Project 3 - The MOS Transistor Noise Margins, VTC and Cadence Simulations

Arthur Hsueh 21582168 UBC - ELEC 402

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1 Designing widths of pull-down transistors

This problem asks to design the widths of the pull-down transistors such that $V_{OL} = 0.1$ V. The general method is to equate I_L , the current from the load resistor/transsitor, to I_{DI} , the drain current of the pull-down transistor. Because we are evaluating for the design requirement of V_{OL} , we take the input as $V_{in} = V_{DD}$, and thus the pull-down transistor will always be in the linear regime.

1.1 Calculations

Resistive load inverter

This is the circuit that contains the $10k\Omega$ resistor. We begin by equating currents,

$$I_R = I_D(linear)$$

$$\frac{V_{DD} - V_{OL}}{R_L} = \frac{W_N}{L_N} \mu_N C_{ox} ((V_{DD} - V_T) V_{OL} - \frac{V_{OL}^2}{2})$$

Values can be substituted in, (constants used will be taken from the Useful_Formula.pdf document on canvas)

$$\frac{1.2 - 0.1}{10000} = \frac{W_N}{0.1 * 10^{-7}} * 270 * 1.6 * 10^{-6} * ((1.2 - 0.4) * 0.1 - \frac{0.1^2}{2})$$

Solving for W_N yields

$$W_N = 3.395 * 10^{-8} m = 33.95 nm$$

Saturated-enhancement-load inverter

This is the circuit that contains the pull-up NMOS transistor with 1.2V gate voltage. Here, the pull-up transistor is operating in the satuation regime $(V_{DS} > V_{GS} - V_T)$. Again, we equate curents to solve,

$$I_{Spull-up}(saturation) = I_D(linear)$$

$$\frac{W_L v_{sat} C_{ox} (V_{DD} - V_{OL} - V_{TL})^2}{(V_{DD} - V_{OL} - V_{TL}) + E_C L_L} = \frac{W_N}{L_N} \mu_N C_{ox} ((V_{DD} - V_T) V_{OL} - \frac{V_{OL}^2}{2})$$

Substituting values,

$$\frac{0.1*10^{-5}*8*10^{6}*1.6*10^{-6}(1.2-0.1-0.4)^{2}}{(1.2-0.1-0.4)+6*0.1*10^{-7}} = \frac{W_{N}}{0.1*10^{-7}}*270*1.6*10^{-6}*((1.2-0.4)*0.1-\frac{0.1^{2}}{2})$$

Solving for W_N yields

$$W_N = 2.765 * 10^-9m = 2.765nm$$

'Linear'-load inverter

This is the circuit that contains the pull-up NMOS transistor with 1.6V gate voltage. Here, the pull-up transistor is operating in the linear regime $(V_{DS} < V_{GS} - V_T)$. This calculation allows for cancellation of many terms Again, we equate currents to solve,

$$I_{Spull-up}(linear) = I_D(linear)$$

Cancelling identical terms yields,

$$W_L((V_{gate} - V_{OL} - V_T)V_{OL} - \frac{V_{OL}^2}{2}) = W_N((V_{DD} - V_T)V_{OL} - \frac{V_{OL}^2}{2})$$

Substituting values,

$$0.1*10^{-7}((1.6-0.1-0.4)*0.1-\frac{0.1^2}{2}) = W_N((1.2-0.4)*0.1-\frac{0.1^2}{2})$$

Solving for W_N yields

$$W_N = 1.4 * 10^{-8} = 14nm$$

1.2 Results

The calculated values of W_N are reiterated below, with all values with units of nm.

Table 1: Calculated widths for each of the 3 inverters

We notice that the resistive load inverter requires the largest width, followed by the 'linear' inverter and then the saturated-enhancement inverter.

When we design for V_{OL} we treating the inverter as if it has been inputted logic high and outputs logic low. So, the pull-down transistor is always in the linear region and can be modelled as a small resistor. So, ideally we want the pull-up network to be comparatively much larger in resistance (voltage divider property applies here). In an ideal inverter, we would experience infinite resistance in the pull-up network, and zero resistance in the pull-down network.

