

Syllabus

- (i) Introduction to comm. system
- (ii) Random signals
- (iii) Distribution and density function
- (iv) Analog communication
- (v) Radio Transmission \rightarrow (Propagation, P.M.F.)
- (vi) Transmission lines
- (vii) Noise

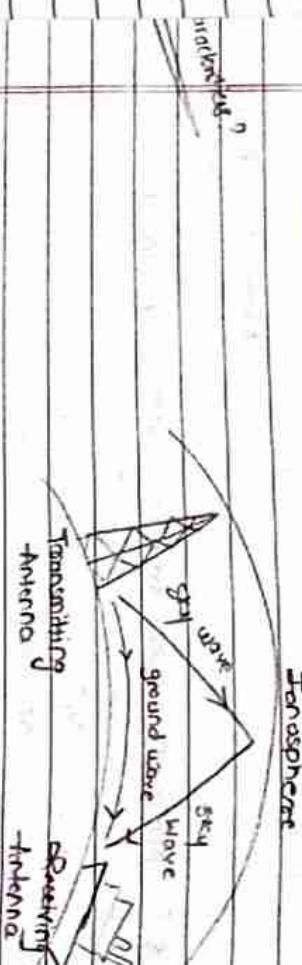
Modes of propagation of wireless communication

> Modes of propagation basically 4 types

1. Ground or source wave propagation upto 2 MHz. EMF induced in the receiver antenna

$$E = \frac{120 \pi h_4 h_5 I_s}{\lambda_d} \text{ V/m}$$

- E/L , where, L is the length of antenna



- Relation of radiated power & received Power by antennas:-
- > Fundamental equation for free space wave propagation
- > Two antennas are placed at some distance in free space as shown in Fig two anten
- Critical frequency

Critical Frequency is the frequency in which above the waves penetrates the ionosphere and below which the waves are reflected back on the earth from the ionosphere.

$$\omega_c = \frac{\sin \theta}{\lambda r} = \sqrt{f - \frac{8 \ln N}{f^2}}$$

$f = f_c$ when $\omega_c = 0$ then $N = N_{\max}$

f_c is MHz per cubic meter. N is electron density.

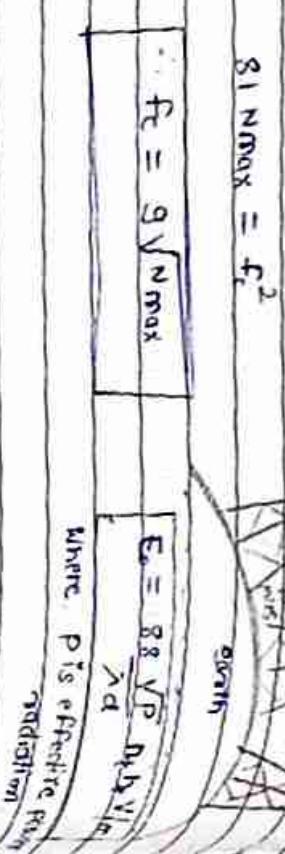
$$w = 0 = \sqrt{1 - g_1 N_{\text{max}} / f_c^2}$$

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$$0 = 1 - g_1 N_{\text{max}} / f_c^2$$

$$g_1 N_{\text{max}} = f_c^2$$

$$g_1 N_{\text{max}} = f_c^2$$



* Maximum Usable Frequency (MUF) $f = f_{\text{muf}}$

$$M = \sin i = \sqrt{1 - g_1 N_m}$$

$$\sin(90^\circ) = \sqrt{f_{\text{muf}}}$$

$$\sin i = \sqrt{1 - g_1 N_m}$$

$$\sin^2 i = \sqrt{1 - \frac{f_c^2}{f_{\text{muf}}^2}}, \quad \sin^2 o = 1 - \frac{f_c^2}{f_{\text{muf}}^2}$$

Terrestrial Microwave Transmission -

$$1 - \sin^2 i = \frac{f_c^2}{f_{\text{muf}}^2}$$

$$\cos^2 o = f_c^2$$

$$-f_{\text{muf}}^2$$

$$-f_c^2 = \cos^2 o (f_{\text{muf}}^2) - f_{\text{muf}}^2 = f_c \sin i$$

These waves are sent b/w 2 microwave stations on the earth (earth station).

- It is the most common form of long-distance communication.
- It requires few repeaters.
- Parabolic dish is used to focused narrow beam.
- $1-10$ GHz frequency.
- It is a line of sight of propagation means transmitter must be visible to the receiver.

Satellite microwave transmission
• It involves space-based stations and a satellite
• It involves earth-based stations
• It involves earth-based stations and a satellite

* Uplink transmission of signal from earth station to satellite

* Downlink transmission of signal from satellite to another earth station

* Satellite sends the signal to another earth station
called uplink and uses a higher frequency.
Satellite receives the signal from another earth station
called downlink and uses a lower frequency.

Space Wave (line of sight) Propagation

* It also called as microwave propagation.

* In space wave propagation,

• High speed transmission is there
• ii) microwaves frequency range 1 GHz to 300 GHz.

* microwave transmission is of two types
• microwave transmission & satellite transmissions

• terrestrial & satellite transmissions

$$P_o = \frac{8\pi}{\lambda d} \frac{P}{n_d} \text{ mW/m}^2$$

where, P is effective Power.


