Digital Control Systems Final CA

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Equilibrium point / Transfer function (p1)

Defining Variables

Equilibrium State

```
St_e = [0;0;0];
In_e = [n*Ib*V;0];
Fe = subs(subs(F,In,In_e),St,St_e);
```

Linearize

A =

Transfer Function

```
syms s
n = size(A,1);
Gp = C*inv(s*eye(n)-A)*B;
ExpFun = matlabFunction(simplifyFraction(Gp, 'Expand', true));
ExpFun = str2func(regexprep(func2str(ExpFun), '\.([/^\\*])', '$1'));
Gp = tf(ExpFun(tf('s')));
for i = 1:length(Gp)
    [num,den] = tfdata(Gp(i));
    Gp(i) = tf(num{1}/den{1}(1),den{1}/den{1}(1));
end
Gp = Gp(1)
Gp =
          -4.875e-06
  s^3 + 0.1173 s^2 + 0.002308 s
Continuous-time transfer function.
[Gp_Num, Gp_Den] = tfdata(Gp); Gp_Num = Gp_Num{1}; Gp_Den = Gp_Den{1};
```

Analog Control (p2)

```
%pidTuner
```

```
Gc = tf([-7.83 -0.001947],[1 0])
```

```
Gc =

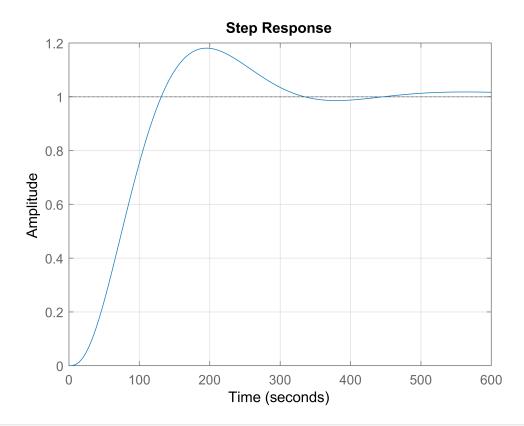
-7.83 s - 0.001947
-----s
```

Continuous-time transfer function.

trans_info = stepinfo(feedback(series(Gc,Gp),1))

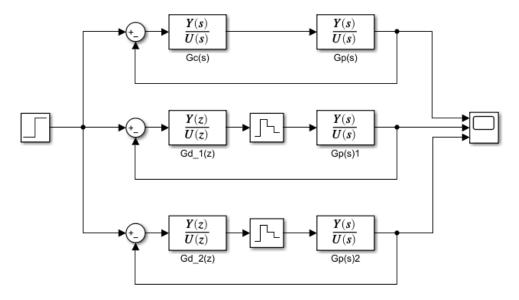
```
trans_info = struct with fields:
    RiseTime: 83.7907
SettlingTime: 312.4786
SettlingMin: 0.9142
SettlingMax: 1.1813
    Overshoot: 18.1258
Undershoot: 0
    Peak: 1.1813
PeakTime: 194.7882
```

```
step(feedback(series(Gc,Gp),1))
grid on
```



[Gc_Num, Gc_Den] = tfdata(Gc); Gc_Num = Gc_Num{1}; Gc_Den = Gc_Den{1};

Digital Control (P3)



```
% 2 < tr/Ts < 10
Ts = round(trans_info.RiseTime/6)</pre>
```

Ts = 14

```
Gd_1 = c2d(Gc,Ts,'tastin')
```

Gd_1 =

-7.844 z + 7.816

----z - 1

Sample time: 14 seconds
Discrete-time transfer function.

Gd_2 = c2d(Gc,Ts,'matched')

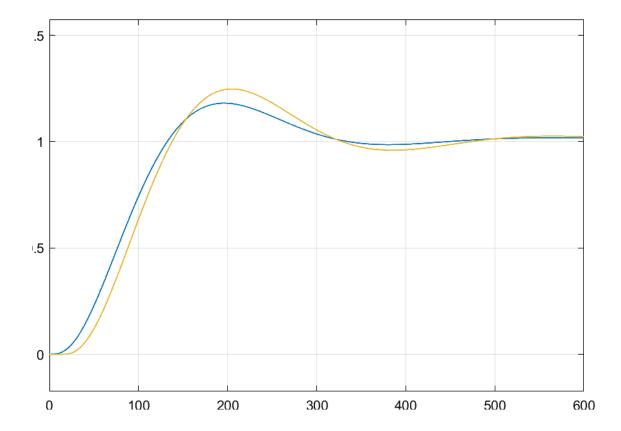
Gd_2 =

-7.844 z + 7.816

----z - 1

Sample time: 14 seconds
Discrete-time transfer function.

[Gd_Num_1, Gd_Den_1] = tfdata(Gd_1); Gd_Num_1 = Gd_Num_1{1}; Gd_Den_1 = Gd_Den_1{1};
[Gd_Num_2, Gd_Den_2] = tfdata(Gd_2); Gd_Num_2 = Gd_Num_2{1}; Gd_Den_2 = Gd_Den_2{1};



Ts = 4

Ts = 4

 $Gd_1 =$

Sample time: 4 seconds

Discrete-time transfer function.

