

where;

A  $\rightarrow$  Falling Film Reactor

B  $\rightarrow$  Cooling Tower

C  $\rightarrow$  Separator

D  $\rightarrow$  Cyclone

E  $\rightarrow$  Electrostatic Precipitator

F  $\rightarrow$  Bleaching Tower

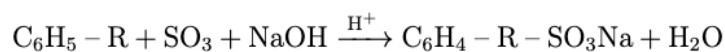
G  $\rightarrow$  Dilution Tank

H  $\rightarrow$  Neutralization Vessel

M1  
M2  
M3 }  $\rightarrow$  Static Mixer

## 1 Reaction information

### 1.1 Main Reaction



Here, we have taken the alkyl group  $-\text{R}$  as C-12:  $-(\text{CH}_2)_{11}\text{CH}_3$

### 1.2 Molecular Weights

Compound	Formula	Molecular Weight (kg/kmol)
Sulfonating Agent	$\text{SO}_3$	80.06
Linear Alkyl Benzene	$\text{C}_6\text{H}_5 - \text{R}$	246.42
Linear Alkyl Benzene Sulfonic Acid	$\text{C}_6\text{H}_4 - \text{R} - \text{SO}_3\text{H}$	326.48
Linear Alkyl Benzene Sulfonate	$\text{C}_6\text{H}_4 - \text{R} - \text{SO}_3\text{Na}$	348.45

Table 1: Molecular Weights of LAB and its Sulfonation Products

## 2 Basis Calculations

We take the production of Linear Alkyl Benzene Sulfonate (LABS) as **1000 kg/day** with an **overall molar conversion of 90%**.

### 2.1 Calculation of Molar and Mass Flow Rates

#### Step 1: Calculate LABS Molar Flow Rate

The molar flow rate of LABS in kmol/hr:

$$\dot{n}_{\text{LABS}} = \frac{\text{Mass Flow Rate}}{\text{Molecular Weight}} = \frac{1000 \text{ kg/day}}{348.45 \text{ kg/kmol}} \times \frac{1}{24 \text{ hr/day}}$$

$$\dot{n}_{\text{LABS}} = 0.12 \text{ kmol/hr}$$

**Step 2: Calculate Molar Flow Rate of LAB and SO<sub>3</sub> in Feed Stream**

Since the overall molar conversion is **90%**, the required molar flow rates of reactants are:

$$\dot{n}_{\text{C}_6\text{H}_5 - \text{R}} = \frac{\dot{n}_{\text{LABS}}}{\text{Conversion}} = \frac{0.12}{0.90} = 0.13 \text{ kmol/hr}$$

$$\dot{n}_{\text{SO}_3} = \dot{n}_{\text{C}_6\text{H}_5 - \text{R}} = 0.13 \text{ kmol/hr}$$

**Step 3: Calculate Mass Flow Rates of All Components**

Using mass flow rate formula:

$$\dot{m} = \dot{n} \times M$$

$$\dot{m}_{\text{C}_6\text{H}_5 - \text{R}} = 0.13 \times 246.42 = 32.03 \text{ kg/hr}$$

$$\dot{m}_{\text{SO}_3} = 0.13 \times 80.06 = 10.41 \text{ kg/hr}$$

$$\dot{m}_{\text{LABS}} = 0.12 \times 348.45 = 41.81 \text{ kg/hr}$$

**2.2 Final Flow Rate Table**

Component	Formula	Molar Flow Rate kmol/hr	Mass Flow Rate kg/hr
Linear Alkyl Benzene (LAB)	C <sub>6</sub> H <sub>5</sub> – R	0.13	32.03
Sulfonating Agent	SO <sub>3</sub>	0.13	10.41
Linear Alkyl Benzene Sulfonic Acid (LABSA)	C <sub>6</sub> H <sub>4</sub> – R – SO <sub>3</sub> H	0.12	41.81

Table 2: Molar and Mass Flow Rates of Reactants and Products

**3 Mass Flow Balances****3.1 Falling-Film Reactor**

**Key Assumptions:**

- **Overall Production Basis:** 1000 kg LABS/day, which is equivalent to:

$$41.81 \text{ kg/hr} = 0.12 \text{ kmol/hr LABS salt}$$

- **Single-Pass Conversion ( $\eta$ ):** 90% (based on total LAB feed).
- **Recycle Efficiency ( $r$ ):** 90% of unreacted LAB is recovered and recycled.



**3.1.1 Step 1: Determine Required LAB Reaction to Meet Final Product**

- From the stoichiometry, we assume:

Moles of LABS salt produced = Moles of LABSA produced = Moles of LAB consumed

- Hence, for 100% conversion, the total LAB required:

$$F_{\text{total}} = 0.12 \text{ kmol/hr}$$

- Given that the single-pass conversion of LAB in the Falling-Film Reactor (FFR) is 90%:

$$F_{\text{total}} = \frac{0.12}{0.9} = 0.133 \text{ kmol/hr}$$

**3.1.2 Step 2: Determine Unreacted LAB and Recycle Stream**

- The molar flow rate of unreacted LAB:

$$F_{\text{unreacted}} = (1 - \eta) \times F_{\text{total}} = 0.1 \times 0.133 = 0.013 \text{ kmol/hr}$$

- With a 95% recovery efficiency, the recycled LAB stream:

$$R = 0.9 \times F_{\text{unreacted}} = 0.9 \times 0.013 = 0.0117 \text{ kmol/hr}$$

**3.1.3 Step 3: Determine the Required Fresh LAB Feed**

- Using the mass balance equation:  $F_{\text{total}} = F_{\text{fresh}} + R$
- Solving for  $F_{\text{fresh}}$ :  $F_{\text{fresh}} = 0.133 - 0.0117 = 0.1213 \text{ kmol/hr}$

**3.1.4 Step 4: SO<sub>3</sub> Requirement in the Reactor**

- The reaction follows a 1:1 molar ratio.
- Hence, the molar flow rate of SO<sub>3</sub> reacted:

$$F_{\text{SO}_3} = F_{\text{total}} \times \eta = 0.133 \times 0.9 = 0.1197 \text{ kmol/hr}$$

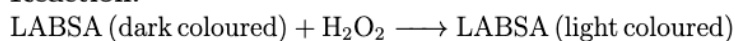
Summary of Molar and Mass Flow Rates

Compound Name	In Mass Flow (kg/hr)	Out Mass Flow (kg/hr)
Linear Alkyl Benzene Sulfonic Acid (LABSA)	-	39.18
Linear Alkyl Benzene (LAB)	32.77	3.2
Sulfur Trioxide (SO <sub>3</sub> )	9.58	-
<b>Total</b>	<b>42.35</b>	<b>42.38</b>

Table 3: Summary of Mass Flow Rates in the Reactor

### 3.2 Bleaching

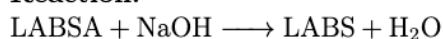
**Reaction:**



- **Key Consideration:** The LABS itself remains chemically unchanged.
- During the bleaching process, impurities present in Linear Alkyl Benzene Sulfonic Acid (LABSA) react with a bleaching agent, such as hydrogen peroxide (H<sub>2</sub>O<sub>2</sub>) or sodium hypochlorite (NaOCl).
- This oxidation effectively removes color impurities without chemically altering the LABSA. Hence, mass flow rate of LABSA remains almost same.

### 3.3 Neutralization

**Reaction:**



- **LABSA Neutralization:**
  - Input molar flow rate of LABSA = 0.12 kmol/hr
  - The reaction follows a 1:1 molar ratio. Hence,  
Molar flow rate of pure NaOH = 0.12 kmol/hr
- **NaOH Requirements:**
  - Mass flow rate of pure NaOH =  $0.12 \times 39.997 = 4.8 \text{ kg/hr}$
  - Given that typical NaOH aqueous solution is 30% w/w,  
Mass flow rate of NaOH solution =  $\frac{4.8}{0.3} = 16 \text{ kg/hr}$

- **Water Contributions:**

- Water content from NaOH solution =  $16 - 4.8 = 11.2$  kg/hr
- Water content from NaOH solution in molar terms =  $\frac{11.2}{18} = 0.62$  kmol/hr
- Water generated by the neutralization reaction =  $0.12$  kmol/hr

- **Total Water Output:**

- Total water output =  $0.62 + 0.12 = 0.74$  kmol/hr
- Mass flow rate =  $0.74 \times 18 = 13.32$  kg/hr

### Summary of Mass Flows

Compound Name	In Mass Flow (kg/hr)	Out Mass Flow (kg/hr)
Linear Alkyl Benzene Sulfonate (LABS)	-	41.81
Linear Alkyl Benzene Sulfonic Acid (LABSA)	39.18	-
Sodium Hydroxide (NaOH)	4.8	-
Water (H <sub>2</sub> O)	11.2	13.32
<b>Total</b>	<b>55.18</b>	<b>55.13</b>

Table 4: Mass Flow Summary of Compounds

## 4 Energy Balance

### 4.1 Falling-Film Reactor

#### Mass Flow Rates:

- Amount of SO<sub>3</sub> reacting:  $\dot{m}_{\text{SO}_3} = 9.58$  kg/hour
- Amount of LAB reacting:  $\dot{m}_{\text{LAB}} = 29.57$  kg/hour
- Amount of LABSA produced:  $\dot{m}_{\text{LABSA}} = 39.18$  kg/hour

#### Heat of Formation:

- SO<sub>3</sub>:  $\Delta H_{f,\text{SO}_3} = -4.936$  kJ/kg
- LAB:  $\Delta H_{f,\text{LAB}} = 0.97$  kJ/kg
- LABSA:  $\Delta H_{f,\text{LABSA}} = -0.53$  kJ/kg

#### Heat of Reaction:

- $\Delta H_{rxn} = \dot{m}_{\text{LABSA}} \times \Delta H_{f,\text{LABSA}} + (\dot{m}_{\text{SO}_3} \times \Delta H_{f,\text{SO}_3} + \dot{m}_{\text{LAB}} \times \Delta H_{f,\text{LAB}})$
- Calculation:  
 $\implies 39.18 \times -0.53 + (9.58 \times -4.936 + 29.57 \times 0.97) = -39.37$  kJ/hr

## 4.2 Heater

### Mass Flow Rates:

- Mass flow rate of unreacted LAB: 0.32 kg/hr
- Mass flow rate of LABSA: 39.18 kg/hr

### Specific Heat Capacity:

- LAB: 2.034 kJ/(kg.K)
- LABSA: 1.6 kJ/(kg.K)

### Temperature Change:

- Inlet stream temperature: 30°C
- Outlet stream temperature: 40°C

### Heat Input:

- $\dot{Q}_{in} = \dot{m}_{LAB} \times C_{P,LAB} \times \Delta T + \dot{m}_{LABSA} \times C_{P,LABSA} \times \Delta T$
- Calculation:  
 $\implies 0.32 \times 2.034 \times 10 + 39.18 \times 1.6 \times 10 = 633.39 \text{ kJ/hr}$

## 4.3 Neutralization

### Heat of Reaction:

- Heat of neutralization: 55.9 kJ/mol

### Molar Flow Rate:

- LABSA: 0.12 kmol/hr

### Total Heat Released:

- $\Delta H_{neutralization} = 0.12 \times 1000 \times 55.9 = 6708 \text{ kJ/hr}$

## 4.4 Overall Balance

- $\dot{Q}_{net} = \Delta H_{rxn} + \dot{Q}_{in} + \Delta H_{neutralization}$
- Calculation:  
 $\implies -39.37 + 633.39 + 6708 = 7302.02 \text{ kJ/hr}$



**Capital cost (only for the reactor):**

Equipment	Design Capacity (gallons)	No. of units	Cost/unit (\$ for year 2014)	Total Cost (\$ for year 2014)
Reactor A (Jacketed reactor & Agitated)	1800	1	64100	64100
Reactor H (Kettle,jacketed & Agitated)	39.63	1	38200	38200

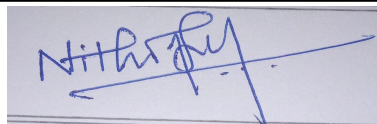
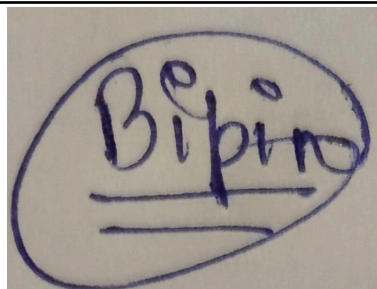
**References:** Provide reference for a research paper or an actual patent.

1. <http://www.matche.com/equipcost/Reactor.html>

**List the contributions of each author:**

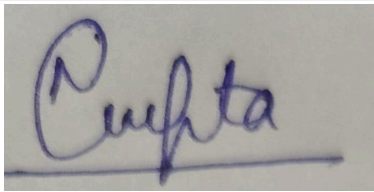
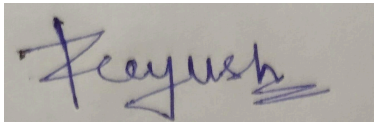
- **Process flow diagram:** Sarthak Singh
- **Material Balance:** Bipin Kumar Jaiswal, Nonit Gupta, Peeyush Sahu
- **Energy Balance:** Bipin Kumar Jaiswal, Nonit Gupta, Peeyush Sahu
- **Capital Cost:** Bipin Kumar Jaiswal

**Sign the pdf and upload.**

Name	Roll No	Signature
Nithin TM (CEO)	230709	
Bipin Kumar Jaiswal	230300	

## CHE261A Patent Application

---

Nonit Gupta	230712	
Peeyush Sahu	230750	
Sarthak Singh	230930	