If we look at the saturated-enhancement-load inverter, the pull-up NMOS transistor is operating in the saturation region which can be modelled as a current source. The closer we are to an ideal current source, $V_{DS} \ll V_{GS} - V_{T}$ the closer we are to an infinite resistance. For the 'linear'-load inverter the pull-up NMOS is operating exactly on the boundary between linear and saturation.

The effective resistance of the pull-up network will directly affect the width of the pull-down network transistors. We want to adjust the pull-down transistor to match the effective resistance of the pull-up network for a low V_{OL} . A high W_N value means a low resistance, and a low W_N value means a high resistance. The calculated values reflect the relative offset of this property. The saturated inverter needs a high resistance to balance for V_OL , the 'linear' inverter need a slightly lower resistance to balance, and the resistive load inverter has a large resistor to pull-up, so it doesn't need as big of a resistance to pull-down.

2 Determining purpose and VTC of unknown circuit

2.1 Circuit Function and Output Swing

The circuit visually resembles a CMOS inverter, but upon further inspection, the position of the PMSO and NMOS transistors are flipped. The output is now at the source of both transistors. Looking at the truth table of the circuit, we can see the circuit appears to output the same logic values as inputted.

Logic IN	Logic OUT
0	0
1	1

Table 2: Logic table of the unknown circuit

So, the circuit functions as a buffer. Thus, the output swings from a valid low to a valid low, and valid high to a valid high. Upon examination at the voltage level we notice that there are some differences, which will be discussed when the voltage transfer characteristics are plotted in the next section.

2.2 Plotting the VTC

For an input of logic 1, $V_{in} = V_{DD} = V_{GS}$, the pull-up NMOS transistor operates in the saturation region, and the pull-down PMOS is off. Here, the output is taken at the source terminals of the transistors. If we take into account the threshold voltage V_T then we can say the **highest** possible output voltage of this gate will always be $V_{DD} - V_T$.

Likewise, for an input logic 0, $V_{in} = 0$ (theoretically) = V_{GD} , the pull down PMOS transistor operates in the saturation region. Again, taking into account the threshold voltage V_T we can say the **lowest** possible output voltage of this gate will always be V_T .

Thus we have the values for V_{OL} and V_{OH}

$$V_{OL} = and V_{OH} = V_{DD} - V_T$$

Below is a general plot of the VTC for the circuit.

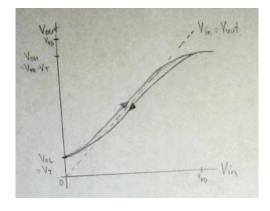


Figure 1: The VTC of the unknown circuit

As the problem states, there is hysteresis in the VTC, because with the way the circuit is set up, when the input is V_{OL} or V_{OH} the output will jump back to a linear operating regime. Looking at the line $V_{in} = V_{out}$, we can see that it intersect the VTC curve at two points, and thus we have two switching voltages. For an input of V_{OL} , the output is expected to be 0 (V_T in reality), and V_{SD} becomes small, which pushing the PMOS back into the linear regime. And likewise for an input of V_{OH} , the output is expected to be V_{DD} , (V_{DD} - V_T in reality), and thus V_{DS} become small, which pushes the NMOS back into the linear regime.

2.3 Gain and Validity of the Circuit

From the VTC plot, we can see that the circuit is not a valid gate. At the low gain areas of the VTC, near the levels of V_{OL} and V_{OH} , it is clear that the gain/slope at those areas are greater than one, which is not what we want. The high gain areas do satisfy a valid gate, but the low gain areas don't. Because of the fact the low gain areas have slopes greater than one, this means that noise is not attenuated, rather amplified.

Another reason this circuit would not function well as a valid gate is because the output voltage level is now narrower, between V_T and $V_{DD} - V_T$. The output will be fed as input to other gates, which ideally would still prefer input ranges of V_{DD} and 0.