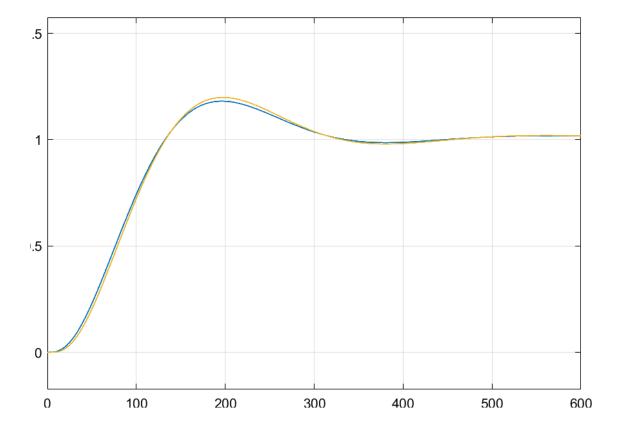
Gd_2 = c2d(Gc,Ts,'matched')

 $Gd_2 =$

Sample time: 4 seconds

Discrete-time transfer function.

```
[Gd_Num_1, Gd_Den_1] = tfdata(Gd_1); Gd_Num_1 = Gd_Num_1{1}; Gd_Den_1 = Gd_Den_1{1};
[Gd_Num_2, Gd_Den_2] = tfdata(Gd_2); Gd_Num_2 = Gd_Num_2{1}; Gd_Den_2 = Gd_Den_2{1};
```



Ts = 40

Ts = 40

Gd_1 = c2d(Gc,Ts,'tastin')

 $Gd_1 =$

Sample time: 40 seconds

Discrete-time transfer function.

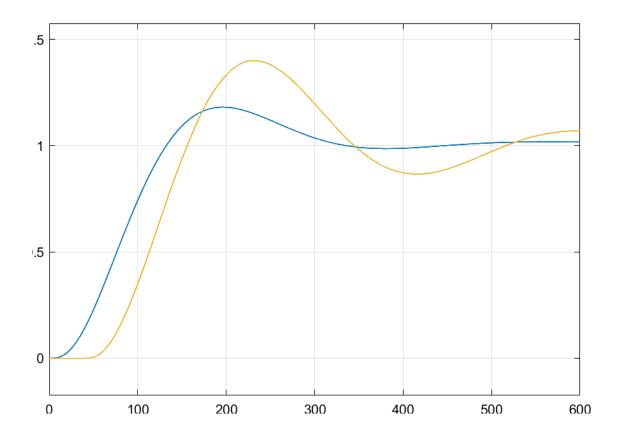
Gd_2 = c2d(Gc,Ts,'matched')

 $Gd_2 =$

Sample time: 40 seconds

Discrete-time transfer function.

```
[Gd_Num_1, Gd_Den_1] = tfdata(Gd_1); Gd_Num_1 = Gd_Num_1{1}; Gd_Den_1 = Gd_Den_1{1};
[Gd_Num_2, Gd_Den_2] = tfdata(Gd_2); Gd_Num_2 = Gd_Num_2{1}; Gd_Den_2 = Gd_Den_2{1};
```



Discrete Transfer Function (p4)

Using c2d in matlab:

```
Gp_d = c2d(Gp,Ts,'zoh')

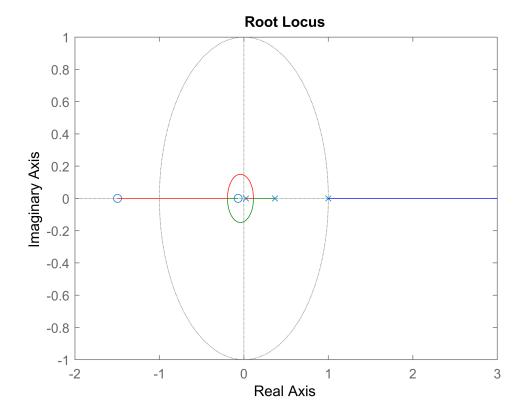
Gp_d =
```

Sample time: 40 seconds
Discrete-time transfer function.

