

## Optimization of a Pb-free all-perovskite tandem solar cell with 30.85% efficiency

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### ABSTRACT

We present simulation results obtained with the SCAPS-1D simulation package of a lead-free all-perovskite tandem solar cell. The top and bottom subcells, consisting of  $\text{MgAl}_3$ , and  $\text{FASnI}_3$ , respectively, were optimized individually by varying material properties such as thickness, electron affinity, and capture cross-section. These standalone optimized subcells are then utilized for the tandem structure. The optimal tandem cell thickness was determined based on short circuit current density ( $J_{\text{SC}}$ ) matching of the standalone subcells by varying the subcells' thickness. A matching  $J_{\text{SC}}$  of  $14.70 \text{ mA/cm}^2$  was obtained for the top and bottom subcell thickness of 983 nm and 1600 nm, respectively. At this current matching condition, the simulation show that a tandem cell would yield a high open-circuit voltage ( $V_{\text{OC}}$ ) of 2.63 V, resulting in an efficiency of 30.85%, significantly higher than that of each subcell.

### 1. Introduction

In single-junction solar cells, the Shockley-Queisser limit bounds the power conversion efficiency (PCE) to about 33% [1]. That is because a single-junction solar cell does not absorb photons with energies lower than the bandgap,  $E_g$ , of the semiconductor absorber. When absorbing photons with energy higher than  $E_g$ , the generated electron and hole will each have excess kinetic energy, which is usually relaxed by phonon interactions and thus heating of the lattice [2]. A tandem solar cell minimizes these spectral losses and converts a higher proportion of sunlight into electricity than a single-junction solar cell. Consequently, a tandem solar cell has a higher Shockley-Queisser limit of 45% [3].

A tandem solar cell consists of two or more different solar cells or absorber layers with different  $E_g$ . The layer with larger  $E_g$  is positioned above the narrow  $E_g$  layer such that the top layer absorbs the higher energy photons and the bottom layer absorbs the lower energy photons. Thus, a tandem solar cell utilizes a wider spectral range and produces a higher photocurrent than a single junction solar cell. Increasing the number of subcells further stretches the theoretical PCE limit to 50%, 54%, and 65% corresponding to three, four, and an infinite number of subcells, respectively [3]. The experimental realization of a tandem solar cell goes back as early as 1978 when a device consisting of AlGaAs/GaAs was seen to have a PCE of ~9% [4]. The top performing

dual-junction tandem solar cells today are mostly some combination of III-V semiconductors and/or silicon such as, GaInAsP/GaInAs ( $32.6 \pm 1.4\%$ ) [5], GaInP/GaAs ( $32.8 \pm 1.4\%$ ) [6], and GaAs/Si ( $32.8 \pm 0.5\%$ ) [7]. The efficiency values of these tandem devices are well above that of their corresponding single-junction counterpart. Despite these impressive performances, the search for alternative solar cells continues due to the high manufacturing cost and complex fabrication method of the III-V semiconductors [8].

Perovskites are currently some of the most promising absorber materials for use in solar cells. Perovskite solar cells (PSC) have seen a remarkable improvement in PCE of 25.5% for single-junction from 3.8% in only a decade. In addition to providing excellent performance, PSC has the edge over current commercial solar cells in terms of cost since it is manufactured from cheap, naturally abundant precursor materials. The most significant advantage that makes perovskite materials ideal candidates as the top subcell in a tandem device is the suitable bandgap and the ability to tune the bandgap [9]. Further, perovskite materials have efficient radiative recombination and excellent light absorption properties combined with ease of fabrication [10]. Current tandem solar cells have complex fabrication schemes since simple methods to deposit the top subcell are often incompatible with the stability of the bottom subcell. For perovskite, however, a wide choice of simple processing techniques, e.g., spin coating [11,12], vacuum deposition [13–15], and

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printing techniques [16–18] are available. Their low temperature ( $\sim 100^\circ$ ) crystallization [19] makes it possible to use the fabrication processes mentioned above without harming the bottom subcell. Indeed, this very young technology has already progressed towards devices approaching the efficiency of the top performing tandem cells mentioned before. Perovskite has been used in tandem solar cells as top subcell with Si (perovskite/Si), CIGS (perovskite/CIGS), and even another perovskite (perovskite/perovskite) that have PCE of 29.2%, 24.2%, and 24.2%, respectively [20].

The use of Si as the bottom subcell presents limiting drawbacks to perovskite tandem solar cells. These include an increase in cost and a reduced throughput [21]. Additionally, using a Si subcell would not be flexible. To that end, intense research is performed on all-perovskite (perovskite/perovskite) tandem solar cells [22,23]. In the short span of four years, the PCE of all-perovskite tandem solar cells has risen to 25.6% in a  $0.049\text{ cm}^2$  device (24.2% in  $1\text{-cm}^2$ -area devices) [24] from an initial value of 6.6% [25].

