Real-ESSI Simulator Domain Specific Language

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http://real-essi.us

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Contents

L	Inpu	ıt, Don	nain Specific Language (DSL) 1991-2005-2010-2011-2012-2015-2016-2017-2020-2021-	3
	1.1	Chapte	er Summary and Highlights	4
	1.2	Introd	uction	4
	1.3	Domai	in Specific Language (DSL), English Language Binding	5
		1.3.1	Running Real-ESSI	5
		1.3.2	Finishing Real-ESSI Program Run	7
		1.3.3	Real-ESSI Variables, Basic Units and Flow Control	8
		1.3.4	Modeling	12
			Modeling, Material Model: Adding a Material Model to the Finite Element Model	14
			Modeling, Material Model: Linear Elastic Isotropic Material Model	15
			Modeling, Material Model: Cross Anisotropic Linear Elastic Material Model	16
			Modeling, Material Model: von Mises Associated Material Model with Linear Isotropic	
			and/or Kinematic Hardening	17
			Modeling, Material Model: von Mises Associated Material Model with Isotropic Hard-	
			ening and/or Armstrong-Frederic Nonlinear Kinematic Hardening	18
			Modeling, Material Model: Drucker-Prager Associated Material Model with Linear	
			Isotropic and/or Kinematic Hardening	19
			Modeling, Material Model: Drucker-Prager Associated Material Model with Isotropic	
			Hardening and/or Armstrong-Frederick Nonlinear Kinematic Hardening \dots	20
			Modeling, Material Model: Drucker-Prager Associated Material Model with Isotropic	
			Hardening and/or Armstrong-Frederick Nonlinear Kinematic Hardening and	
			Nonlinear Duncan-Chang Elasticity	21
			Modeling, Material Model: Drucker-Prager Nonassociated Material Model with Linear	
			Isotropic and/or Kinematic Hardening	22
			Modeling, Material Model: Drucker-Prager Nonassociated Material Model with Linear	
			Isotropic and/or Armstrong-Frederick Nonlinear Kinematic Hardening	23

Modeling, Material Model: Hyperbolic Drucker-Prager Nonassociated Material Model	
with Linear Isotropic and/or Armstrong-Frederick Nonlinear Kinematic Hard-	
ening	25
Modeling, Material Model: Rounded Mohr-Coulomb Associated Linear Isotropic Hard-	
ening Material Model	27
Modeling, Material Model: Cam Clay Material Model	28
Modeling, Material Model: von Mises Associated Multiple Yield Surface Material Model 2	29
Modeling, Material Model: von Mises Associated Multiple Yield Surface Material Model	
that Matches G/G_{max} Curves $\dots \dots \dots$	30
Modeling, Material Model: Drucker-Prager Nonassociated Multi-Yield Surface Material	
Model	31
Modeling, Material Model: Drucker-Prager Nonassociated Material Model that Matches	
G/G_{max} Curves	33
Modeling, Material Model: Rounder Mohr-Coulomb Nonassociated Multi-Yield Surface	
Material Model	35
Modeling, Material Model: Tsinghhua Liquefaction Material Model	37
Modeling, Material Model: SANISand Material Model, version 2004	39
Modeling, Material Model: SANISand Material Model, version 2008	1
Modeling, Material Model: Cosserat Linear Elastic Material Model	14
Modeling, Material Model: von Mises Cosserat Material Model	15
Modeling, Material Model: Uniaxial Linear Elastic, Fiber Material Model 4	l 6
Modeling, Material Model: Stochastic Uniaxial Linear Elastic Model	17
Modeling, Material Model: Stochastic Uniaxial Nonlinear Armstrong Frederick Model . 4	18
Modeling, Material Model: Uniaxial Nonlinear Concrete, Fiber Material Model, version	
02	50
Modeling, Material Model: Faria-Oliver-Cervera Concrete Material	51
Modeling, Material Model: Plane Stress Layered Material	52
Modeling, Material Model: Uniaxial Nonlinear Steel, Fiber Material Model, version 01 5	53
Modeling, Material Model: Uniaxial Nonlinear Steel, Fiber Material Model, version 02 5	54
Modeling, Material Model: Plane Stress Plastic Damage Concrete Material 5	55
Modeling, Material Model: Plane Stress Rebar Material	6
Modeling, Nodes: Adding Nodes	57
Modeling, Nodes: Adding Stochastic Nodes	8
Modeling, Nodes: Define Nodal Physical Group	59
Modeling, Nodes: Adding Nodes to Nodal Physical Group	50

Modeling, Nodes: Removing Nodal Physical Group	61
Modeling, Nodes: Print Nodal Physical Group	62
Modeling, Nodes: Removing Nodes	63
Modeling, Nodes: Adding Nodal Mass, for 3DOFs and/or 6DOFs	64
Modeling, Finite Element: Adding Finite Elements	65
Modeling, Finite Element: Define Finite Element Physical Group	66
Modeling, Finite Element: Adding Elements to Physical Element Group	67
Modeling, Finite Element: Remove Physical Finite Element Group	68
Modeling, Finite Element: Print Physical Finite Element Group	69
Modeling, Finite Element: Remove Finite Element	70
Modeling, Finite Element: Truss Element	71
Modeling, Finite Element: Kelvin-Voigt Element	72
Modeling, Finite Element: Inerter Element	73
Modeling, Finite Element: Shear Beam Element	74
Modeling, Finite Element: Stochastic Shear Beam Element	75
Modeling, Finite Element: Elastic Beam–Column Element	76
Modeling, Finite Element: Large Displacement Elastic Beam–Column Element, with	
Corotational Transformation	79
Modeling, Finite Element: Timoshenko Elastic Beam–Column Element	80
Modeling, Finite Element: Timoshenko Elastic Beam–Column Element with Directional	
Shear Correction Coefficients	82
Modeling, Finite Element: Adding 1D Fiber to a Beam Cross Section	84
Modeling, Finite Element: Adding Fiber Section to the Finite Element Model	85
Modeling, Finite Element: 3D Displacement Based Fiber Beam-Column Element	86
Modeling, Finite Element: 3D Displacement Based Fiber Beam-Column Element with	
Corotational Coordinate Transformation	87
Modeling, Finite Element: 3DOF+6DOF=9DOF Beam-Column Element	88
Modeling, Finite Element: 4 Node ANDES Shell with Drilling DOFs	90
Modeling, Finite Element: 3 Node ANDES Shell with Drilling DOFs	91
Modeling, Finite Element: 4 Node Shell NLDKGQ, or 4 Node Shell Xin-Zheng-Lu	92
Modeling, Finite Element: Inelastic Layered Shell Section	93
Modeling, Finite Element: ElasticMembranePlaneStress Element (to be removed!)	94
$Modeling, \ Finite \ Element: \ Inelastic Membrane Plane Stress \ Element \ (to \ be \ removed!) .$	95
Modeling, Finite Element: SuperElementLinearElasticImport	96
Modeling, Finite Element: 8 Node Brick Element	98

Modeling, Finite Element: 20 Node Brick Element	100
Modeling, Finite Element: 27 Node Brick Element	102
Modeling, Finite Element: Variable 8-27 Node Brick Element	104
Modeling, Finite Element: 8 Node Brick u-p Element	106
Modeling, Finite Element: 20 Node Brick u-p Element	109
Modeling, Finite Element: 27 Node Brick u-p Element	112
Modeling, Finite Element: 8 Node Brick u-p-U Element	115
Modeling, Finite Element: 20 Node Brick u-p-U Element	118
Modeling, Finite Element: 27 Node Brick u-p-U Element	121
Modeling, Finite Element: 8 Node Cosserat Brick Element	124
Modeling, Finite Element: Bonded Contact/Interface/Joint Element	125
${\sf Modeling, Finite \; Element: \; Coupled \; Bonded \; Contact/Interface/Joint \; Element \; . \; . \; . \; . }$	126
${\sf Modeling,FiniteElement:ForceBasedDryHardContact/Interface/JointElement..}$	127
${\sf Modeling, Finite \; Element: \; Force \; Based \; Dry \; Soft \; Contact/Interface/Joint \; Element } . .$	128
Modeling, Finite Element: Force Based Coupled Hard Contact/Interface/Joint Element	130
Modeling, Finite Element: Force Based Coupled Soft Contact/Interface/Joint Element	132
Modeling, Finite Element: Stress Based Dry Hard Contact/Interface/Joint Element	
with Elastic Perfectly Plastic Shear Behavior	134
Modeling, Finite Element: Stress Based Dry Hard Contact/Interface/Joint Element	
with Nonlinear Hardening Shear Behavior	136
Modeling, Finite Element: Stress Based Dry Hard Contact/Interface/Joint Element	
with Nonlinear Hardening and Softening Shear Behavior	138
Modeling, Finite Element: Stress Based Dry Soft Contact/Interface/Joint Element with	
Elastic Perfectly Plastic Shear Behavior	141
Modeling, Finite Element: Stress Based Dry Soft Contact/Interface/Joint Element with	
Nonlinear Hardening Shear Behavior	143
Modeling, Finite Element: Stress Based Dry Soft Contact/Interface/Joint Element with	
Nonlinear Hardening and Softening Shear Behavior	145
Modeling, Finite Element: Stress Based Coupled Hard Contact/Interface/Joint Element	
with Elastic Perfectly Plastic Shear Behavior	148
Modeling, Finite Element: Stress Based Coupled Hard Contact/Interface/Joint Element	
with Nonlinear Hardening Shear Behavior	150
Modeling, Finite Element: Stress Based Coupled Hard Contact/Interface/Joint Element	
with Nonlinear Hardening and Softening Shear Behavior	152