Root Locus

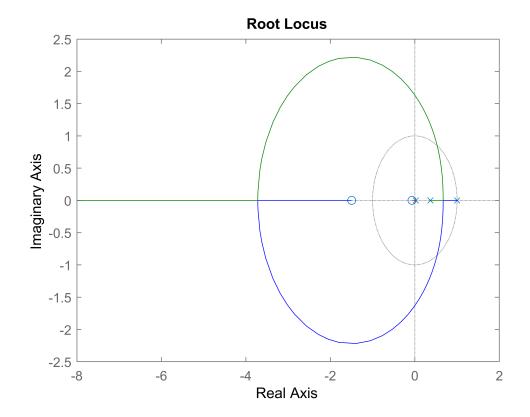
For Positive k:

rlocus(Gp_d)

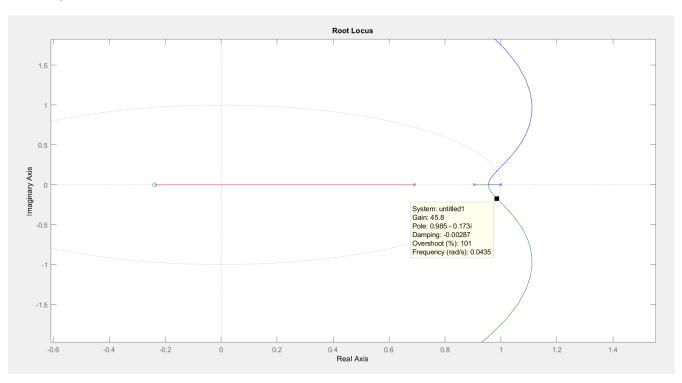


For Negative k:

rlocus(-Gp_d)



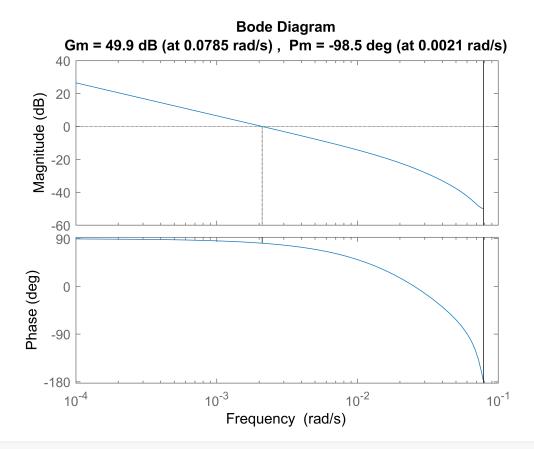
Deciding the Stable Threshold:



Therefore => -45.8<k<0

Bode plot

margin(Gp_d)



[Gm,Pm,Wgm,Wpm] = margin(Gp_d)

Warning: The closed-loop system is unstable.

Gm = 311.1157 Pm = -98.5242 Wgm = 0.0785 Wpm = 0.0021

Design a controler (p5)

Deciding The two major closed loop poles by the given information :

$$\begin{split} t_s &= \frac{4}{\zeta \omega_n} \text{ , } MP = \mathrm{e}^{-\frac{\zeta \omega_n}{\sqrt{1-\zeta^2}}} \to \zeta^2 = 1 - \frac{16}{(t_s \ln MP)^2} \\ t_s &= 100 \text{ , } MP = 0.2 \to \zeta = \pm 0.9994 \text{ , } \omega_n = 0.04 \text{ , } if \ T = 10 \to \frac{w_s}{w_d} \cong 453 \gg 8 \\ \to \begin{cases} |z| = e^{-\zeta \omega_n T} = 0.4493 \\ < z = T \ w_n \sqrt{1-\zeta^2} = 0.0277 \ rad = 1.587^\circ \end{cases} \end{split}$$

```
Ts = 10;
Gp
```

```
Gp = -4.875e-06
-----s^3 + 0.1173 s^2 + 0.002308 s
```

Continuous-time transfer function.

$$Gp_d = c2d(Gp,Ts,'zoh')$$

```
Gp_d =
    -0.0006143 z^2 - 0.00186 z - 0.000342
    z^3 - 2.176 z^2 + 1.485 z - 0.3093

Sample time: 10 seconds
Discrete-time transfer function.
```

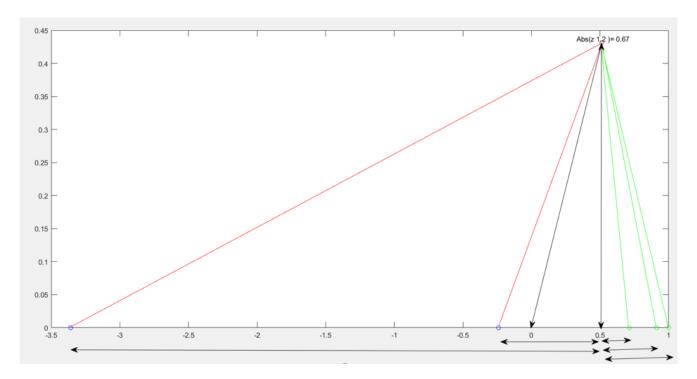
```
[num,den]=tfdata(Gp_d);
```

Calculate The zeros, Poles and the Gain of the Discrete Transfer Function:

```
[z,p,k] = tf2zp(num{1},den{1})
```

```
z =
    -2.8306
    -0.1967
p =
    1.0000
    0.7788
    0.3972
k = -6.1431e-04
```

