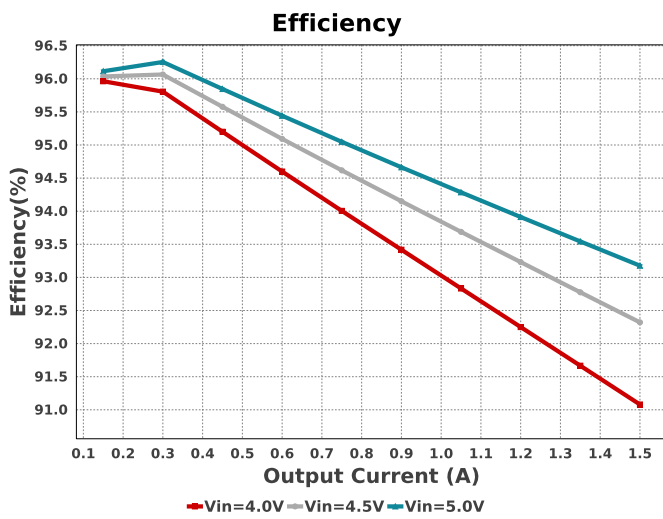
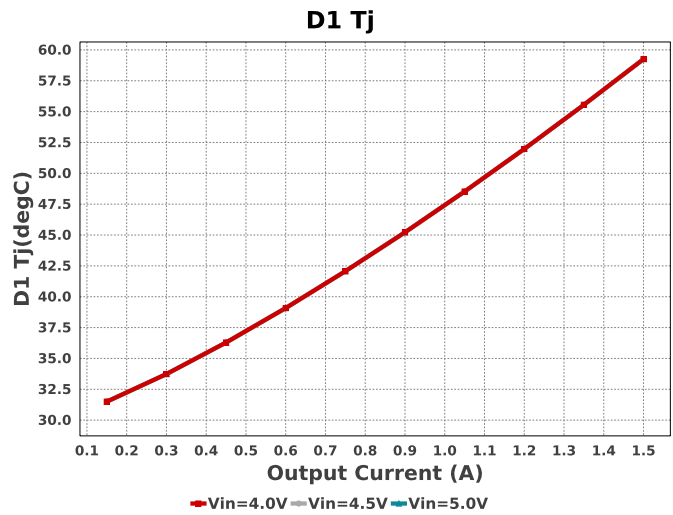
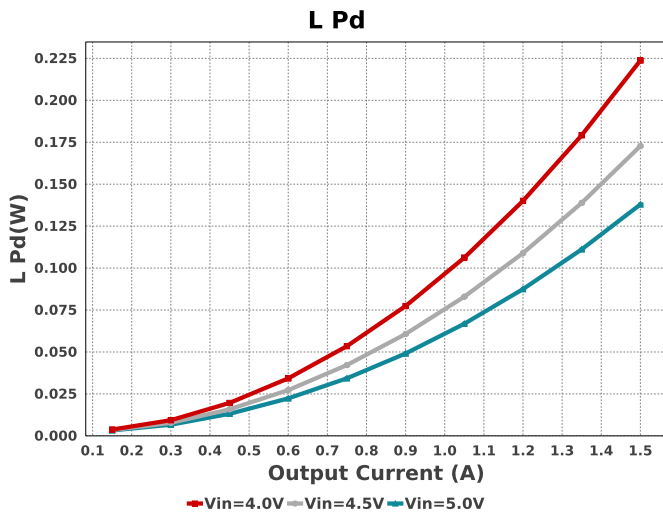
The LM5157-Q1 is qualified for Automotive applications. All passives and other components selected in this design may not be qualified for Automotive applications. The user is required to verify that all components in the design meet the qualification and safety requirements for their specific application.