Modeling, Finite Element: Stress Based Coupled Soft Contact/Interface/Joint Element
with Elastic Perfectly Plastic Shear Behavior
Modeling, Finite Element: Stress Based Coupled Soft Contact/Interface/Joint Element
with Nonlinear Hardening Shear Behavior
Modeling, Finite Element: Stress Based Coupled Soft Contact/Interface/Joint Element
with Nonlinear Hardening and Softening Shear Behavior
Modeling, Finite Element: Neoprene Isolator Finite Element
Modeling, Finite Element: Lead Core Rubber Isolator/Dissipator Element
Modeling, Finite Element: Frictional Pendulum Isolator/Dissipator Finite Element ver-
sion01
Modeling, Finite Element: Frictional Pendulum Isolator/Dissipator Finite Element ver-
sion03
Modeling, Damping: Adding Rayleigh Damping
Modeling, Damping: Adding 3rd Order Caughey Damping
Modeling, Damping: Adding 4th Caughey Damping
Modeling, Constraints and Supports: Adding Constraints or Supports
Modeling, Constraints and Supports: Adding Stochastic Constraints or Supports 170
Modeling, Constraints and Supports: Free Constraint or Support
Modeling, Constraints and Supports: Add Tied/Connected Main-Fillower Nodes for
the Same DOFs
Modeling, Constraints and Supports: Adding Tied/Connected, Main-Follower Nodes
for Different DOFs
Modeling, Constraints and Supports: Remove Tied/Connected Main-Follower equal
DOFs
Modeling, Constraints and Supports: Adding Single Point Constraint to Nodes \dots 175
Modeling, Acceleration Field: Adding Acceleration/Inertia Field
Modeling, Loads: Nodal Loads
Modeling, Loads: Nodal Path Loads
Modeling, Loads: Nodal Loads From Reactions
Modeling, Loads: Selfweight Element Load
Modeling, Loads: Selfweight Nodal Load
Modeling, Loads: 8 Node Brick Surface Load with the Constant Pressure $\dots \dots 183$
Modeling, Loads: 8 Node Brick Surface Load with Variable Pressure
Modeling, Loads: 20Node Brick Surface Load with the Constant Pressure 185
Modeling, Loads: 20 Node Brick, Surface Load with Variable Pressure

Modeling, Loads: 27 Node Brick Surface Load with the Constant Pressure 187
Modeling, Loads: 27 Node Brick Surface Load with Variable Pressure
Modeling, Loads: Removing Loads
Modeling, Loads: Domain Reduction Method, DRM
Modeling, Wave Field for Creating DRM Loads: Add Wave Field
Modeling, Wave Field for Creating DRM Loads: Deconvolution
Modeling, Wave Field for Creating DRM Input: Motions
Modeling, Wave Field for Creating DRM Input: Forces
Modeling, Wave Field for Creating DRM Loads: Add Inclined Plane Wave Field from
Incident SV Wave Potential Magnitude
Modeling, Wave Field for Creating DRM Loads: Add Inclined Plane Wave Field from
Incident SV Wave Time Series Signal
Modeling, Wave Field for Creating DRM Loads: Add Inclined Plane Wave Field from
Incident P Wave Potential Magnitude
Modeling, Wave Field for Creating DRM Loads: Add Inclined Plane Wave Field from
Incident P Wave Time Series Signal
Modeling, Wave Field for Creating DRM Loads: DRM Inclined Motion
${\sf Modeling,\ Imposed\ Motions:\ through\ Loads,\ Motion\ Time\ History,\ Constant\ Time\ Step\ 211}$
Modeling, Imposed Motions: through Loads, Stochastic Motion Time History, Constant
Time Step
Modeling, Imposed Motions: through Loads, Stochastic Random Process Motions,
Constant Time Step
Modeling, Imposed Motions: through Loads, Motion Time History, Variable Time Step 215
Modeling, Imposed Motions: Adding Load for Uniform Acceleration Time History 216
Modeling, Imposed Motions: Remove Imposed Motions
Modeling, Random Variable: Adding Gaussian Random Variables
Modeling, Random Variable: Adding Gaussian Random Variables with Location 219
Modeling, Random Variable: Adding Lognormal Random Variables
Modeling, Random Variable: Adding Lognormal Random Variables with Location \dots 221
Modeling, Random Variable: Adding Lognormal Random Variables using Logarithmic
Input
Modeling, Random Variable: Adding Lognormal Random Variables using Logarithmic
Input with Location
Modeling, Random Variable: Adding Gamma Random Variables using Shape and Scale
Parameters

Modeling, Random Variable: Adding Gamma Random Variables using Shape and Scale	
Parameters with Location	225
Modeling, Random Variable: Adding Gamma Random Variables using Mean and Stan-	
dard Deviation Parameters	226
Modeling, Random Variable: Adding Gamma Random Variables using Mean and Stan-	
dard Deviation Parameters with Location	227
Modeling, Random Variable: Adding Weibull Random Variables using Shape and Scale	
Parameters	228
Modeling, Random Variable: Adding Weibull Random Variables using Shape and Scale	
Parameters with Location	229
Modeling, Random Variable: Remove Random Variables	230
Modeling, Random Variable: Hermite Polynomial Chaos Expansion	231
Modeling, Random Variable: Output Hermite Polynomial Chaos Expansion Result	232
${\sf Modeling,\ Random\ Variable:\ Hermite\ Polynomial\ Chaos\ Expansion\ \&\ Output\ Results\ .}$	233
Modeling, Random Field: Adding Random Field with Dimension and Order	234
Modeling, Random Field: Define Global Dimension Index of Random Field	235
Modeling, Random Field: Define Global Dimension Index of Random Field from File	
Input	236
Modeling, Random Field: Set Number of Polynomial Chaos Terms of Random Field .	237
Modeling, Random Field: Adding Random Field with Zero Correlation	238
Modeling, Random Field: Adding Random Field with Exponential Correlation	239
Modeling, Random Field: Adding Random Field with Triangular Correlation	240
Modeling, Random Field: Adding Random Field with Exponentially Damped Cosine	
Correlation	241
Modeling, Random Field: Adding Random Field with Gaussian Correlation	242
Modeling, Random Field: Remove Random Fields	243
Modeling, Random Field: Adding Random Variable to Random Field	244
Modeling, Random Field: Remove Random Variable From Random Field	245
Modeling, Random Field: Hermite Polynomial Chaos Karhunen Loève Expansion	246
Modeling, Random Field: Hermite Polynomial Chaos Karhunen Loève Expansion with	
Inverse Order	247
Modeling, Random Field: Hermite Polynomial Chaos Karhunen Loève Expansion with	
Number of FE Elements Larger than Dimension of Hermite Polynomials	248
Modeling, Random Field: Hermite Polynomial Chaos Karhunen Loève Expansion Using	
HDF5 Input	250

	Modeling, Random Field: Hermite Polynomial Chaos Karhunen Loève Expansion with	
	Inverse Order Using HDF5 Input	252
	Modeling, Random Field: Output Hermite Polynomial Chaos Karhunen Loève Expan-	
	sion Result	254
	Modeling, Random Field: Adding Random Field from Hermite Polynomial Chaos	
	Karhunen Loève Expansion HDF5 File	256
	Modeling, Random Field: Adding Random Field from Marginal Distribution and Cor-	
	relation	258
	Modeling, Random Field: Add Triple Product of Hermite Polynomial Chaos Basis	259
	Modeling, Random Field: Add Double Product of Hermite Polynomial Chaos Basis	260
	Modeling, Random Field: Generate Triple Product of Hermite Polynomial Chaos Basis	261
	Modeling, Random Field: Generate Double Product of Hermite Polynomial Chaos Basis	263
	Modeling, Random Field: Add Triple Product of Hermite Polynomial Chaos Basis Using	
	HDF5 Input	265
	Modeling, Random Field: Add Double Product of Hermite Polynomial Chaos Basis	
	Using HDF5 Input	267
	Modeling, Solid-Fluid Interaction: Adding Solid-Fluid Interface	269
	Modeling, Solid-Fluid Interaction: Defining Solid-Fluid Interface, ESSI Element Nodes	270
	${\sf Modeling, Solid-Fluid\ Interaction:\ Defining\ Solid-Fluid\ Interface,\ ESSI\ Element\ Faces\ .}$	271
	Modeling, Solid-Fluid Interaction: Defining Solid-Fluid Interface FOAM Nodes	273
	Modeling, Solid-Fluid Interaction: Defining Solid-Fluid Interface FOAM Faces	274
1.3.5	Simulation	276
	Simulation, Solvers: Sequential Solvers	277
	Simulation, Solvers: Parallel Solvers	278
	Simulation: Static Solution Advancement	281
	Simulation: Dynamic Solution Advancement with the Constant Time Step	282
	Simulation: Dynamic Solution Advancement with Variable Time Step	283
	Simulation: Generalized Eigenvalue Analysis	284
	Simulation: Displacement Control	285
	Simulation: Load, Control, Factor Increment	286
	Simulation: Dynamic Integrator, Newmark Method	287
	Simulation: Dynamic Integrator, Hilber Hughes Taylor, HHT, α Method	288
	Simulation: Absolute Convergence Criteria	289
	Simulation: Average Convergence Criteria	290
	Simulation: Relative Convergence Criteria	291

		Simulation: Solution Algorithms	292
		Simulation: Constitutive Integration Algorithm	293
		Simulation: Status Check	29!
		Simulation: Save State	296
		Simulation: Restart Simulation	297
		Simulation: Return Value for simulate Command	298
		Simulation: New Elastic Loading Case	308
		Simulation: Combine Elastic Load Cases	309
		Simulation, Dynamic Solution Advancement for Solid-Fluid Interaction	310
		Simulation, Dynamic Solution Advancement for Stochastic Finite Element Method $$. $$	31
		Simulation, Sobol Sensitivity Analysis	312
		Simulation: 3D 3C Wave Field Inversion	316
	1.3.6	Output Options	318
		Output Options: Enable/Disable Output	319
		Output Options: Enable/Disable Element Output	320
		Output Options: Enable/Disable Displacement Output $\ldots \ldots \ldots \ldots$	32
		Output Options: Enable/Disable Acceleration Output	322
		Output Options: Enable/Disable Asynchronous Output	323
		Output Options: Output Every n Steps	324
		Output Options: Output Support Reactions	325
1.4	Checki	ng the Model	326
1.5	Constit	cutive Testing	327
1.6	List of	Available Commands (tentative, not up to date)	329
1.7	List of	reserved keywords	339
1.8	Integra	ted Development Environment (IDE) for DSL	352
1.9	Mesh (Generation using GiD	353
1.10	Model	Development and Mesh Generation using gmesh	354
1.11	Model	Input File Editing using Sublime	355

Chapter 1

Input, Domain Specific Language (DSL)

1991-2005-2010-2011-2012-2015-2016-2017-2020-2021-

1.1 Chapter Summary and Highlights

1.2 Introduction

This chapter presents the domain specific language developed for the Real-ESSI. The language was designed with a primary goal of developing FEA models and interfacing them with various Real-ESSI functionalities. In addition to that, syntax is used to self-document models, provide physical-unit safety, provide common flow control structures, provide modularity to scripting via user functions and "include" files, and provide an interactive environment within which models can be created, validated and verified.

The development of Real-ESSI Domain specific language (DSL) (the Finite Element Interpreter, 田) is based on LEX (Lesk and Schmidt, 1975) and YACC (Johnson, 1975).

Self-documenting ensures that the resulting model script is readable and understandable with little or no reference to the users manual. This is accomplished by providing a command grammar structure and wording similar to what would be used in a natural language description of the problem.