Designing a Lead/Lag Controller depending on the position of zeros and poles :



$$\begin{cases} \theta_1 = 180 - \tan^{-1}\left(\frac{0.4493\sin(0.0277)}{0.7788 - 0.4493\cos(0.0277)}\right) * \frac{180}{\pi} = 177.838^* \\ \theta_2 = 180 - \tan^{-1}\left(\frac{0.4493\sin(0.0277)}{1 - 0.4493\cos(0.0277)}\right) * \frac{180}{\pi} = 178.706^* \\ \theta_3 = \tan^{-1}\left(\frac{0.67\sin(0.0277)}{0.4493\cos(0.0277) - 0.3972}\right) * \frac{180}{\pi} = 19.6646^* \end{cases} , \begin{cases} \varphi_1 = \tan^{-1}\left(\frac{0.4493\sin(0.0277)}{0.1967 + 0.4493\cos(0.0277)}\right) * \frac{180}{\pi} = 1.104^* \\ \varphi_2 = \tan^{-1}\left(\frac{0.4493\sin(0.0277)}{0.4493\cos(0.0277) - 0.3972}\right) * \frac{180}{\pi} = 19.6646^* \end{cases}$$

$$\varphi_1 + \varphi_2 - \theta_1 - \theta_2 - \theta_3 = -349.717 \rightarrow -374.8876 + 360 = -14.8876^\circ \rightarrow reduced\ phase$$

$$G_D(z) = \frac{k(z + \alpha)}{z + \beta} , Assume \rightarrow z + \alpha = z + 0.7123 \rightarrow \alpha = 0.7123$$

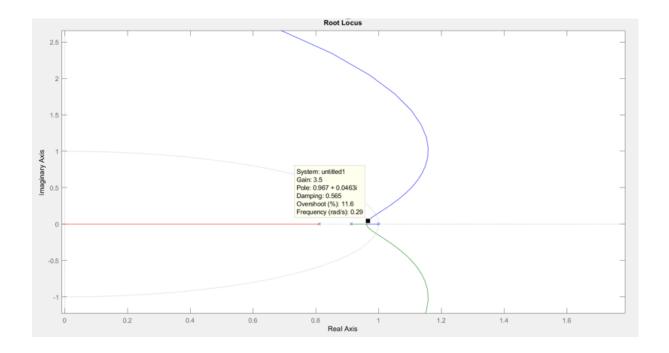
$$\Rightarrow G_D(z)G(z) = -\frac{6.1431 * 10^{-4}\ k\ (z + 0.1967)(z + 2.8306)}{(z - \beta)(z - 0.3972)(z - 0.7788)} \rightarrow \varphi_1 + \varphi_2 - \theta' - \theta_2 - \theta_3 = -360$$

$$\Rightarrow 360 + 1.104 + 0.217 - 177.838 - 19.6646 = \theta' = 163.8184^\circ \rightarrow \tan^{-1}\left(\frac{0.4493\sin(0.0277)}{\beta - 0.4493\cos(0.0277)}\right) * \frac{180}{\pi} = 16.1816^\circ \end{cases}$$

$$\Rightarrow \beta = 0.492$$

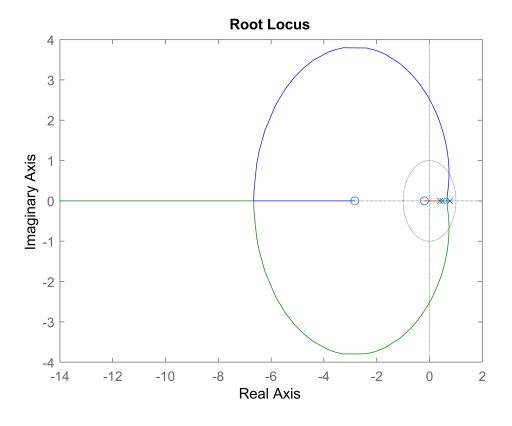
So, Reconstructing the Open loop Transfer function without the coefficient k : Gp(z)*G(z)

$$Gop_pre = tf(-6.1431*10^-4*conv([1 0.1967],[1 2.8306]),conv(conv([1,-0.492],[1,-0.3972]), [1,-0.3972]), [1,-0.3972])$$

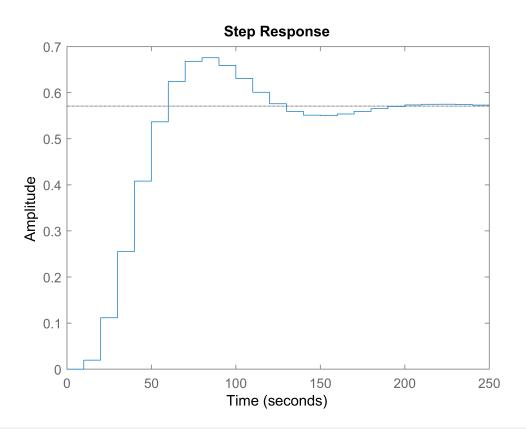


Decide to choose the controller coeffient form root locus

rlocus(-Gop_pre)



step(feedback(-32*Gop_pre,1))



stepinfo(step(feedback(-32*Gop_pre,1)))

