Chapter 1

Introduction

In advancing the LTCC face, the coal and rock structures are affected by the mining disturbance [7]. As a result, it is difficult for the roof to form an effective self-bearing structure [8,9], and the roof collapse occurs over the stability threshold. The impact of roof instability on the working face makes the stability of the coal wall worse, increasing the probability of rib spalling [10]. On the other hand, different bearing conditions of hydraulic support have a significant impact on the subsidence and collapse of roofs [11,12]. Therefore, the movement instability of the roof is closely related to the bearing characteristics of the hydraulic support.

Underground geological conditions are increasingly complex. Scholars have investigated the structural properties and movement laws of the roof. Many theoretical models have been proposed to study the structural characteristics of the roof [13–15]. These models have given a basic understanding of roof activities. Zhang [16] studied the structural parameters of the roof in the LTCC face and summed up the impact of immediate roof characteristics on mine pressure. Based on the energy variation principle, Yu et al. [7] simulated the collapse of the roof and explained the mine pressure. In addition to theoretical models, in situ monitoring tests play important roles in understanding the movement and failure of roof [17,18]. However, because of the complexity of geological conditions, in situ monitoring tests may not be carried out extensively. To solve this situation, some scholars use physically similar simulation tests to analyze the movement laws of the roof [10,19]. However, such important in situ factors as the initial stress cannot be considered in physically similar simulation tests. In contrast, numerical simulations may be more feasible to study the problems. Many investigators have attempted to simulate the coal mining process and the movement laws of the roof [9,20,21]. The stress and types of failure in the coal seam were investigated by Behera et al. [22]. By numerical simulation and underground measurement, Pang et al. [23] discovered the mechanical mechanism of rock fracture instability and the mining stress development law in the deep stope.

However, as a result of the complex and changeable geological conditions, various coupling states will be formed between the roof and the hydraulic support [24–27]. The safety of the hydraulic support could not be guaranteed by a single analysis of the movement laws of the roof. Consequently, the primary focus of underground safety support has moved to the investigation of the interaction between the roof and the hydraulic support. Wang et al. [28–30] divided the interaction between the roof and the hydraulic support into strength coupling, stiffness coupling, and stability coupling. In addition, they qualitatively described the adaptability of the hydraulic support under different coupling states. With the development of numerical simulation, some scholars have extended the interaction between the roof and the hydraulic support to their respective interiors [31,32]. Thus, the movement characteristics of the roof and the bearing capacity of the hydraulic support are more intuitively reflected. Arasteh et al. [33] investigated the features of roof caving in the LTCC face by numerical simulation. In addition, they generated a summary of the bearing capacity of the hydraulic support. Through theoretical analysis and numerical simulation, Rajwa et al. [34] analyzed the influence of roof strength and different support states of the canopy on the stability of the working face.

Abstract: In longwall top coal caving (LTCC), due to the fractures and migration of top coal, the roof will break and collapse, which causes serious impact damage to hydraulic support. Therefore, we aimed to reveal the relationship between the roof instability effect and the bearing characteristics for hydraulic support in the LTCC face. Based on the occurrence conditions of the mining area in the Barapukuria Coal Mining, The instability model of the upper immediate roof was established, and the working resistance of hydraulic support was derived. Secondly, the dynamic coupling model of roof-top coal-hydraulic support was established in LS-DYNA and the crushing degree of top coal and the bearing characteristics of the hydraulic support in different roof instability fields were analyzed. The results show that the main factors affecting the working resistance of hydraulic support are the fracture positions of the upper immediate roof, the acting force of the lower immediate roof, and the distributions of the gangue is the goaf. The rotary instability of the upper immediate roof at the coal wall brings serious impact effects, resulting in fractures in front of the coal wall and a large amount of crushed coal concentrated at the front end of the canopy.The cursing degree of top coal significantly impacts the canopy, especially the back end of the canopy and the hinged pin shaft, which is prone to bending fracture.The research results can provide reference and experience for the stability control of roof strata and the structutal optimization of hydraulic support.

Analysis of roof instability effect:

The rock strata that cannot be self-stabilized and collapse in the caving zone are col lectively referred to as the immediate roof [14]. Due to the rock strata’s different fracture locations and lithology, there are two types of immediate roofs: the lower immediate roof and the upper immediate roof. In order to quantitatively analyze the impact load caused by the instability of the upper immediate roof on the hydraulic support [41], the thickness HZ of the immediate roof can be defined as Equation (1): and the upper immediate roof. In order to quantitatively analyze the impact load caused by the instability of the upper immediate roof on the hydraulic support [41], the thickness Hz of the immediate roof can be defined as Equation (1):

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where Hz is the thickness of the immediate roof, m; H is the cutting height, m; T is the thickness of the top coal; SA is the subsidence of the main roof, m; C is the thickness of residual coal, m; KA is a constant under certain roof conditions , which is set to 1.4. The subsidence of the main roof SA can be defined as Equation (2):

where Ks is the main roof subsidence coefficient, which is set to 0.2. The thickness of residual coal C can be defined as Equation (3):

