

## Tutorial-27

Q 4) A student has designed an NMOS Telescope differential amplifier with following specifications:

$$I_0 = 32 \mu A, V_{OV} = 0.4 V, \mu_n C_{ox} = 200 \mu A/V^2, \mu_p C_{ox} = 100 \mu A/V^2,$$

$$|V_{tp}| = V_{tn} = 1 V, \lambda = \frac{1}{100 V}, V_{DD} = 5 V, \text{ if the channel}$$

$$\text{length } L = 0.2 \mu, C_L = 10 pF. \text{ Find}$$

$$(V_{D,sat} = V_{OV})$$

a)  $V_{PB}$  required to bias

transistors in saturation in (V)

$$\begin{aligned} V_{PB} &= V_{DD} - V_{D,sat8} - V_{SG6} \\ &= V_{DD} - V_{D,sat8} - V_{D,sat6} - V_{TH} \\ &= V_{DD} - 2V_{D,sat} - V_{TH} \end{aligned}$$

$$C_L = 5 - 2(0.4) - 1 = 3.2 V$$

b)  $V_{NB}$  Required to bias transistors in saturation in (V)

$$\begin{aligned} V_{NB} &= V_{D,sat0} + V_{D,sat1} + V_{D,sat4} + V_{TH} \\ &= V_{D,sat0} + V_{D,sat1} + V_{D,sat4} + V_{TH} \\ &= 3V_{D,sat} + V_{TH} \\ &= 3(0.4) + 1 = 2.2 V. \end{aligned}$$

c) Output Common mode range in unity feedback (V).

In unity feedback,

$$\text{For } M_2 \text{ to be in Sat } V_{out} \leq V_X + V_{TH2}$$

$$\text{For } M_4 \text{ to be in Sat } V_{out} \geq V_{NB} - V_{TH4}$$

$$V_X = V_{NB} - V_{SG4}$$

$$\underbrace{V_{NB} - V_{TH4}}_{V_{O,min}} \leq V_{out} \leq V_{NB} - V_{SG4} + V_{TH2}$$

$$= (V_{NB} - \underbrace{(V_{SG4} - V_{TH2})}_{V_{OV}})_{V_{O,max}}$$

$$\text{OCMR} = V_{o, \text{max}} - V_{\text{min}} = V_{TH4} - (V_{GS4} - V_{TH2})$$

$$= 1 - 0.4 = 0.6 \text{ V}$$

d) Gain

$$\text{Gain} = -G_m R_{\text{out}}, \quad G_m = g_m \quad R_{\text{out}} = R_{\text{up}} \parallel R_{\text{down}}$$

$$R_{\text{up}} = g_m r_o^2 = R_{\text{down}} \Rightarrow R_{\text{out}} = \frac{g_m r_o^2}{2}$$

$$\text{Gain} = g_m^2 \frac{r_o^2}{2}$$

$$g_m = \sqrt{2 I_D \mu_n C_{ox} \frac{W}{L}} = \frac{2 I_D}{V_{\text{ov}}} = \frac{I_{\text{tail}}}{V_{\text{ov}}} = \frac{32}{0.4} = 80 \text{ mS}$$

$$r_o = \frac{1}{\lambda I_D} = \frac{2}{\lambda I_{\text{tail}}} = \frac{2 \times 100}{32} = 6.25 \text{ M}\Omega$$

$$\text{Gain} = g_m^2 \frac{r_o^2}{2} = 12,5000$$

e) Bandwidth

$$\text{Bandwidth} = \frac{1}{R_{\text{out}} C_L} = \frac{1}{g_m^2 \frac{r_o^2}{2} C_L} = 64 \text{ Mrad/s}$$

f) charging rate of capacitor  $C_L$  (V/ $\mu$ s), if  $M_1$  gate is at  $V_{\text{dd}}$  &  $M_2$  gate is at 0V.

$M_1$  only turns ON &  $M_2$  is OFF, entire current flows through  $M_1$ , that is mirrored by current mirror & charges the output capacitor.

$$\frac{dV_o}{dt} = \frac{I}{C_L} = \frac{32}{10} = 3.2 \text{ V}/\mu\text{s}$$



9)  $W_1, W_8$  in  $\mu m$

$W_1$  (NMOS)