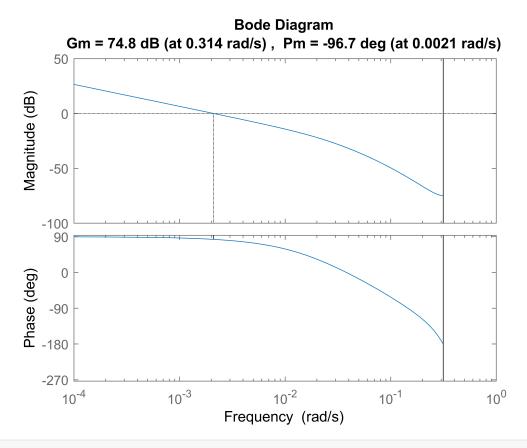
```
ans = struct with fields:
    RiseTime: 3.4343
    SettlingTime: 18.5526
    SettlingMin: 0.5367
    SettlingMax: 0.6758
        Overshoot: 17.6908
    Undershoot: 0
        Peak: 0.6758
        PeakTime: 9
```

$Gop = -32*Gop_pre$

Comparing the features per plot (p6)

Bode plot (Uncontrolled system)

margin(Gp_d)



```
[Gm,Pm,Wgm,Wpm] = margin(Gp_d)
```

```
Warning: The closed-loop system is unstable.
```

Gm = 5.5026e+03 Pm = -96.7192 Wgm = 0.3142 Wpm = 0.0021

BW_us = bandwidth(Gp_d)

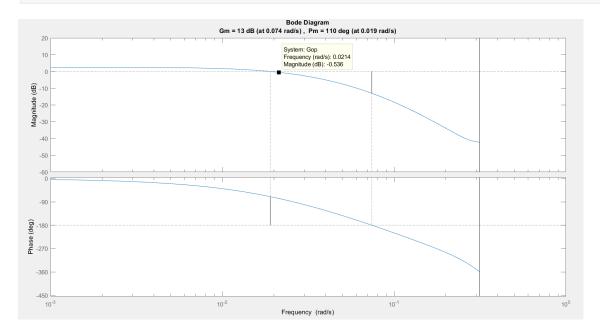
 $BW_us = Inf$

So the obtaind Bandwidth for the uncontrolled system is infinity, meaning there is no threshold found that we have a significant gain(This is due to the fact that the bode plot is strictly decreasing from the very first).

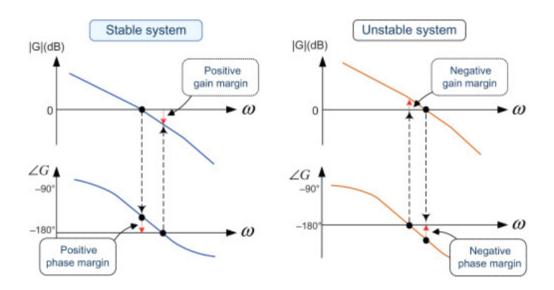
Bode Plot (Controlled system)

```
margin(Gop)
[Gm,Pm,Wgm,Wpm] = margin(Gop)
```

BW_cs = bandwidth(Gop)



As you can see, The result obtained from the bandwidth function and calculated bandwidth from the bode plot (-3db fall) are approximatly the same.



Gain margin is defined as the amount of change in open-loop gain needed to make a closed-loop system unstable. The gain margin is the difference between 0 dB and the gain at the phase cross-over frequency that gives a phase of -180° . If the gain $|GH(j\omega)|$ at the frequency of $\angle GH(j\omega)=-180^\circ$ is greater than 0 dB as shown in the left above figure, meaning a positive gain margin, then the closed-loop system is stable.

Phase margin is defined as the amount of change in open-loop phase needed to make a closed-loop system unstable. The phase margin is the difference in phase between -180° and the phase at the gain cross-over frequency that gives a gain of 0 dB. If the phase $\angle GH(j\omega)$ at the frequency of $|GH(j\omega)|=1$ is

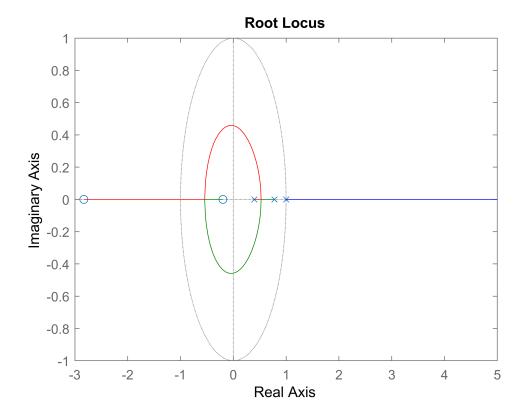
greater than -180° as shown in the above left figure, meaning a positive phase margin, the closed-loop system is stable.