FEA analysis is unitless, that is, all calculations are carried out without referencing a particular unit system. This leaves the task of unit correctness up to the user of FEA analysis. This represents a recurring source of error in FEA analysis. Physical unit safety is enforced in Real-ESSI by implementing all base variables as physical quantities, that is, all variables have a unit associated with it. The adimensional unit is the base unit for those variables which have no relevant unit (like node numbers). Command calls are sensitive to units. For example, the node creation command call expects the node coordinates to be input with the corresponding units (length in this case). Additionally, the programming/command language naturally supports operation with units like arithmetic operations (quantities with different unit types will not add or subtract but may be multiplied). This approach to FEA with unit awareness provides an additional layer of security to FEA calculations, and forces the user to carefully think about units. This can help catch some common mistakes.

The Real-ESSI language provides modularity through the include directive/command, and user functions. This allows complex analysis cases to be parameterized into modules and functions which can be reused in other models.

Finally, an emphasis is placed on model verification and validation. To this end, Real-ESSI provides an interactive programming environment with all the ESSI syntax available. By using this environment, the user can develop tests to detect errors in the model that are not programming errors. For example, the user can query nodes and elements to see if they are set to appropriate states. Also, several standard tools are provided to check element validity (Jacobian, etc.).

The ESSI language provides reduced model development time by providing the aforementioned features along with meaningful error reporting (of syntax and grammatical errors), a help system, command completion and highlighting for several open source and commercial text editors.

Some additional ideas are given by Dmitriev (2004), Stroustrup (2005), Niebler (2005), Mernik et al. (2005), Ward (2003), etc.

1.3 Domain Specific Language (DSL), English Language Binding

Overview of the language syntax.

- Each command line has to end with a semicolon ";"
- Comment on a line begins with either "//" or "!" and last until the end of current line.
- Units are required (see more below) for all quantities and variables.
- Include statements allow splitting source into several files
- All variables are double precision (i.e. floats) with a unit attached.
- All standard arithmetic operations are implemented, and are unit sensitive.
- Internally, all units are represented in the base SI units (m s kg).
- The syntax ignores extra white spaces, tabulations and newlines. Wherever they appear, they are there for code readability only. (This is why all commands need to end with a semicolon).
- The user should be familiar with the list of the reserved keywords from Section 1.7 on page 339.

1.3.1 Running Real-ESSI

At the command line type "essi", to get to the ESSI prompt and start Real-ESSI in interactive mode.

Command line output

```
The Finite Element Interpreter Endeavor

The Real-ESSI Simulator
Modeling and Simulation of Earthquakes, and Soils, and Structures 
and their Interaction

Sequential processing mode.

Version Name : Real-ESSI Global Release, June2018. Release date: 
Jun 13 2018 at 11:02:19. Tag: adc085ae70

Version Branch : GLOBAL_RELEASE
Compile Date : Jun 13 2018 at 14:36:56

Compile User : jeremic
Compile Sysinfo : sokocalo 4.13.0-43-generic x86_64 GNU/Linux
```

```
Runtime User : jeremic
Runtime Sysinfo : sokocalo 4.13.0-43-generic x86_64 GNU/Linux
Time Now : Jun 13 2018 at 15:32:52
Days From Release : 0
PostProcessing Compatible Version: ParaView 5.1.2
PostProcessing Compatible Version: ESSI-pvESSI Date: Feb 15 2018 at 
11:00:28. Tag: 58fe430a19

Static startup tips:

* Remember: Every command ends with a semicolon ';'.

* Type 'quit;' or 'exit;' to finish.

* Run 'essi -h' to see available command line options.
```

A number of useful information about Real-ESSI is printed on the screen. From here, commands can be input manually or a file may be included via the include command which is as follows.

```
1 include "foobar.fei";
```

to include the file foobar.fei.

A more efficient way to start Real-ESSI and analyze an example is to pass input file name to the command line. Real-ESSI command to execute an input file immediately is done by issuing the following command: essi -f foobar.fei. This will execute essi directly on input file foobar.fei. After executing the file, the essi interpreter will continue in interactive mode unless the command line flag -n or --no-interactive is set. A list of command line options is available by calling essi from the command line as essi -h.

Command line output

```
The Finite Element Interpreter Endeavor
  The Real-ESSI Simulator
  Modeling and Simulation of Earthquakes, and Soils, and Structures \hookleftarrow
  and their Interaction
  Sequential processing mode.
Version Name
                  : Real-ESSI Global Release, June2018. Release date: \hookleftarrow
   Jun 13 2018 at 11:02:19. Tag: adc085ae70
                 : GLOBAL_RELEASE
Version Branch
Compile Date
                  : Jun 13 2018 at 14:36:56
Compile User
                  : jeremic
Compile Sysinfo : sokocalo 4.13.0-43-generic x86_64 GNU/Linux
                : jeremic
Runtime User
Runtime Sysinfo : sokocalo 4.13.0-43-generic x86_64 GNU/Linux
                  : Jun 13 2018 at 16:22:08
Time Now
Days From Release : 0
PostProcessing Compatible Version: ParaView 5.1.2
```

```
PostProcessing Compatible Version: ESSI-pvESSI Date: Feb 15 2018 at \hookleftarrow
   11:00:28. Tag: 58fe430a19
Static startup tips:
 * Remember: Every command ends with a semicolon ';'.
 * Type 'quit;' or 'exit;' to finish.
 * Run 'essi -h' to see available command line options.
The Real-ESSI Simulator
Modeling and Simulation of Earthquakes, and Soils, and Structures and \hookleftarrow
   their Interaction
Usage: essi [-cfhnsmbe FILENAME]
  -c --cpp-output
                                   : Output cpp version of the model.
 -f --filename [FILENAME]
                                  : run ESSI on a FILENAME.
 -h --help
                                  : Print this message.
  -n --no-interactive
                                   : Disable interactive mode.
 -s --set-variable
                                  : Set a variable from the command line.
  -d --dry-run
                                   : Do not execute ESSI API calls. \hookleftarrow
  Just parse.
 -m --model-name [NAME]
                                  : Set the model name from the \hookleftarrow
  command line.
  -p --profile-report [FILENAME] : Set the filename for the profiler \hookleftarrow
  report (and activate lightweight profiling)
Example to set a variable name from command line:
    essi -s a=10,b=20,c=30
Runs ESSI with variables a, b, and c set to 10, 20 and 30 respectively.
At this time, only ESSIunits::unitless variables can be set.
```

1.3.2 Finishing Real-ESSI Program Run

To properly finish Real-ESSI program run, and save and close all the output files, user has to use final, closure command:

```
1 bye;
```

Command bye; has to be included at the end of input file script, or at the end of each interactive/interpretative session. Command bye; ensures that Real-ESSI program gracefully exits simulation, and that all the output files are properly saved and closed. Proper finishing of simulation using Real-ESSI Simulator is very much necessary, while the choice of command bye; is done as an homage to Professor Knuth and his Literate Programming endeavor (Knuth, 1984), that is driving much of the Real-ESSI DSL development.

There are a number of alternative final commands, for example:

```
1 exit;
2 quit;
3 zdravo;
```

```
4
    vozdra;
 5
    dvojka;
 6
    voljno;
 7
    zaijian;
 8
    tschuess;
 9
    geia-sou;
10
    tchau;
11
    sair;
12
    khoda-hafez;
13
    doei;
14
    nasvidenje;
15
    ajde-bok;
16
    izhod;
17
    konec;
18
    czesc;
19
     ciao;
20
     hoscakal;
```

These additional, alternative final commands can all be written using original scripts:

```
zdravo ↔ здраво
vozdra ↔ воздра
dvojka ↔ двојка
voljno ↔ вољно
zaijian ↔ 再见
tschuess ↔ tschüss
geia-sou ↔ γεια σου
khoda-hafez ↔ hosçakal
```

1.3.3 Real-ESSI Variables, Basic Units and Flow Control

Variables are defined using the assignment (=) operator. For example,

```
var_x = 7;  //Results in the variable x be set to 7 (unitless)
var_y = 3.972e+2;  //Scientific notation is available.
```

The language contains a list of reserved keywords. Throughout this documentation, reserved keywords are highlighted in blue or red.

All standard arithmetic operations are available between variables. These operations can be combined arbitrarily and grouped together with parentheses.

```
var_a = var_x + var_y;  // Addition
var_b = var_x - var_y;  // Subtraction
var_c = var_x * var_y;  // Product
var_d = var_x / var_y;  // Quotient
var_e = var_y % var_x;  // Modulus (how many times x fits in y)
```

The 'print' command can be used to display the current value of a variable.

```
print var_x;
print var_y;
print var_a;
print var_b;
print var_c;
print var_d;
print var_e;
```

Command line output

```
var_x = 7 []
var_y = 397.2 []
var_a = 404.2 []
var_b = -390.2 []
var_c = 2780.4 []
var_d = 0.0176234 []
var_e = 5.2 []
```

Here the "unit" (sign) [] means that the quantities are unitless.

The command 'whos' is used to see all the currently defined variables and their values. After a fresh start of essi, needed to clear up all the previously defined variables, command whos;' produces a list of predefined variables:

Command line output

```
ESSI > whos;
Declared variables:
                           86400 [s]
  *
         Day =
         GPa =
                               1 [GPa]
  *
                            3600 [s]
        Hour =
  *
          Hz =
                               1 [Hz]
         MPa =
                                1 [MPa]
      Minute =
                               60 [s]
  *
           N =
                                1 [N]
          Pa =
                                1 [Pa]
        Week =
                          604800 [s]
  *
                                1 [cm]
  *
           cm =
                          0.3048 [m]
        feet =
          ft =
                          0.3048 [m]
```

```
9.81 [m*s^-2]
            g
                           0.0254 [m]
         inch =
           kN =
                                1 [kN]
          kPa =
                                1 [kPa]
           kg =
                                1 [kg]
                          4448.22 [N]
          kip =
           km
                                1 [km]
                     6.89476e+06 [Pa]
          ksi =
          lbf =
                         4.44822 [N]
          lbm =
                        0.453592 [kg]
            m =
                                1 [m]
                          1609.35 [m]
         mile =
                                1 [mm]
           mm =
           pi =
                          3.14159 []
                          6894.76 [Pa]
          psi =
            s =
                               1 [s]
         yard =
                           0.9144 [m]
         locked variable
ESSI >
```

Predefined variables shown above have a preceding asterisk to show they are locked variables which cannot be modified. The purpose of these locked variables are to provide names for units. Imperial units are also supported as shown above.

The units for variable are shown between the brackets. Note that unit variables have the same name as their unit, which is not the case for user defined variables. Variables preceded by a star (*) are locked variables which can't be modified.

For example, the variable 'm' defines 'meter'. So to define a new variable L1 which has meter units we do:

Even though L2 was created with millimeter units, it is stored in base units.

```
print L2; displays
```

Command line output

```
L2 = 0.04 [m]
```

As additional examples, let us define few forces:

```
1 F1 = 10*kN;
2 F2 = 300*N;
3 F3 = 4*kg*g;
```

Here g is the predefined acceleration due to gravity.

