

# CS174A : Introduction to Computer Graphics

Royce 190  
TT 4-6pm

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# Curves

- Parametric – cubic blending functions
  - There is a slightly different way of looking at this interpolation process.
    - It allows us to see what exactly is going on.
  - Lets substitute those interpolating coefficients into the polynomial itself – generalize things a bit.

$$\mathbf{p}(u) = \mathbf{u}^T \mathbf{c} = \mathbf{u}^T \mathbf{M}_I \mathbf{p}, \text{ or } \mathbf{p}(u) = \mathbf{b}(u)^T \mathbf{p}, \text{ where } \mathbf{b}(u) = \mathbf{M}_I^T \mathbf{u}$$

$$\mathbf{b}(u) = \begin{bmatrix} b_0(u) \\ b_1(u) \\ b_2(u) \\ b_3(u) \end{bmatrix}$$

# Curves

- Parametric – cubic blending functions
  - If we express  $\mathbf{p}(u)$  in terms of these cubic blending polynomials we get

$$\mathbf{p}(u) = b_0(u)\mathbf{p}_0 + b_1(u)\mathbf{p}_1 + b_2(u)\mathbf{p}_2 + b_3(u)\mathbf{p}_3$$

$$b_0(u) = -\frac{9}{2}\left(u - \frac{1}{3}\right)\left(u - \frac{2}{3}\right)(u - 1),$$

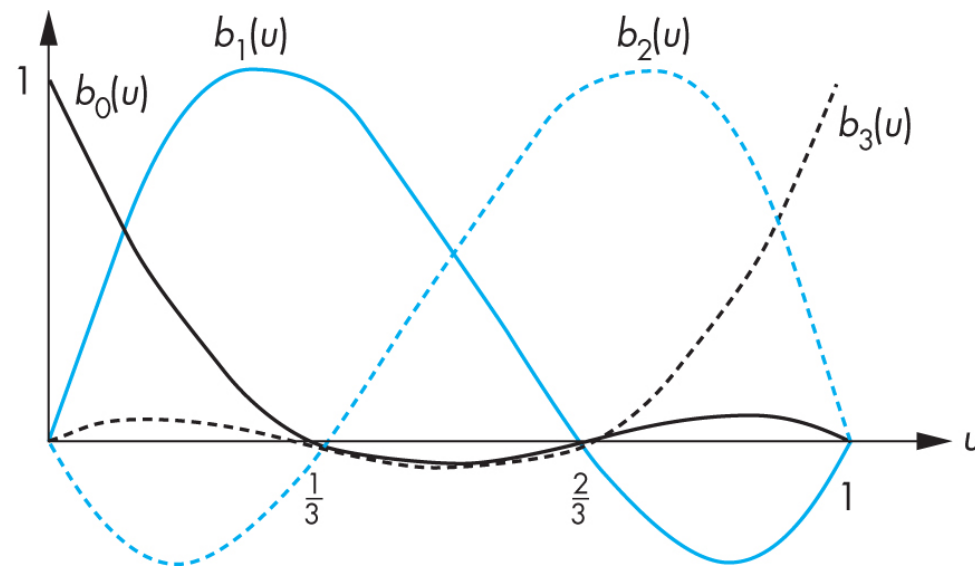
$$b_1(u) = -\frac{27}{2}u\left(u - \frac{2}{3}\right)(u - 1),$$

$$b_2(u) = -\frac{27}{2}u\left(u - \frac{1}{3}\right)(u - 1),$$

$$b_3(u) = \frac{9}{2}u\left(u - \frac{1}{3}\right)\left(u - \frac{2}{3}\right).$$