So far, the best performing PSC are mostly manufactured from organic lead halide-based materials. The use of Pb, however, poses a major environmental and health threat, as pointed out by many researchers [26–28]. Therefore, one currently researched avenue is the search for Pb-free alternatives. One potential substitute of Pb, and the most extensively explored one, is Sn [29–32]. Currently, most of the highly efficient Sn-based PSCs use  $\text{FASnI}_3$  perovskite [33–38].  $\text{FASnI}_3$  has excellent properties like high charge-carrier mobilities, while progress is being made in overcoming its current shortcomings like low efficiency and poor chemical stability [39–41]. Another element, Ge, which is in the same group as Pb and Sn, is also a potential substitute for Pb. Ge-based perovskites are expected to show similar solid-state properties to their Pb and Sn analogs [42,43] and  $\text{MAGeI}_3$  has the potential to become an alternative to  $\text{MAPbI}_3$  [44]. Indeed, theoretical studies show that  $\text{MAGeI}_3$  possesses remarkable hole and electron conductive behavior and adequate stability compared to that of  $\text{MAPbI}_3$  [43]. Furthermore, the high bandgap of  $\sim 1.9\text{ eV}$  that has been found in the experimentally realized  $\text{MAGeI}_3$ , [45,46] makes it a perfect choice for a top subcell in a tandem solar cell.

In this manuscript, we consider  $\text{MAGeI}_3$  as the top subcell and  $\text{FASnI}_3$  as the bottom subcell for the simulation of an all-perovskite tandem solar cell using the SCAPS-1D [47] package. First, the bottom subcell was simulated to fit experimental data, followed by detailed optimization on parameters such as the electron affinity, capture cross-section, and thickness. Next, similar optimization was done for the top subcell. The PCEs of the optimized standalone top and bottom subcells were found to be 23.69% and 19.84%, respectively. For the tandem structure, the current matching condition was achieved by varying the thickness of both subcells.

## 2. Simulation approach

In a multijunction tandem solar cell, the two subcells can be considered as two diodes connected in series. Thus, the same current flows through the subcells, which is the current of the tandem solar cell. The voltage of the tandem cell is the sum of the voltages in the subcells. Since SCAPS-1D does not fully support a multijunction solar cell, the top and bottom subcells were separately simulated. In between the two cells, we introduced a recombination layer of ITO with a thickness of 20 nm. We follow the simulation method [48–53] in which the top subcell is illuminated by standard AM 1.5G 1 sun, and the bottom subcell is illuminated by the spectra filtered by the top subcell, given by,

$$S(\lambda) = S_0(\lambda) \cdot \exp \left( \sum_{i=1}^4 -a_i(\lambda)d_i \right) \quad (1)$$

where  $S(\lambda)$  is the filtered spectrum,  $S_0(\lambda)$  is the spectrum incident on the top subcell,  $a_i(\lambda)$  is the absorption coefficient of the  $i$ th material and  $d_i$  is the thickness of the  $i$ th material. In our case  $i = 1, 2, 3$ , and 4 corresponds

to  $\text{TiO}_2$ ,  $\text{MAGeI}_3$ , Spiro – OMeTAD, and ITO, respectively. Under this condition, the value of the short circuit current ( $J_{SC}$ ) of the two subcells is matched by varying their thickness to simulate the final tandem cell.

A schematic representation of the tandem structure is also shown in Fig. 1. The absorption coefficient of  $\text{TiO}_2$ ,  $\text{MAGeI}_3$ , Spiro-OMeTAD, and ITO are taken from literature [54–57]. All the basic input values used in the simulation are taken from literature and listed in Table 1.

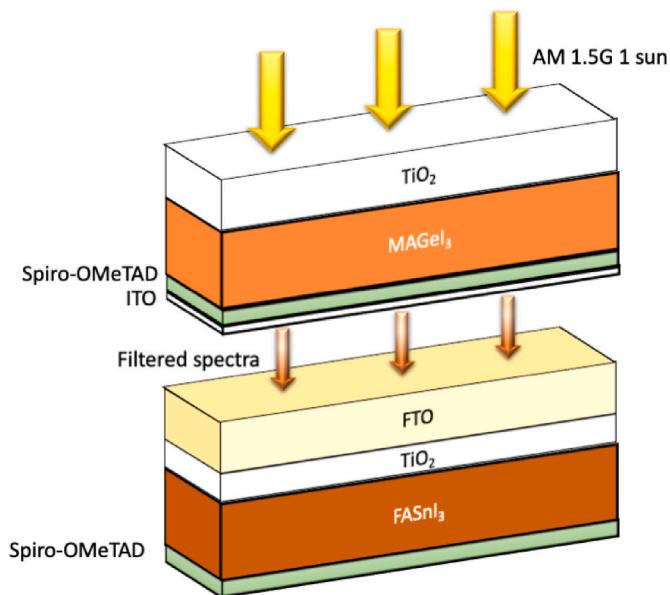
## 3. Results and discussion

### 3.1. Optimization of parameters for each subcell

Experimental data was used to calibrate parameters for the  $\text{FASnI}_3$  cell. We reproduce the experimental results for formamidinium [40] using the values presented in Table 1. As shown in Table 2, the simulation result mimics the experimental value closely. Here  $V_{OC}$  is the open-circuit voltage,  $J_{SC}$  is the short circuit current density, FF is the fill factor, and PCE is the power conversion efficiency.