Arithmetic operations do check (and enforce) for unit consistency. For example, foo = L1 + F1; produces an error because units are not compatible. However, bar = L1 + L2; is acceptable. On the other hand,

multiplication, division and modulus, always work because the result produces a quantity with new units (except when the adimensional quantity is involved).

```
1 A = L1*L2;
2 Stress_n = F1 / A;
```

Units for all variables are internally converted to SI units (kg - m - s) and stored in that unit system. Variables can be *displayed* using different units by using the [] operator. This does not change the variable, it just displays the value of variable with required unit. For example,

```
print Stress_n; //Print in base SI units.
print Stress_n in Pa; //Print in Pascal
print Stress_n in kPa; //Print in kilo Pascal
```

Command line output

```
Stress_n = 250000 \text{ [kg*m^-1*s^-2]}

Stress_n = 250000 \text{ [Pa]}

Stress_n = 250 \text{ [kPa]}
```

The DSL provides functions to test the physical units of variables. For example,

```
print isForce(F1);
```

Will print an adimensional, Boolean 1 because F1 has units of force. While,

```
print isPressure(F);
```

will print an adimensional, Boolean 0. The language also provides comparison of quantities with same units (remember all values are compared in SI Units).

```
print F1 > F2;
```

will print an adimensional, Boolean 1 since F1 is greater than F2.

The program flow can be controlled with if and while statements, i.e.:

```
if (isForce(F1))
1
2
3
                  // This will be executed
  print F1;
4
  };
5
6
  if (isForce(L1))
7
   print L1;
                  // This will not.
8
  };
```

Note the necessary semicolon (;) at the closing brace. Unlike C/C++, the braces are always necessary. Closing colon is also always necessary.

The "else" statement is also available:

```
1
      (isForce(L1))
2
  {
3
   print L1;
                  // This will not execute
4
  else
5
  {
6
7
   print L2;
                  // This will execute instead
8
  };
```

While loops are also available:

```
i = 0;
while(i < 10)
{
  print i;
  i = i +1;
};
</pre>
```

1.3.4 Modeling

This section details ESSI modeling commands. Angle brackets <> are used for quantity or variable placeholder, that is, they indicate where user input goes. Within the angle brackets, the expected unit type is given as well, i.e.. <L> means the command expects an input with a value and a length unit. The symbol <.> represents the adimensional quantity.

In addition to that, the vertical bar | ("OR" sign)) is used to separate two or more keyword options, i.e. [a|b|c] is used indicate keyword options a or b or c. The symbol |...| is used to denote where several long options exist and are explained elsewhere (an example of this is available below in a material model definitions).

All commands require unit consistency. Base units, SI or other can be used as indicated below:

- length, symbol L, units [m, inch, ft]
- mass, symbol M, units [kg, lbm],
- time, symbol T, units [s]

Derived units can also be used:

- angle, symbol rad (radian), unit [dimensionless, L/L]
- force, symbol N (Newton), units $[N, kN, MN, M*L/T^2]$,
- stress, symbol Pa (Pascal), units $[Pa, kPa, MPa, N/L^2, M/L/T^2]$

- ullet strain, symbol (no symbol), units [L/L]
- mass density, symbol (no symbol), units $\lceil M/L^3 \rceil$
- force density, symbol (no symbol), units $[M/L^2/T^2]$

All models have to be named: model name "model_name_string"; This is important as output files are named based on model name.

Each loading stage has to be named as well. A new loading stage¹ is defined like this:

new loading stage "loading stage name string";

In addition to model name, loading stage name is used for output file name for given loading stage.

¹See more in section 101.4.5 on page 97 in Jeremić et al. (1989-2025).

Modeling, Material Model: Adding a Material Model to the Finite Element Model

Adding constitutive material model to the finite element model/domain is done using command:

- Material number # (or alternatively No) is a distinct integer number used to uniquely identify this
 material.
- Mass density should be defined for each material (even if only static analysis is performed, for example
 if self weight is to be used as a loading stage).
- Depending on material model, there will be additional material parameters that are defined for each material model/type below:

Starting with version 03-NOV-2015 all elastic-plastic material models require explicit specification of the constitutive integration algorithm. More information on this can be found in 1.3.5. Only the material linear_elastic_isotropic_3d_LT ignores this option.

Choices for material_type are listed below.

