

DiffusionPreliminary concepts

A composition variable quantifies the amount of substance or material present in the system.

Examples:-

i) substitutional solid : Al-Li, Al-Cu

$$\text{mole fraction } X_A = \frac{n_A}{n_A + n_B} \quad n_A = \text{No of A atoms}$$

$$X_B = \frac{n_B}{n_A + n_B} \quad n_B = \text{No of B atoms}$$

$$X_A + X_B = 1$$

usually has a length scale  
in its definition  
e.g. volume (V)

Concentration

$$c_A = \frac{n_A}{V} = \frac{n_A / n_A + n_B}{V / (n_A + n_B)} = \frac{x_A}{V_m}$$

↓  
molar volume

$$c_B = \frac{n_B}{V} = \frac{x_B}{V_m}$$

2) Interstitial atoms : C in Fe  $\rightarrow$  Fe<sub>x</sub>

Li in LaO<sub>2</sub>  $\rightarrow$  Li<sub>x</sub>LaO<sub>2</sub> (cathode material)

H in Pd  $\rightarrow$  Storage

$$x = \frac{n}{M} \quad M = \text{No of interstitial sites}$$

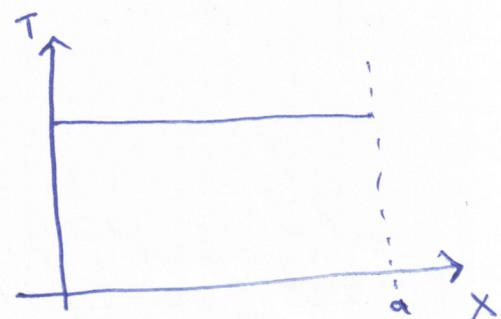
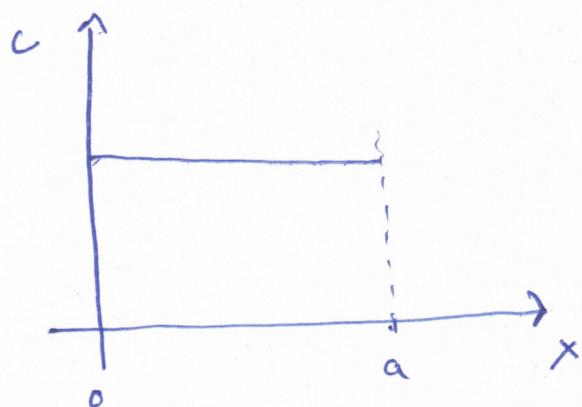
(or)  
No of unit cells

$$c = \frac{n}{V}$$

A single phase in equilibrium  
 $\rightarrow$  constant  $T$  and  $P$ , no ~~or~~ inhomogeneous stresses

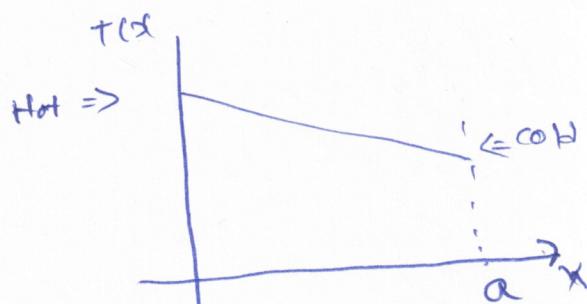
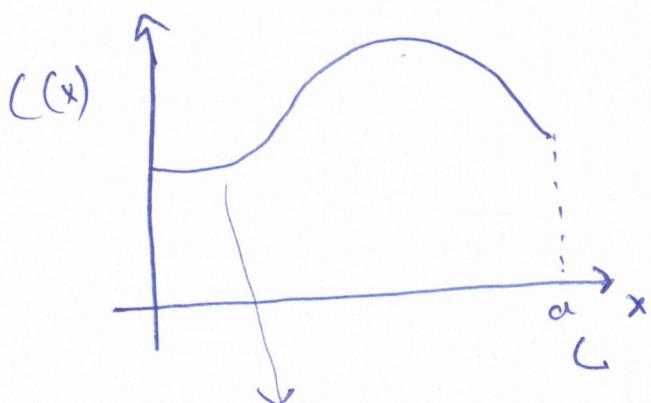
$\Rightarrow$  means it has constant ( $\infty$ ) uniform concentration and Temperature