Our approach optimized three parameters: the electron affinity of the transport layers, the cross-section of defects, and the thickness of each of the layers in the device. The band offsets play essential roles in the performance of the solar cells ([64]). The conduction band offset (CBO) is defined as the difference between the electron affinities of the perovskite and the electron transport layer (ETL). The valence band offset (VBO) is defined as the difference between the electron affinities of the hole transport layer (HTL) and the perovskite plus the difference between the bandgaps of the HTL and the perovskite. To investigate the effect of CBO and VBO, we varied the electron affinity of the ETL and the HTL.

It was found that decreasing the electron affinity of  $\text{TiO}_2$  from its initial value of 3.9 eV to 3.5 eV improves the PCE from 1.73% to 8.56%, as shown in Fig. 2 (a), since all parameters decrease monotonically as the electron affinity increases. The initial electron affinity of the HTL (the spiro-OMeTAD) of 2.2 eV (PCE of 1.73%) gives the best performance. Increasing the electron affinity will increase the filling factor and the open-circuit voltage while reducing the short circuit current to zero. As shown in Fig. 2, for  $\text{FASnI}_3$ , a CBO of about 0 eV gives optimum performance and as the value of CBO drops, so does the performance. As for the effect of VBO, we see that the optimum performance is in the 0–0.3 eV range. For other VBO values, the efficiency decreases. These



**Fig. 1.** Schematic device structure of the simulated lead-free halide tandem solar cell.

**Table 1**  
Basic parameters used in the simulation.

Parameters	Spiro-OMeTAD	TiO <sub>2</sub>	MAGel <sub>3</sub>	FASnI <sub>3</sub>	FTO
Thickness (nm)	200	350	600	350	400
Bandgap (eV)	3	3.2	1.9	1.41	3.5
Electron affinity (eV)	2.2	3.9	3.98	3.52	4
Dielectric permittivity	3	9 <sup>a</sup>	10	8.2	9
Density of states in CB (cm <sup>-3</sup> )	1 × 10 <sup>19</sup>	1 × 10 <sup>19</sup>	1 × 10 <sup>16</sup>	1 × 10 <sup>18</sup>	2.2 × 10 <sup>18</sup>
Density of states in VB (cm <sup>-3</sup> )	1 × 10 <sup>19</sup>	1 × 10 <sup>19</sup>	1 × 10 <sup>16</sup>	1 × 10 <sup>18</sup>	10 <sup>19</sup>
Thermal velocity of electron (cm/s)	1 × 10 <sup>7</sup>				
Thermal velocity of hole (cm/s)	1 × 10 <sup>7</sup>				
Electron mobility (cm <sup>2</sup> /Vs)	1 × 10 <sup>-4</sup>	20	162 <sup>b</sup>	22	20
Hole mobility (cm <sup>2</sup> /Vs)	1 × 10 <sup>-4</sup>	10	101 <sup>b</sup>	22	10
Donor density (cm <sup>-3</sup> )	0	1 × 10 <sup>17</sup>	1 × 10 <sup>9</sup>	0	2 × 10 <sup>19</sup>
Acceptor density (cm <sup>-3</sup> )	2 × 10 <sup>19</sup>	0	1 × 10 <sup>9</sup>	7 × 10 <sup>16</sup>	0
Defect density (cm <sup>-3</sup> )	1 × 10 <sup>15</sup>	1 × 10 <sup>15</sup>	1 × 10 <sup>16</sup>	10 <sup>15</sup>	10 <sup>15</sup>
References	[58]	[59]; [60]	[61,62]	[63]	[63]