2.4 Validation using CAD Tools

Below is the schematic that describes the circuit defined in the problem

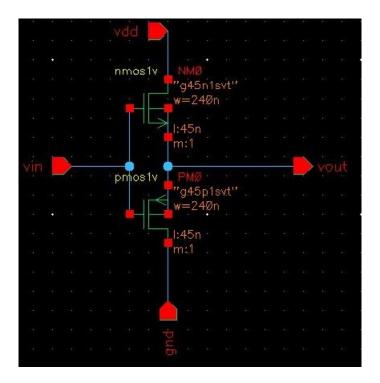


Figure 2: Schematic of the Buffer circuit

The plot is simulated using a V_{DD} value of 6V. Below is VTC plot of the buffer circuit.

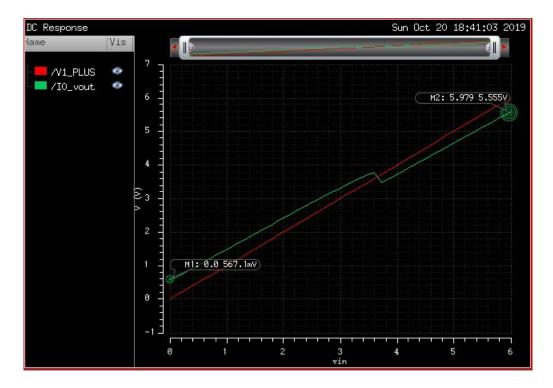


Figure 3: The simulated VTC of the circuit

We can see from the endpoints of the green line, the V_{out} plot that the output will always be between the bound of V_T (about 0.5V in this case), and $V_{DD} - V_T$ (about 5.5 in this case). The hystersis effect was not as exaggerated as I had thought, and this is probably because I forgot to take into account that the overall deviation from an ideal buffer, isn't that great.

3 Finding the Threshold Voltage and Body Bias of an NMOS Transistor

3.1 Finding the Body Bias γ

Using the circuit defined in the problem, we can use the basic properties of the V_{DS} vs I_D curve to find the threshold voltage for any V_{SB} . First we make the schematic for an NMOS in Cadence.

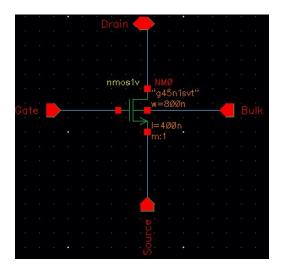


Figure 4: Schematic for L = 400nm NMOS

Then we can make the symbol for the nmos and connect sources and ground just like defined in the problem.

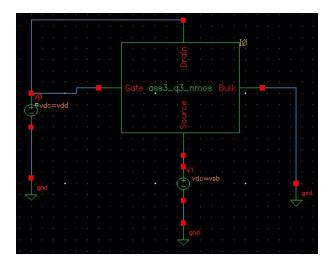


Figure 5: Circuit for L = 400 nm NMOS

We can sweep the gate and drain connected source at any V_{SB} to obtain the the V_{DS} vs I_D plot and get the threshold voltage. For the case of L = 400nm and V_{SB} = 0, the plot is shown

below. The source voltage is swept from 0 to 5V.

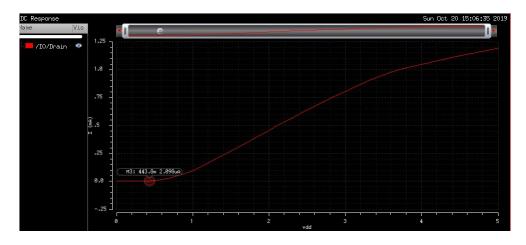


Figure 6: V_{DS} vs I_D plot for L = 400nm NMOS at $V_{SB} = 0$

The vdd value at which the current begins to rise is taken as the threshold voltage. Here, because $V_{SB} = 0$, the vdd value of 443.8mV is V_{T0} . For values where V_{SB} is not equal to zero we must obtain $V_{GS} = V_{TN} = V_G - V_{SB}$ in order to perform correct calculations. The method used to find values of V_{TN} will only be visually shown once to prevent cluttering in the report.