e.g. block of metal like sheet pure iron



usually materials are out of equilibrium

non uniform  $\Downarrow$  concentration ( $\infty$ ) temperature

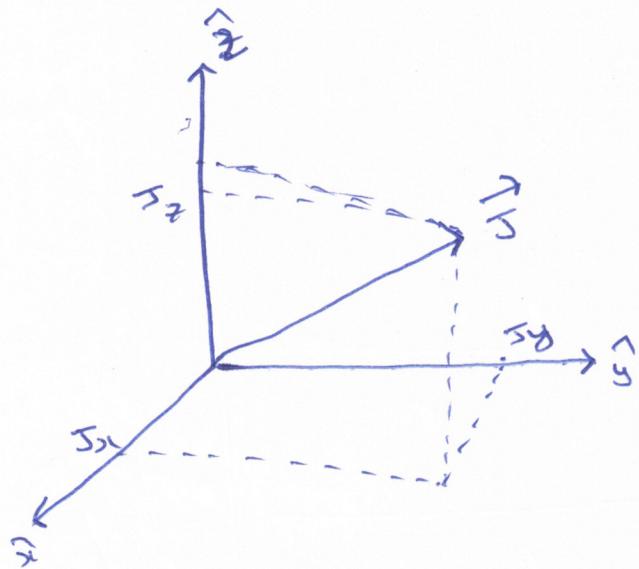


- $\rightarrow$  This creates a diffusion event moving the material towards equilibrium (uniform distribution)
- $\rightarrow$  concentration variation creates diffusive "Flux"

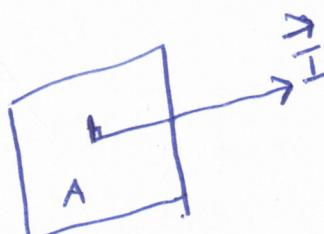
- FLUX
- \* a measure of flow per unit area
  - \* usually denoted by  $\vec{J}$  (a vector)
  - \* Flux can be different in different directions

$$\vec{J} = (J_x, J_y, J_z)$$

$$\vec{J} = J_x \hat{x} + J_y \hat{y} + J_z \hat{z}$$



$\vec{J}$  is equal to the net number of atoms that cross a unit area per unit time



current of atoms passing area the surface

$$\vec{J} = \frac{\vec{I}}{A}$$

units:

1) mole fraction:  $x_A = \frac{n_A}{n_A + n_B} = \text{unitless}$

2) concentration:  $C_A = \frac{n_A}{V} = \text{mole/m}^3$

3) flux:  $J_A = \frac{\text{no. of atoms crossing per area per time}}{\text{mole}} = \frac{\text{mole}}{\text{m}^2 \cdot \text{s}} = \frac{\text{mole}}{\text{cm}^2 \cdot \text{s}}$

↑ common to use  
cm

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Fick's First Law - phenomenological observation  
 (or)  
 empirical observation

→ It is a constitutive relation that links two physical quantities typically "cause" and "effect".  
 e.g. Interstitial atoms (only one species) diffusing

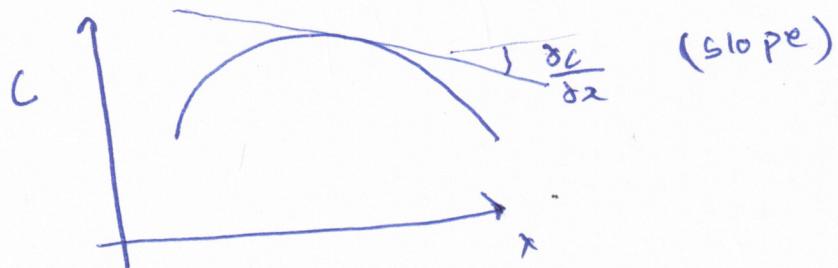
$$\vec{J} = -D \vec{\nabla} c$$

gradient operator - this operation turns a scalar field into a vector

$$\vec{\nabla} = \left( \frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z} \right)$$

$$\vec{\nabla} c = \left( \frac{\partial c}{\partial x}, \frac{\partial c}{\partial y}, \frac{\partial c}{\partial z} \right)$$

in 1-dimension  $\rightarrow J = -D \frac{\partial c}{\partial x}$



$D$  = diffusion coefficient  
 = tells you how mobile the atoms are in the system