1.2

line of sight distance is d .

$$d(\text{straight}) = 3.57 [\sqrt{h_1} + \sqrt{h_2}] \text{ km}$$

Antenna

i) Transmitting antenna



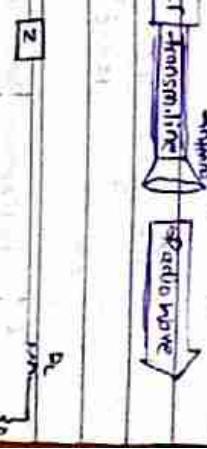
ii) Receiving antenna



- Line of sight distance increases after refraction
- Line of sight distance $d = 4.12 [\sqrt{h_1} + \sqrt{h_2}] \text{ km}$
- Satellite communication coverage area is more and having higher bandwidth for use, as compared to terrestrial communication
- Satellite communication is costly i.e. launching of satellites into geosynchronous orbit is costly
- Satellite communication having larger propagation delay as compared to the terrestrial communication.
- Atmospheric attenuation due to air & water
- Bad signal received at receiver during rain & fog
- Microwave signals transmitted using line of sight principle, therefore, the satellite signal reaches only some part of the earth.

- Source is an ideal source generator
- Transmission line having characterised impedance Z_0

$$\boxed{\text{where } Z_0 = (R_L + R_s) + jX_0}$$



where, R_s - Radiation resistance (Ω)
 X_0 - Characteristic impedance
 R_L - Load resistance
 j - Imaginary component of antenna impedance

R_s - is ohmic losses, ideally $R_s = 0$

2 - internal impedance of source used to interface b/w the line and the antenna, it is integrated in such a way that, the max. power is delivered from source to the antenna.

$$\boxed{Z_0 = R_s + jX_0}$$

$$\boxed{N_0 = N_t - N_c}$$

At resonance

$$\frac{V_A}{V_R} = 0 \quad |Z_R| = R$$

- length of Antenna

$$\lambda = \frac{c}{f} = \frac{300,000,000 \text{ meters}}{3 \times 10^6 \text{ MHz}} \text{ or } \lambda = 300 \text{ meters}$$

Vertical Antennas

$$J = \frac{\lambda}{4} = \frac{75}{4} \text{ meters} = 75 \text{ m}, \text{ if } f = 15 \text{ MHz}$$

Fundamental relation of EM wave for radiation:

Differentiating the above equation w.r.t. time, radiation

$$-charges place \frac{dI}{dt} = q \times \frac{dv}{dt}$$

Horizontal Antennas

Single Wire transmission

- a) If a charge is not moving, no current, no radiation is there.

$$J = \frac{\lambda}{2} = \frac{150 \text{ meters}}{2} = 0.01 \text{ m}, \text{ if } f = 15 \text{ GHz}$$

$$15 \times 10^3 \text{ m} \times 3 \times 10^8 \text{ m/s} = 15 \times 10^3 \text{ Hz}$$

- b) If charge is moving with uniform velocity:

- i) There is no acceleration or deceleration (dc current) and no radiation if the wire is straight and indefinite in extent.

- ii) Radiation takes place if the charges are accelerated and decelerated by making different provisions such as wire is curved, bent, discontinuous, terminated,

RADIATION MECHANISM

Mechanism of radiating energy as electromagnetic waves.

Antennae emits waves generated and detached from

Electromagnetic waves are generated and detached from antenna when it is connected to the source.

Single wire radiation

In conducting wires current flows when it is connected to the source.

Free radiation.

$$J = \frac{charge \times velocity}{dt}$$



If charge is oscillating in a time motion (ac current) it radiates even if the wire is straight.

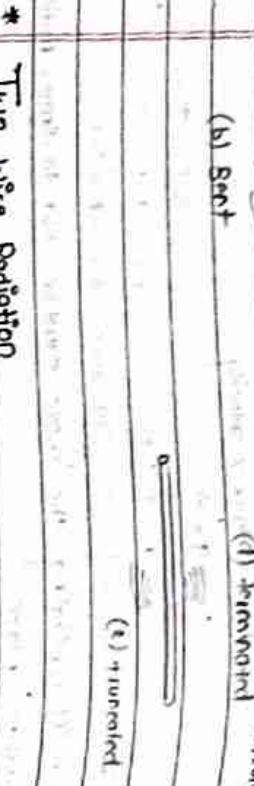
- Transmission lines (circuit) is in resonance maximum radiation takes place.