If a closed-loop system is stable, both the gain margin and the phase margin need to be positive. So as we can see from the above bode plots, the uncontrolled system has a negative phase margin, so it is unstable and the controlled system has the positive phase and gain margin which is why it is stable. In general, the phase margin of 30–60 degrees and the gain margin of 2–10 dB are desirable in the closed-loop system design. A system with a large gain margin and phase margin is stable but has a sluggish response (Means slow to respond), while the one with a small gain margin and phase margin has a less sluggish response but is oscillatory (It has ups and downs).

Root Locus (Uncontrolled system)

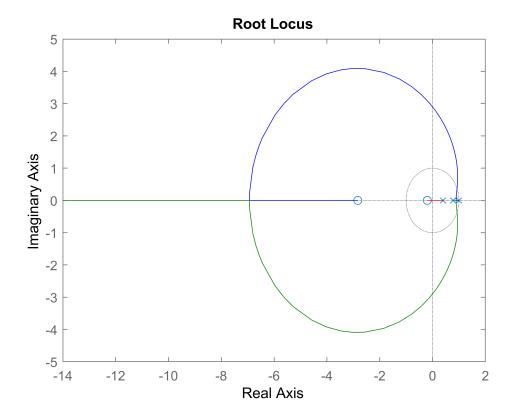
For Positive k:

```
rlocus(Gp_d)
```



For Negative k:

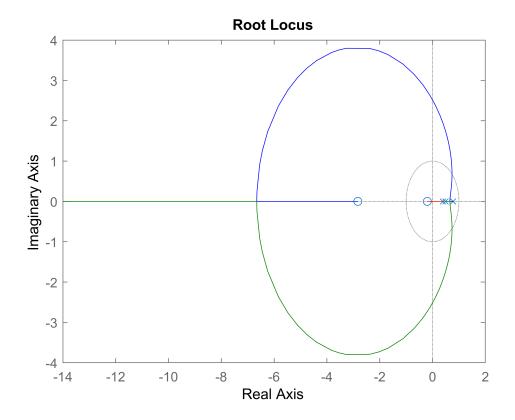
rlocus(-Gp_d)



Root Locus (Controlled system)

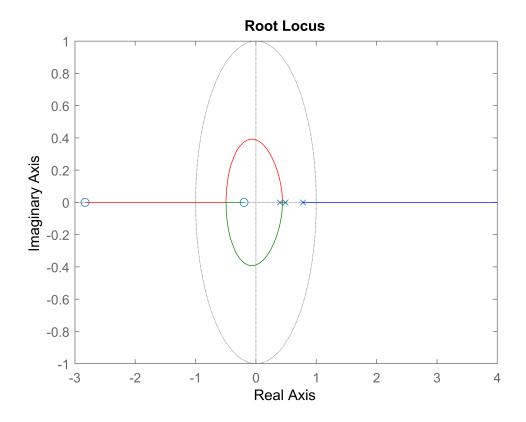
For positive k:

rlocus(Gop)



For negative k:

rlocus(-Gop)



DeadBeat controller (p7)

$$G(z) = -6.1431e - 04 * \frac{(z + 2.8306)(z + 0.1967)}{(z - 1)(z - 0.7788)(z - 0.3972)} = a * z^{-1} + \cdots$$

* The First Sentence of G(z) starts with the term $z^{-1} \to F(z) = f_1 z^{-1} + f_2 z^{-2}$

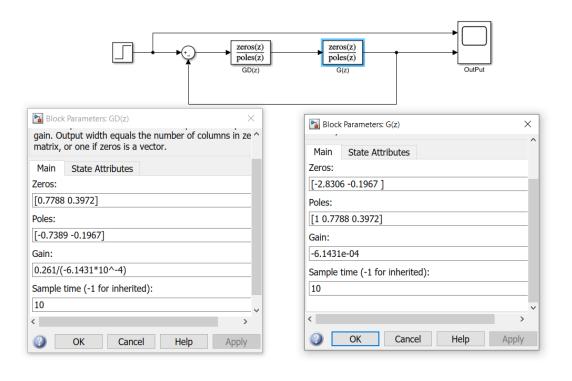
$$\begin{cases} F(z) = (1+2.8306z^{-1})(m_1z^{-1}) \\ 1 - F(z) = (1-z^{-1})(1+n_1z^{-1}) \end{cases} \rightarrow \begin{cases} f_1 + n_1 - 1 = 0 \\ f_2 - n_1 = 0 \\ f_1 - m_1 = 0 \\ f_2 - 2.8306 m_1 = 0 \end{cases}$$
Solve $[\{f_1 + n_1 - 1 = 0, f_2 - n_1 = 0, f_1 - m_1 = 0, f_2 - 2.8306 m_1 = 0 \end{cases}$