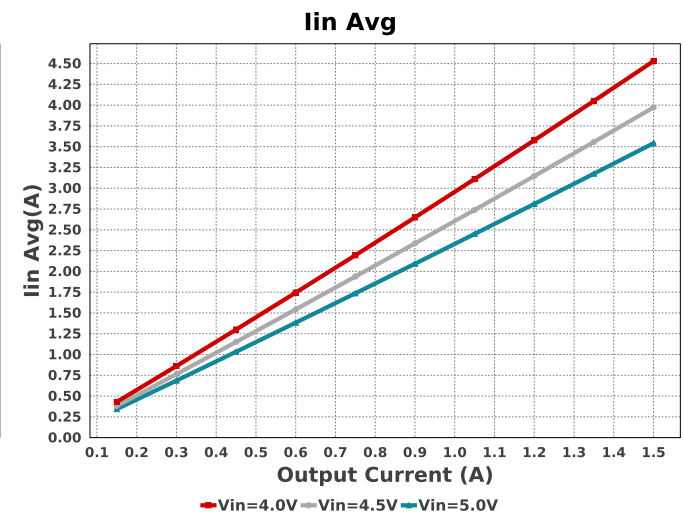
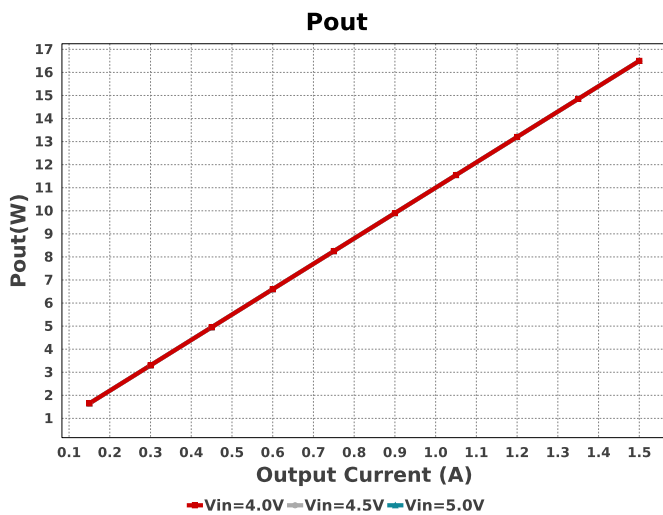
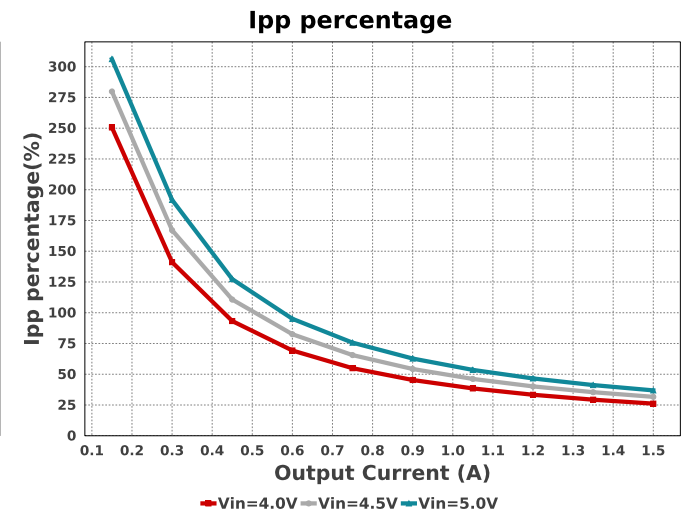
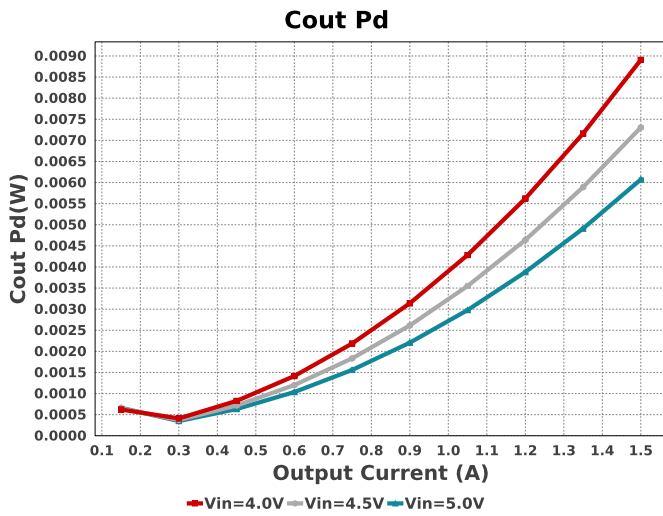
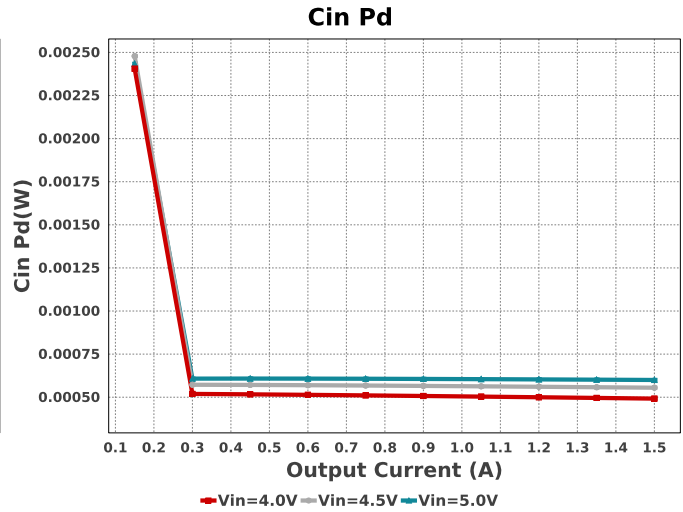
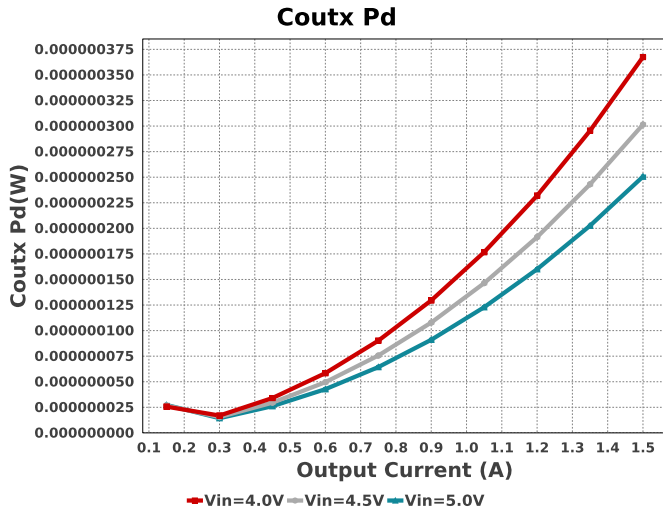
Electrical BOM