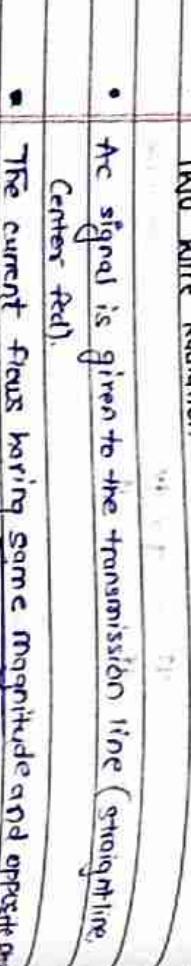
(c) discontinuous



100



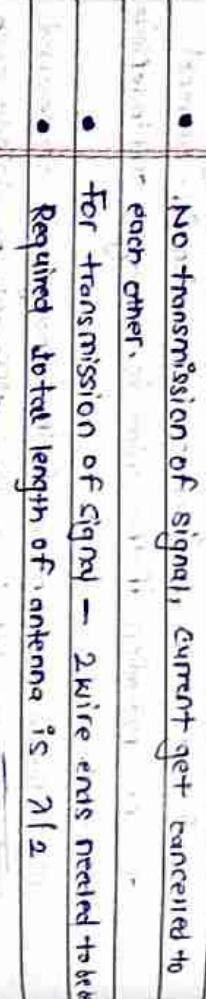
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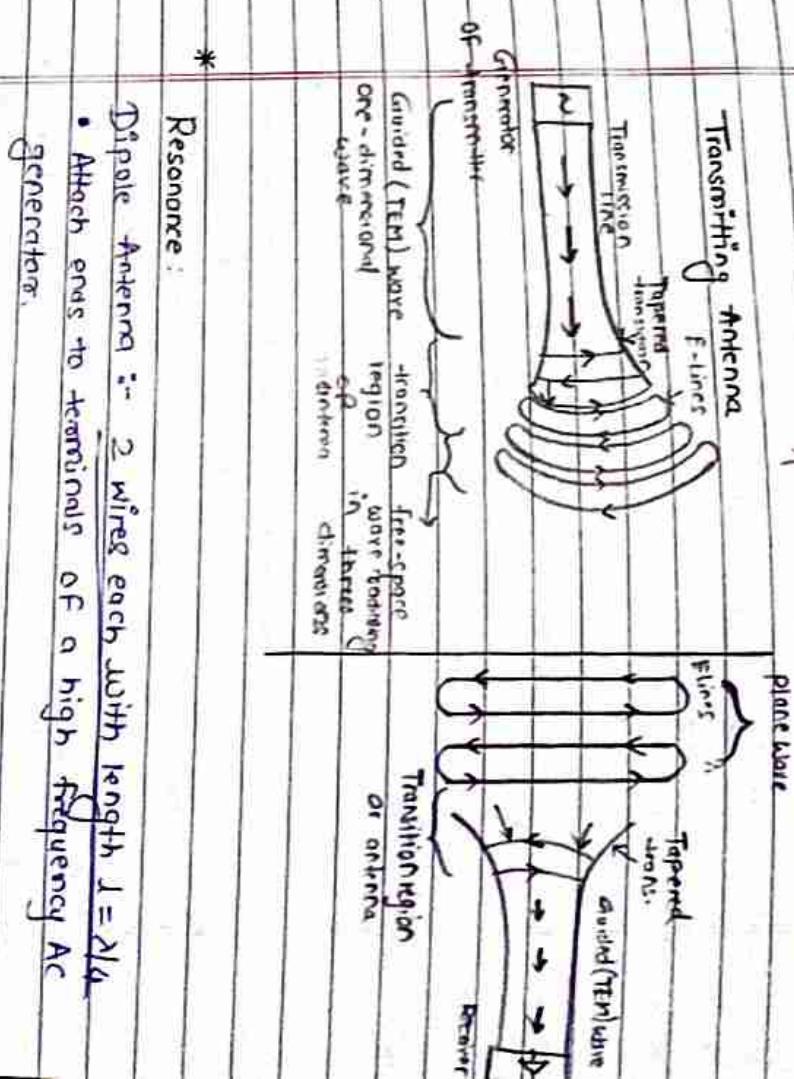
The current flows having some magnitude and opposite signal is given to the transmission line (straight line). Center fed).



125



Required total length of antenna is $\frac{\lambda}{2}$



Receiving Antenna



Radiation Mechanism

Radiation in Dipole: Dipole means separation of charges from molecule in dielectric medium. Distance between poles is $d \ll \lambda$



- first stage (pulse applied to the dipole)
 - AC signal (pulses) are moving outward to the end. Then charges are moving outward due to the end. The electric field lines form the end. The charges expand like a soap bubble with velocity $v = c$ in free space
 - (a) electric field line or wave front with charges at end of dipole move out as charges go in

Second stage (middle)

- The charges are reflected (bounce back)
 - The charges move towards the generator (due to force of attraction)
 - (b) At charges pass the midpoint the field lines cut twice

Third stage:

- The next negative pulse is given again
 - charges moves with velocity of $v = c$ but in opposite direction and reaches to the end



Fourth stage:

- At the same time electric field lines between the charges expand and are reflected from the end and bounces back again due to force of attraction

charges are neutralizing at the center.

When no charges on the poles electromagnetic waves are detached from the dipole.