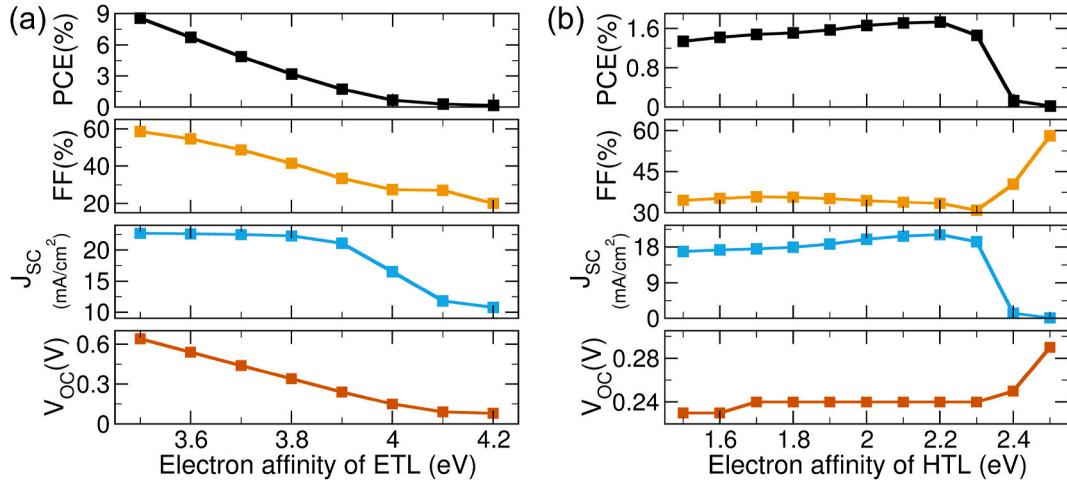
  

Interface	Spiro/MAGel <sub>3</sub>	MAGel <sub>3</sub> /TiO <sub>2</sub>	Spiro/FASnI <sub>3</sub>	FASnI <sub>3</sub> /TiO <sub>2</sub>
Defect density (cm <sup>-3</sup> )	1 × 10 <sup>16</sup>	1 × 10 <sup>16</sup>	1 × 10 <sup>16</sup>	1 × 10 <sup>16</sup>
Capture cross-section (cm <sup>2</sup> )	1 × 10 <sup>-19</sup>	1 × 10 <sup>-19</sup>	1 × 10 <sup>-19</sup>	1 × 10 <sup>-19</sup>
Energetic distribution	Gauss	Gauss	Gauss	Gauss

<sup>a</sup> [60].<sup>b</sup> [62].

**Table 2**  
Comparison of simulation and experimental results for the FASnI<sub>3</sub> cell.

Method	V <sub>OC</sub> (V)	J <sub>SC</sub> (mA/cm <sup>2</sup> )	FF (%)	PCE (%)
Simulation	0.244	21.09	33.53	1.73
Experimental	0.234	20.45	36.00	1.71



**Fig. 2.** PCE, FF, J<sub>SC</sub>, and V<sub>OC</sub> for the FASnI<sub>3</sub> subcell as a function of electron affinity of (a) the electron transport layer and (b) the hole transport layer for the FASnI<sub>3</sub> device.

results agree with the literature [63,64].

Defects at the interfaces play a crucial role in the performance of the devices since interface traps are the dominant recombination channel for PSC [65]. Trap-assisted Shockley–Read–Hall (SRH) recombination [66,67] is described by the following expression

$$R_{SRH} = \frac{np - n_i^2}{\tau \left( p + n + 2n_i \cosh \left[ \frac{E_f - E_t}{kT} \right] \right)}, \quad \tau = \frac{1}{\sigma N_t v_{th}}, \quad (2)$$

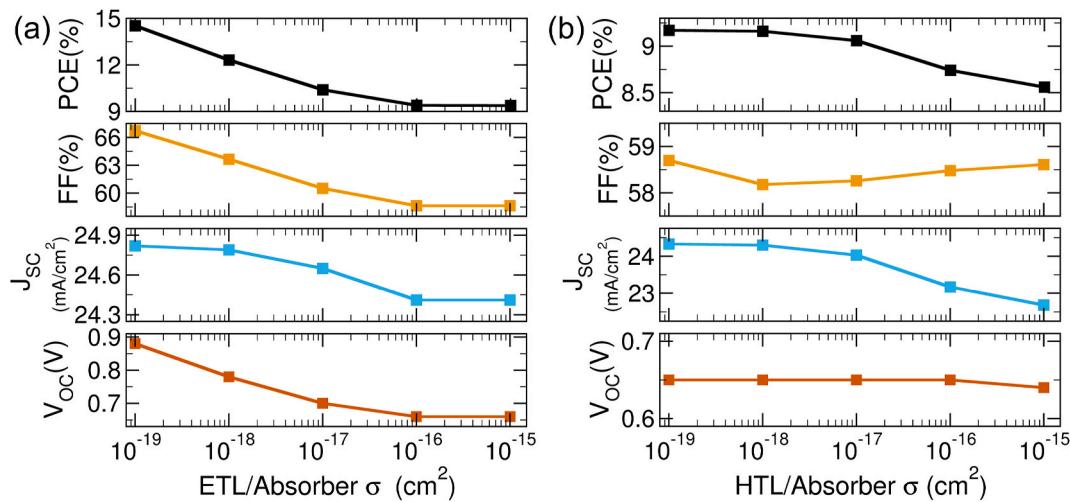
where the electron and hole concentrations are given by  $n$  and  $p$ ,  $n_i$  is the intrinsic carrier concentration,  $\tau$  is the carrier lifetime,  $N_t$  and  $E_t$  are the defect concentration and defect energy level,  $v_{th}$  is the thermal velocity of the carriers, and  $\sigma$  is the carriers capture cross-section. Since the capture cross-section is reported to have a significant effect on the device performance [68], we are interested in calibrating our simulation results to experiment; thus, we investigated the effect of capture cross-section at the ETL/absorber (TiO<sub>2</sub>/FASnI<sub>3</sub>) and the HTL/absorber interface (FASnI<sub>3</sub>/SpiroOMeTAD).

The results presented in Fig. 3 help us determine the effects on performance from each interface. The ETL/absorber interface shows that decreasing the capture cross-section improves the performance significantly. The PCE increases since all three parameters (FF, J<sub>SC</sub>, and V<sub>OC</sub>) increase as the cross-section of trap defects is reduced at the PSC/TiO<sub>2</sub> interface. At the HTL/absorber interface, the open-circuit voltage is constant over a considerable cross-section range and thus limits the maximal PCE.

