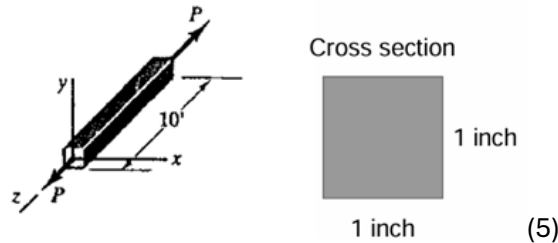


1. Below is a bar with square cross-section loaded with a tensile stress P – if the change in length is 2' (inches), calculate the strains in x , y and z axes considering no volume change.



$$\epsilon_z = 2/10 = 0.2$$

From volume constancy, $10 \times 1 \times 1 = 12 \times (1 - \Delta x)(1 - \Delta y)$

Considering $\Delta x = \Delta y$ (since square cross section)

$$10 = 12(1 - \Delta x)^2; \Delta x = 0.0872$$

$$\epsilon_x = \epsilon_y = -0.0872$$

You can verify: $\epsilon_x + \epsilon_y + \epsilon_z = -0.872 - 0.872 + 0.2 = 0.02 \approx 0$

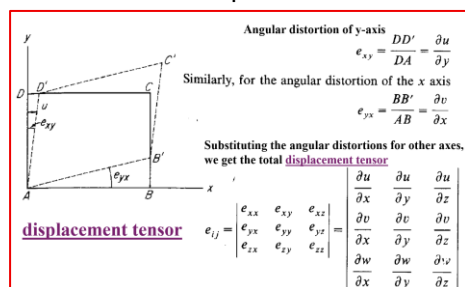
2. What, according to you would be the 2-D stress matrices for the following cases: a) pure shear, b) uniaxial compression, c) hydrostatic compression. (2 x 3=6)

a) $\sigma_{ij} = \begin{pmatrix} 0 & \tau & 0 \\ \tau & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$ b) $\sigma_{ij} = \begin{pmatrix} -\sigma & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$ c) $\sigma_{ij} = \begin{pmatrix} \sigma & 0 & 0 \\ 0 & \sigma & 0 \\ 0 & 0 & \sigma \end{pmatrix}$

3. a) What is a displacement tensor – write down the tensor form.

$$e_{ij} = \begin{pmatrix} e_{xx} & e_{xy} & e_{xz} \\ e_{yx} & e_{yy} & e_{yz} \\ e_{zx} & e_{zy} & e_{zz} \end{pmatrix}$$

- b) Describe the components of the tensor.



- c) What are the different components of this tensor? And state the characteristics of the tensors

(2+3+2+3=10)

The displacement tensor can be written as

$$e_{ij} = \frac{1}{2}(e_{ij} + e_{ji}) + \frac{1}{2}(e_{ij} - e_{ji})$$

$$e_{ij} = \epsilon_{ij} + \omega_{ij}$$

$$\epsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

$$\omega_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right)$$

$$\epsilon_{ij} = \begin{bmatrix} \epsilon_{xx} & \epsilon_{xy} & \epsilon_{xz} \\ \epsilon_{yx} & \epsilon_{yy} & \epsilon_{yz} \\ \epsilon_{zx} & \epsilon_{zy} & \epsilon_{zz} \end{bmatrix} = \begin{bmatrix} \frac{\partial u}{\partial x} & \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & \frac{1}{2} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) \\ \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) & \frac{\partial v}{\partial y} & \frac{1}{2} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) \\ \frac{1}{2} \left(\frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \right) & \frac{1}{2} \left(\frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \right) & \frac{\partial w}{\partial z} \end{bmatrix} \quad (2-42)$$

$$\omega_{ij} = \begin{bmatrix} \omega_{xx} & \omega_{xy} & \omega_{xz} \\ \omega_{yx} & \omega_{yy} & \omega_{yz} \\ \omega_{zx} & \omega_{zy} & \omega_{zz} \end{bmatrix} = \begin{bmatrix} 0 & \frac{1}{2} \left(\frac{\partial u}{\partial y} - \frac{\partial v}{\partial x} \right) & \frac{1}{2} \left(\frac{\partial u}{\partial z} - \frac{\partial w}{\partial x} \right) \\ \frac{1}{2} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right) & 0 & \frac{1}{2} \left(\frac{\partial v}{\partial z} - \frac{\partial w}{\partial y} \right) \\ \frac{1}{2} \left(\frac{\partial w}{\partial x} - \frac{\partial u}{\partial z} \right) & \frac{1}{2} \left(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z} \right) & 0 \end{bmatrix}$$

Note that ϵ_{ij} is a symmetric tensor since $\epsilon_{ij} = \epsilon_{ji}$, that is, $\epsilon_{xy} = \epsilon_{yx}$, etc. ω_{ij} is an antisymmetric tensor since $\omega_{ij} = -\omega_{ji}$, that is, $\omega_{xy} = -\omega_{yx}$. If $\omega_{ij} = 0$, the deformation is said to be irrotational.

4. Objective questions

(2x7 = 14)

- True strain is additive – T/F? **T**
- What are the stress invariants?

$$I_1: \text{Sum of diagonal element} \quad I_1 = \sigma_{xx} + \sigma_{yy} + \sigma_{zz}$$

$$I_2: \text{Sum of determinants of minors} \quad I_2 = \begin{vmatrix} \sigma_{xx} & \sigma_{yx} \\ \sigma_{xy} & \sigma_{yy} \end{vmatrix} + \begin{vmatrix} \sigma_{yy} & \sigma_{zy} \\ \sigma_{yz} & \sigma_{zz} \end{vmatrix} + \begin{vmatrix} \sigma_{xx} & \sigma_{zx} \\ \sigma_{xz} & \sigma_{zz} \end{vmatrix}$$

$$I_3: \text{Determinant of tensor} \quad I_3 = \begin{vmatrix} \sigma_{xx} & \sigma_{yx} & \sigma_{zx} \\ \sigma_{xy} & \sigma_{yy} & \sigma_{zy} \\ \sigma_{xz} & \sigma_{yz} & \sigma_{zz} \end{vmatrix}$$

- How many slip systems does BCC material have and their types? **12 {110}<111> + 12 {112}<111> + 24 {123}<111> = 48**
- In edge dislocation, the burgers vector is parallel to the dislocation line – T/F? **F**
- Formation of twins is the root cause for strain hardening in metals – T/F? **F**
- In a wire drawing process, a copper rod (3.2 mm radius) is drawn through a die (2.50 mm radius). What is the force required to deform the copper? Is it sufficient to break the wire after it has been formed? (given: yield strength is 150 MPa at 0% cold work and 390 MPa at 40% cold work).

$$\% \text{cold work} = (A_f - A_o)/A_o * 100\% = 39\% (\sim 40\%)$$

$$\text{Force required to deform the wire, } F = 150 * \pi * (3.2)^2 = 4825 \text{ N}$$

$$\text{Stress on the wire after passing through the die} = F/A_f = 4825/(\pi * (2.5)^2) = 246 \text{ MPa.}$$

This stress is less than the yield strength of Cu, 390 MPa at 40% elongation.

- Zn and Ti have c/a ratio of 1.856 and 1.587 respectively – which one can slip on prismatic plane?

As Zn has a c/a ratio more than ideal value of 1.633, slip will occur on the **basal plane** with low critical resolved shear stress. But for Ti with lesser than ideal c/a ratio, slip will occur **on prismatic planes i.e. {10-10}**.