Once enough data points have been obtained, we apply the equation

$$V_{TN} = V_{T0} + \gamma(\sqrt{V_{SB} + |2\phi_F|} - \sqrt{|2\phi_F|})$$

and substitute the obtained values, where $|2\phi_F| = 0.88\text{V}$ as defined in the question. The result is essentially a plot of a linear equation, with the independent variable γ being the slope. For this problem, I will be using 6 data points equally split between $0\text{V} \leq V_{SB} \leq 1.8\text{V}$.

3.1.1 L = 400 nm NMOS

Using the method described above, we obtain the data points shown below. The values are in volts

V_{SB}	V_G	$V_{TN} = V_{GS}$
0	0.4438	0.4438
0.36	0.8560	0.4960
0.72	1.2650	0.5450
1.08	1.6550	0.5750
1.44	2.0440	0.6000
1.80	2.4190	0.6190

Table 3: Voltages obtained from simulation for the L = 400 nm NMOS

Applying the respective values to the equation from before, we obtain the plot to get γ

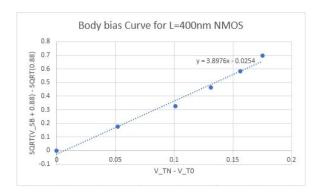


Figure 7: Body Bias plot for L=400nm Transistor

Taking the slope on the plot, get obtain $\gamma = 3.8976$, and $V_{T0} = 0.4438$.

$3.1.2 \quad L = 100 \text{nm NMOS}$

We now change the L of the NMOS to 100nm and apply the same method. The data points are shown in the table below, with values in volts.

V_{SB}	V_G	$V_{TN} = V_{GS}$
0	0.4650	0.4650
0.36	0.8792	0.5192
0.72	1.3320	0.6120
1.08	1.7280	0.6480
1.44	2.1080	0.6680
1.80	2.4580	0.6580

Table 4: Voltages obtained from simulation for the L = 100nm NMOS

Applying the respective values to the equation from before, we obtain the plot to get γ

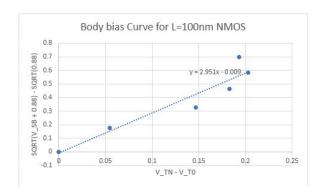


Figure 8: Body Bias plot for L=100nm Transistor

Taking the slope on the plot, get obtain $\gamma = 2.951$, and $V_T 0 = 0.4650$.

We can see that the reducing the value of L for the NMOS transistor creates a slight increase in the threshold voltage for the same source-body bias values. Looking back at the current equations for a transistor, this makes sense as we saw that the current I_d was inversely proportional to the term L_n .

3.1.3 Netlist

The netlist for this problem is attached with the submission of the report, but for direct reading it is included here.

```
// Library name: ELEC402
// Cell name: ass3_q3
// View name: schematic
subckt ass3_q3 Bulk Drain Gate Source
NM0 (Drain Gate Source Bulk) g45n1svt w=(800n) l=100n nf=1 as=112f
ad=112f ps=1.88u pd=1.88u nrd=175m nrs=175m sa=140n sb=140n sd=160n sca=55.42636
scb=0.04134 scc=0.00529 m=(1) ends ass3_q3
// End of subcircuit definition.

// Library name: ELEC402
// Cell name: ass3_q3_tb2
// View name: schematic
I0 (0 V0_PLUS V0_PLUS V1_PLUS) ass3_q3
V1 (V1_PLUS 0) vsource dc=vsb type=dc
V0 (V0_PLUS 0) vsource dc=vdd type=dc
```

3.2 Confirming the value of $|2\phi_F|$

The value ϕ_F is a value that is dependent on the doping of the materials and the temperature. So, the value we are using for $2\phi_F$ is currently assuming the conditions of the material and the environment temperature.

In the case where we are given other parameters of the transistor that define the body-effect coefficient γ , we could use the same method of obtaining V_{GS} , but for only a single V_{SB} .