Radiated waves in free space



Normalized Antenna Power Pattern

Radiation intensity (W/m^2)

$$P_r = \eta_r r^2$$

$$\rho = \frac{\eta_r}{4\pi}$$

Gain

Gain is calculated in two ways

Gain w.r.t isotropic antenna - Power gain

Gain w.r.t test antenna - Directive gain

Power gain

$\text{Gain (dg)} = \frac{\text{Maximum intensity of test antenna}}{\text{Intensity of isotropic antenna (reference)}}$

Directive gain (directive (D))

$\text{Gain (dg)} = \frac{\text{Max. Intensity of test antenna}}{\text{Average intensity of the same antenna}}$

Fundamental Parameters of Antenna

Fundamental parameters of antennas

> Different parameters (Generated - Wt.),

Transmitter power (W_T),

Attenuation loss (W_L):

Total radiated power (W_R):

$$\text{W}_R = \text{W}_T + \text{W}_L$$

$$\text{Power density (W)}$$

$$P_r = \frac{\text{W}_R}{4\pi r^2}$$

$$\text{W}_A = \int \int P_r \, ds$$

Attenuation loss $\text{W}_L = 0$

$$ds = r^2 \sin\theta d\theta d\phi$$

Efficiency of antenna

$$\eta = \frac{G_P}{G_d}$$

When $\eta = 100\%$, or $K=1$ means lossless antenna at that time $G_P = G_d$

Antenna Efficiency

$$\eta = \frac{W_r}{W_r + W_L}$$

$W_r \rightarrow$ total radiated power
 $W_L \rightarrow$ ohmic loss power

Antenna bandwidth

$$\Delta\omega = \omega_2 - \omega_1 = \omega_r = \text{band width}$$

$$2\pi\Delta F = 2\pi f_r$$

$$\Delta f = \frac{f_r}{Q}$$

f_r = centre or resonant or designed frequency

$$Q = \frac{\text{Total energy stored by Antenna}}{\text{energy dissipated or radiated per cycle}}$$

Polarization

It is the direction of electric field intensity of least one electromagnetic waves during the passage of full cycle

Types of polarization

- 1) Linear polarization
- 2) Circular polarization
- 3) Elliptical polarization

Effective Aperture :

$$A_e = \frac{W_{\text{received}}}{P_r} = \frac{\text{Power received per unit area}}{\text{Power density}}$$

Antenna Temperature :

$$T_a = \frac{SA_e}{K} \quad , \quad S \text{ is Power received per unit bandwidth}$$

$$K = \text{Boltzmann's constant} = 1.98 \times 10^{-23} \text{ J/K}$$

Effective length (λ_e)

Active length through that the antenna radiates energy

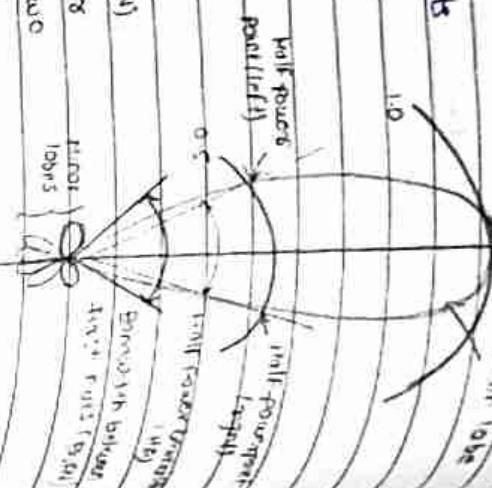
$$\lambda_e = \frac{V_{\text{rms}}}{E_{\text{rms}}} \text{ m or wavelength}$$

Antenna Beam - Width

Half - Power beam width

half power beam width is

the angle between the half-power (-3dB) points of the main lobe.



First-null beam width

(FNBW)

first null beam width (FNBW) is defined as the angular difference between the two nulls enclosing the main beam.

Bandwidth generally expressed in terms of centre frequency

$$B.W. \cdot \% = \frac{\text{operating range}}{\text{centre frequency}} \times 100$$

Q. Suppose antenna operates b/w min. freq. 45 MHz to max. frequency of 100 MHz then band width is

Determine the bandwidth in terms of :

$$\Rightarrow B.W. \% = \frac{8 \text{ MHz} \times 100}{102 \text{ MHz}} = 7.84\%$$

operating range of antenna $\Rightarrow 100 - 45 = 55 \text{ MHz}$

$$\text{centre frequency} = \frac{100 + 45}{2} = \frac{145}{2} = 72.5 \text{ MHz}$$

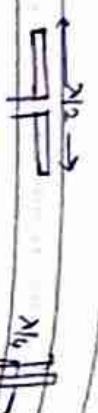
$$\therefore \text{Bandwidth} = \frac{\text{operating range}}{\text{centre freq.}} \times 100$$

$$= \frac{55}{72.5} \times 100$$

$\therefore 7.84\%$

Types of antennas

Wire Antenna



wire antennas are

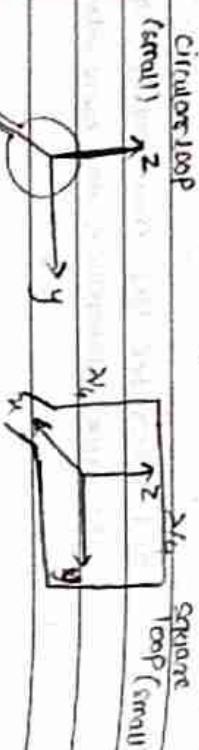
seen everywhere - on

automobiles, buildings, ships,

aircrafts, and so on.

loop antennas are of various shapes -

circular, rectangle, square, ellipse, etc



Aperture Antennas

- Used for aircraft and spacecraft applications

- Covered with a dielectric material to protect them from hazardous conditions of the environment (rapid change)

Antenna Arrays

- It gives directional property, to receive the signal from long distance transmitting antennas.