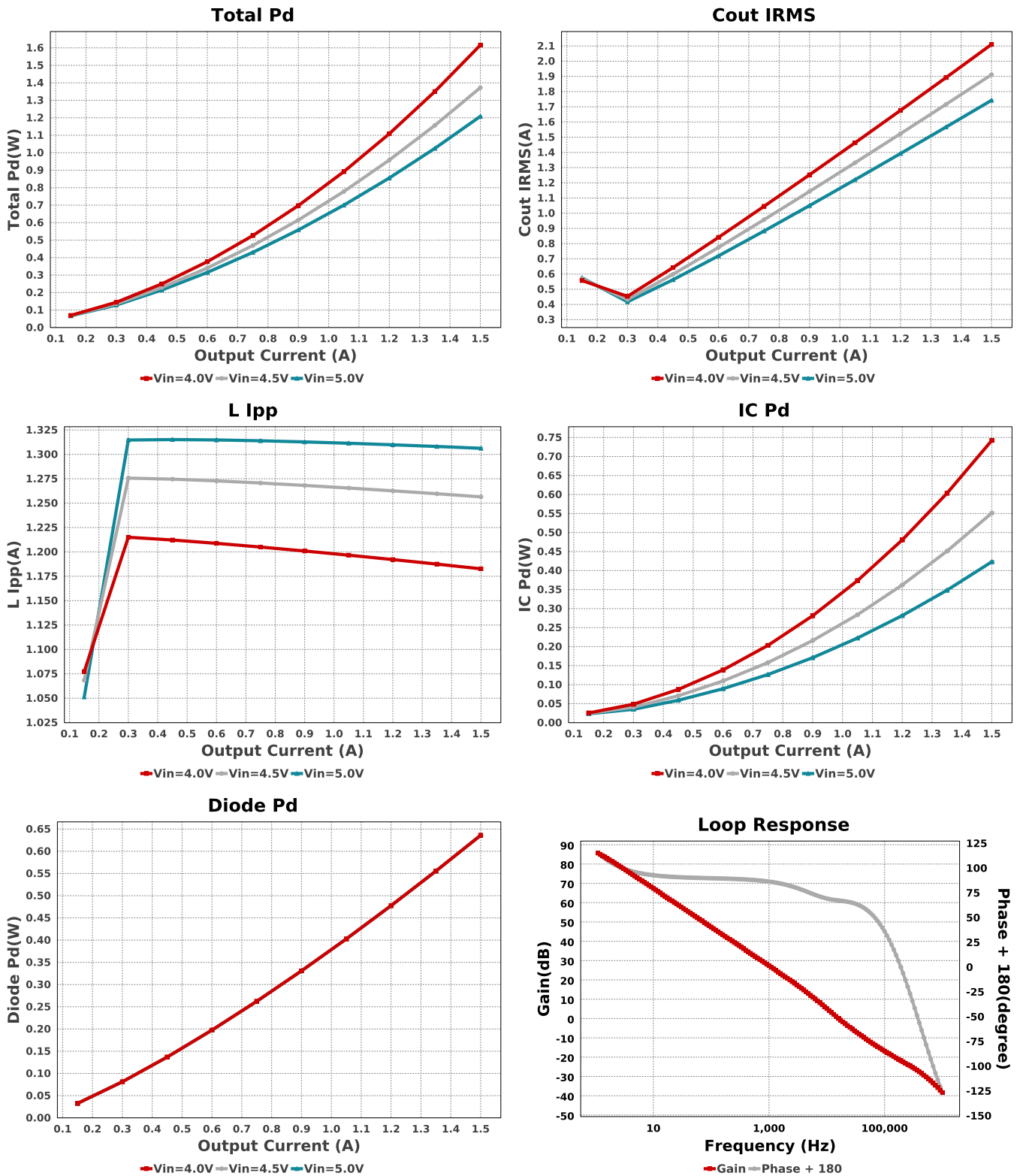
Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cbias	MuRata	GRM155R71A104KA01D Series= X7R	Cap= 100.0 nF ESR= 1.0 mOhm VDC= 10.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Ccomp	MuRata	GRM155R71C153KA01D Series= X7R	Cap= 15.0 nF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Ccomp2	MuRata	GRM1555C1E301JA01D Series= C0G/NP0	Cap= 300.0 pF ESR= 1.0 mOhm VDC= 25.0 V IRMS= 0.0 A	1	\$0.02	0402 3 mm ²
Cin	MuRata	GRM21BR71A225KA01L Series= X7R	Cap= 2.2 uF ESR= 4.22 mOhm VDC= 10.0 V IRMS= 2.08454 A	1	\$0.03	0805 7 mm ²
Cout	MuRata	GRM31CR71E106KA12L Series= X7R	Cap= 10.0 uF ESR= 4.0 mOhm VDC= 25.0 V IRMS= 6.0 A	2	\$0.06	1206_180 11 mm ²
Coutx	MuRata	GRM155R71C104KA88D Series= X7R	Cap= 100.0 nF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.01	0402 3 mm ²
Css	MuRata	GRM033R70J103KA01D Series= X7R	Cap= 10.0 nF ESR= 1.0 mOhm VDC= 6.3 V IRMS= 0.0 A	1	\$0.01	0201 2 mm ²

Name	Manufacturer	Part Number	Properties	Qty	Price	Footprint
Cvcc	Taiyo Yuden	EMK107B7105KA-T Series= X7R	Cap= 1.0 uF ESR= 1.0 mOhm VDC= 16.0 V IRMS= 0.0 A	1	\$0.01	 0603 5 mm²
D1	International Rectifier	30BQ040TRPBF	VF@Io= 530.0 mV VRRM= 40.0 V	1	\$0.19	 SMC 83 mm²
L1	TDK	VLP8040T-1R0N	L= 1.0 uH 11.0 mOhm	1	\$0.22	 VLP8040 113 mm²
Rcomp	Vishay-Dale	CRCW0402768RFKED Series= CRCW..e3	Res= 768.0 Ohm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm²
Rfbb	Vishay-Dale	CRCW04022K49FKED Series= CRCW..e3	Res= 2.49 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm²
Rfbt	Vishay-Dale	CRCW040224K9FKED Series= CRCW..e3	Res= 24.9 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm²
Rt	Vishay-Dale	CRCW04029K53FKED Series= CRCW..e3	Res= 9.53 kOhm Power= 63.0 mW Tolerance= 1.0%	1	\$0.01	 0402 3 mm²
U1	Texas Instruments	XLM5157QRTERQ1	Switcher	1	\$0.90	RTE0016K 16 mm²