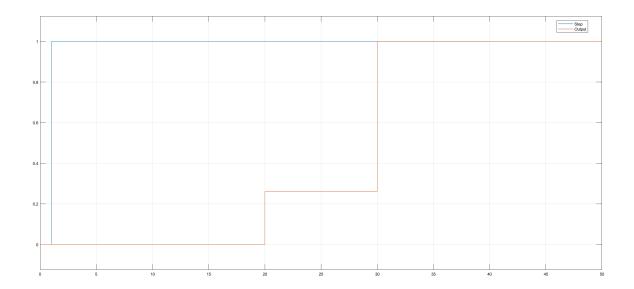
Solve[$\{f1 + n1 - 1 = 0, f2 - n1 = 0, f1 - m1 = 0, f2 - 2.8306 * m1 = 0\}$, $\{f1, n1, f2, m1\}$]

 $\{\,\{\text{f1}\rightarrow\text{0.261056, n1}\rightarrow\text{0.738944, f2}\rightarrow\text{0.738944, m1}\rightarrow\text{0.261056}\,\}\,\}$

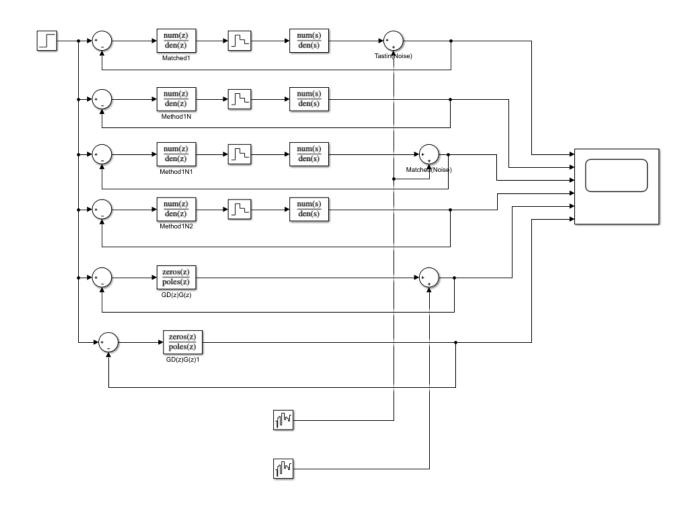
$$\rightarrow F(z) = 0.261z^{-1} + 0.7389z^{-2}$$

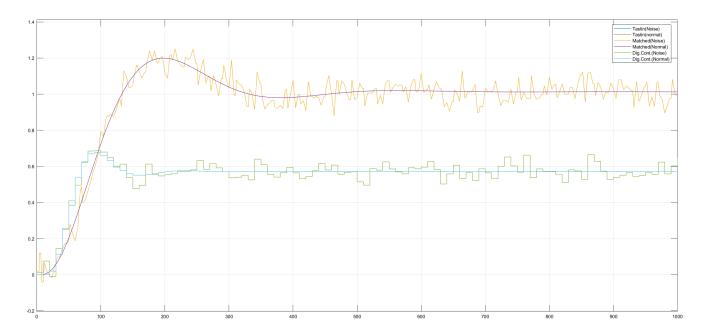
$$\rightarrow G_D(z) = \frac{F(z)}{\left(1 - F(z)\right)G(z)} = \frac{0.261(1 - 0.7788z^{-1})(1 - 0.3972z^{-1})}{-6.1431e - 04(1 + 0.7389z^{-1})(1 + 0.1967z^{-1})}$$





Comparing controllers (p8)





So The Digital Controller in part 5, Outperforms in comparsion with the Matched and Tastin Methods to resist with the white Noise.

*Tastin and Matched Methods Overlapped since the Digital controllers obtained for both of them are similar

(This is due to The fact that the Discretized version of the analog PD controller is the same for both case)

State space (p9)

Discrete State Space

```
y1 0
```

Continuous-time state-space model.

```
sys_d = c2d(sys,Ts)
sys_d =
 A =
          x1
  x2
  х3
 B =
  x1 -4.635e-05
  x2 7.434e-06
        0.2787
  x3
  C =
     x1 x2 x3
  y1 1 0 0
 D =
     u1
  y1 0
Sample time: 4 seconds
Discrete-time state-space model.
```

G = sys_d.A; H = sys_d.B;

Controllable & Observable

```
n = size(G,1);
M = [];
N = [];
for i = 0:n-1
    M = [M G^i*H];
    N = [N ; C*G^i];
end
Μ
   -0.0000
           -0.0003 -0.0007
   0.0000 0.0000 0.0000
   0.2787
          0.1926
                   0.1332
fprintf('Rank(M):%i\n',rank(M))
Rank(M):3
if rank(M) == n
    disp('(G,H) is controllable')
```

```
end
(G,H) is controllable
Ν
N =
    1.0000
               0
    1.0000 -17.1293 -0.0004
    1.0000 -32.6285 -0.0014
fprintf('Rank(N):%i\n',rank(N))
Rank(N):3
if rank(N) == n
    disp('(G,C) is observable')
end
(G,C) is observable
% Hankel Matrix
if rank(N*M) == n
    disp('State space is minimal')
end
```