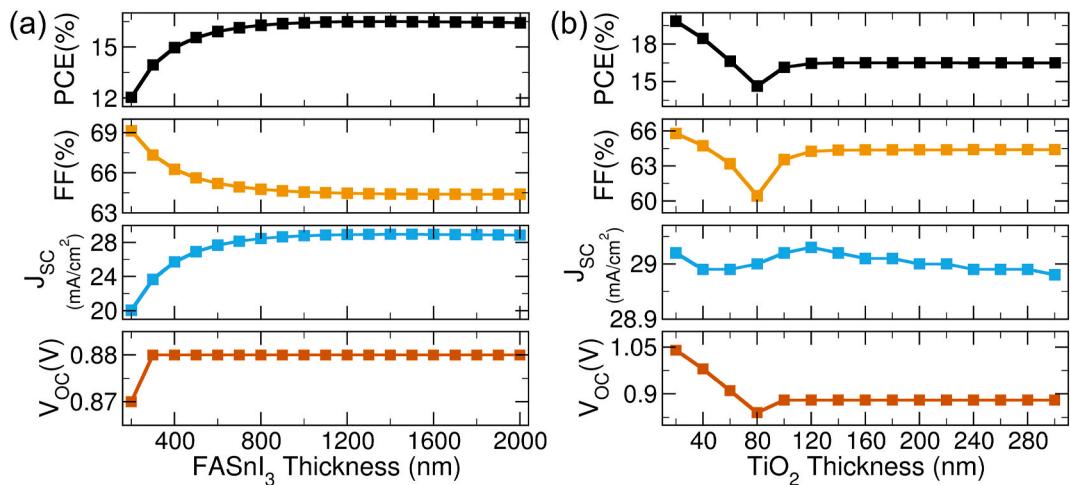
The thickness of each layer in a solar cell plays an essential role in the device's overall performance. The two competing effects determine the optimal thickness, *viz.*, absorption of incoming photons, and recombination center at the bulk. The absorption of incoming photons increases with increasing thickness per Beer-Lamberts law,  $I = I_0 \exp(-\alpha x)$ , enhancing the number of photo-generated charge carriers and consequently increasing J<sub>SC</sub>. However, at the same time, an increase in thickness increases the number of recombination centers, which hinders the charge carriers from contributing to J<sub>SC</sub>. Thus, it is crucial to find the optimum value of thickness by varying it for each layer.

For a tandem solar cell, the thickness has other especial importance too. Since the top subcell filters the light before it reaches the bottom subcell, minimizing the top subcell thickness is vital for an excellent overall performance. Thickness is also used as the parameter that is varied to obtain the current matching condition.

We explored the effect of thickness of each of the layers on the so far optimized device. In Fig. 4 (a), we see that increasing the thickness of FASnI<sub>3</sub> improves PCE until reaching a thickness of about 1400 nm,



**Fig. 3.** PCE, FF, J<sub>SC</sub>, and V<sub>OC</sub> as a function of capture cross-section at (a) the ETL/absorber interface and (b) the HTL/absorber interface for the FASnI<sub>3</sub> absorber.



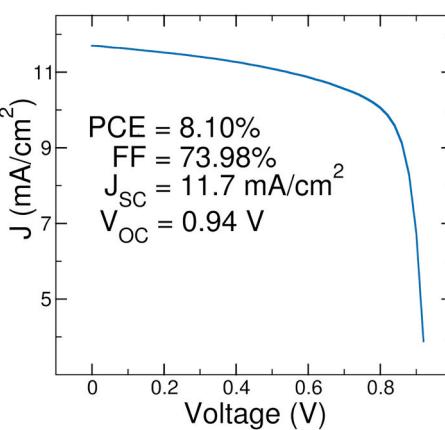
**Fig. 4.** PCE, FF, J<sub>SC</sub>, and V<sub>OC</sub> as a function of (a) absorber thickness and (b) ETL thickness.

where the PCE saturates. The thickness of the HTL has minimal effect on the performance of the device. Our calculations show that the PCE will stay around 16.5%, FF at 64.5%, J<sub>SC</sub> at 28.97 mA/cm<sup>2</sup>, and V<sub>OC</sub> at 0.88 V over a range of thickness of 20–200 nm. The ETL thickness, however, affects the V<sub>OC</sub> and the FF, which are more prominent for the thinner films. Thus the PCE of the device is maximal for a 20 nm TiO<sub>2</sub> film, as shown in Fig. 4 (b). The final configuration for the optimized FASnI<sub>3</sub> subcell and the current-voltage (I-V) characteristics are presented in Table 3.