Operating Values

#	Name	Value	Category	Description
1.	Cin IRMS	343.203 mA	Capacitor	Input capacitor RMS ripple current
2.	Cin Pd	497.07 μ W	Capacitor	Input capacitor power dissipation
3.	Cout IRMS	2.149 A	Capacitor	Output capacitor RMS ripple current
4.	Cout Pd	9.236 mW	Capacitor	Output capacitor power dissipation
5.	D1 Tj	68.358 degC	Diode	D1 junction temperature
6.	Diode Pd	833.88 mW	Diode	Diode power dissipation
7.	IC Ipk	5.147 A	IC	Peak switch current in IC
8.	IC Pd	764.67 mW	IC	IC power dissipation
9.	IC Tj	61.581 degC	IC	IC junction temperature
10.	IC Tolerance	10.0 mV	IC	IC Feedback Tolerance
11.	ICThetaJA	41.3 degC/W	IC	IC junction-to-ambient thermal resistance

#	Name	Value	Category	Description
12.	I _{in} Avg	4.586 A	IC	Average input current
13.	I _{pp} percentage	25.927 %	Inductor	Inductor ripple current percentage (with respect to average inductor current)
14.	L I _{pp}	1.189 A	Inductor	Peak-to-peak inductor ripple current
15.	L P _d	229.31 mW	Inductor	Inductor power dissipation
16.	C _{in} P _d	497.07 μW	Power	Input capacitor power dissipation
17.	C _{out} P _d	9.236 mW	Power	Output capacitor power dissipation
18.	Diode P _d	833.88 mW	Power	Diode power dissipation
19.	IC P _d	764.67 mW	Power	IC power dissipation
20.	L P _d	229.31 mW	Power	Inductor power dissipation
21.	Total P _d	1.842 W	Power	Total Power Dissipation
22.	BOM Count	16	System	Total Design BOM count
23.	Cross Freq	13.581 kHz	System	Bode plot crossover frequency
24.	Duty Cycle	67.054 %	System	Duty cycle
25.	Efficiency	89.957 %	System	Steady state efficiency
26.	FootPrint	272.0 mm ²	System	Total Foot Print Area of BOM components
27.	Frequency	2.108 MHz	System	Switching frequency
28.	Gain Marg	-20.145 dB	System	Bode Plot Gain Margin
29.	I _{out}	1.5 A	System	I _{out} operating point
30.	Low Freq Gain	84.735 dB	System	Gain at 1Hz
31.	Mode	CCM	System	Conduction Mode
32.	Phase Marg	62.495 deg	System	Bode Plot Phase Margin
33.	P _{out}	16.5 W	System	Total output power
34.	Total BOM	\$1.57	System	Total BOM Cost
35.	V _{in}	4.0 V	System	V _{in} operating point
36.	V _{in} p-p	34.064 mV	System	Input Source ripple voltage
37.	V _{out}	11.0 V	System	Operational Output Voltage
38.	V _{out} Actual	11.0 V	System	V _{out} Actual calculated based on selected voltage divider resistors
39.	V _{out} Tolerance	2.855 %	System	V _{out} Tolerance based on IC Tolerance (no load) and voltage divider resistors if applicable
40.	V _{out} p-p	68.961 mV	System	Peak-to-peak output ripple voltage

Design Inputs

Name	Value	Description
I _{out}	1.5	Maximum Output Current
V _{in} Max	5.0	Maximum input voltage
V _{in} Min	4.0	Minimum input voltage
V _{out}	11.0	Output Voltage
base_pn	LM5157-Q1	Base Product Number
source	DC	Input Source Type
T _a	30.0	Ambient temperature

WEBENCH® Assembly

Component Testing

Some published data on components in datasheets such as Capacitor ESR and Inductor DC resistance is based on conservative values that will guarantee that the components always exceed the specification. For design purposes it is usually better to work with typical values. Since this data is not always available it is a good practice to measure the Capacitance and ESR values of C_{in} and C_{out} , and the inductance and DC resistance of $L1$ before assembly of the board. Any large discrepancies in values should be electrically simulated in WEBENCH to check for instabilities and thermally simulated in WebTHERM to make sure critical temperatures are not exceeded.