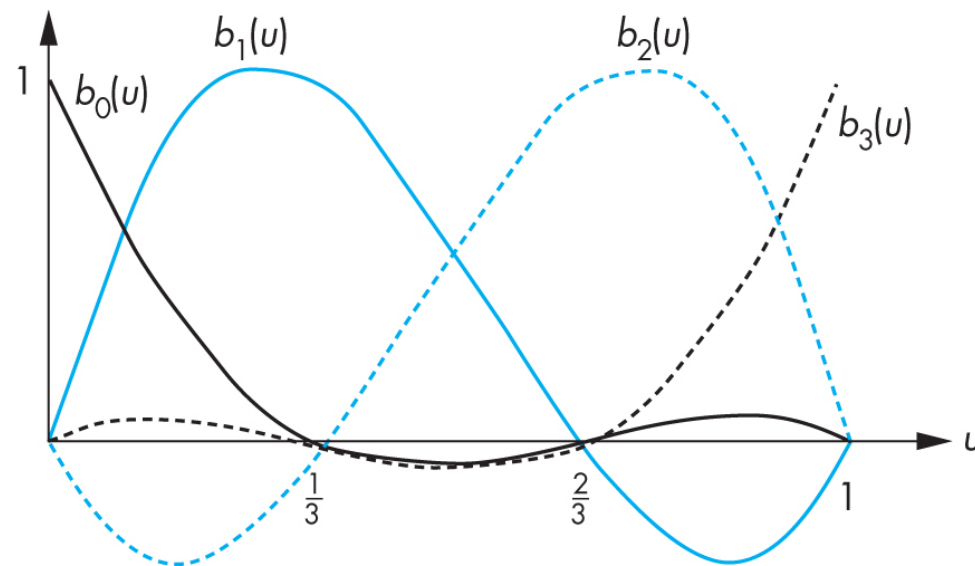
# Curves

- Parametric – cubic blending functions
  - Which lets you see how each of the blending equations factors into the interpolation.
    - What we want to see



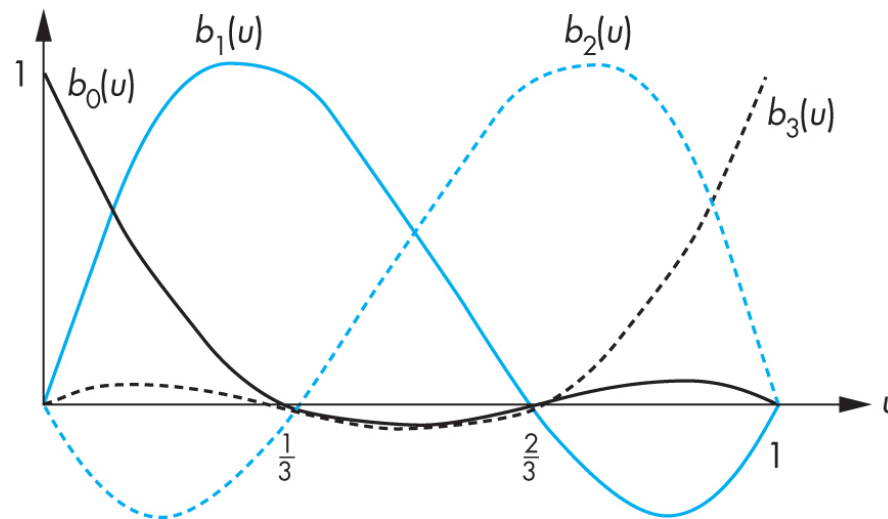
# Curves

- Parametric – cubic blending functions
  - You can see how each is not particularly smooth
    - This is because we are insisting the interpolation pass through each of the control points.



# Curves

- Parametric – cubic blending functions
  - Higher degree polynomials would have even more pronounced swings.
  - Recall, there is also no way to enforce derivatives at the endpoints makes this form of limited use.



# Curves

- Parametric – Hermite form
  - While able to form a curve (or surface) using the cubic interpolating polynomial, it has some issues.
  - Let's look at the Hermite form which allows some additional control over the derivatives at the ends of the curve.
  - Here we only consider the control points  $\mathbf{p}_0$  and  $\mathbf{p}_3$ , which from our previous example we have the first two conditions

$$\mathbf{p}_0 = \mathbf{p}(0) = \mathbf{c}_0,$$

$$\mathbf{p}_3 = \mathbf{p}(1) = \mathbf{c}_0 + \mathbf{c}_1 + \mathbf{c}_2 + \mathbf{c}_3.$$

# Curves

- Parametric – Hermite form
  - We can get the other two conditions if we assume the derivatives at  $u=0$  and  $u=1$  are known.