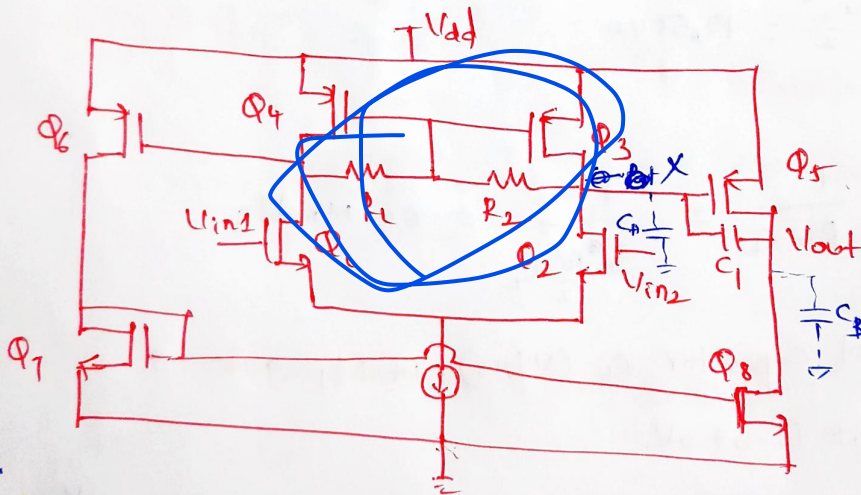
$$\frac{I_p}{2} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{ov})^2 \Rightarrow W = \frac{I \times L}{\mu_n C_{ox} (V_{ov})^2} = 0.2 \mu$$

$W_8$  (PMOS)

$$I_{/2} = \frac{1}{2} \mu_p C_{ox} \frac{W}{L} (V_{ov})^2 \Rightarrow W = \frac{I \times L}{\mu_p C_{ox} (V_{ov})^2} = 0.4 \mu$$

$$W_1 + W_8 = 0.6 \mu$$

Q1) Assuming only a single (dominant) pole, find the Unity Gain Bandwidth (in Mrads) for the given Two stage op-amp with common-mode feedback. Assume  $g_m$  of all transistors as  $8 mS$ ,  $r_o = 115 k\Omega$ ,  $R_1 = R_2 = 60 k\Omega$ ,  $C_1 = 5 pF$ . ~~with~~



Sol:

Unity gain Bandwidth for a single pole system

$$= 3dB \text{ bandwidth} \times \text{Diff mode DC gain (pole freq)}$$

Dominant pole is present at node 'X'.  $C_1$  is Miller cap

Q1

$$C_A = C_1 \left( 1 + g_m \frac{r_o}{2} \right)$$

$$R_{out} = r_{o2} || r_{o3} || p = \frac{r_o}{2} || p = \frac{p r_o}{2p + r_o}$$

$$DC \text{ gain} = \left( g_{m1} \frac{p r_o}{2p + r_o} \right) \cdot \left( g_{m2} \frac{r_o}{2} \right) = g_m^2 \frac{p r_o^2}{2(2p + r_o)}$$

Unity Gain Bandwidth (UGB)

$$= g_m^2 \frac{p r_o}{2(2p + r_o)} \times \frac{1}{\frac{p r_o}{2p + r_o} C_1 \left( 1 + g_m \frac{r_o}{2} \right)}$$

$$= \frac{g_m^2 r_o}{C_1 (2 + g_m r_o)} = \frac{204899.77 \text{ rad/s}}{1995.566 \text{ rad/s}}$$

Q2) Consider the circuit shown below. Bias Voltages  $V_{B1}$ ,  $V_{B2}$  and bias currents in all branches keep the transistors in saturation. Calculate the ratio of magnitude of pole frequency at node X to magnitude of pole frequency at node Y.

Take:  $V_{dd} = 3.3V$ ,  $R_D = 2k\Omega$ ,  $R_S = 0.1k\Omega$

$g_{m1} = 5 \text{ mS}$ ,  $g_{m2} = 2 \text{ mS}$ ,  $g_{m3} = 1 \text{ mS}$

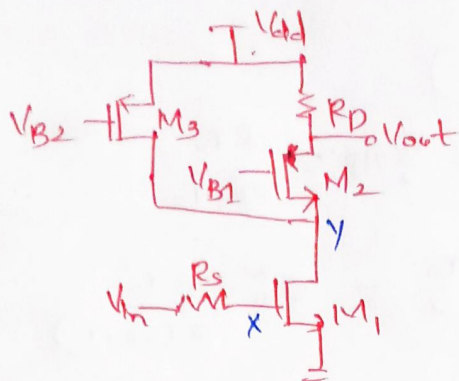
$C_{gs1} = 14 \text{ fF}$   $C_{gd1} = 6 \text{ fF}$   $C_{db1} = 3 \text{ fF}$   $C_{sb1} = 2 \text{ fF}$

$C_{gs2} = 14 \text{ fF}$   $C_{gd2} = 7 \text{ fF}$   $C_{db2} = 5 \text{ fF}$   $C_{sb2} = 7 \text{ fF}$

