

Article

# Implication of vegetation response to climate change for mountain grasslands

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## Abstract:

1. Evaluate default PET models
2. Evaluate calibrated PET models
3. Sensitivity analysis and model uncertainty of calibrated PET models
4. Implication of elevated CO<sub>2</sub> in PET models
5. Implication of warming in PET models
6. Combined effect of warming and elevated CO<sub>2</sub> in PET models
7. Evaluation, Sensitivity analysis and model uncertainty of calibrated PET models
8. Conclusion

**Keywords:** keyword 1; keyword 2; keyword 3 (list three to ten pertinent keywords specific to the article, yet reasonably common within the subject discipline.)

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## 2. Evaluation of PET models

### 2.1. Evaluation of PET models with default coefficients

same Rn same rh same T...

Penman

$$E = \frac{1}{\lambda \rho_w} \frac{\Delta(R_n - G) + K_u \gamma (a_w + b_w u_2)(e_s - e_a)}{\Delta + \gamma} \quad (1)$$

where  $a_w$  and  $b_w$  are wind function coefficients that are usually receive a local or regional calibration. Parameter  $K_u = 6.43$  for ET in  $\text{mmd}^{-1}$  and  $K_u = 0.268$  for ET in  $\text{mmhour}^{-1}$ . Penman [1] used for clipped grass [2]  $a_w = 1.0$  and  $b_w = 0.537$ , respectively, for wind speed in  $\text{ms}^{-1}$ ,  $e_s - e_a$  in kPa and grass ETo in  $\text{mmd}^{-1}$ . The equations were intended for use with daily computations. In application of the 1963 Penman, saturation vapor pressure is traditionally based on mean daily air temperature rather than on Tmax and Tmin [3].

Penman-Monteith [2]

$$E = \frac{1}{\lambda} \frac{\Delta(R_n - G) + \rho_a c_p (e_s - e_a) / r_{ah}}{\left[ \Delta + \gamma \left( 1 + \frac{r_s}{r_{ah}} \right) \right]} \quad (2)$$

Priestley-Taylor [2]

$$E = \frac{1.26}{\lambda} \frac{\Delta}{\Delta + \gamma} (R_n - G) \quad (3)$$

Kimberley-Penman [2]

$$E = \frac{1}{\lambda \rho_w} \frac{\Delta(R_n - G) + K_u \gamma (a_w + b_w u_2)(e_s - e_a)}{\Delta + \gamma} \quad (4)$$

where:

$$a_w = 0.4 + 1.4 \exp - \left[ \left( \frac{J - 173}{58} \right)^2 \right] \quad (5)$$

$$b_w = 0.605 + 0.345 \exp - \left[ \left( \frac{J - 243}{80} \right)^2 \right] \quad (6)$$

Hamon

Turc-

Makink [2]

$$ET_0 = 0.61 \frac{\Delta}{\Delta + \gamma} \frac{R_s}{2.45} - 0.12 \quad (7)$$

Doorenbos and Pruitt [4]

$$ET_0 = c \frac{\Delta}{\Delta + \gamma} \frac{R_s}{2.45} - 0.3 \quad (8)$$

where c is the calibration factor that is a function of rh and ud. allen and pruit [5]:

$$c = 1.066 - 0.00128 RH_{mean} + 0.045 u_d - 0.0002 RH_{mean} u_d - 0.0000315 (RH_{mean}^2) - 0.001103 (u_d)^2 \quad (9)$$

$u_d$  has limits  $0 < u_d < 10 \text{ ms}^{-1}$ .