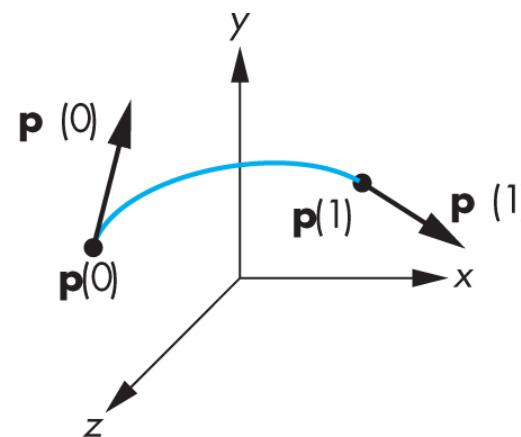
$$\mathbf{p}'(u) = \mathbf{c}_1 + 2u\mathbf{c}_2 + 3u^2\mathbf{c}_3.$$

$$\mathbf{p}'_0 = \mathbf{p}'(0) = \mathbf{c}_1,$$

$$\mathbf{p}'_3 = \mathbf{p}'(1) = \mathbf{c}_1 + 2\mathbf{c}_2 + 3\mathbf{c}_3.$$

– In matrix form

$$\mathbf{q} = \begin{bmatrix} \mathbf{p}_0 \\ \mathbf{p}_3 \\ \mathbf{p}'_0 \\ \mathbf{p}'_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 1 & 1 & 1 & 1 \\ 0 & 1 & 0 & 0 \\ 0 & 1 & 2 & 3 \end{bmatrix} \mathbf{c}.$$





# Curves

- Parametric – Hermite form
  - Once again, solving for  $\mathbf{c}$  we get

$\mathbf{c} = \mathbf{M}_H \mathbf{q}$ , where

$$\mathbf{M}_H = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ -3 & 3 & -2 & -1 \\ 2 & -2 & 1 & 1 \end{bmatrix}.$$

- $\mathbf{M}_H$  is the Hermite geometry matrix

# Curves

- Parametric – Hermite form
  - Once again we get the resulting polynomials

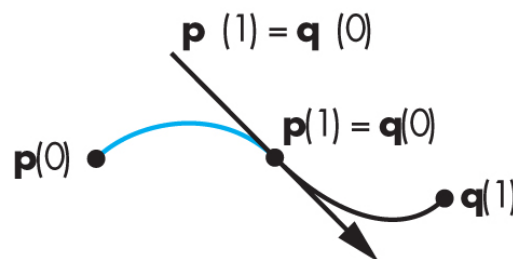
$$\mathbf{p}(u) = \mathbf{u}^T \mathbf{c} = \mathbf{u}^T \mathbf{M}_H \mathbf{q}, \text{ or } \mathbf{p}(u) = \mathbf{b}(u)^T \mathbf{q}, \text{ where } \mathbf{b}(u) = \mathbf{M}_H^T \mathbf{u}$$

$$\mathbf{b}(u) = \begin{bmatrix} 2u^3 - 3u^2 + 1 \\ -2u^3 + 3u^2 \\ u^3 - 2u^2 + u \\ u^3 - u^2 \end{bmatrix}$$

- The blending functions can be used in the same way as before for the cubic interpolating polynomial.

# Curves

- Parametric – Hermite form
  - Here, if we hold the derivative to be the same across curve segments, at the join, we get continuity.



- Curves connecting at their endpoints have  $C^0$  parametric continuity.
- If the derivatives also match we call that  $C^1$  parametric continuity – like above figure.
- If the derivatives are only proportional to each other we call this  $G^1$  geometric continuity.

# Curves

- Parametric – Bézier form
  - Cannot really compare cubic interpolating polynomial to Hermite.
    - Both are cubic in degree
    - But, they do not use the same data (control points)
  - We can use all **four** control points of the cubic interpolating polynomial to approximate the Hermite curve – this is called the Bézier form.
    - Probably heard of this one, named after Pierre Bézier who worked for Renault in France in the 1960's

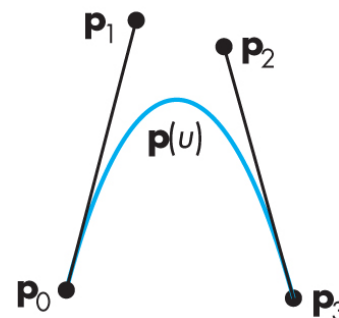
# Curves

- Parametric – Bézier form
  - We, again, use endpoints  $\mathbf{p}_0$  and  $\mathbf{p}_3$  and insist that our interpolation pass through these values.

$$\mathbf{p}_0 = \mathbf{p}(0) = \mathbf{c}_0,$$

$$\mathbf{p}_3 = \mathbf{p}(1) = \mathbf{c}_0 + \mathbf{c}_1 + \mathbf{c}_2 + \mathbf{c}_3.$$

- Bézier, instead of using  $\mathbf{p}_1$  and  $\mathbf{p}_2$  for interpolation instead used them to approximate the tangents at  $u=0$  and  $u=1$ .