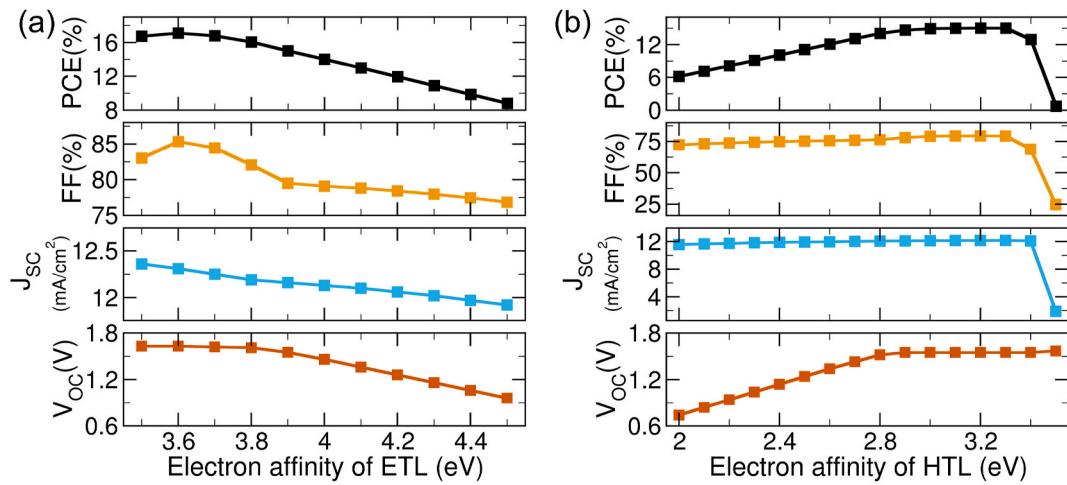
The MAGel<sub>3</sub> subcell was simulated with the values presented in Table 1. The corresponding J-V curve and the I-V characteristics are

**Table 3**  
Device performance for the optimized FASnI<sub>3</sub> subcell.

Parameters	Spiro-OMeTAD	TiO <sub>2</sub>	FASnI <sub>3</sub>	HTL/ FASnI <sub>3</sub>	FASnI <sub>3</sub> / ETL
Electron affinity (eV)	2.2	3.5	3.52	–	–
Capture cross-section (cm <sup>2</sup> )	–	–	–	$1 \times 10^{-19}$	$1 \times 10^{-19}$
Thickness (nm)	200	20	1400	–	–
I-V characteristics					
V <sub>OC</sub> (V)	J <sub>SC</sub> (mA/cm <sup>2</sup> )	FF (%)	PCE (%)		
1.04	29.02	65.78	19.84		



**Fig. 5.** Simulated J-V curve and I-V characteristic for the initial MAGel<sub>3</sub> subcell.



**Fig. 6.** PCE, FF,  $J_{SC}$ , and  $V_{OC}$  for the  $\text{MAGeI}_3$  subcell as a function of electron affinity of (a) the electron transport layer and (b) the hole transport layer for the  $\text{MAGeI}_3$  device.

However, for the ETL, the maximum filling factor is achieved when the electron affinity is set to 3.6 eV. Thus, the optimal PCE of 17.11% is found for the electron affinity of 3.6 eV. Fig. 6 (b) shows the electron affinity for the HTL. We found that the  $V_{OC}$  increases linearly with electron affinity until saturating at a value of 1.55 V once the affinity reaches around 2.9 eV. The  $J_{SC}$  increases as the electron affinity increases slowly until reaching a value of 12.17  $\text{mA/cm}^2$  at an affinity of 3.3 eV, afterward, it declines. Similarly, the filling factor presents a slowly increasing trend with an increase of electron affinity. The maximum FF is 79.51% at an electron affinity of 3.2 eV. The PCE has a maximum value of 15.01% when the electron affinity of the HTL is set to 3.2 eV.

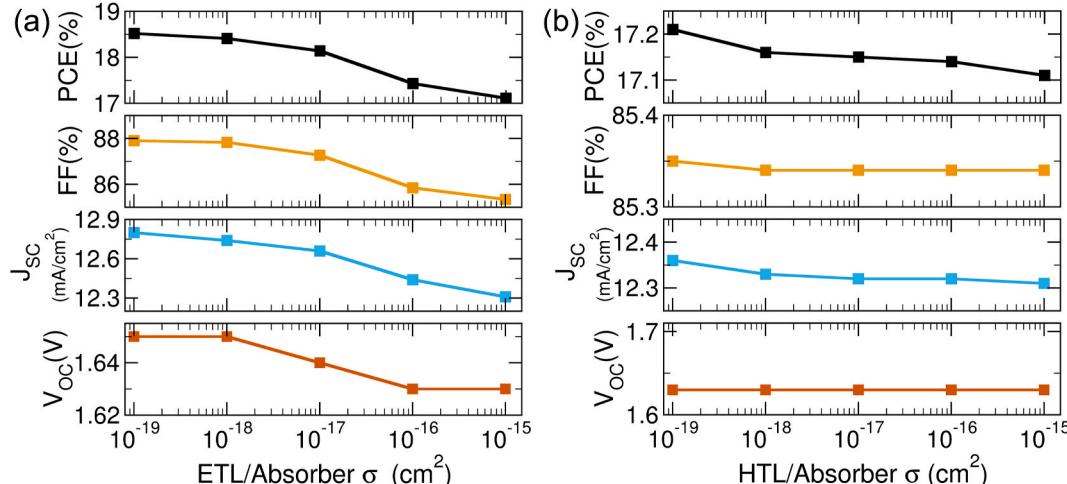
Using this optimized electron affinity value, we examined the effect of capture cross-section at the interfaces. The results shown in Fig. 7 show that capture cross-section does not have as much impact on the performance of  $\text{MAGeI}_3$  as it does in the  $\text{FASnI}_3$ . At the ETL/absorber interface, decreasing the capture cross-section improves the performance since all three parameters (FF,  $J_{SC}$ , and  $V_{OC}$ ) increase as the cross-section of the trap defects is reduced. At the HTL/absorber interface, the three parameters stay constant over the cross-section range considered with a minimal increase as the cross-section is reduced and thus the 17.21% PCE. From these values, the capture cross-section used for the rest of the simulations of  $\text{MAGeI}_3$  were kept unchanged.