$C_{gs3} = 10 \text{ fF}$   $C_{gd3} = 4 \text{ fF}$   $C_{db3} = 4 \text{ fF}$   $C_{sb3} = 3 \text{ fF}$

Assume drain-source small signal resistance of the transistors to be large.





sd: pole freq at x =  $\frac{1}{2\pi R_x C_x}$

$$C_y = C_{gs} + (1 + |A_{v1}|) C_{gd1}$$

$$A_{v1} = -g_{m1} \left( \frac{1}{g_{m2}} \right)$$

$$(n_{o1}, g_{o2} = n_{o3} \rightarrow \infty)$$

$$R_x = R_s$$

$$P_x = \frac{1}{2\pi R_s [C_{gs1} + (1 + \frac{g_{m1}}{g_{m2}}) C_{gd1}]} = 45.495 \text{ GHz}$$

Pole frequency at y =  $\frac{1}{2\pi R_y C_y}$        $R_y = \frac{1}{g_{m2}}$

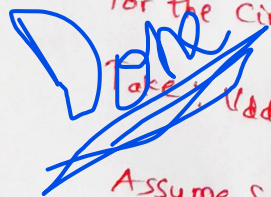
$$C_y = C_{db1} + C_{gs2} + C_{gb2} + C_{gd3} + C_{ab3} + \left(1 + \frac{1}{|A_{v1}|}\right) C_{gd1}$$

$$\frac{1}{|A_{v1}|} = \frac{g_{m2}}{g_{m1}}$$

$$P_y = \frac{1}{2\pi \left(\frac{1}{g_{m2}}\right) [C_y]} = \frac{1}{2\pi \times \frac{1}{2} \times \frac{202}{5}} = 7.878 \text{ GHz}$$

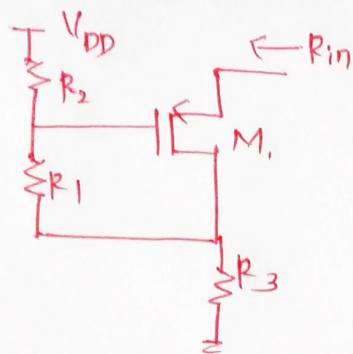
$$\text{Ratio} = \frac{P_x}{P_y} = \frac{45.495}{7.878} = 5.775$$

Q3) Determine the small signal input resistance  $R_{in}$  (in k $\Omega$ ) for the circuit shown below.

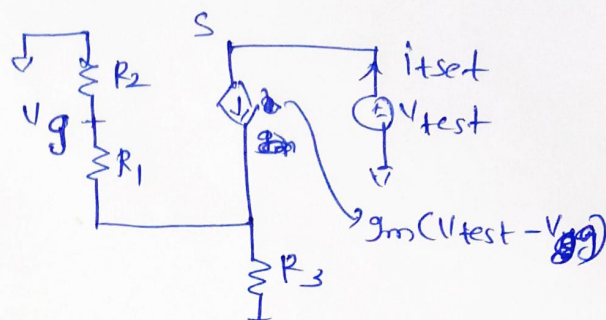


Ass:  $V_{DD} = 10V$ ,  $R_1 = 7k\Omega$ ,  $R_2 = 18k\Omega$ ,  $R_3 = 2k\Omega$ ,  $g_{m1} = 2.8 \text{ mS}$

Assume Source-drain small signal resistance of the transistor to be large.



Sol:



$$i_{test} = g_m (V_{test} - V_g) \quad \text{--- (1)}$$

$$V_g = \frac{g_m (V_{test} - V_g) R_3}{R_3 + R_1 + R_2} \times R_2$$

Current division

$$V_g \left[ 1 + \frac{g_m R_3 R_2}{R_1 + R_2 + R_3} \right] = \frac{g_m V_{test} R_2 R_3}{R_1 + R_2 + R_3}$$

$$V_g = \frac{V_{test} \cdot g_m R_2 R_3}{R_1 + R_2 + R_3 + g_m R_3 R_2} \quad \text{--- (2)}$$

from (1) & (2)

$$\frac{i_{test}}{V_{test}} = \frac{g_m (R_1 + R_2 + R_3) + g_m^2 R_2 R_3 - g_m^2 R_2 R_3}{R_1 + R_2 + R_3 + g_m R_2 R_3}$$

$$R_{in} = \frac{V_{test}}{i_{test}} = \frac{1}{g_m} \left[ \frac{R_1 + R_2 + R_3 + g_m R_2 R_3}{R_1 + R_2 + R_3} \right]$$

$$= \frac{1}{g_m} \left[ 1 + \frac{g_m R_2 R_3}{R_1 + R_2 + R_3} \right]$$

$$R_{in} = 1.6904 \text{ k}\Omega$$