4 Capacitance of a PMOS transistor

4.1 Computing gate capacitances

The value C_{ox} is used consistently, so it is computed first.

$$C_{ox} = \frac{\epsilon_{ox}}{t_{ox}}$$

We are taking the value ϵ_{ox} as the one shown in lecture $4.2 * \epsilon_0$ for SiO_2 , and $t_{ox} = 4$ nm. So,

$$C_{ox} = \frac{4.2 * 8.854 * 10^{-12}}{4 * 10^{-9}}$$
$$C_{ox} = 9.2967 * 10^{-3} Fm^{-1}$$

We also need to include overlap capacitance.

$$C_{ov} = C_{ox} * L_{diffusion}$$

 $C_{ov} = 9.2967 * 10^{-3} * 22 * 10^{-9}$
 $C_{ov} = 0.2045 \, \text{fF} \mu \text{m}^{-1}$

Worst case gate capacitance

The worst case gate capacitance also includes the overlap capacitances. It is given by

$$C_g = C_{ox} * W * L + 2 * C_{ov}$$

Because we want per unit width capacitance, we ignore the W term an only include L. Substituting in,

$$C_g = 9.2967 * 10^{-3} * 180 * 10^{-9} + 2 * C_{ov}$$

$$C_g = 2.0824 \, \text{fF} \mu \text{m}^{-1}$$

Calculating C_{GS} , C_{GD} and C_{GB}

So, to calculated the 3 quantities, we use the equations, shown in the table below.

	Cutoff	Linear	Saturation
C_{GS}	0	$\frac{1}{2}C_{ox}WL + C_{ov}$	$\frac{2}{3}C_{ox}WL + C_{ov}$
C_{GD}	0	$\frac{1}{2}C_{ox}WL + C_{ov}$	0
C_{GB}	$C_{ox}WL$	0	0

Table 5: Equations used to calculate capacitances

Substituting the repsective values yields the table below, where all values are in fF.

	Cutoff	Linear	Saturation
C_{GS}	0	2.8354	3.08644
C_{GD}	0	2.8354	0
C_{GB}	1.5061	0	0

Table 6: Calculated capacitances for PMOS

4.2 Computing worst case capacitance

To compute worst case capacitance C_j we need to first find base junction capacitance C_{jb} and the built in potential ϕ_B . First we find ϕ_B using the values given, and the n_i value used in the lectures in the equation

$$\phi_B = \frac{kT}{q} \ln \frac{N_A N_D}{n_i^2}$$

Substituting and solving yields

$$\phi_B = 0.9358 \, \text{V}$$

For C_{ib} we use the equation

$$C_{jb} = \sqrt{\frac{\epsilon_{Si}q}{2\phi_B} \frac{N_A N_D}{n_i^2}}$$

Substituting and solving yields

$$C_{jb} = 0.5151 \, \text{fF} \mu \text{m}^{-2}$$

The general equation to solve for the drain junction capacitance is

$$C_{j} = \frac{C_{jb} * (Y + x_{j}) * W}{(1 - \frac{V_{j}}{\phi_{B}})^{m}}$$

where V_j is the base-drain junction voltage and m = 0.5. If we assume the n-well is a rectangular prism, the worst case takes into account the side edges of the well. The worst case junction voltage would be 0V.

$$C_j = C_{jb} * ((Y + x_j) * W + 2 * W * x_j)$$

Substituting known values yields

$$C_{i_{worstcase}} = 0.78804 \, \text{fF}$$

4.3 Computing drain junction capacitance

4.3.1
$$V_D = 1.8V, V_B = 0V$$

Here $V_j = -1.8$ V. Substituting the known values into the previous general equation yields

$$C_j = 0.2982 \, \mathrm{fF}$$

4.3.2
$$V_D = 0V, V_B = 0V$$

Here $V_j = 0$ V. Substituting the known values into the previous general equation yields

$$C_j = 0.5099 \, \text{fF}$$

5 Calcaulting Vs of 2-input NOR gates

The first thing to do is to get the circuit for the NOR gate at the transistor level. We use the method taught in class

- 1. Take the dual of the original function: $F = \overline{A+B}$ becomes $F = \overline{\overline{A+B}} = A+B$.
- 2. Create the NMOS pull-down network: A + B means parallel NMOS.
- 3. Create the PMOS pull-up network: parallel NMOS means series PMOS.
- 4. Combine the two networks: The result is the circuit shown below.