1.4 List of Available Commands (tentative, not up to date)

```
add acceleration field # <.> ax = <accel> ay = <accel> az = <aaccel> ;
  |add constraint equal_dof with master node # <.> and slave node # <.> \hookleftarrow
      dof to constrain <.>;
  add constraint equal_dof with node # <.> dof <.> master and node # \leftrightarrow
3
      <.> dof <.> slave;
  add damping # <.> to element # <.>;
  add damping # <.> to node # <.>;
6 add damping # <.> type Caughey3rd with a0 = <1/time> a1 = <time> a2 = \leftrightarrow
      <time^3> stiffness_to_use = \leftrightarrow
      <Initial_Stiffness|Current_Stiffness|Last_Committed_Stiffness>;
7 add damping # <.> type Caughey4th with a0 = <1/time> a1 = <time> a2 = \leftrightarrow
      <time^3> a3 = <time^5> stiffness_to_use = \leftarrow
      <Initial_Stiffness|Current_Stiffness|Last_Committed_Stiffness>;
8 add damping # <.> type Rayleigh with a0 = <1/time> a1 = <time> \leftrightarrow
      stiffness\_to\_use = \leftarrow
      <Initial_Stiffness|Current_Stiffness|Last_Committed_Stiffness>;
  add domain reduction method loading # <.> hdf5_file = <string> ←
      scale_factor = <.>;
10 add domain reduction method loading # <.> hdf5_file = <string>;
   add element # <.> type 20NodeBrick using <.> Gauss points each \leftrightarrow
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>
      material # <.>;
12 add element # <.> type 20NodeBrick with nodes (<.>, <.>, <.>, \leftrightarrow
      <.>, <.>, <.>) use material # <.>;
  add element # <.> type 20NodeBrick_up using <.> Gauss points each \leftarrow
13
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>, \leftarrow
      material \# <.> and porosity = <.> alpha = <.> rho_s = <M/L^3>
      rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle
      K_s = \langle stress \rangle K_f = \langle stress \rangle;
  |add element # <.> type 20NodeBrick_up with nodes (<.>, <.>, <.>, \leftarrow
      <.>, <.>, <.>) use material # <.> and porosity = <.> alpha = <.> \leftrightarrow
      rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle \leftrightarrow
      k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
  add element # <.> type 20NodeBrick_upU using <.> Gauss points each ↔
15
      material # <.> and porosity = <.> alpha = <.> rho_s = <M/L^3> \leftrightarrow
      rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle
```

```
K_s = \langle stress \rangle K_f = \langle stress \rangle;
16 add element # <.> type 20NodeBrick_upU with nodes (<.>, <.>, \leftrightarrow
      <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> alpha = \leftrightarrow
      <.> rho_s = <M/L^3> rho_f = <M/L^3> k_x = <L^3T/M> k_y = \leftrightarrow
      <L^3T/M> k_z = <L^3T/M> K_s = <stress> K_f = <stress>;
   add element # <.> type 27NodeBrick using <.> Gauss points each \leftrightarrow
17
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>
      <.>, <.>, <.>, <.>, <.>) use material # <.>;
   add element # <.> type 27NodeBrick with nodes (<.>, <.>, <.>, \leftarrow
18
      <.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>) use material # <.>;
   add element # <.> type 27NodeBrick_up using <.> Gauss points each \leftrightarrow
19
      <.>, <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> \leftrightarrow
      alpha = <.> rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y \leftrightarrow
      = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
   add element # <.> type 27NodeBrick_up with nodes (<.>, <.>, <.>, \leftarrow
20
      <.>, <.>, <.>) use material # <.> and porosity = <.> alpha = <.> \leftrightarrow
      rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle \leftrightarrow
      k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
21 add element # <.> type 27NodeBrick_upU using <.> Gauss points each \leftarrow
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>, \leftarrow
      <.>, <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> \leftrightarrow
      alpha = <.> rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y \leftrightarrow
      = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
22 add element # <.> type 27NodeBrick_upU with nodes (<.>, <.>, \leftarrow
      <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> alpha = \leftrightarrow
      <.> rho_s = <M/L^3> rho_f = <M/L^3> k_x = <L^3T/M> k_y = \leftrightarrow
      <L^3T/M> k_z = <L^3T/M> K_s = <stress> K_f = <stress>;
23
   add element # <.> type 3NodeShell_ANDES with nodes (<.>, <.>) \leftarrow
      use material # <.> thickness = <l> ;
   add element # <.> type 4NodeShell_ANDES with nodes (<.>, <.>, \leftarrow
24
      <.>) use material # <.> thickness = <l> ;
25
   add element # <.> type 4NodeShell_MITC4 with nodes (<.>, <.>, \leftarrow
      <.>) use material # <.> thickness = <L>;
   add element # <.> type 4NodeShell_NewMITC4 with nodes (<.>, <.>, ←
      <.>) use material # <.> thickness = <L>;
   add element # <.> type 8_27_NodeBrick using <.> Gauss points each \hookleftarrow
27
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>
```

```
<.>, <.>, <.>, <.>, <.>) use material # <.>;
   add element # <.> type 8_27_NodeBrick with nodes (<.>, <.>, <.>, \leftarrow
28
      <.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>) use material # <.>;
29
   add element # <.> type 8_27_NodeBrick_up using <.> Gauss points each \hookleftarrow
      <.>, <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> \hookleftarrow
      alpha = <.> rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y \leftrightarrow
      = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
  add element # <.> type 8_27_NodeBrick_up with nodes (<.>, <.>, \leftarrow
30
      <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> alpha = \leftrightarrow
      <.> rho_s = <M/L^3> rho_f = <M/L^3> k_x = <L^3T/M> k_y = \leftrightarrow
      \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
   add element # <.> type 8_27_NodeBrick_upU using <.> Gauss points each \leftrightarrow
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>
      <.>, <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> \leftrightarrow
      alpha = <.> rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y \leftrightarrow
      = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
32
   add element # <.> type 8_27_NodeBrick_upU with nodes (<.>, <.>, \leftarrow
      <.>, <.>, <.>, <.>) use material # <.> and porosity = <.> alpha = \leftrightarrow
      <.> rho_s = <M/L^3> rho_f = <M/L^3> k_x = <L^3T/M> k_y = \leftrightarrow
      <L^3T/M> k_z = <L^3T/M> K_s = <stress> K_f = <stress>;
33 add element # <.> type 8NodeBrick using <.> Gauss points each \leftrightarrow
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>) use \hookleftarrow
      material # <.>;
   add element # <.> type 8NodeBrick with nodes (<.>, <.>, <.>, \leftrightarrow
34
      <.>, <.>, <.>, <.>) use material # <.>;
   add element # <.> type 8NodeBrick_up using <.> Gauss points each \leftrightarrow
35
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>) use \hookleftarrow
      material # <.> porosity = <.> alpha = <.> rho_s = <M/L^3> rho_f \leftrightarrow
      = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle K_s = \langle L^3T/M \rangle
      <stress> K_f = <stress>;
   add element # <.> type 8NodeBrick_up with nodes (<.>, <.>, <.>, \leftrightarrow
36
      <.>, <.>, <.>, <.>) use material # <.> porosity = <.> alpha = <.> \leftrightarrow
      rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle \leftrightarrow
      k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
   add element # <.> type 8NodeBrick_upU using <.> Gauss points each \hookleftarrow
37
      direction with nodes (<.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>) use \leftarrow
      material # <.> porosity = <.> alpha = <.> rho_s = <M/L^3> rho_f \hookleftarrow
      = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle k_z = \langle L^3T/M \rangle K_s = \langle L^3T/M \rangle
```

```
<stress> K_f = <stress>;
    add element # <.> type 8NodeBrick_upU with nodes (<.>, <.>, <.>, \leftarrow
38
        <.>, <.>, <.>, <.>) use material # <.> porosity = <.> alpha = <.> \leftrightarrow
       rho_s = \langle M/L^3 \rangle rho_f = \langle M/L^3 \rangle k_x = \langle L^3T/M \rangle k_y = \langle L^3T/M \rangle \leftrightarrow
       k_z = \langle L^3T/M \rangle K_s = \langle stress \rangle K_f = \langle stress \rangle;
    add element # <.> type beam_9dof_elastic with nodes (<.>, <.>) \hookleftarrow
        cross_section = <area> elastic_modulus = <F/L^2> shear_modulus = \leftrightarrow
       <F/L^2> torsion_Jx = <length^4> bending_Iy = <length^4> bending_Iz \leftrightarrow
       = <length^4> mass_density = <M/L^3> xz_plane_vector = (<.>, <.>, \hookleftarrow
        <.> ) joint_1_offset = (<L>, <L>, <L> ) joint_2_offset = (<L>, \leftrightarrow
  add element # <.> type beam_displacement_based with nodes (<.>, <.>) \leftrightarrow
40
       with # <.> integration_points use section # <.> mass_density = \leftrightarrow
       <M/L^3> IntegrationRule = "" xz_plane_vector = (<.>, <.>, <.> ) \leftrightarrow
       joint_1_offset = (\langle L \rangle, \langle L \rangle, \langle L \rangle) joint_2_offset = (\langle L \rangle, \langle L \rangle);
41 add element # <.> type beam_elastic with nodes (<.>, <.>) \leftrightarrow
       cross_section = \langle area \rangle elastic_modulus = \langle F/L^2 \rangle shear_modulus = \leftrightarrow
       <F/L^2> torsion_Jx = <length^4> bending_Iy = <length^4> bending_Iz \Leftrightarrow
       = <length^4> mass_density = <M/L^3> xz_plane_vector = (<.>, <.>, \leftrightarrow
        <.> ) joint_1_offset = (<L>, <L>, <L> ) joint_2_offset = (<L>, \hookleftarrow
       <L>, <L>);
42 add element # <.> type beam_elastic_lumped_mass with nodes (<.>, <.>) \leftarrow
       cross_section = <area> elastic_modulus = <F/L^2> shear_modulus = \leftrightarrow
       <F/L^2> torsion_Jx = <length^4> bending_Iy = <length^4> bending_Iz <
       = <length^4> mass_density = <M/L^3> xz_plane_vector = (<.>, <.>, \leftrightarrow
        <.> ) joint_1_offset = (<L>, <L>, <L> ) joint_2_offset = (<L>, \hookleftarrow
       <L>, <L>);
43 add element # <.> type BeamColumnDispFiber3d with nodes (<.>, <.>) \leftrightarrow
       number_of_integration_points = <.> section_number = <.> \hookleftarrow
       mass_density = \langle M/L^3 \rangle xz_plane_vector = (<.>, <.>, <.>) \leftrightarrow
        joint_1_offset = (<L>, <L>, <L> ) joint_2_offset = (<L>, <L>, <L> );
    add element # <.> type HardContact with nodes (<.>, <.>) \leftarrow
        axial\_stiffness = \langle F/L \rangle shear_stiffness = \langle F/L \rangle normal_damping = \longleftrightarrow
        <F/L> tangential_damping = <F/L> friction_ratio = <.> \leftrightarrow
        contact_plane_vector = (<.>, <.>, <.>);
45
   add element # <.> type HardWetContact with nodes (<.>, <.>) \leftrightarrow
        axial_stiffness = \langle F/L \rangle shear_stiffness = \langle F/L \rangle normal_damping = \leftrightarrow
       <F/L> tangential_damping = <F/L> friction_ratio = <.> \leftarrow
        contact_plane_vector = (<.>, <.>, <.>);
    add element # <.> type ShearBeam with nodes (<.>, <.>) cross_section \hookleftarrow
46
        = <1^2> use material # <.>;
    add element # <.> type SoftContact with nodes (<.>, <.>) \leftrightarrow
47
       initial_axial_stiffness = <F/L> stiffening_rate = <m^-1> ↔
        shear_stiffness = <F/L> normal_damping = <F/L> tangential_damping \leftrightarrow
       = \langle F/L \rangle friction_ratio = \langle . \rangle contact_plane_vector = (\langle . \rangle, \langle . \rangle, \leftarrow
```

```
<.>);
   add element # <.> type SoftWetContact with nodes (<.>, <.>) \hookleftarrow
48
       initial_axial_stiffness = \langle F/L \rangle stiffening_rate = \langle m^-1 \rangle \leftarrow
       shear_stiffness = \langle F/L \rangle normal_damping = \langle F/L \rangle tangential_damping \leftrightarrow
      = \langle F/L \rangle friction_ratio = \langle . \rangle contact_plane_vector = (\langle . \rangle, \langle . \rangle, \leftrightarrow)
       <.>);
49
   add element # <.> type truss with nodes (<.>, <.>) use material # <.> \leftrightarrow
       cross_section = <length^2> mass_density = <M/L^3> ;
   add element # <.> type variable_node_brick_8_to_27 using <.> Gauss \leftrightarrow
50
       points each direction with nodes (<.>, <.>, <.>, <.>, <.>, \leftrightarrow
       <.>, <.>, <.>, <.>, <.>, <.>, <.>, <.>) use material # <.>;
   add elements (<.>) to physical_element_group "string";
   add fiber # <.> using material # <.> to section # <.> \leftrightarrow
52
       fiber_cross_section = <area> fiber_location = (<L>,<L>);
   add imposed motion # <.> to node # <.> dof DOFTYPE \hookleftarrow
53
       displacement_scale_unit = <displacement> displacement_file = ←
       "disp_filename" velocity_scale_unit = <velocity> velocity_file = \leftrightarrow
       "vel_filename" acceleration_scale_unit = <acceleration> \leftrightarrow
       acceleration_file = "acc_filename";
54
   add imposed motion # <.> to node # <.> dof DOFTYPE time_step = <t> \leftrightarrow
       displacement_scale\_unit = <length> displacement_file = \leftrightarrow
       "disp_filename" velocity_scale_unit = <velocity> velocity_file = \leftrightarrow
       "vel_filename" acceleration_scale_unit = <acceleration> \leftrightarrow
       acceleration_file = "acc_filename";
55
   add load # <.> to all elements type self_weight use acceleration \hookleftarrow
       field # <.>;
56 add load # <.> to element # <.> type self_weight use acceleration \leftarrow
       field # <.>;
   add load # <.> to element # <.> type surface at nodes (<.> , <.> , \hookleftarrow
57
       <.> , <.>) with magnitude <.>;
58
   add load # <.> to element # <.> type surface at nodes (<.> , <.> , \hookleftarrow
       <.> , <.>) with magnitudes (<.> , <.> , <.>);
   add load # <.> to element # <.> type surface at nodes (<.> , <.> , \leftrightarrow
59
       <.> , <.>, <.>, <.>, <.>) with magnitude <.>;
60
   add load # <.> to element # <.> type surface at nodes (<.> , <.> , \hookleftarrow
       <.> , <.>, <.>, <.>, <.>, <.>) with magnitudes (<.> , <.> , \leftarrow
       <.>, <.>, <.>, <.>, <.>);
  add load # <.> to element # <.> type surface at nodes (<.> , <.> , \hookleftarrow
61
       <.> , <.>, <.>, <.>, <.>, <.>, <.>) with magnitude <.>;
   add load # <.> to element # <.> type surface at nodes (<.> , <.> , \hookleftarrow