Soldering Component to Board

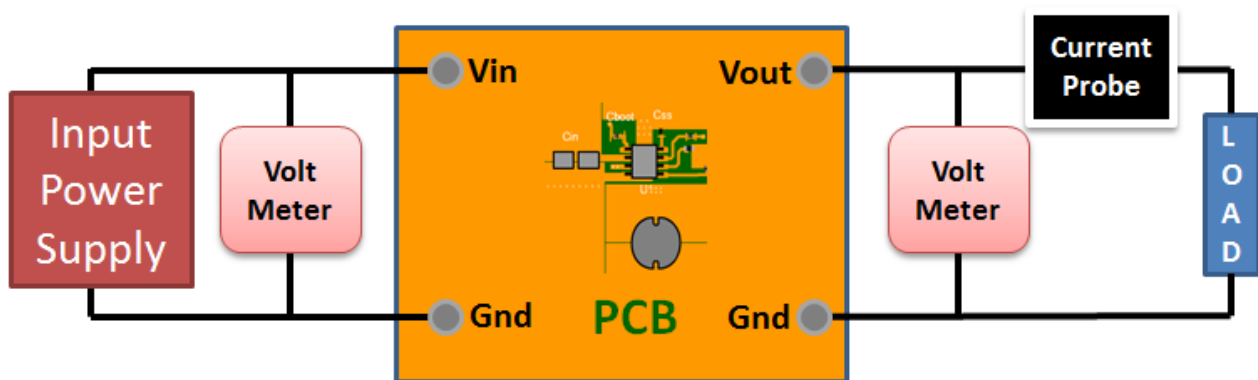
If board assembly is done in house it is best to tack down one terminal of a component on the board then solder the other terminal. For surface mount parts with large tabs, such as the DPAK, the tab on the back of the package should be pre-tinned with solder, then tacked into place by one of the pins. To solder the tab down to the board place the iron down on the board while resting against the tab, heating both surfaces simultaneously. Apply light pressure to the top of the plastic case until the solder flows around the part and the part is flush with the PCB. If the solder is not flowing around the board you may need a higher wattage iron (generally 25W to 30W is enough).

Initial Startup of Circuit

It is best to initially power up the board by setting the input supply voltage to the lowest operating input voltage 4.0V and set the input supply's current limit to zero. With the input supply off connect up the input supply to V_{in} and GND. Connect a digital volt meter and a load if needed to set the minimum load of the design from V_{out} and GND. Turn on the input supply and slowly turn up the current limit on the input supply. If the voltage starts to rise on the input supply continue increasing the input supply current limit while watching the output voltage. If the current increases on the input supply, but the voltage remains near zero, then there may be a short or a component misplaced on the board. Power down the board and visually inspect for solder bridges and recheck the diode and capacitor polarities. Once the power supply circuit is operational then more extensive testing may include full load testing, transient load and line tests to compare with simulation results.

Load Testing

The setup is the same as the initial startup, except that an additional digital voltmeter is connected between V_{in} and GND, a load is connected between V_{out} and GND and a current meter is connected in series between V_{out} and the load. The load must be able to handle at least rated output power + 50% (7.5 watts for this design). Ideally the load is supplied in the form of a variable load test unit. It can also be done in the form of suitably large power resistors. When using an oscilloscope to measure waveforms on the prototype board, the ground leads of the oscilloscope probes should be as short as possible and the area of the loop formed by the ground lead should be kept to a minimum. This will help reduce ground lead inductance and eliminate EMI noise that is not actually present in the circuit.



Design Assistance

1. Master key : 9A72BF0622A6C67039BB59A99E182A90[v1]
2. **LM5157-Q1** Product Folder : <http://www.ti.com/product/LM5157%2DQ1> : contains the data sheet and other resources.

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