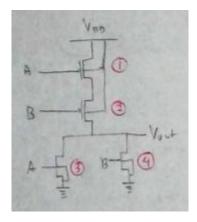


Figure 9: Circuit for a 2-input NOR gate

5.1 Theoretical calculations

For the theoretical calculations, we first need to define the values we are using for calculations (some will also be used for simulation).

- $V_{DD} = 1.8 \text{ V}$, because for simulation, we are using the GPDK45 specs.
- $V_{TN} = |V_{TP}| = 0.4$ V, assuming they are the same type, where values are taken from Useful_Formula.pdf on Canvas.
- $L_N = L_P$, which will cancel out in calculations.
- $E_{CN} = 6 \text{ V} \mu \text{m}^{-1}$ and $E_{CP} = 24 \text{ V} \mu \text{m}^{-1}$, which are are taken from Useful_Formula.pdf on Canvas, but will also notably cancel out.
- $W_N = 6\lambda = 135\,\mathrm{nm}$ and $W_P = 24\lambda = 675\,\mathrm{nm}$, which are defined by the problem and the fact we are using 45nm technology.

For referencing of the transistors in the calculations, each transistor has been numbered in the circuit drawing.

5.1.1 One input switching

For the case of one input switching, we take the input A to be logic 0 and the input B to be the one that switches. To get the value of V_S we simply need to equate currents at the V_{out}

node. Because we are calculating for V_S , the conditions for this calcultion are therefore

$$V_B = V_{out} = V_S$$
 and $V_A = 0$

We notice that PMOS1 and PMOS2 are operating in the saturation, and NMOS4 is also operating in saturation. NMOS3 is operating in the cut-off region. The the currents that matter for this case are the drain currents of PMOS2 and NMOS4.

$$I_{D-nmos4}(saturation) = I_{D-pmos2}(saturation)$$

Using the same equations used in section 1, cancelling identical terms and approximating yields the equation

$$2\chi^{2}(V_{S}-V_{TN})^{2} = (V_{DD}-2V_{TP}-V_{S})^{2}$$
 where $\chi = \sqrt{\frac{\frac{W_{N}}{E_{CN}L_{N}}}{\frac{W_{P}}{E_{CP}L_{P}}}}$

Now we can solve for V_S

$$V_S = \frac{V_{DD} + V_{TN}\chi - 2 * V_{TP}}{\chi + 1}$$

Substituting the values from before yields the value of V_S

$$V_S = 0.7167 \,\text{V}$$

5.1.2 Two inputs tied together

For the case of two inputs being tied together, we take similar conditions to the previous case, except now the input A is also equal to V_S

$$V_A = V_B = V_{out} = V_S$$

Thus PMOS2, NMOS3 and NOMS4 are operating in saturation and PMOS1 is operating in the linear regime. The currents that matter for this case are the drain currents of PMOS4 and the sum of the drain currents of NMOS3 and NMOS4.

$$I_{D-nmos4}(saturation) + I_{D-nmos3}(saturation) = I_{D-pmos2}(saturation)$$

Because the NMOS transistors are the same we can just take 2 drain currents of the NMOS

$$2*I_{D-nmos}(saturation) = I_{N-pmos2}(saturation)$$

Using the same equations used in section 1, cancelling identical terms and approximating yields the equations

$$2\chi^2(V_S - V_{TN})^2 = (\frac{V_{DD} - 3 * V_S}{2} - V_{TP})^2$$
 where $\chi = \sqrt{\frac{\frac{W_N}{E_{CN}L_N}}{\frac{W_P}{E_{CP}L_P}}}$

Now we can solve for V_S

$$V_S = \frac{V_{DD} + V_{TN}\chi * 2\sqrt{2} - 2 * V_{TP}}{2\sqrt{2}\chi + 3}$$

Substituting the values from before yields the value of V_S

$$V_S = 0.36381 \,\mathrm{V}$$

5.2 Simulation Results

Below is the schematic made for the NOR gate.