       <.> , <.>, <.>, <.>, <.>, <.>) with magnitudes (<.> , <.> , \leftrightarrow
       <.> , <.> , <.> , <.> , <.> , <.> , <.> , <.> ;
63 add load # <.> to node # <.> type from_reactions;
```

```
add load # <.> to node # <.> type linear FORCETYPE = <force or \hookleftarrow
       moment>; //FORCETYPE = Fx Fy Fz Mx My Mz F_fluid_x F_fluid_y \leftrightarrow
       F_fluid_z
   |add load # <.> to node # <.> type path_series FORCETYPE = <force or \leftrightarrow
65
       moment> time_step = <time> series_file = "filename";
66
   add load # <.> to node # <.> type path_time_series FORCETYPE = <force \hookleftarrow
       or moment > series_file = "filename";
   add load # <.> to node # <.> type self_weight use acceleration field \hookleftarrow
67
       # <.>;
68 add mass to node # <.> mx = <mass> my = <mass> mz = <mass> {\tt Imx} = \hookleftarrow
       <mass*length^2> Imy = <mass*length^2> Imz = <mass*length^2>;
  add mass to node # <.> mx = <mass> my = <mass> mz = <mass>;
69
   add material # <.> type CamClay mass_density = <M/L^3> M = <.> lambda \leftrightarrow
70
       = <.> kappa = <.> e0 = <.> p0 = <F/L^2> Poisson_ratio = <.> \leftrightarrow
       initial_confining_stress = <F/L^2>
71 add material # <.> type DruckerPrager mass_density = \langle M/L^3 \rangle \leftrightarrow
       elastic_modulus = <F/L^2> poisson_ratio = <.> druckerprager_k = <> ↔
       kinematic_hardening_rate = <F/L^2> isotropic_hardening_rate = ←
       <F/L^2> initial_confining_stress = exp;
72 add material # <.> type DruckerPragerArmstrongFrederickLE \leftrightarrow
       mass_density = \langle M/L^3 \rangle elastic_modulus = \langle F/L^2 \rangle poisson_ratio = \leftrightarrow
       <.> druckerprager_k = <> armstrong_frederick_ha = <F/L^2> <--</pre>
       armstrong_frederick_cr = <F/L^2> isotropic_hardening_rate = ←
       <F/L^2> initial_confining_stress = <F/L^2>;
73
  add material # <.> type DruckerPragerArmstrongFrederickNE ↔
       mass_density = <M/L^3> DuncanChang_K = <.> DuncanChang_pa = \leftarrow
       \langle F/L^2 \rangle DuncanChang_n = \langle F/L^2 \rangle \leftrightarrow
       {\tt DuncanChang\_nu = <.> druckerprager\_k = <> armstrong\_frederick\_ha = \leftarrow}
       \langle F/L^2 \rangle armstrong_frederick_cr = \langle F/L^2 \rangle isotropic_hardening_rate \leftrightarrow
       = <F/L^2> initial_confining_stress = <F/L^2>;
   add material # <.> type DruckerPragerNonAssociateArmstrongFrederick \hookleftarrow
74
       mass_density = \M/L^3> elastic_modulus = \F/L^2> poisson_ratio = \mbox{} \hookrightarrow
       <.> druckerprager_k = <> armstrong_frederick_ha = <F/L^2> ←
       armstrong_frederick_cr = <F/L^2> isotropic_hardening_rate = ←
       \langle F/L^2 \rangle initial_confining_stress = \langle F/L^2 \rangle plastic_flow_xi = \langle Y/L^2 \rangle
       plastic_flow_kd = <> ;
75
   add material # <.> type DruckerPragerNonAssociateLinearHardening \hookleftarrow
       mass_density = \langle M/L^3 \rangle elastic_modulus = \langle F/L^2 \rangle poisson_ratio = \leftarrow
       <.> druckerprager_k = <> kinematic_hardening_rate = <F/L^2> \leftrightarrow
       isotropic_hardening_rate = <F/L^2> initial_confining_stress = ←
       <F/L^2> plastic_flow_xi = <> plastic_flow_kd = <> ;
  add material # <.> type DruckerPragervonMises mass_density = <M/L^3> ←
76
       elastic_modulus = <F/L^2> poisson_ratio = <.> druckerprager_k = <> \hookleftarrow
       kinematic_hardening_rate = <F/L^2> isotropic_hardening_rate = ←
       <F/L^2> initial_confining_stress = exp;
```

```
add material # <.> type linear_elastic_crossanisotropic mass_density \leftarrow
       = <mass_density> elastic_modulus_horizontal = \langle F/L^2 \rangle \leftrightarrow
       elastic_modulus_vertical = \langle F/L^2 \rangle poisson_ratio_h_v = \langle . \rangle \leftarrow
       poisson_ratio_h_h = <.> shear_modulus_h_v = <F/L^2>;
78
   |add material \# <.> type linear_elastic_isotropic_3d mass_density = \leftrightarrow
       <M/L^3> elastic_modulus = <F/L^2> poisson_ratio = <.>;
79
   add material # <.> type linear_elastic_isotropic_3d_LT mass_density = ←
       <M/L^3> elastic_modulus = <F/L^2> poisson_ratio = <.>;
   add material # <.> type roundedMohrCoulomb mass_density = \langle M/L^3 \rangle \leftrightarrow
80
       elastic_modulus = \langle F/L^2 \rangle poisson_ratio = \langle . \rangle RMC_m = \langle . \rangle RMC_qa = \langle . \rangle
       <F/L^2> RMC_pc = <F/L^2> RMC_e = <.> RMC_eta0 = <.> RMC_Heta = \leftarrow
       <F/L^2> initial_confining_stress = <F/L^2>
   add material # <.> type sanisand2004 mass_density = <M/L^3> e0 = <.> \hookleftarrow
81
       sanisand2004_G0 = <.> poisson_ratio = <.> sanisand2004_Pat = <math>\leftarrow
       \langle stress \rangle sanisand2004_p_cut = \langle . \rangle sanisand2004_Mc = \langle . \rangle
       sanisand2004_c = <.> sanisand2004_lambda_c = <.> sanisand2004_xi = <math>\hookleftarrow
             sanisand2004_ec_ref = <.> sanisand2004_m = <.>
       sanisand2004_h0 = <.> sanisand2004_ch = <.> sanisand2004_nb = <.> \leftrightarrow
       sanisand2004\_A0 = <.> sanisand2004\_nd = <.> sanisand2004\_z\_max = \leftarrow
             sanisand2004_cz = <.> initial_confining_stress = <stress> ;
82
   add material # <.> type sanisand2004_legacy mass_density = \langle M/L^3 \rangle e0 \leftrightarrow
       = <.> sanisand2004_G0 = <.> poisson_ratio = <.> sanisand2004_Pat = \leftrightarrow
                   sanisand2004_p_cut = <.> sanisand2004_Mc = <.>
       <stress>
       sanisand2004_c = <.> sanisand2004_lambda_c = <.> sanisand2004_xi = <math>\leftrightarrow
             sanisand2004_ec_ref = <.> sanisand2004_m = <.>
       sanisand2004_h0 = <.> sanisand2004_ch = <.> sanisand2004_nb = <.> \leftrightarrow
       sanisand2004\_A0 = <.> sanisand2004\_nd = <.> sanisand2004\_z\_max = \leftarrow
             sanisand2004_cz = <.> initial_confining_stress = <stress>
       algorithm = <explicit|implicit> number_of_subincrements = <.> \leftrightarrow
       maximum_number_of_iterations = <.> tolerance_1 = <.> tolerance_2 \leftrightarrow
       = <.>:
83
   add material # <.> type sanisand2008 mass_density = <M/L^3> e0 = <.> \leftrightarrow
        sanisand2008\_G0 = <.> sanisand2008\_K0 = <.> sanisand2008\_Pat = <math>\leftrightarrow
       <stress> sanisand2008_k_c = <.> sanisand2008_alpha_cc = <.> \leftarrow
       sanisand2008_c = <.> sanisand2008_xi = <.> sanisand2008_lambda = <math>\leftrightarrow
             sanisand2008_ec_ref = <.> sanisand2008_m = <.>
       sanisand2008_h0 = <.> sanisand2008_ch = <.> sanisand2008_nb = <math>\leftrightarrow
       <.> sanisand2008_A0 = <.> sanisand2008_nd = <.> sanisand2008_p_r \leftrightarrow
       = <.> sanisand2008_rho_c = <.> sanisand2008_theta_c = <.> \leftrightarrow
       sanisand2008_X = <.> sanisand2008_z_max = <.> sanisand2008_cz = <math>\leftrightarrow
             sanisand2008_p0 = <stress> sanisand2008_p_in = <.>
       algorithm = <explicit | implicit > number_of_subincrements = <.> ←
       maximum_number_of_iterations = <.> tolerance_1 = <.> tolerance_2 \leftrightarrow
       = <.>;
```

```
add material # <.> type uniaxial_concrete02 compressive_strength = \leftrightarrow
84
        \langle F/L^2 \rangle strain_at_compressive_strength = <.> crushing_strength = \leftrightarrow
        <F/L^2> strain_at_crushing_strength = <.> lambda = <.> \leftarrow
        tensile_strength = <F/L^2> tension_softening_stiffness = <F/L^2>;
    add material # <.> type uniaxial_elastic elastic_modulus = <F/L^2> ↔
85
        viscoelastic_modulus = <mass / length / time> ;
86 add material # <.> type uniaxial_steel01 yield_strength = \langle F/L^2 \rangle \leftrightarrow
        elastic_modulus = \langle F/L^2 \rangle strain_hardening_ratio = \langle . \rangle a1 = \langle . \rangle \leftrightarrow
        a2 = <.> a3 = <> a4 = <.> ;
    add material # <.> type uniaxial_steel02 yield_strength = \langle F/L^2 \rangle \leftrightarrow
87
        elastic_modulus = <F/L^2> strain_hardening_ratio = <.> R0 = <.> \leftrightarrow
        cR1 = <.> cR2 = <.> a1 = <.> a2 = <.> a3 = <> a4 = <.>;
   |add material # <.> type vonMises mass_density = <M/L^3> \leftrightarrow
88
        elastic_modulus = \langle F/L^2 \rangle poisson_ratio = \langle . \rangle von_mises_radius = \leftrightarrow
        F/L^2 kinematic_hardening_rate = F/L^2 \leftrightarrow
        isotropic_hardening_rate = <F/L^2> ;
    add material # <.> type vonMisesArmstrongFrederick mass_density = \leftrightarrow
        <M/L^3> elastic_modulus = <F/L^2> poisson_ratio = <.> \leftrightarrow
        von_mises_radius = <> armstrong_frederick_ha = <F/L^2> ←
        armstrong_frederick_cr = <F/L^2> isotropic_hardening_rate = ←
        \langle F/L^2 \rangle ;
   add node # <.> at (<length>, <length>, <length>) with <.> dofs;
90
91
    add nodes (<.>) to physical_node_group "string";
    add section # <.> type elastic3d elastic_modulus = <F/L^2> \leftrightarrow
        cross_section = \langle L^2 \rangle bending_Iz = \langle L^4 \rangle bending_Iy=\langle L^4 \rangle \leftrightarrow
        torsion_Jx=<L^4>;
93
    add section # <.> type Elastic_Membrane_Plate elastic_modulus = \leftrightarrow
        <F/L^2> poisson_ratio = <.> thickness = <length> mass_density = \leftrightarrow
        <M/L^3>;
   add section # <.> type FiberSection TorsionConstant_GJ = <F*L^2>
95 add section # <.> type Membrane_Plate_Fiber thickness = <length> use \leftrightarrow
        material # <.>;
96 add single point constraint to node # <.> dof to constrain <dof_type> ←
        constraint value of <corresponding unit>;
97
   add uniform acceleration # <.> to all nodes dof <.> time_step = <T> ←
        scale_factor = <.> initial_velocity = <L/S> acceleration_file = <--
        <string>;
   check mesh filename;
98
    compute reaction forces;
    define algorithm With_no_convergence_check / Newton / Modified_Newton;
100
    define convergence test Norm_Displacement_Increment / \hookleftarrow
101
        Energy_Increment / Norm_Unbalance / \hookleftarrow
        Relative_Norm_Displacement_Increment / Relative_Energy_Increment / \hookleftarrow
        Relative_Norm_Unbalance tolerance = <.> maximum_iterations = <.> \hookleftarrow
        verbose_level = <0>|<1>|<2>;
```

```
define dynamic integrator Hilber_Hughes_Taylor with alpha = <.>;
102
103 define dynamic integrator Newmark with gamma = <.> beta = <.>;
    define load factor increment <.>;
104
105 define NDMaterial constitutive integration algorithm Forward_Euler;
   define NDMaterial constitutive integration algorithm \hookleftarrow
106
       Forward_Euler_Subincrement number_of_subincrements =<.>;
107
    define NDMaterial constitutive integration algorithm \hookleftarrow
       Forward_Euler|Forward_Euler_Subincrement|Backward_Euler|Backward_Euler_Subin
       yield_function_relative_tolerance = <.> stress_relative_tolerance ←
       = <.> maximum_iterations = <.>;
    define physical_element_group "string";
108
109 define physical_node_group "string";
110 define solver ProfileSPD / UMFPack;
    define static integrator displacement_control using node # <.> dof \leftrightarrow
111
       DOFTYPE increment <length>;
112 disable asynchronous output;
113 disable element output;
114 disable output;
    enable asynchronous output;
115
116 enable element output;
117
    enable output;
118 | fix node # <.> dofs <.>;
119
   fix node # <.> dofs all;
120 free node # <.> dofs <.>;
121 help;
122 | if (.) { } else {};
123 | if (.) { };
124 model name "name_string";
125 new loading stage "name_string";
126
    output every <.> steps;
127
    output non_converged_iterations;
128
    output support reactions;
129 | print <.>;
   print element # <.>;
130
131 | print node # <.>;
132 print physical_element_group "string";
    print physical_node_group "string";
133
134 remove constraint equal_dof node # <.>;
135 remove displacement from node # <.>;
136 remove element # <.>;
137 remove imposed motion # <.>;
138 | remove load # <.>;
139 remove node # <.>;
140 remove physical_node_group "string";
141 remove strain from element # <.>;
```

```
142
    remove physical_element_group "string";
143
    runTest;
144
    set output compression level to <.>;
    simulate <.> steps using static algorithm;
    simulate <.> steps using transient algorithm time_step = <time>;
146
147
    simulate <.> steps using variable transient algorithm time_step = \hookleftarrow
        <time> minimum_time_step = <time> maximum_time_step = <time> \hookleftarrow
        number_of_iterations = <.>;
148 simulate constitutive testing BARDETMETHOD use material # <.> \leftrightarrow
        scale_factor = <.> series_file = <string> sigma0 = ( <F/L^2> , \leftrightarrow
        <F/L^2> , <F/L^2> , <F/L^2> , <F/L^2> , <F/L^2> ) verbose_output \hookleftarrow
        = <.>
149
    simulate constitutive testing constant mean pressure triaxial strain \hookleftarrow
        control use material # <.> strain_increment_size = <.> ←
        maximum_strain = <.> number_of_times_reaching_maximum_strain = <.>;
    simulate constitutive testing <code>DIRECT_STRAIN</code> use material # <.> \hookleftarrow
150
        scale_factor = <.> series_file = <string> sigma0 = ( <F/L^2> , <math>\leftarrow
        \langle F/L^2 \rangle , \langle F/L^2 \rangle , \langle F/L^2 \rangle , \langle F/L^2 \rangle ) verbose_output = \leftrightarrow
        <.>
    simulate constitutive testing drained triaxial strain control use \hookleftarrow
151
        material # <.> strain_increment_size = <.> maximum_strain = <.> ↔
        number_of_times_reaching_maximum_strain = <.>;
152
    simulate constitutive testing undrained simple shear use material # \leftrightarrow
        <.> strain_increment_size = <.> maximum_strain = <.> \leftrightarrow
        number_of_times_reaching_maximum_strain = <.>;
153
   simulate constitutive testing undrained triaxial stress control use \hookleftarrow
        material # <.> strain_increment_size = <.> maximum_strain = <.> \leftrightarrow
        number_of_times_reaching_maximum_strain = <.>;
154
    simulate constitutive testing undrained triaxial use material # <.> \leftrightarrow
        strain_increment_size = <.> maximum_strain = <.> ←
        number_of_times_reaching_maximum_strain = <.>;
    simulate using eigen algorithm number_of_modes = <.>;
155
    ux uy uz Ux Uy Uz rx ry rz;
156
    while (.) { };
157
    whos;
158
```