- It needs multiple antenna elements to achieve this goal.

- Arrange the antenna elements, to get maximum radiation in a particular direction and minimum in other directions.

Reflector Antennas

- for longer distance communication reflector antenna is used

- large dimensions are needed to achieve the high gain.

Micro Strip Antennas :

- If consist of a metallic patch on a grounded substrate with different configurations (rectangular and circular patches)
- Now a day these antennas are used for government and commercial applications.
- It is mechanically robust - mounted on rigid surfaces.
- It is very flexible in terms of resonant frequency and polarization pattern.

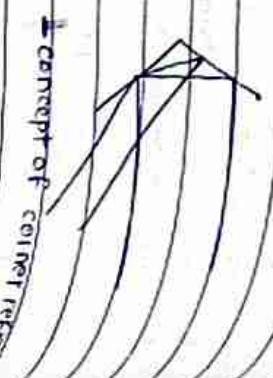
- Used in aircraft, spacecraft, satellites, cars and mobile telephones.

to transmit or to receive the signals after miles

- Another form of reflector is corner reflector, used in radar, radio astronomy, and for microwave communication.



- parabolic reflector

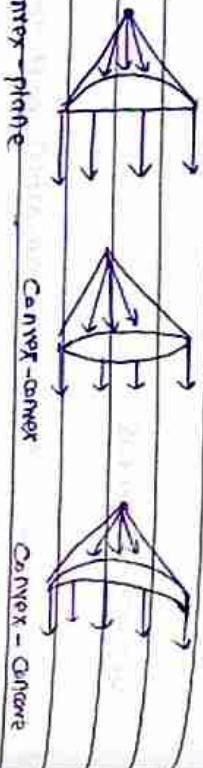


length of receiving antenna,

$$l = \frac{\lambda}{4} = \frac{0.33}{4} = 0.0833 \text{ m} = 8.33 \text{ cm}$$

Lens Antennas

- It is used for higher frequency signal communications
- It avoid energy distribution spreading in undesired directions by different lenses
- Incident diverged energy converted into plane wave front by this lens antenna.



- (a) lens antenna with index of refraction n_1

Ex: A mobile is located 5 km away from a base station, and uses a vertical $\lambda/4$ monopole antenna with gain of 3.5 dB to receive cellular radio signal. The carrier frequency used is 900 MHz. Find the length of the antenna.

$$f = \frac{c}{\lambda} \Rightarrow \frac{9 \times 10^8}{900 \times 10^6} = 0.33 \text{ m}$$

* Basics of satellite *

- service type of satellites
 - > Fixed Service Satellite (FSS)
 - > Broadcast Service Satellite (BSS)
- EX : Point to Point communication
- EX : Satellite television / Radio

- > Mobile Service Satellite (MSS)
 - > Satellite phones

- Convex-plane Convex-concave Convex-concave

* Types of satellites

- Satellite orbits
 - GEO (geostationary earth orbit)
 - LEO (low earth orbit)
 - MEO (medium earth orbit)
 - Molniya orbit
 - HAPS (high altitude platform)



Relation b/w watts and dBm

$$P(\text{dBm}) = 10 \log_{10} [P(\text{W})]$$

$$P(\text{dB}) = 10 \log_{10} [P(\text{W})]$$

$$V(\text{dB}) = 20 \log_{10} [V(\text{Volts})]$$

P(W)	P(dBm)	V(V)	P(dB)
100	20	100	20
10	10	10	10
1	0	1	0
10^{-1}	-10	10^{-1}	-10
10^{-2}	-20	10^{-2}	-20
10^{-6}	-60	10^{-6}	-60

- Frequency Bands
- Different kinds of satellites use different frequency bands
- L > L-band : 1 to 2 GHz, used by MSS (Mobile Service Sat)
- S > S-Band : 2 to 3 GHz, used by MSS, NASA, deep space sat
- C > C-band : 4 to 8 GHz, used by FSS (Fixed Satellite Service)
- X > X-Band : 8 to 10.5 GHz, used by FSS and in terrain imaging, ex. military and meteorological satellite
- Ku > Ku-Band : 12.5 to 18 GHz, used by FSS and BS (Broadband Satellite Service) (DBS - direct broadcast satellite)
- K > K-band : 18 to 26.5 GHz, used by FSS and BS
- Ka > Ka-Band : 26.5 to 40 GHz, used by FSS

Q. A mobile is located 6km away from a base station, and uses a vertical $\lambda/4$ monopole antenna with a gain of 3dB to receive cellular radio signals. The carrier frequency used is 800 MHz. Find the length of the antenna.