(3)

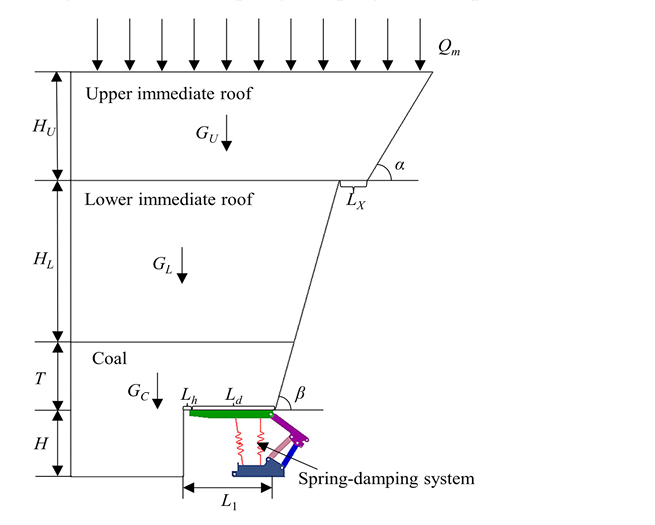


Fig-:Coupling mechanical model of roof-top coal-hydraulic support

According to the location and lithology of the root, the instability of the upper immediate roof is the main factor causing the pressure on the working face.The different crushing conditions of the lower strata directly affect the stability and rotation angle of the upper immediate roof.In addition, the instability of the roof has a certain lag.Therefore, the fracture line of the roof is located on the extension line of the coal wall and roof cutting, respectively.There are three forms of the upper immediate roof instability sliding instability at the coal wall , rotary instability at the coal wall, and rotary instability at the roof cutting.The instability model of the upper immediate roof is established, as shown in fig

The horizontal force cannot be transmitted after the rock strata breaks, which results in the upper immediate roof presenting a cantilever beam state.Different crushing conditions directly affect the cantilever beam’s instability forms.Fig 4a shows that the cantilever beam showed sliding instability at the coal wall.The working resistance of the hydraulic support can be definded as Equation (4)

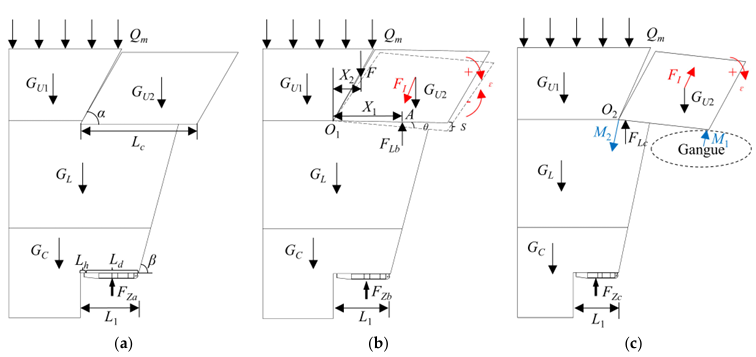


Fig: Instability model of the upper immediate roof; (a) sliding instability at the coal wall, (b)Rotary instability at the top coal, (c)Rotary instability at the roof cutting

Because of rotary instability, the impact load will be transferred to the lower immediate roof and top coal. This will make the support resistance of the hydraulic support go up.Usually, the fracture length of the upper immediate roof is the same, but fracture positions differ.Figure 4b shows that the cantilever beam rotated with instability at the coal wall.In the initial state of the rotary , the working resistance of the hydraulic support can be definded as Equation

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Where 1 is the working resistance of the hydraulic support under the initial state of the rotary instability at the coal wall, kN;F is the additional force of the overlying strata,kN;GC is the gravity of the top coal, kN; GL is the gravity of the lower immediate roof, kN;GU1 is the gravity of unbroken upper immediate roof,kN; GU2 is the gravity of the cantilever beam, kN.

According to Equation(5), the working resistance is impacted by the additional force of overlying strata.Figure 4b demonstrates that the support force of the lower immediate roof acts at the A.According to the moment balance,the additional force can be defined as Equation (6)

Where Lc is the length of the cantilever beam, m; X1 is the length of the lower immediate roof support positions from the rotary center O1,m; X2 is the length of the additional force position from the rotary center O1,m.

Due to the lower immediate roof force, the cantilever beam began to slow subsidence.According to the d`Alembert principle, the greater the acceleration during decelebration, the greater the inertial force and the stronger the impact on hydraulic support.As shown in Figure 4b, the working resistance of the hydraulic support can be defined as Equation (7)

Where is the working resistance of the hydraulic support under the deceleration state of the rotary instability at the coal wall,kN; is the lower immediate roof force,kN;