1.5 List of reserved keywords

The following keywords are reserved and cannot be used as variables in a script or interactive session. Doing so would result in a syntax error.

First Order (commands)

```
1
   a0
 2
   a1
 3
   a2
  a3
5
   acceleration
7 | acceleration_depth
  acceleration_file
8
   acceleration_filename
   acceleration_scale_unit
10
11
   add
   algorithm
13
   algorithm
14 | all
15 | all
16
   allowed_subincrement_strain
17
   alpha
   alpha1
18
19
   alpha2
20
   and
21
   angle
22
   armstrong_frederick_cr
   armstrong_frederick_ha
24 asynchronous
25
   at
26
27
   axial_penalty_stiffness
   axial_stiffness
29 | axial_viscous_damping
30 ay
31
   az
32
   bending_Iy
33
   bending_Iz
34 | beta
35 Beta
36 beta_min
37
   case
38 cases
39
   characteristic_strength
40
   check
41 chi
42 | cohesion
43 combine
44
   compression
45 | compressive_strength
```

```
46
   compressive_yield_strength
47 | compute
48 | confinement
49 | confinement_strain
50 constitutive
51
   constrain
52 | constraint
53 | contact_plane_vector
54 | control
55
   convergence
56
   cR1
57
   cR2
58 cross_section
59
   crushing_strength
60
   Current_Stiffness
61
   cyclic
62
   damage_parameter_An
63
   damage_parameter_Ap
64
   damage_parameter_Bn
65 damping
66 define
67
   depth
68
   dilatancy_angle
   dilation_angle_eta
70 dilation_scale
71 direction
72 disable
73
   displacement
   displacement_file
75 | displacement_scale_unit
76 dof
77
  dofs
78 dofs
79
   domain
80
   druckerprager_k
81 | DuncanChang_K
82 | DuncanChang_n
83 | DuncanChang_nu
84 | DuncanChang_pa
85
   DuncanChang_sigma3_max
   DYNAMIC_DOMAIN_PARTITION
87
   e0
88
   each
   elastic
89
90
   elastic_modulus
   elastic_modulus_horizontal
92 | elastic_modulus_vertical
93 | element
94 elements
95
   else
96
   enable
97 | every
```

```
98
   factor
99
   fiber
    fiber_cross_section
100
101
    fiber_location
102
    field
103
    file
104
    fix
   fluid
105
106
    free
107
    friction_angle
108
    friction_ratio
109
    from
110
    gamma
111
    Gamma
112
    Gauss
    generate
113
114
    GoverGmax
115 | h_in
116 hardening_parameters_of_yield_surfaces
117 | hardening_parameters_scale_unit
118 | hdf5_file
119 hdf5_filenames_list
120
    help
121
    if
122
    imposed
123
    Imx
124
    Imy
125
    Imz
126
    in
127
    inclined
128
    increment
129
    initial_axial_stiffness
130
    initial_confining_stress
131
    initial_elastic_modulus
132
    initial_shear_modulus
133 | initial_shear_stiffness
134 | initial_velocity
135
    integration
136
    integration_points
137
    IntegrationRule
138
    integrator
139
    interface
140
    isotropic_hardening_rate
    joint_1_offset
141
    joint_2_offset
142
143 K_f
144 K_s
145 k_x
146 | k_y
147
    k_z
148
    kappa
149 | kd_in
```

```
150
    kinematic_hardening_rate
151
    lambda
152
    level
153 | line_search_beta
154
    line_search_eta
155
    line_search_max_iter
156
    liquefaction_Alpha
157
    liquefaction_c_h0
158 | liquefaction_Dir
159
    liquefaction_dre1
160
    liquefaction_Dre2
161
    liquefaction_EXPN
162
    liquefaction_gamar
    liquefaction_mdc
163
164 | liquefaction_mfc
165
    liquefaction_pa
166
    liquefaction_pmin
167
    load
168
   load_factors_list
169
    loading
170
    local_y_vector
    local_z_vector
171
172 M
173 | M_in
174
    magnitude
175
    magnitudes
176
    mass
177
    mass_density
178 master
179 material
180 max_axial_stiffness
181 | maximum_iterations
182 maximum_number_of_iterations
183
    maximum_strain
184 | maximum_stress
185 | maximum_time_step
186 method
187
    minimal
    minimum_time_step
188
189
    model
190 model
    moment_x_stiffness
191
192
    moment_y_stiffness
193
    monotonic
194
    motion
195
    mu
196
    mx
197
    mу
198
    mz
199
    name
200
    NDMaterial
201 | new
```

```
202 |
    newton_with_subincrement
203 node
204 nodes
205 | number_of_cycles
206 | number_of_files
207
    number_of_increment
208 | number_of_integration_points
209 number_of_iterations
210 | number_of_layers
211 | number_of_modes
212 number_of_subincrements
213
    number_of_times_reaching_maximum_strain
214 of
215
    output
216
    output
217
    output_filename
218
    0g
219
    parallel
220 | peak_friction_coefficient_limit
221
    peak_friction_coefficient_rate_of_decrease
222 | penalty_stiffness
223 | pi1
224
    pi2
225 pi3
226 | plastic_deformation_rate
227 plastic_flow_kd
228 plastic_flow_xi
229 plot
230 | point
231 points
232 | poisson_ratio
233 poisson_ratio_h_h
234 | poisson_ratio_h_v
235 porosity
236 | print
237 propagation
238 pure
239 R0
240 radiuses_of_yield_surface
241 radiuses_scale_unit
242 rate_of_softening
243 reduction
244 | reference_pressure
245 remove
246
    rempve
247
    residual_friction_coefficient
248 restart
249 restart_files
250 results
251 | rho_a
252
    rho_f
253 | rho_s
```

```
254
    rho_w
255
    RMC_e
256
    RMC_eta0
    RMC_Heta
257
258
    RMC_m
259
    RMC_pc
260
    RMC_qa
    RMC_shape_k
261
262
    rounded_distance
263
    runTest
264
    sanisand2004\_A0
265
    sanisand2004_c
    sanisand2004_ch
266
267
    sanisand2004_cz
268
    sanisand2004_ec_ref
269
    sanisand2004_G0
270
    sanisand2004_h0
271
    sanisand2004_lambda_c
272
    sanisand2004_m
273
    sanisand2004_Mc
274
    sanisand2004_nb
275
    sanisand2004_nd
276
    sanisand2004_p_cut
277
    sanisand2004_Pat
278
    sanisand2004_xi
279
    sanisand2004_z_max
280
    sanisand2008_A0
281
    sanisand2008_alpha_cc
282
    sanisand2008_c
283
    sanisand2008_ch
284
    sanisand2008_cz
285
    sanisand2008_ec_ref
286
    sanisand2008_G0
287
    sanisand2008_h0
288
    sanisand2008_K0
289
    sanisand2008_k_c
290
    sanisand2008_lambda
291
    sanisand2008_m
292
    sanisand2008_nb
293
    sanisand2008_nd
294
    sanisand2008_p0
295
    sanisand2008_p_in
296
    sanisand2008_p_r
297
    sanisand2008_Pat
298
    sanisand2008_rho_c
299
    sanisand2008_theta_c
300
    sanisand2008_X
301
    sanisand2008_xi
302
    sanisand2008_z_max
303
    save
304
    scale_factor
    SCOTCHGRAPHPARTITIONER
```

```
306
    section
307 | section_number
308
    sequential
309
    series_file
310
    set
311
    shear
312 | shear_length_ratio
313 | shear_modulus
314 | shear_modulus_h_v
315 | shear_stiffness
    shear_viscous_damping
316
317
    shear_zone_thickness
318 | ShearStrainGamma
319
    sigma0
320 | simulate
321 | single
322
    size_of_peak_plateau
323 | sizes_of_yield_surfaces
324 slave
325 slave
326 soil
327
    soil_profile_filename
328
    soil_surface
329 solid
330 solver
331 stage
332 steps
333
    steps
334
    stiffening_rate
335 | stiffness_to_use
336 strain
337 | strain_at_compressive_strength
338 strain_at_crushing_strength
339
    strain_hardening_ratio
340 | strain_increment_size
341 stress
342 | stress_increment_size
343 | stress_relative_tolerance
344 | sub-stepping
345
    surface
346 | surface_vector_relative_tolerance
347 tensile_strength
348 | tensile_yield_strength
349
    tension_softening_stiffness
350 test
351 test
352 testing
353 thickness
354 | time_step
355
    to
356
    tolerance_1
357 | tolerance_2
```

```
358
   torsion_Jx
359 | torsional_stiffness
360 | TorsionConstant_GJ
361
    total_number_of_shear_modulus
362
    total_number_of_yield_surface
363
    triaxial
364
    type
365
    uniaxial
366
    uniaxial_material
367
    uniform
368 unit_of_acceleration
369
    unit_of_damping
370 unit_of_rho
371
    unit_of_vs
372 | use
373 using
374
    value
375 | velocity_file
376 | velocity_scale_unit
377 | verbose_output
378 viscoelastic_modulus
379
    von_mises_radius
380
    wave
381
    wave1c
382 wave3c
383
    while
384 whos
385
    with
386 | xi_in
387 | xz_plane_vector
388
    yield_function_relative_tolerance
389
    yield_strength
390 | yield_surface_scale_unit
391
392
    У
393
    z
```