# Curves

- Parametric – Bézier form
  - Approximating the tangent results in the following conditions.

$$\mathbf{p}'(0) \approx \frac{\mathbf{p}_1 - \mathbf{p}_0}{\frac{1}{3}} = 3(\mathbf{p}_1 - \mathbf{p}_0),$$

$$\mathbf{p}'(1) \approx \frac{\mathbf{p}_3 - \mathbf{p}_2}{\frac{1}{3}} = 3(\mathbf{p}_3 - \mathbf{p}_2).$$

gives

$$\mathbf{p}_0 = \mathbf{c}_0,$$

$$3\mathbf{p}_1 - 3\mathbf{p}_0 = \mathbf{c}_1,$$

$$3\mathbf{p}_3 - 3\mathbf{p}_2 = \mathbf{c}_1 + 2\mathbf{c}_2 + 3\mathbf{c}_3,$$

$$\mathbf{p}_3 = \mathbf{c}_0 + \mathbf{c}_1 + \mathbf{c}_2 + \mathbf{c}_3.$$

# Curves

- Parametric – Bézier form
  - Once again, we have four equations and four unknowns.
  - Solving for  $\mathbf{c}$

$$\mathbf{c} = \mathbf{M}_B \mathbf{p}$$

where

$$\mathbf{M}_B = \begin{bmatrix} 1 & 0 & 0 & 0 \\ -3 & -3 & 0 & 0 \\ 3 & -6 & 3 & 0 \\ -1 & 3 & -3 & 1 \end{bmatrix}$$

- $\mathbf{M}_B$  is the Bézier geometry matrix.

# Curves

- Parametric – Bézier form

- The cubic polynomial is then

$$\mathbf{p}(u) = \mathbf{u}^T \mathbf{M}_B \mathbf{p}.$$

- Which is used in exactly the same manner as the cubic interpolating polynomial we saw earlier.
    - If the control points are overlapped you should see that we still have  $C^0$  continuity at the join.
    - We do not have  $C^1$  continuity like with Hermite because there are different approximations for the tangent.



# Curves

- Parametric – Bézier form
  - However, there are some useful benefits to this form.
  - Let's look at the blending functions

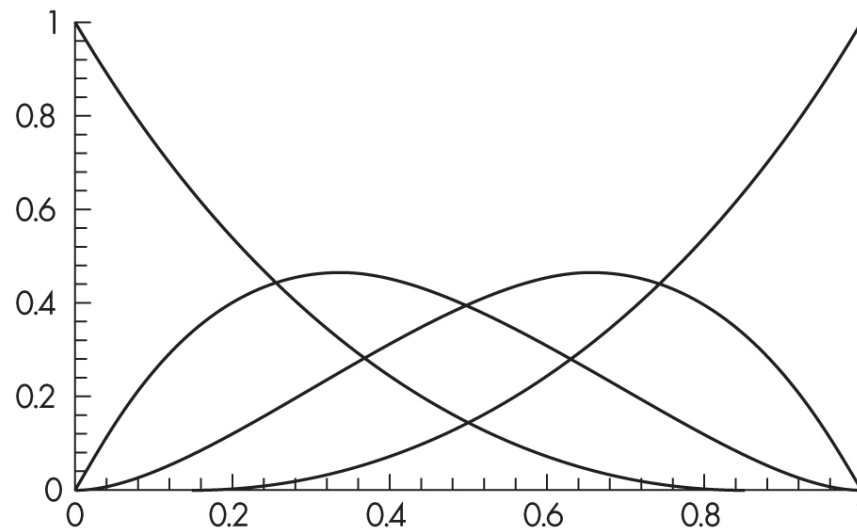
$$\mathbf{p}(u) = \mathbf{b}(u)^T \mathbf{p},$$

where

$$\mathbf{b}(u) = \mathbf{M}_B^T \mathbf{u} = \begin{bmatrix} (1-u)^3 \\ 3u(1-u)^2 \\ 3u^2(1-u) \\ u^3 \end{bmatrix}.$$