Finally, the thicknesses of all the layers were varied. As seen from

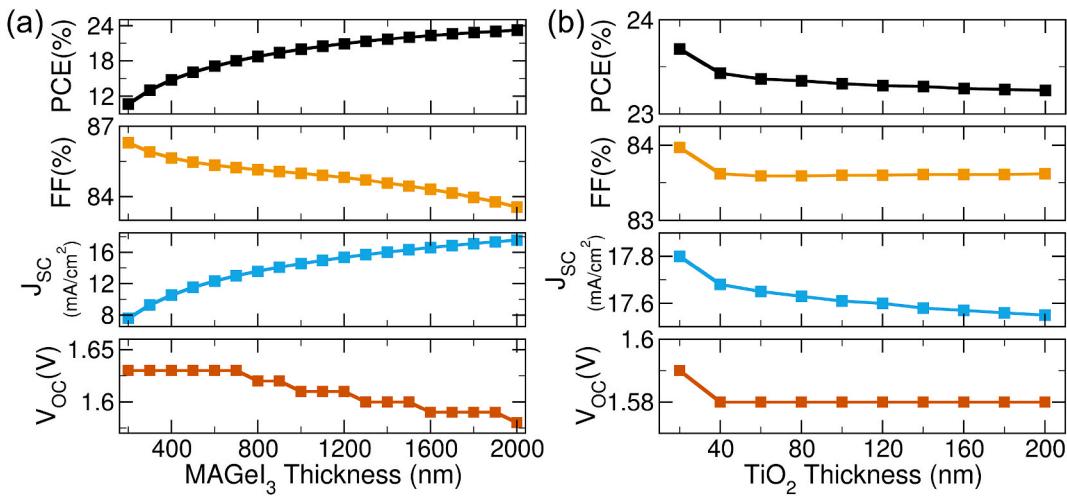
Fig. 8 (a), the PCE improves with increasing thickness of  $\text{MAGeI}_3$ . The rate of increase as the film thickness increases is not saturating as it was in the FA-based cell until reaching a thickness of 2000 nm. We have chosen 2000 nm as the thickness of  $\text{MAGeI}_3$ . The thickness of the HTL has minimal effect on the overall performance of the device. For the HTL layer, our calculations show that the PCE will stay around 23.24%, FF around 83.6%,  $J_{SC}$  at 17.55  $\text{mA/cm}^2$ , and  $V_{OC}$  at 1.58 V over a range of thickness from 20 to 200 nm. There is a decrease for all three parameters as the thickness of the ETL increases and, since the top subcell should be as thin as possible so that more light can reach the bottom cell, we choose 20 nm for HTL and ETL. The final configuration for the optimized  $\text{MAGeI}_3$  subcell and the I-V characteristics is summarized in Table 4.

### 3.2. Tandem solar cell simulation

In simulating the tandem solar cell, the bottom subcell is illuminated by the light filtered by the top subcell. The filtered light is calculated using Eqn. (1) and thus, the current matching condition (the top and bottom subcell having the same  $J_{SC}$ ) is satisfied. We note that a thinning of the top subcell is required to match the  $J_{SC}$  of the bottom subcell. To find the right combination of thickness, filtered spectra  $S(\lambda)$  for several different thicknesses of the top subcell are calculated. The thickness of the bottom cell is also varied for each spectrum. Fig. 9 presents the simulated  $J_{SC}$  of the top subcell (black line) as a function of thickness



**Fig. 7.** PCE, FF,  $J_{SC}$ , and  $V_{OC}$  as a function of capture cross-section at (a) the ETL/absorber interface and (b) the HTL/absorber interface for the  $\text{MAGeI}_3$  absorber.

Fig. 8. PCE, FF,  $J_{SC}$ , and  $V_{OC}$  as a function of (a) absorber thickness and (b) ETL thickness.

**Table 4**  
Optimized  $\text{MAGeI}_3$  subcell.

Parameters	Spiro-OMeTAD	$\text{TiO}_2$	$\text{MAGeI}_3$	HTL/ $\text{MAGeI}_3$	$\text{MAGeI}_3$ /ETL
Electron affinity (eV)	3.2	3.6	3.98	–	–
Capture cross-section ( $\text{cm}^2$ )	–	–	–	$1 \times 10^{-15}$	$1 \times 10^{-15}$
Thickness (nm)	20	20	2000	–	–
I-V characteristics					
$V_{OC}$ (V)	$J_{SC}$ ( $\text{mA/cm}^2$ )	FF (%)	PCE (%)		
1.59	17.80	83.97	23.69		