Second Order (inside commands)

```
1 20NodeBrick

2 20NodeBrick_up

3 20NodeBrick_upU

4 27NodeBrick_up

6 27NodeBrick_upU

7 3NodeShell_ANDES

8 4NodeShell_ANDES

9 4NodeShell_MITC4

10 4NodeShell_NewMITC4

11 8_27_NodeBrick

12 8_27_NodeBrick_up

13 8_27_NodeBrick_upU
```

```
14 | 8NodeBrick
15 | 8NodeBrick_fluid_incompressible_up
16 | 8NodeBrick_up
17 | 8NodeBrick_upU
18 | Absolute_Norm_Displacement_Increment
19
   Absolute_Norm_Unbalanced_Force
20 arclength_control
21 | Average_Norm_Displacement_Increment
22 | Average_Norm_Unbalanced_Force
23 Backward_Euler
24 BARDETMETHOD
25 beam_9dof_elastic
26 | beam_displacement_based
27 | beam_elastic
28 | beam_elastic_lumped_mass
29 | BeamColumnDispFiber3d
30 | BearingElastomericPlasticity3d
31 BFGS
32 BondedContact
33 CamClay
34 | Caughey3rd
35 Caughey4th
   constant mean pressure triaxial strain control
   Cosserat8NodeBrick
38 | Cosserat_linear_elastic_isotropic_3d
39 | Cosserat_von_Mises
40 DIRECT_STRAIN
41
   displacement_control
42 DOFTYPE
43 domain reduction method
44 drained triaxial strain control
45 DruckerPrager
46 DruckerPragerArmstrongFrederickLE
   DruckerPragerArmstrongFrederickNE
48 DruckerPragerMultipleYieldSurface
49 | DruckerPragerMultipleYieldSurfaceGoverGmax
50 | DruckerPragerNonAssociateArmstrongFrederick
   DruckerPragerNonAssociateLinearHardening
52 DruckerPragervonMises
53 dynamic
54 | eigen
55 elastic3d
56 | Elastic_Membrane_Plate
57 | ElasticFourNodeQuad
58 | Energy_Increment
59 | equal_dof
60 | F_fluid_x
61 F_fluid_y
62 F_fluid_z
63 FiberSection
64 | ForceBasedCoupledHardContact
65 | ForceBasedCoupledSoftContact
```

```
66 ForceBasedElasticContact
67 ForceBasedHardContact
68 | ForceBasedSoftContact
69 FORCETYPE
70 Forward_Euler
71
    Forward_Euler_Subincrement
72 from_reactions
73 | Fx
74 Fy
75 | Fz
76 | Hilber_Hughes_Taylor
77
    HyperbolicDruckerPragerArmstrongFrederick
78 | HyperbolicDruckerPragerLinearHardening
    HyperbolicDruckerPragerNonAssociateArmstrongFrederick
80 | HyperbolicDruckerPragerNonAssociateLinearHardening
81 linear
82
    linear_elastic_crossanisotropic
83 | linear_elastic_isotropic_3d
84 | linear_elastic_isotropic_3d_LT
85 | Membrane_Plate_Fiber
86 | Modified_Newton
87 | Mx
88 My
89 Mz
90 Newmark
91 Newton
92 | non_converged_iterations
93 NonlinearFourNodeQuad
    Norm_Displacement_Increment
95 | Norm_Unbalance
96 Parallel
97 path_series
98 path_time_series
99 petsc
100 | petsc_options_string
101 | physical_element_group
102 | physical_node_group
103 | Pisano
104 | PlaneStressLayeredMaterial
105 | PlaneStressRebarMaterial
106 | PlasticDamageConcretePlaneStress
107 pressure
108 ProfileSPD
109 Rayleigh
110 reaction forces
111 | reactions
112 | Relative_Energy_Increment
113 | Relative_Norm_Displacement_Increment
114 Relative_Norm_Unbalance
115 Relative_Norm_Unbalanced_Force
116
    roundedMohrCoulomb
117 RoundedMohrCoulombMultipleYieldSurface
```

```
118 sanisand2004
119 sanisand2004_legacy
120 sanisand2008
    self_weight
121
122
    ShearBeam
123
    solid fluid interaction transient
124
    static
125
    StressBasedCoupledHardContact_ElPPlShear
126
    {\tt StressBasedCoupledHardContact\_NonLinHardShear}
127
    {\tt StressBasedCoupledHardContact\_NonLinHardSoftShear}
128
    {\tt StressBasedCoupledSoftContact}
129
    {\tt StressBasedCoupledSoftContact\_ElPPlShear}
    {\tt StressBasedCoupledSoftContact\_NonLinHardShear}
130
131
    {\tt StressBasedCoupledSoftContact\_NonLinHardSoftShear}
132 | StressBasedHardContact_ElPPlShear
133
    StressBasedHardContact_NonLinHardShear
    {\tt StressBasedHardContact\_NonLinHardSoftShear}
134
135
    StressBasedSoftContact_ElPPlShear
136 | StressBasedSoftContact_NonLinHardShear
    {\tt StressBasedSoftContact\_NonLinHardSoftShear}
137
138
    SuperElementLinearElasticImport
139
    support
140
    surface
141
    transient
142
    truss
143 | TsinghuaLiquefactionModelCirclePiPlane
    TsinghuaLiquefactionModelNonCirclePiPlane
145
    UMFPack
146
    undrained simple shear
147 undrained triaxial
148
    undrained triaxial stress control
149 uniaxial_concrete02
150 uniaxial_elastic
151
    uniaxial_steel01
152 uniaxial_steel02
153 variable transient
154 | variable_node_brick_8_to_27
155 | vonMises
156
    vonMisesArmstrongFrederick
157
    vonMisesMultipleYieldSurface
158
    \verb|vonMisesMultipleYieldSurfaceGoverGmax| \\
159
    With_no_convergence_check
160
161
    beta
    gamma
162
163
    delta
164
165
    ux
166
    uy
167
    uz
168
    rx
169
   ry
```

```
170
    rz
171
    Ux
172
    Uу
173
    UΖ
174
    p
175
    Μ
176
    m
177
    kg
178
    S
179
    cm
180
    mm
181
    km
182
    Ηz
183
    Minute
184
    Hour
185
    Day
186
    Week
187
    ms
188
    ns
189
    N
190
    kN
191
    Рa
192
    kPa
193
    MPa
194
    GPa
195
    pound
196
    1bm
197
    lbf
198
    inch
199
    in
200
    feet
201
    ft
202
    yard
203
    mile
204
    psi
205 ksi
206
   kip
207
208
    рi
209
210 NUMBER_OF_NODES
211 NUMBER_OF_ELEMENTS
    CURRENT_TIME
212
213
    NUMBER_OF_SP_CONSTRAINTS
    NUMBER_OF_MP_CONSTRAINTS
214
215
    NUMBER_OF_LOADS
216
    IS_PARALLEL
217
    SIMULATE_EXIT_FLAG
218
    then
219
    while
220
    do
221
    let
```

```
222
    vector
223
224
    cos
225
    sin
226
    tan
227
    cosh
228
    sinh
229
    tanh
230
    acos
231
    asin
232
    atan
233
    atan2
234
    sqrt
235
    exp
236
    log10
    ceil
237
238
    fabs
239
    floor
240
    log
```

1.6 Integrated Development Environment (IDE) for DSL

1.7 Mesh Generation using GiD

- 1. Download the latest version of GiD from http://www.gidhome.com/, and also get a temporary license (or purchase it...).
- 2. Download essi.gid.tar.gz, unpack it (tar -xvzf essi.gid.tar.gz) in problemtypes directory that is located in GiD's root directory.
- 3. When you run GiD, you will see essi in "Data > Problem types", and can start using it...
- 4. A simple movie with instructions for mesh generation is available: (Link to a movie, 11MB).

1.8 Model Development and Mesh Generation using gmesh

1.9 Model Input File Editing using Sublime

http://www.sublimetext.com/