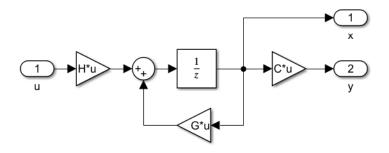
State space is minimal

DeadBeat controller from the state space (p10)

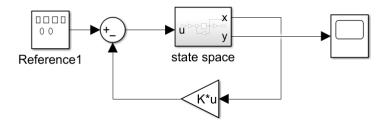
```
W = [];
for i = 0:n-2
    W = [W ; flip(a(1:end-1-i)) 1 zeros(1,i)];
end
T = M*W;
K_deadbeat = -flip(a)*inv(T)
```

```
K_deadbeat =
   1.0e+05 *
   -0.0403   1.3010   0.0001
```

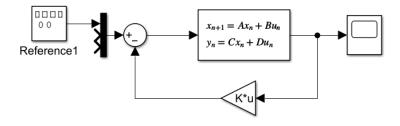
In order to achive the states, we need to implement the system with delay block:



Then simply connect the state feedback controller:



The other way is implement it as discrete state space block and connect the state feedback controller. But we need to set the C matrix equal to eye(3) because we need all the states in the output:



Deadbeat controller with full rank observer (p11)

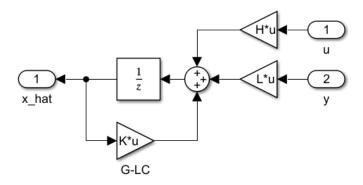
```
% x[k+1] = (G-LC)x[k] + Hu[k] + Ly[k]
G_new = transpose(G);
H_new = transpose(C);
```

L = transpose(acker(G_new,H_new,zeros(n-1,1)))

$$\dot{\hat{x}} = (A - LC) * \hat{x} + Bu + Ly$$

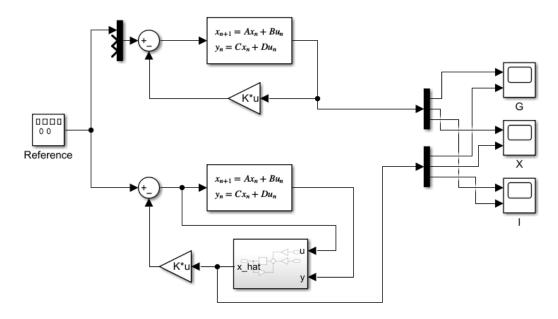
$$\begin{cases} k \to L^T \\ B \to C^T \to \det(\lambda I - (A - LC)) = \det(\lambda I - (A^T - L^T C^T)) \\ A \to A^T \end{cases}$$

So the block of observer is something like this:

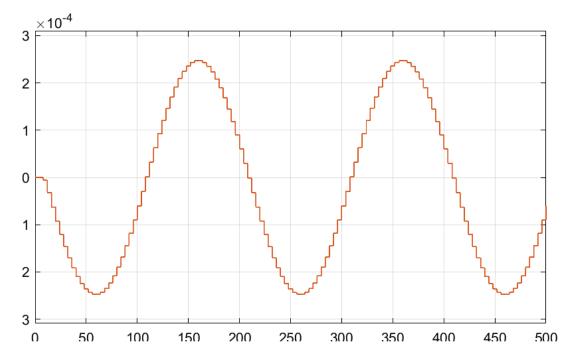


To compare states from system without observer and system with observer we impelement the circuit below.

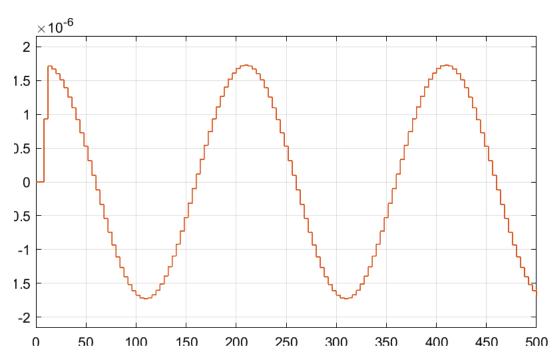
The input is a sinous signal with the frequency of 0.005Hz.



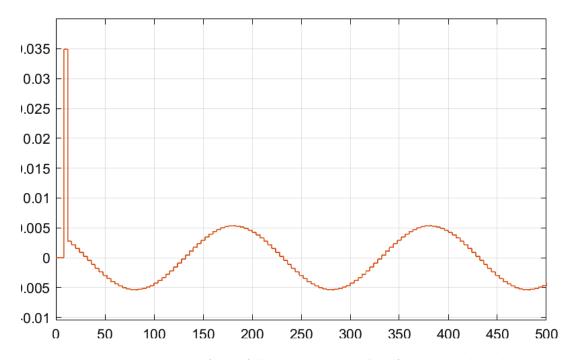
G:



X:



l:



As we can see, observer prefectly follows the states. But if we apply the initial conditions, we can see the error between them that converges to zero over the time.

initial condition = 0.1

G:

