

Delta Parallel Robot - Kinematic Study

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1 BASIC GEOMETRY

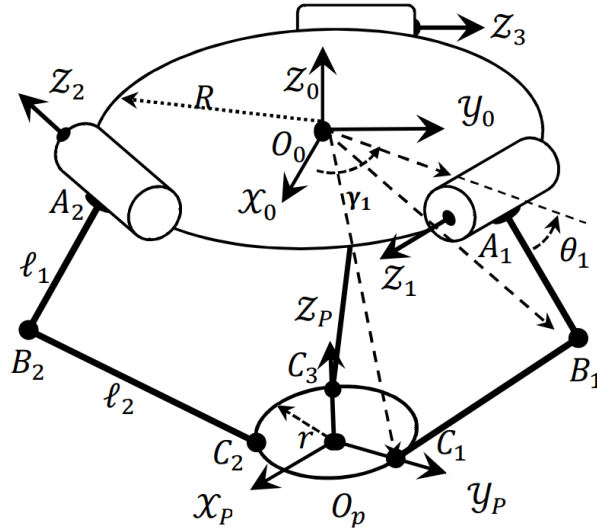


Figure 1.1: Delta Parallel Robot schematic

The first value definition is regarding the distance of the actuator joint and base frame center:

$$R_i = \overline{O_0 A_i}$$

And then the center of the End-Effector's distance with the nearest universal joint:

$$r_i = \overline{O_P C_i}$$

The length of each drive link will be:

$$L_i = \overline{A_i B_i}$$

And the length of the driven link will be:

$$l_i = \overline{B_i C_i}$$

The angles between x_0 and $\overline{O_0 A_i}$ are equal to γ_i . The angles between x_P and $\overline{O_P C_i}$ are equal to β_i . The angles between the horizon and the drive link are θ_i , Where $i = 1, 2, 3$

2 FORWARD KINEMATICS

We'll first write down the kinematic chain. The position of A_i in relation to the $\{0\}$ frame:

$$\overline{O_0 A_i} = [R_i \cos \gamma_i \quad R_i \sin \gamma_i \quad 0]^T \quad (2.1)$$

The position of B_i in relation to the $\{0\}$ frame:

$$\overline{O_0 B_i} = \begin{bmatrix} (L_i \cos \theta_i + R_i) \cos \gamma_i \\ (L_i \cos \theta_i + R_i) \sin \gamma_i \\ -L_i \sin \theta_i \end{bmatrix} \quad (2.2)$$

The position of $\{P\}$ frame origin point in relation to the $\{0\}$ frame:

$$\overline{O_0 O_P} = [X_P \quad Y_P \quad Z_P]^T \quad (2.3)$$

The position of C_i in relation to the $\{P\}$ frame

$$\overline{O_P C_i} = [r_i \cos \beta_i \quad r_i \sin \beta_i \quad 0]^T \quad (2.4)$$

The position of C_i in relation to the $\{0\}$ frame:

$$\overline{O_0 C_i} = \begin{bmatrix} X_P + r_i \cos \beta_i \\ Y_P + r_i \sin \beta_i \\ Z_P \end{bmatrix} \quad (2.5)$$

With that the kinematic chain has ended. The next step is to use a "good" constraint as the solution of the kinematic chain which in this case is the lengths of the driven links:

$$l_i = |\overline{O_0 B_i} - \overline{O_0 C_i}| \quad (2.6)$$

With expanding the mentioned equation we will have the following:

$$\overline{O_0 B_i} - \overline{O_0 C_i} = \begin{bmatrix} (L_i \cos \theta_i + R_i) \cos \gamma_i - r_i \cos \beta_i - X_P \\ (L_i \cos \theta_i + R_i) \sin \gamma_i - r_i \sin \beta_i - Y_P \\ -L_i \sin \theta_i - Z_P \end{bmatrix} \quad (2.7)$$

From the Eq. 2.7 we can write:

$$X_P^2 + Y_P^2 + Z_P^2 + a_i X_P + b_i Y_P + c_i Z_P + d_i = 0 \quad (2.8)$$

Where:

$$\begin{aligned} a_i &= -2(L_i \cos \theta_i + R_i) \cos \gamma_i + 2r_i \cos \beta_i \\ b_i &= -2(L_i \cos \theta_i + R_i) \sin \gamma_i + 2r_i \sin \beta_i \\ c_i &= 2L_i \sin \theta_i \\ d_i &= (R_i + L_i \cos \theta_i)^2 + r_i^2 + L_i^2 \sin^2 \theta_i - 2r_i(R_i + L_i \cos \theta_i) \cos(\gamma_i - \beta_i) - l_i^2 \end{aligned} \quad (2.9)$$

There will be a system of equations as depicted below:

$$\begin{aligned} X_P^2 + Y_P^2 + Z_P^2 + a_1 X_P + b_1 Y_P + c_1 Z_P + d_1 &= 0 \\ X_P^2 + Y_P^2 + Z_P^2 + a_2 X_P + b_2 Y_P + c_2 Z_P + d_2 &= 0 \\ X_P^2 + Y_P^2 + Z_P^2 + a_3 X_P + b_3 Y_P + c_3 Z_P + d_3 &= 0 \end{aligned} \quad (2.10)$$

or:

$$\begin{aligned} A_1 X_P + B_1 Y_P + C_1 Z_P + D_1 &= 0 \\ A_2 X_P + B_2 Y_P + C_2 Z_P + D_2 &= 0 \end{aligned} \quad (2.11)$$

Where:

$$\begin{aligned} A_1 &= a_1 - a_2 & B_1 &= b_1 - b_2 & C_1 &= c_1 - c_2 & D_1 &= d_1 - d_2 \\ A_2 &= a_1 - a_3 & B_2 &= b_1 - b_3 & C_2 &= c_1 - c_3 & D_2 &= d_1 - d_3 \end{aligned} \quad (2.12)$$

So it becomes a linear system of equations.

$$\begin{cases} X_P = m_1 Z_P + n_1 \\ Y_P = m_2 Z_P + n_2 \end{cases} \quad (2.13)$$

Where:

$$\begin{aligned} m_1 &= \frac{B_2 C_3 - B_3 C_2}{A_2 B_3 - A_3 B_2} & n_1 &= \frac{B_2 D_3 - B_3 D_2}{A_2 B_3 - A_3 B_2} \\ m_2 &= \frac{A_3 C_2 - A_2 C_3}{A_2 B_3 - A_3 B_2} & n_2 &= \frac{A_3 D_2 - A_2 D_3}{A_2 B_3 - A_3 B_2} \end{aligned} \quad (2.14)$$

3 INVERSE KINEMATICS

We'll start off with using the Eq. 2.7 which will help us find θ_i :

$$\begin{aligned} & \left[-2r_i L_i \sin \beta_i \sin \gamma_i - 2r_i L_i \cos \beta_i \cos \gamma_i - 2L_i X_P \cos \gamma_i - 2L_i Y_P \sin \gamma_i + 2R_i L_i \right] \cos \theta_i \\ & + 2L_i Z_P \sin \theta_i + X_P^2 + Y_P^2 + Z_P^2 + L_i^2 - l_i^2 + R_i^2 + r_i^2 - 2R_i r_i \sin \beta_i \sin \gamma_i - 2R_i r_i \cos \beta_i \cos \gamma_i \\ & + 2r_i X_P \cos \beta_i + 2r_i Y_P \sin \beta_i - 2R_i X_P \cos \gamma_i - 2R_i Y_P \sin \gamma_i = 0 \end{aligned} \quad (3.1)$$

or:

$$A_i \cos \theta_i + B_i \sin \theta_i + D_i = 0 \quad (3.2)$$

and using the half angle solution:

$$\theta_i = 2 \arctan \left(\frac{-B_i \pm \sqrt{B_i^2 + A_i^2 - D_i^2}}{D_i - A_i} \right) \quad (3.3)$$

4 REFERENCES

Kinematic Analysis of Delta Parallel Robot: Simulation Study - A. Eltayeb