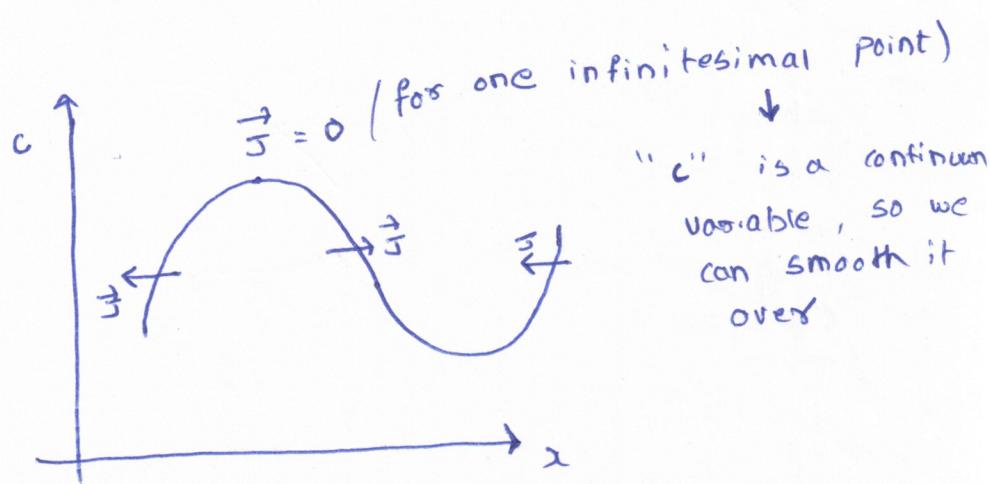
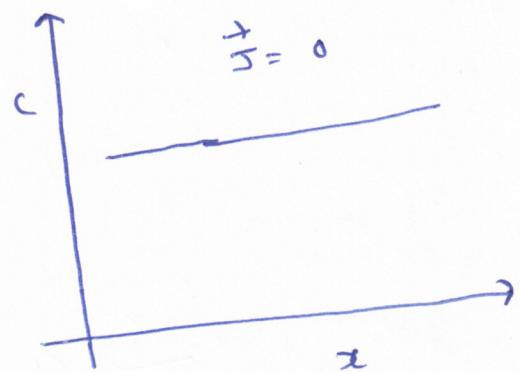
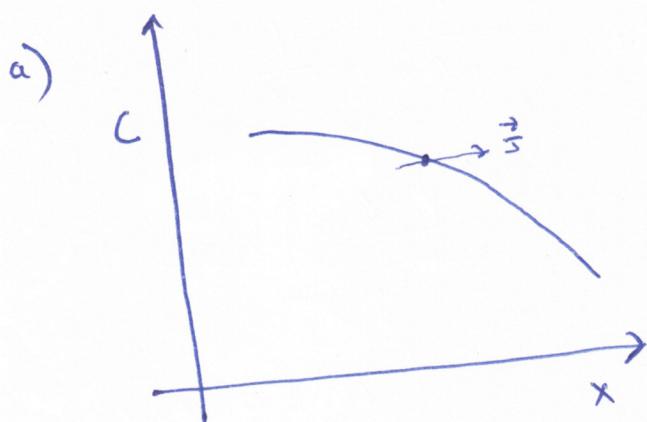
} depends on many factors such as  $T$ , crystal structure, atomic size etc

large  $D \Rightarrow$  mobile atoms  
 small  $D \Rightarrow$  sluggish atoms

units of  $P$ :

$$\frac{J}{\frac{\partial C}{\partial x}} = \frac{\frac{\text{mole}}{\text{cm}^2 \cdot \text{s}}}{\frac{\frac{\text{mole}}{\text{cm}^3}}{\text{cm}}} = \frac{\text{cm}^4}{\text{cm}^2 \cdot \text{s}} = \text{cm}^2/\text{s}$$

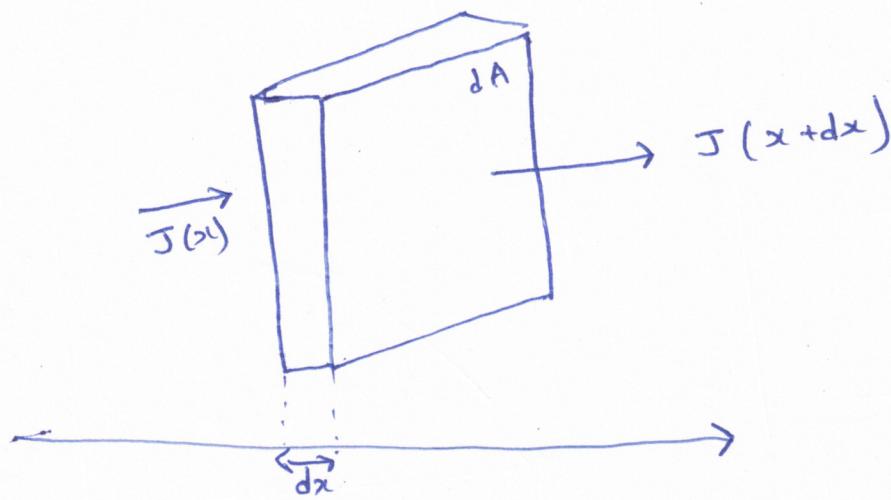
Imp  $\rightarrow$  Fick's 1<sup>st</sup> law indicate that atoms diffuse down their concentration gradient  
→ what is the direction of flux?



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Ficks Second Law: so far  $\vec{J} = -D \vec{\nabla} C$   
 ↳ brings time 't' into the picture

- This is a conservation equation
  - atoms don't disappear → conserved
  - atoms in x-direction
- e.g.: 1-dimension, flux  $J$  is in x-direction



$$\text{Volume, } V = dA \cdot dx$$

- No of particles in the volume,  $V = C \cdot dA \cdot dx$
- Rate of change of particles in  $V = \frac{d}{dt} (C dA dx)$

why do the number of particles change?  
 \* The incoming flux is different from outgoing flux

- No. of particles flowing in at  $x$  per time  
 $= dA \cdot J(x)$
- No. of particles flowing out at  $x+dx$  per time  
 $= dA \cdot J(x+dx)$   
↑ Taylor expansion  
 $= dA \cdot \left[ J(x) + \frac{\partial J}{\partial x} dx + (dx)^2 \right]$
- Net no of particles flowing through the volume,  $V = dA \left( J(x) - \left[ J(x) + \frac{\partial J}{\partial x} dx \right] \right) = \cancel{dA} \cdot \frac{\partial J}{\partial x} dx$

Both should be equal

$$\frac{\partial (C \Delta A \Delta x)}{\partial t} = -\Delta A \frac{\partial J}{\partial x} \Delta x$$
$$\Rightarrow \boxed{\frac{\partial C}{\partial t} = -\frac{\partial J}{\partial x}}$$

generalized

to 3-D

$$\Rightarrow \boxed{\frac{\partial C}{\partial t} = -\vec{\nabla} \cdot \vec{J}}$$

$$\vec{\nabla} \cdot \vec{J} = \text{divergence of } J$$
$$= \frac{\partial J_x}{\partial x} + \frac{\partial J_y}{\partial y} + \frac{\partial J_z}{\partial z}$$

Summary of Fick's 2 laws

1<sup>st</sup> law

$$\vec{J} = -D \vec{\nabla} C$$

→ constitutive equation

→ D is a materials constant

→ empirical equation

Does 2<sup>nd</sup> law valid if we

as species? what are sinks or sources of  
vacancies? Ans:- defects such as dislocation, GB's

2<sup>nd</sup> law

$$\frac{\partial C}{\partial t} = -\vec{\nabla} \cdot \vec{J}$$

→ conservation equation

→ valid if particles are not created or destroyed

consider vacancies

$$\frac{\partial C}{\partial t} = n - \vec{\nabla} \cdot \vec{J}$$

n = Source or sink term  
rate of creation or destruction of particles

taking care of

→ Let's combine the two laws

$$\frac{\partial c}{\partial t} = \vec{\nabla} \cdot (D \vec{\nabla} c)$$

if  $D$  is constant

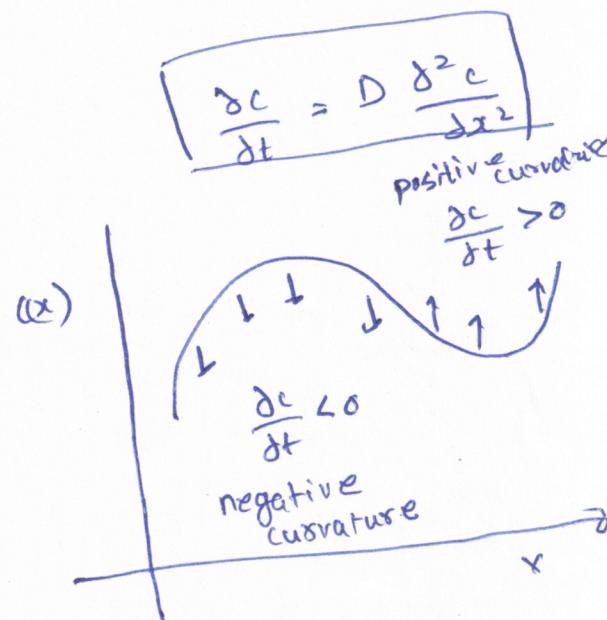
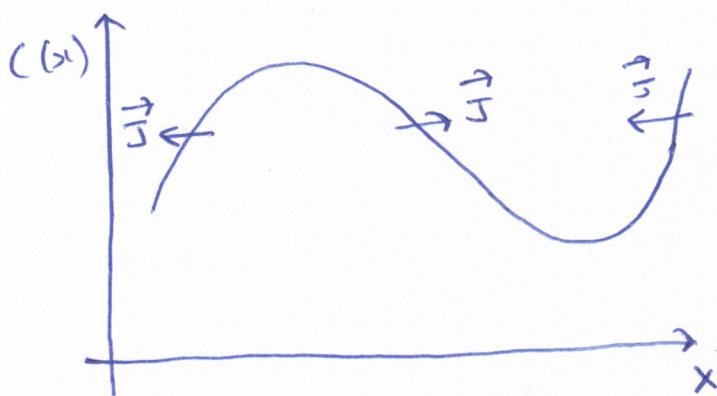
$$\boxed{\frac{\partial c}{\partial t} = D \nabla^2 c}$$

$\nabla^2$  = laplacian operator

$$\nabla^2 c = \frac{\partial^2 c}{\partial x^2} + \frac{\partial^2 c}{\partial y^2} + \frac{\partial^2 c}{\partial z^2}$$

→ physical interpretation

$$J = -D \frac{\partial c}{\partial x}$$



new comments on diffusivity: It connects two vectors,  $\vec{J}$  and  $\vec{\nabla} c$   $\Rightarrow$  Hence its a  $2^{nd}$  order tensor

$$\begin{pmatrix} J_x \\ J_y \\ J_z \end{pmatrix} = - \underbrace{\begin{pmatrix} D_{xx} & D_{xy} & D_{xz} \\ D_{yx} & D_{yy} & D_{yz} \\ D_{zx} & D_{zy} & D_{zz} \end{pmatrix}}_{\text{tensor}} \begin{pmatrix} \frac{\partial c}{\partial x} \\ \frac{\partial c}{\partial y} \\ \frac{\partial c}{\partial z} \end{pmatrix}$$

for isotropic materials, cubic symmetry

$$D_{xx} = D_{yy} = D_{zz} = D, \quad D_{ij} = 0 \quad \text{if } i \neq j$$

→ If diffusivity changes with concentration  $D(c)$

$$\frac{\partial c}{\partial t} = \nabla \cdot [D(c) \nabla c]$$

$$\Rightarrow \frac{\partial c}{\partial t} = D(c) \frac{\partial^2 c}{\partial x^2} + \frac{d D(c)}{d c} \left( \frac{\partial c}{\partial x} \right)^2$$

→ If diffusivity function of time,  $D(t)$

$$\frac{\partial c}{\partial t} = \nabla \cdot [D(t) \nabla c] = D(t) \nabla^2 c$$

we can do change of variable

$$T_D = \int_0^t D(t') dt'$$

$$\frac{\partial c}{\partial t} = \frac{\partial c}{\partial T_D} \frac{\partial T_D}{\partial t} = \left( \frac{\partial c}{\partial T_D} \right) D(t)$$

$$\Rightarrow \boxed{\frac{\partial c}{\partial T_D} = \nabla^2 c}$$

similar to master eqn

some times replace  $D(t)$  with  $\int_0^t D dt$  in the solution

If

diffusivity is fn of direction

$$J_i = - \sum_j D_{ij} \frac{\partial c}{\partial x_j}$$

$$\frac{\partial c}{\partial t} = \hat{D}_{11} \frac{\partial^2 c}{\partial x_1^2} + \hat{D}_{22} \frac{\partial^2 c}{\partial x_2^2} + \hat{D}_{33} \frac{\partial^2 c}{\partial x_3^2}$$

$$\hat{D} = \begin{bmatrix} \hat{D}_{11} & 0 & 0 \\ 0 & \hat{D}_{22} & 0 \\ 0 & 0 & \hat{D}_{33} \end{bmatrix}$$

eigenvalues

$$[\hat{x}_1, \hat{x}_2, \hat{x}_3]$$

eigen vectors

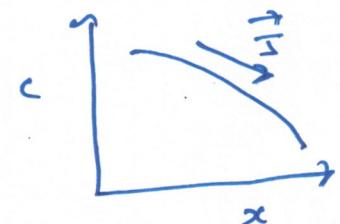
Finite

difference

method :-

- This is a way to solve differential equations
- Let's take an example of diffusion

Fick's First law:  $\vec{J} = -D \frac{\partial c}{\partial x}$   
 ↓  
 Flux



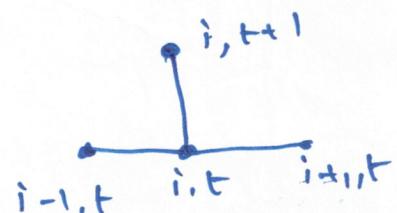
Fick's second law:  $\frac{\partial c}{\partial t} = -\frac{\partial J}{\partial x}$

⇒ Diffusion eq:  $\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2}$

For constant  $D$

$$\Rightarrow \frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2}$$

→ Forward differencing (explicit)



$$\frac{\partial c}{\partial t} = \frac{c_i^{t+1} - c_i^t}{\Delta t}$$

$$\frac{\partial^2 c}{\partial x^2} = D \left( \frac{c_{i+1}^t - 2c_i^t + c_{i-1}^t}{\Delta x^2} \right)$$

$$\Rightarrow c_i^{t+1} = c_i^t + \left( \frac{D \Delta t}{\Delta x^2} \right) \left( \frac{c_{i+1}^t - 2c_i^t + c_{i-1}^t}{\Delta x^2} \right)$$

$\downarrow$

$$\Delta \leq \frac{1}{2}$$

$$\Rightarrow c_i^{t+1} = c_i^t (1 - 2\alpha) + \alpha (c_{i+1}^t + c_{i-1}^t)$$

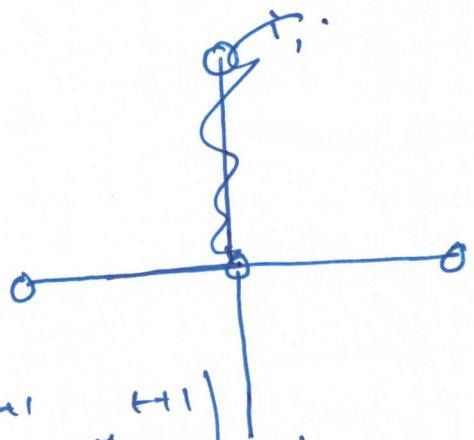
$\downarrow$   
 $\lambda \leq \frac{1}{2}$

→ Go to ~~the~~

→ Backward differencing

$$\frac{\partial c}{\partial t} = D \frac{\partial^2 c}{\partial x^2}$$

$$\Rightarrow \frac{\partial c}{\partial t} = \frac{c_i^{t+1} - c_i^t}{\Delta t}$$



$$\text{But } \left. \frac{\partial^2 c}{\partial x^2} \right|_{t+1} = D \left( \frac{\phi_{i+1}^{t+1} - 2\phi_i^{t+1} + \phi_{i-1}^{t+1}}{\Delta x^2} \right)_{ij}$$

$$\Rightarrow -\alpha c_{i-1}^{t+1} + (1 + 2\alpha) c_i^{t+1} - \alpha \phi c_{i+1}^{t+1} = \phi c_i^t$$

→ always stable.  
Boundary conditions:-

1) Dirichlet BC :- Concentration is given  
 $c(x=0) = 0$   
 $c(x=1) = 2$

2) Newman BC :- Flux is given

$$\frac{\partial c}{\partial x} \Big|_{x=0} = 2$$

$$\Rightarrow -D \frac{\partial c}{\partial x} \Big|_{x=d} = 2$$

3) Mixed BC :-

Explicit Method: when  $D$  depends on  $x$   $(1-D)$

$$\frac{\partial C}{\partial t} = D \frac{\partial}{\partial x} \left( D \frac{\partial C}{\partial x} \right) = \left( \frac{\partial C}{\partial x} \frac{\partial D}{\partial x} + D \frac{\partial^2 C}{\partial x^2} \right)$$

new term  
does not depend on ' $t$ '

$$\Rightarrow \frac{C_i^{t+1} - C_i^t}{\Delta t} = \frac{(C_{i+1}^t - C_i^t)}{\Delta x} \frac{(D_{i+1} - D_i)}{\Delta x} +$$

$$\frac{D_i}{\Delta x^2} \left( C_{i+1}^t - 2C_i^t + C_{i-1}^t \right)$$

$$\Rightarrow C_i^{t+1} = C_i^t + \frac{\Delta t}{\Delta x^2} \left[ (C_{i+1}^t - C_i^t) \frac{(D_{i+1} - D_i)}{D_i} + (C_{i+1}^t - 2C_i^t + C_{i-1}^t) \right]$$

$$\Rightarrow C_i^{t+1} = C_i^t + \beta \left[ \frac{C_{i+1}^t D_{i+1} - C_{i+1}^t D_i - C_i^t D_{i+1} + C_i^t D_i}{D_i} + \frac{C_{i+1}^t - \beta D_i C_i + D_i C_{i-1}}{D_i} \right]$$

$$\Rightarrow C_i^{t+1} = C_i^t \left( 1 - \beta (D_{i+1} + D_i) \right) + C_{i+1}^t (\beta D_{i+1}) + C_{i-1}^t (\beta D_i)$$

Implicit Method: when  $D$  depends on  $x$  ( $1-D$ )

$$\frac{\partial c}{\partial t} = \frac{\partial}{\partial x} \left( D \frac{\partial c}{\partial x} \right) = \frac{\partial c}{\partial x} \frac{\partial D}{\partial x} + D \frac{\partial^2 c}{\partial x^2}$$

↑ no "t" in  $D$

$$\Rightarrow \frac{c_i^{t+1} - c_i^t}{\Delta t} = \frac{c_{i+1}^{t+1} - c_i^{t+1}}{\Delta x} \frac{D_{i+1} - D_i}{\Delta x} + \\ D_i \left( \frac{c_{i+1}^{t+1} + c_{i-1}^{t+1} - 2c_i^{t+1}}{\Delta x^2} \right)$$

$$\Rightarrow c_i^{t+1} = c_i^t + \left( \frac{4t}{\Delta x^2} \right) \left( (c_{i+1}^{t+1} - c_i^{t+1}) \right) \left( (D_{i+1} - D_i) \right) \\ + \beta D_i \left( c_{i+1}^{t+1} + c_{i-1}^{t+1} - 2c_i^{t+1} \right)$$

$$\Rightarrow c_i^{t+1} = c_i^t + \beta \left[ D_{i+1}^{t+1} c_{i+1}^{t+1} - D_i^{t+1} c_{i+1}^{t+1} - D_{i+1}^{t+1} c_i^{t+1} \right. \\ \left. + D_i^{t+1} c_i^{t+1} + D_i^{t+1} c_{i-1}^{t+1} + D_i^{t+1} c_{i-1}^{t+1} - D_i^{t+1} c_i^{t+1} \right]$$

$$\Rightarrow \boxed{-\beta D_{i+1} c_{i+1}^{t+1} + (1 + \beta D_{i+1} + D_i) c_i^{t+1} - \beta D_i c_{i-1}^{t+1} = c_i^t}$$