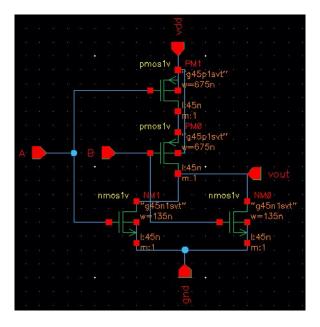


Figure 10: Schematic for the NOR gate

5.2.1 One input switching

Below is the testbench schematic made for the NOR gate with only one input switching.

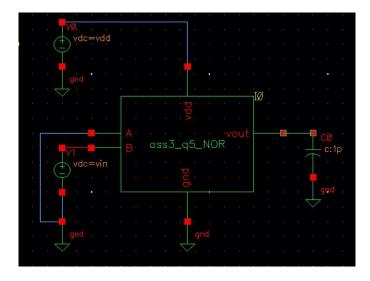


Figure 11: Testbench schematic for the one input switching NOR gate

We can obtain V_S by simulating the VTC of the testbench circuit. The result is shown below.

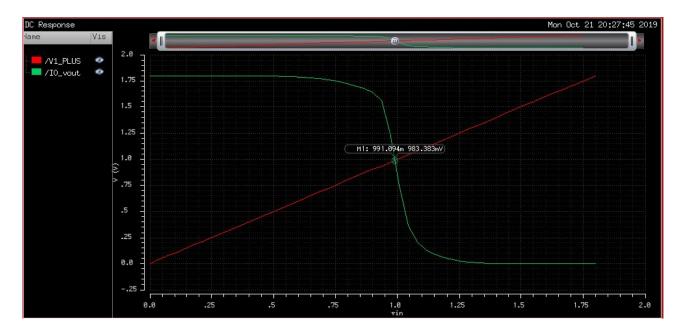


Figure 12: VTC of the one input switching NOR gate

From the plot we can see that V_S is simulated to be at a value of approximately 1 V.

5.2.2 Two inputs tied together

Below is the testbench schematic made for the NOR gate with only both inputs switching.

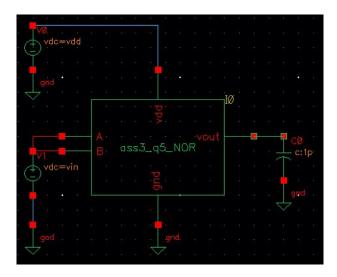


Figure 13: Testbench schematic for the one input switching NOR gate

We can obtain V_S by simulating the VTC of the testbench circuit. The result is shown below.

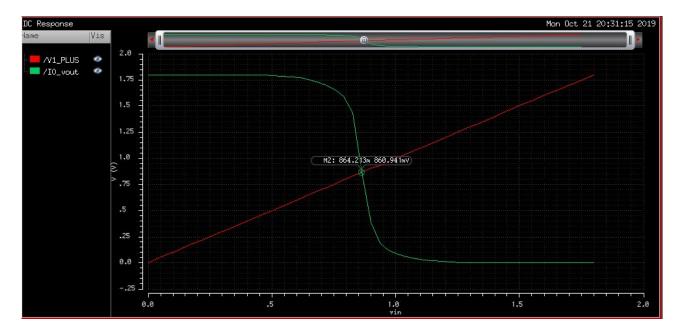


Figure 14: VTC of the one input switching NOR gate

From the plot we can see that V_S is simulated to be at a value of approximately 0.861 V.

5.2.3 Explaining the Discrepancy between theory and simulation

Based on the simulations, we can see that the theoretical value is off the simulated value by approximately 30-40 percent. There are two main sources of error: the calculation values (such as $V_T N$ and $V_T P$) and approximations done in the calculations.

For the calculation values, we used values that were defined separately from this assignment, so they would not be exactly the same as the actual specifications of the transistor. If we look at the threshold values, we saw in Section/Problem 3 threshold voltage values that were not the used value of $0.4 \,\mathrm{V}$, rather somewhat higher. This value plays a large role in the equations derived for V_S and thus may have affected the 'real' value of V_S .

The approximations made in the derivation of the equation for the switching voltage also may have impacted the 'real' value of V_S , although not by much.

6 Noise Margins of a Saturated-enhancement load inverter

Below is a schematic of the circuit itself. Because the GPDK package is defined for 45nm technology, the lowest possible length is 120nm. So instead of 1μ m and 100nm lengths, I am using 120nm and 1.2μ m. Below is the schematic for the circuit.

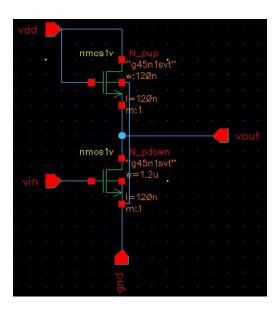


Figure 15: Schematic for the saturated-enhancment load inverter

For the testbench, the typical components vdc, and cap are used. The value of the capcitors were specially chosen to be $2 \,\mathrm{fF} \mu\mathrm{m}^{-1}$. The input is set to sweep from values of 0 and V_{DD} . The testbench schematic is shown below

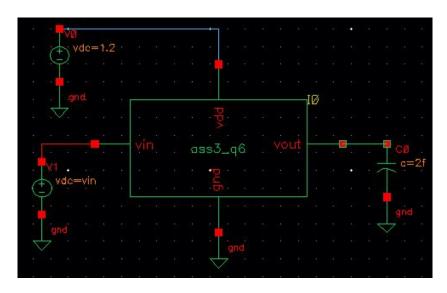


Figure 16: Testbench schematic for the saturated-enhancment load inverter

Running the simulation, the resulting VTC plot is shown below. We also take the derivative of the output to find V_{IL} and V_{IH} where the slope is equal to -1.

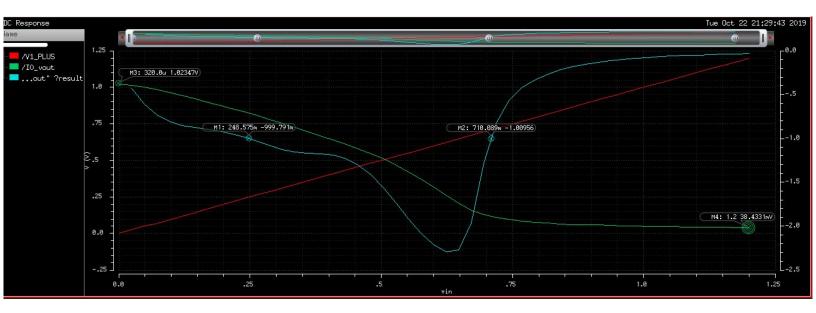


Figure 17: VTC of the saturated-enhancement load inverter

The values important for calculating noise margin are V_{IL} , V_{IH} , V_{OL} and V_{OH} , and are noted by the selected points in the waveform. The values are not too clear in the image, so for clarity they are shown in the table below, with units in volts.

$$\begin{array}{c|cccc} V_{IL} & V_{IH} & V_{OL} & V_{OH} \\ \hline 0.24858 & 0.71008 & 0.03843 & 1.0236 \end{array}$$

Table 7: Noise margin voltages from the waveform

We use the following equations to calculte for noise margins.

$$NM_L = V_{IL} - V_{OL}$$
 and $NM_H = V_{OH} - V_{IH}$

Substituting the values in the table above will yield the noise margin values

$$NM_L = 210.15 \,\text{mV}$$
 and $NM_H = 313.52 \,\text{mV}$

We can attribute the large high noise margin NM_H due to the large width of the pull-down NMOS transistor (10 * L). As we learned in class, the saturated-enhancement load inverter is a ratioed inverter, meaning the performance of the inverter is dependent on a ratio of specifications. For this inverter, this ratio is dependent on the gate widths and lengths of both transistors.