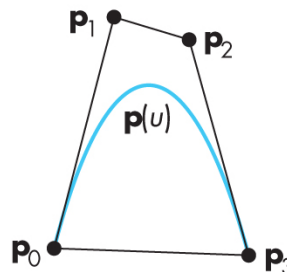
# Curves

- Parametric – Bézier form



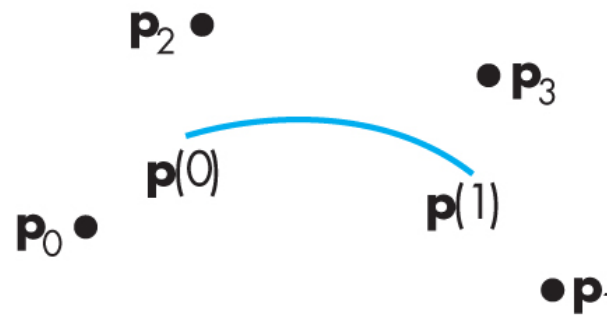
# Curves

- Parametric – Bézier form
  - Zero values are only at the ends of the interval
    - Ensures a smooth interpolation over the interval  $[0,1]$
  - We also see that while  $0 < u < 1$ ,
    - the blending functions are also  $b(u) < 1$
    - This condition is called a *convex sum*.
    - Which implies that the curve will be contained within the *convex hull* of the control points.
    - Useful in interactive design of curves and surfaces.



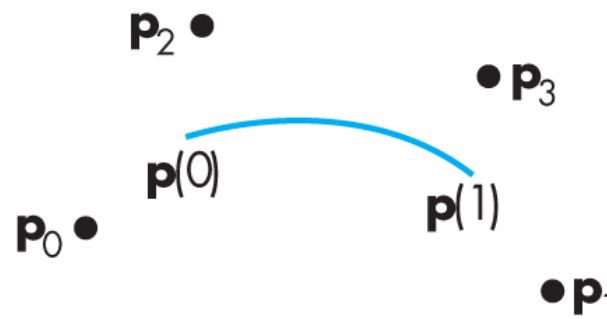
# Curves

- Parametric – Cubic B-Splines
  - Bezier curves – only achieve  $C^0$  continuity, mathematically speaking.
  - Can achieve  $C^1$  by matching the tangents.
  - If we relax the condition that interpolation must pass through the control points we can achieve  $C^2$  continuity using a cubic B-spline.



# Curves

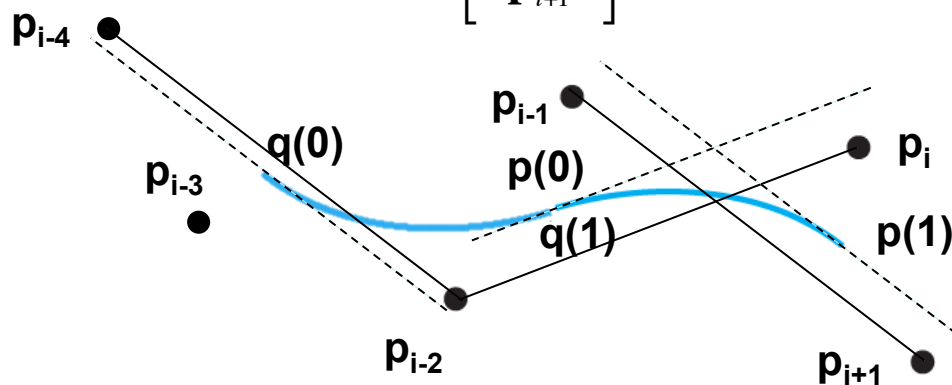
- Parametric – Cubic B-Splines
  - Previously, as we varied  $u$  from 0 to 1 the curve spanned over all four control points.
  - Consider, instead, spanning over only the middle two control points.