Given, $f = 800 \text{ MHz}$

$$\lambda = \frac{c}{f} = \frac{3 \times 10^8}{800 \times 10^6} = 0.375 \text{ m}$$

length of antenna ; $L = \lambda/4 = 0.375/4 = 0.09375 \text{ m}$

4

$$L = 0.09375 \text{ m}$$

Analog Communication:

- Amplitude Modulation
- Types of amplitude modulation.
- Modulation index.
- Power relation in AM.
- Current relation in AM.
- AM Transmitter.
- Angle modulation & its types
- Relationship between FM and PM

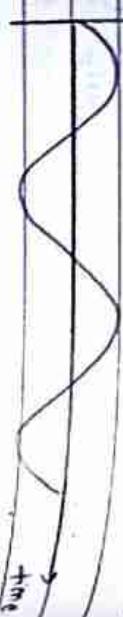
Analog Communication :- Periodic Analog Signals

Periodic analog signals can be in three

- Simple form or
- Composite form

- A simple periodic signal is sine wave
- A composite periodic signal is composed of multiple sinusoidal waves and decomposed into numbers of sine waves

Sine wave:-

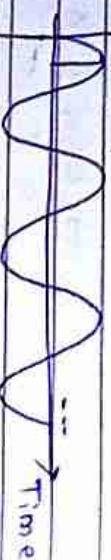


period $\frac{1}{12}$

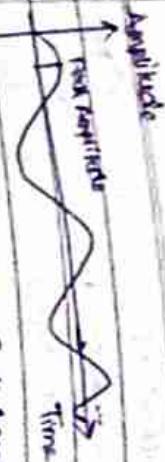
6 periods in 1 s \rightarrow frequency 6 Hz

- Draw : Two signals with the same phase and frequency but different amplitudes.

Amplitude \uparrow peak amplitude

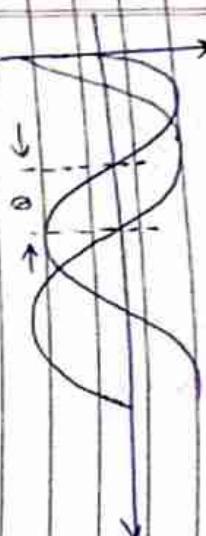


- of a signal with high peak amplitude



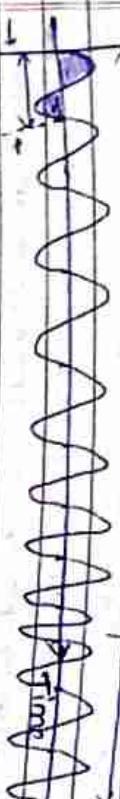
b) A signal with low peak amplitude

- * Draw - different phase, same frequency & amplitudes.



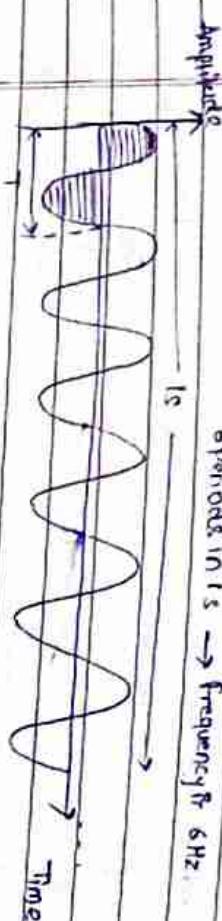
c) Two signals with the same amplitude and phase, but different frequencies

Amplitude \uparrow period \downarrow \rightarrow Frequency is 12 Hz



period $\frac{1}{12}$

6 periods in 1 s \rightarrow frequency 6 Hz



Period: $\frac{1}{6}\text{ s}$

- b) A signal with frequency of 6 Hz .



frequency domain

- Ex :- A sine wave is offset of $\frac{1}{4}$ cycle with respect to time 0. What is its phase in degrees and radians? And draw the nature of signal in time domain.



Soln we know that 1 complete cycle is 360° , therefore $\frac{1}{4}$ cycle is 90° .

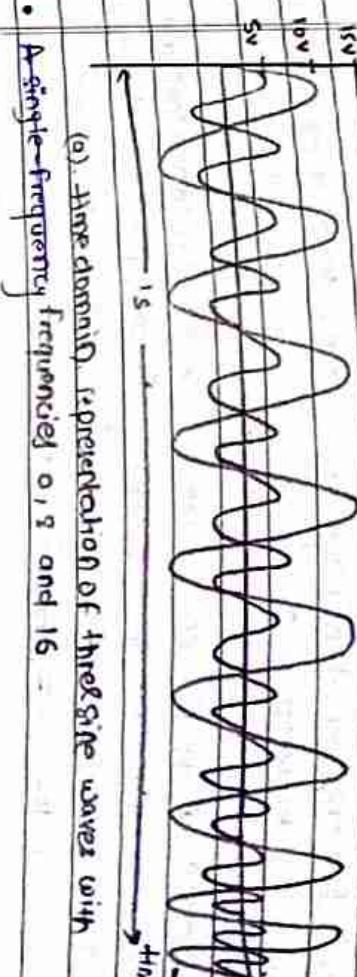
$$\frac{1}{4} \times 360 = 90$$



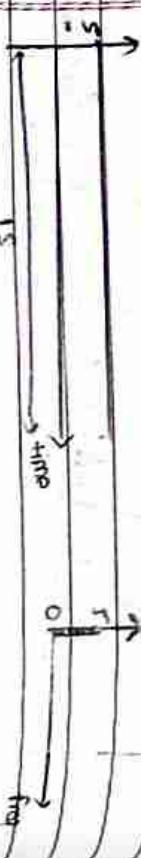
$$\begin{aligned} &= 60 \text{ rad} \\ &\approx 60 \times \frac{\pi}{180} \text{ rad} \\ &= \frac{\pi}{3} \text{ rad} \quad \approx 1.047 \text{ rad} \end{aligned}$$

Signals in frequency domain

- A complete sine wave in time domain for 1 second represented by a one single spike in the frequency domain.
- Draw the Nature of signal, 8Hz frequency with $\frac{1}{4}$ amplitude



- (a) Time domain representation of three sine waves with a single-frequency frequencies 0, 8 and 16.