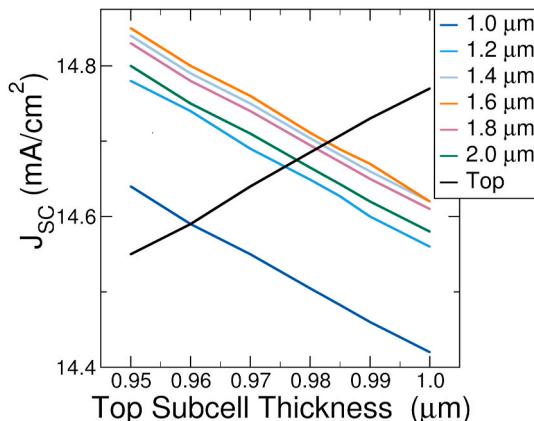


Fig. 9. Simulated  $J_{SC}$  of the top subcell (black line) as a function of thickness and the  $J_{SC}$  of the bottom subcell for several thicknesses (color lines). The matching condition requires that equal short circuit current flows in the device thus for each thickness of the bottom subcell there is one particular thickness of the top subcell.

along with the short-circuit current of the bottom subcell for several thicknesses (color lines). The best current matching condition is obtained with a top subcell thickness of 983 nm and bottom subcell thickness of 1600 nm, both having  $J_{SC} = 14.70 \text{ mA/cm}^2$ . The J-V curve for this configuration and those of the individual subcells are shown in Fig. 10. The I-V characteristics are presented in Table 5.

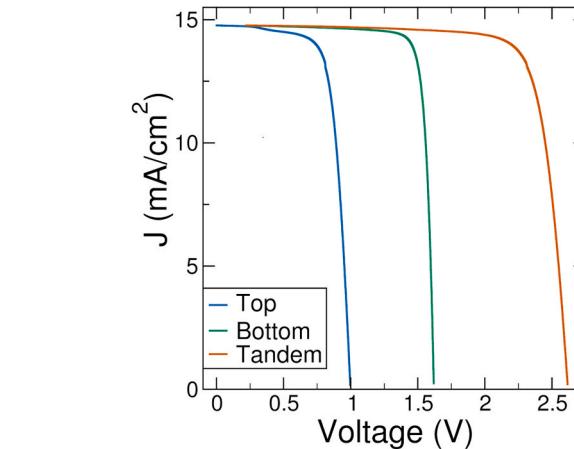


Fig. 10. Simulated J-V curve of the individual top subcell, the bottom subcell, and the tandem cell under the current matching condition.

**Table 5**  
I-V characteristics of the individual subcells and the tandem cell.

Cell	$V_{OC}$ (V)	$J_{SC}$ ( $\text{mA/cm}^2$ )	FF (%)	PCE (%)
Top subcell	1.62	14.70	85.44	20.31
Bottom subcell	1.01	14.70	71.68	17.10
tandem	2.63	14.70	79.80	30.85

#### 4. Conclusion

In this study, the numerical simulation of a monolithic 2-terminal all-perovskite tandem solar cell has been analyzed. The electron affinity of the electron and hole transport layers, the cross-section of defects, and the thickness of each component were varied using the SCAPS-1D solar cell simulator to understand their effect on the PCE. The simulation of the tandem device was done with the bottom subcell being illuminated with the light filtered by the top subcell, thus ensuring a realistic analysis. Given the current matching condition, our simulation results showed that the  $J_{SC}$  of the tandem device is limited by the  $J_{SC}$  of the bottom subcell. Thinning of the top subcell is necessary to match the current across the device. While the  $J_{SC}$  of the tandem device is smaller than the currents of the optimized individual subcells, a high  $V_{OC}$  of 2.63 V in the tandem device results in a significantly higher PCE of 30.85% compared to that of individual subcells.

The optimal thickness of the subcells found was  $1.6\ \mu\text{m}$  and  $983\ \text{nm}$ . The calculated PCE for those thicknesses will be higher than experimental values, given that the calculations consider only the dominant scattering channel, trap defects at the interface, and ignore scattering at grain boundaries. However, if we reduce the thickness of both cells to be below  $1\ \mu\text{m}$ , we still see a large PCE. For instance, when the thickness of the  $\text{FASnI}_3$  is set to  $1\ \mu\text{m}$ , the current matching condition requires the layer  $\text{MAGeI}_3$  to be  $961\ \text{nm}$  and the results we obtain are that the  $J_{\text{SC}}$  is  $14.6\ \text{mA/cm}^2$ ,  $V_{\text{OC}}$  is  $2.63\ \text{V}$ , FF is 80%, and PCE is reduced from the optimal 30.85% to 30.73%. Overall, these results suggest that lead-free perovskites can compete with lead-based devices in all-perovskite tandem solar cells. Further improvement in the performance of the tandem device can be achieved by utilizing a bottom subcell that can provide higher  $J_{\text{SC}}$ .

## CRediT authorship contribution statement

**Arman U. Duha:** Conceptualization, Methodology, Software, Validation, Formal analysis, Investigation, Data curation, Writing – original draft, Writing – review & editing, Visualization. **Mario F. Borunda:** Conceptualization, Validation, Data curation, Writing – original draft, Writing – review & editing, Visualization, Project administration, Funding acquisition, Supervision.

## Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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