# Curves

- Parametric – Cubic B-Splines
  - By matching conditions at  $p(0)$  with  $q(1)$  we can achieve  $C^2$  continuity by solving for  $M$ .

$$p(u) = u^T M p, \text{ where } p = \begin{bmatrix} p_{i-2} \\ p_{i-1} \\ p_i \\ p_{i+1} \end{bmatrix}, \text{ and } q(u) = u^T M q, \text{ where } q = \begin{bmatrix} p_{i-3} \\ p_{i-2} \\ p_{i-1} \\ p_i \end{bmatrix}.$$

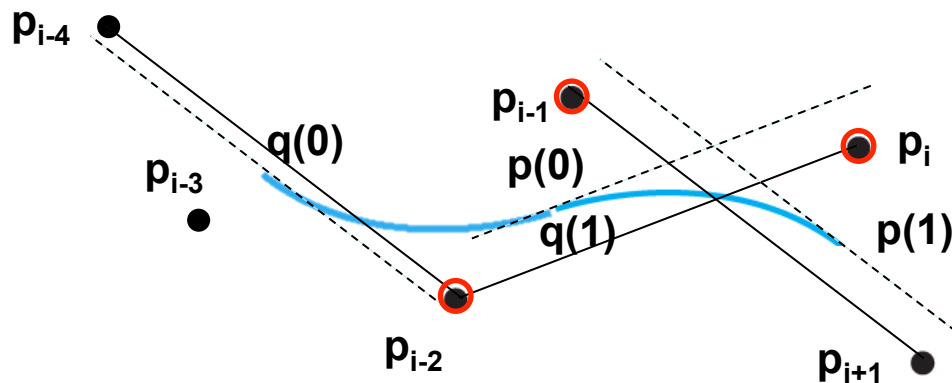


# Curves

- Parametric – Cubic B-Splines
  - We again use symmetric approximations for the tangent at the joint point to get

$$\mathbf{p}(0) = \mathbf{q}(1) = \frac{1}{6}(\mathbf{p}_{i-2} + 4\mathbf{p}_{i-1} + \mathbf{p}_i) = \mathbf{c}_0,$$

$$\mathbf{p}'(0) = \mathbf{q}'(1) = \frac{1}{2}(\mathbf{p}_i - \mathbf{p}_{i-2}) = \mathbf{c}_1.$$

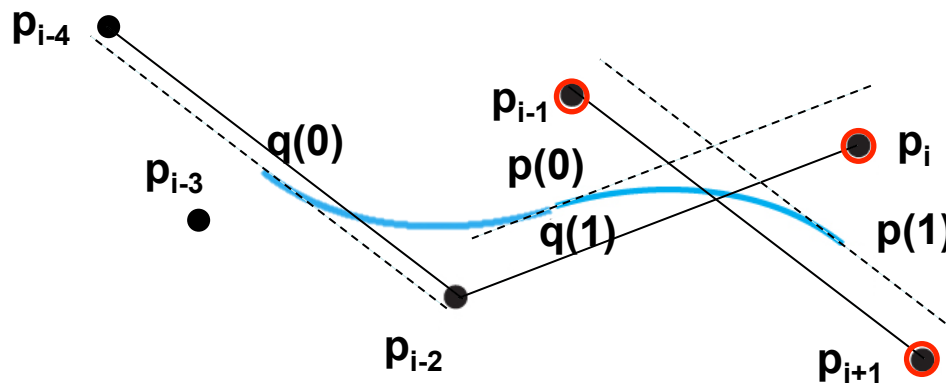


# Curves

- Parametric – Cubic B-Splines
  - Applying the same conditions at  $p(1)$ 
    - We basically just slide down to the next set of control points.

$$p(1) = \frac{1}{6}(p_{i-1} + 4p_i + p_{i+1}) = c_0 + c_1 + c_2 + c_3,$$

$$p'(1) = \frac{1}{2}(p_{i+1} - p_{i-1}) = c_1 + 2c_2 + 3c_3.$$





# Curves

- Parametric – Cubic B-Splines
  - We now have four equations for the coefficients of  $\mathbf{c}$ .
  - Allowing us to solve for  $\mathbf{M}$
  - Really,  $\mathbf{M}_S$ , the B-spline geometry matrix, which is

$$\mathbf{M}_S = \frac{1}{6} \begin{bmatrix} 1 & 4 & 1 & 0 \\ -3 & 0 & 3 & 0 \\ 3 & -6 & 3 & 0 \\ -1 & 3 & -3 & 1 \end{bmatrix}$$

# Curves

- Parametric – Cubic B-Splines
  - We now have  $C^2$  continuity at the joins but at a cost of three times as much work.
    - Have to interpolate between each set of control points.
  - $C^2$  continuity not only connects the segments
    - It matches the tangents
    - It also matches the curvature
    - Very useful properties when modeling real world materials
    - Difficult to use as the *curve does not pass through any of the control points*
      - » Not intuitive