- Q. draw the 8Hz frequency signal in time and frequency domain



- (b) Frequency-domain representation of the three signals

- A single-frequency sine wave is not useful in communication systems we need to send a composite signal,

i.e. a signal is made by many simple sine waves.

- If signal is composite, then it is having bandwidth.
- The bandwidth of a composite signal is the difference between the highest and the lowest frequency in that composite signal.

* Frequency Calculation :

Ex: The period of signal is 100ms. What is its frequency in kilohertz?

→ first we change 100ms to seconds, and then we calculate the frequency from the period ($f = \frac{1}{T}$)

$$100 \text{ ms} = 100 \times 10^{-3} \text{ s} = 10^{-2} \text{ s}$$

$$f = \frac{1}{T} = \frac{1}{10^{-2}} \text{ Hz} = 10 \text{ Hz} = 10 \times 10^{-3} \text{ kHz} = 0.01 \text{ kHz}$$

Can send through line ?

$$\Rightarrow 112,000 \text{ bps}$$

$$\text{then for } 8 \text{ kHz} \rightarrow$$

bandwidth is 4 kHz → 51200 bps

Bandwidth -

Capacity of the system

In networking, bandwidth measured by 2 ways → 42.2 Gbps
Higher bandwidth gives higher data rate.

* Bandwidth in Hertz

- It is the range of frequencies that a channel can pass.

* Bandwidth in bit per second

- It is the speed of bit transmission in channel or link.

Ex: The bandwidth of a subscriber line is 4 kHz for voice or data. The bandwidth of this line for data transmission can be up to 56,000 bps using a sophisticated modem to change the digital signal to analog. If the telephone company improves the quality of the line and increases the bandwidth to 6 kHz, how much bps

$$\text{then for } 8 \text{ kHz} \rightarrow$$

$$\frac{56,000}{4} = 14,000$$

Propagation time and transmission time

$$\text{Propagation time} = \frac{\text{distance travelled}}{\text{Propagation Speed}}$$

$$\text{Transmission time} = \frac{\text{Message length}}{\text{Bandwidth of Network}}$$

- Ex - What are the propagation time and transmission time for a 2.5-Mbyte message (an e-mail) if the bandwidth of the network is 1 Gbps? Assume that the distance between the sender and the receiver is 12,000 km and travels at the speed of 2.4×10^8 m/s.

Soln - The propagation and transmission time :-

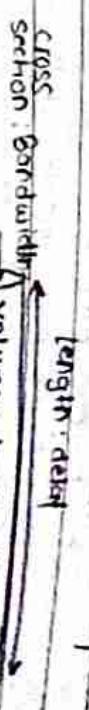
$$\text{Propagation time} = \frac{12,000 \times 10^3}{2.4 \times 10^8} = \frac{120 \times 10^6}{2.4 \times 10^8} = \frac{6 \times 10^3}{24 \times 10^6} = \frac{1}{20} = 50 \text{ ms}$$

$$\text{Transmission time} = \frac{2500 \times 8}{10^9} = 0.020 \text{ ms}$$

- The message is short and the bandwidth is high, that's why the dominant factor is the propagation time, transmission time can be ignored.

Bandwidth delay product

• Think about : Link of starting and end point of elbow hollow pipe. The cross section of pipe represents the bandwidth. Length of the pipe represents the delay. Then the volume of the pipe defines the bandwidth-delay product



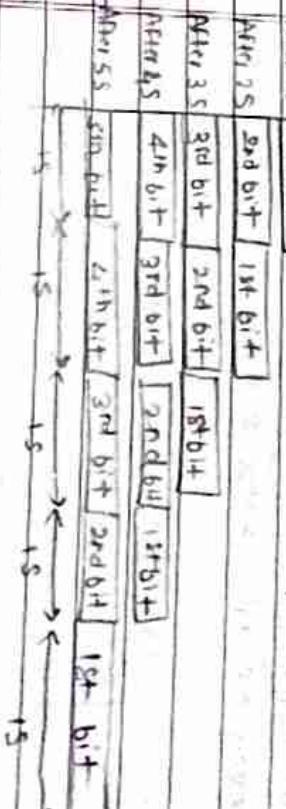
Ex - Bandwidth 1 Gbps, delay = 5 s, draw the representation of transmission of signal from sender to receiver.