Hargreaves [6]

$$ET_0 = 0.0023 (T_{max} - T_{min})^{0.5} (T_{mean} + 17.8) \frac{R_a}{\lambda \rho_w} \quad (10)$$

Ra is average daily exoatmospheric radiation(extra terrestrial) Blaney-Criddle [2]

Jensen-Haise [2] -  $ET_r$  is alfalfa reference ET

$$ET_r = \frac{1}{\lambda} C_r (T - T_x) R_s \quad (11)$$

$C_r$  and  $T_x$  should be constant for a given area... Later Jensen defined:

$$C_r = \frac{1}{C_1 + C_2 C_H} \quad (12)$$

$$C_H = \frac{5}{e_2 + e_1} \quad (13)$$

$e_2$  and  $e_1$  are the saturation vapor pressures in kPa at the mean daily maximum and mean daily minimum temperatures, respectively, for the average warmest month of the year in an area, and  $C_1$  and  $C_2$  are constants ( $C_2 = 13$  degrees F or 7.3 degrees C).

$$C_1 = 38 - (2Elev/305) \quad (14)$$

$$T_x = -2.5 - 1.4(e_2 - e_1) - Elev/550 \quad (15)$$

#### 2.1.1. Inputs

$R_n$  net longwave radiation

$$R_n l = f_{cd} (a_1 + b_1 \sqrt{e_a}) \sigma T^4 \quad (16)$$

if 24-hour or longer time steps...  $T^4$  transforms to  $(T_{max}^4 - T_{min}^4)/2$ .

$\sigma$  is for daily values  $4.901 \times 10^{-9} \text{ MJm}^{-2}\text{d}^{-1}\text{K}^{-4}$  with  $R_{nl}$  in  $\text{MJm}^{-2}\text{d}^{-1}$

for hourly calculations  $\sigma = 2.042 \times 10^{-10} \text{ MJm}^{-2} \text{h}^{-1}\text{K}^{-4}$ ,  $R_{nl}$  is in  $\text{MJm}^{-2} \text{h}^{-1}$ .

Wright and Jensen [7] developed an expression for  $f_{cd}$ :

$$f_{cd} = a \frac{R_s}{R_{SO}} + b \quad (17)$$

$a$  and  $b$  are empirical coefficients. General  $a = 1.3$ ,  $b = 0.3$ ,  $a_1 = 0.39$  and  $b_1 = 0.158$

#### 2.1.2. Evaluation of calibrated/validated PET models

TEXT

#### 2.1.3. Evaluation of calibrated PET models

TEXT

### 3. Results

This section may be divided by subheadings. It should provide a concise and precise description of the experimental results, their interpretation as well as the experimental conclusions that can be drawn.

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#### 3.1. Subsection

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Bulleted lists look like this:

- 60 • First bullet
- 61 • Second bullet
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- 64 1. First item
- 65 2. Second item
- 66 3. Third item

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71       Text

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entry 1	data	data
entry 2	data	data

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73       Text

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75       This is an example of an equation:

$$a + b = c \quad (18)$$

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78 **Theorem 1.** *Example text of a theorem.*

79       The text continues here. Proofs must be formatted as follows:

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## Abbreviations

The following abbreviations are used in this manuscript:

MDPI Multidisciplinary Digital Publishing Institute

DOAJ Directory of open access journals

TLA Three letter acronym

LD linear dichroism

## Appendix A

### Appendix A.1

The appendix is an optional section that can contain details and data supplemental to the main text. For example, explanations of experimental details that would disrupt the flow of the main text, but nonetheless remain crucial to understanding and reproducing the research shown; figures of replicates for experiments of which representative data is shown in the main text can be added here if brief, or as Supplementary data. Mathematical proofs of results not central to the paper can be added as an appendix.

## Appendix B

All appendix sections must be cited in the main text. In the appendixes, Figures, Tables, etc. should be labeled starting with 'A', e.g., Figure A1, Figure A2, etc.

1. Penman, H.L. Vegetation and hydrology. *Soil Science* **1963**, *96*, 357.
2. ASCE-EWRI. The ASCE standardized reference evapotranspiration equation. *Technical Committee Rep. to the Environmental and Water Resources Institute of ASCE from the Task Committee on Standardization of Reference Evapotranspiration* **2005**.
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7. Wright, J.L.; Jensen, M.E. Peak water requirements of crops in southern Idaho. *Proceedings of the American Society of Civil Engineers, Journal of the Irrigation and Drainage Division* **1972**, *98*, 193–201.

**Sample Availability:** Samples of the compounds ..... are available from the authors.

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