Sender

$$\text{Bandwidth: } 1 \text{ Gbps}$$

Delay: 5 s

Receiver

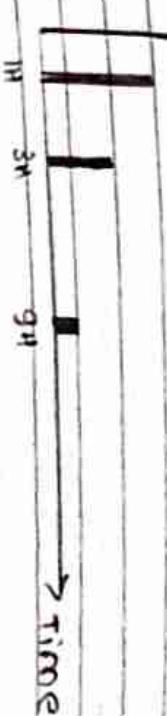


Ex - Bandwidth is 5 bps & delay is 5 s, draw the representation of transmission of signal from sender to receiver

Composite signal

- > periodic
- > non-periodic

Amplitude



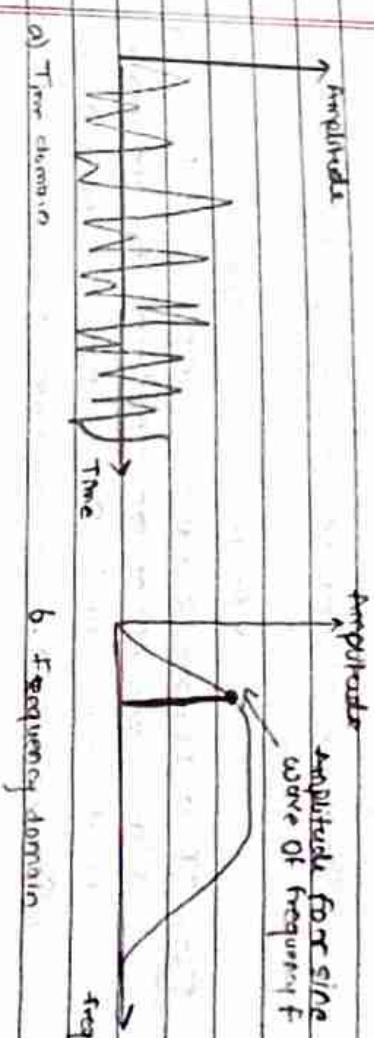
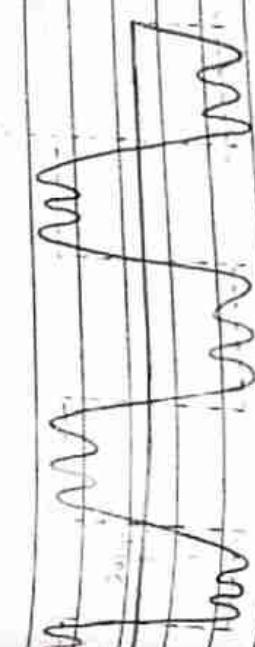
frequency-domain decomposition of the composite signal

- If the composite signal is non periodic, the decomposition gives a series of signals with continuous frequencies
- If the composite signal is periodic, the decomposition gives a series of signals with discrete frequencies

A non periodic composite signal : Ex : Signal created by a microphone or a telephone set, when a word or too is pronounced Generates non periodic composite signal.

The time and frequency domains of a non-periodic signal.

Fig. Shows a periodic composite signal with frequency of center three cosine systems, each with a different frequency of 1Hz, 3Hz & 9Hz



a) Time domain

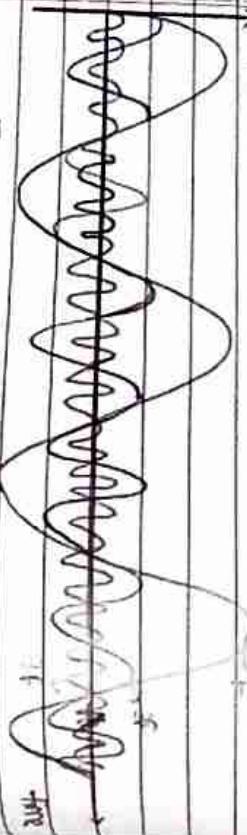
b) Frequency domain

Decompose the composite period signal in the time and frequency

* Bandwidth and signal frequency

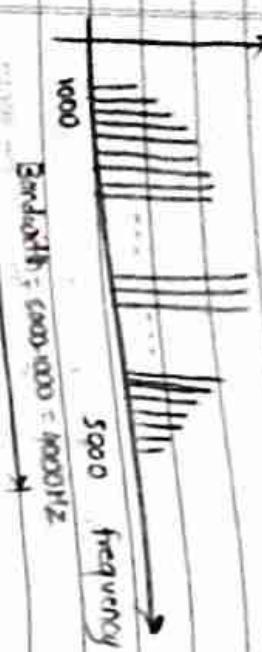
Amplitude

- The bandwidth of a composite signal is the difference between the highest and the lowest frequencies contained in the signal



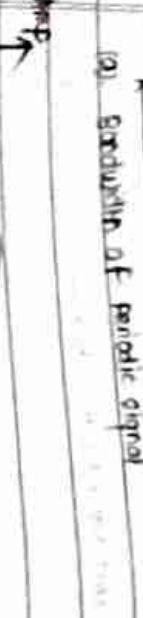
- Time domain decomposition of a composite signal

Amp



- (a) Bandwidth of periodic signal

Amp



- Bandwidth = $600 - 1000 = 400\text{Hz}$

bandwidth = $600 - 400 = 200\text{Hz}$

bandwidth = $600 - 400 = 200\text{Hz}$

- (b) Bandwidth of non-periodic signal

- The bandwidth of periodic and non-periodic component signals

Ex: A non periodic composite signal has a bandwidth of 200Hz .

With a middle frequency of 140 kHz and peak amplitude of 60V . The two extreme frequencies have an amplitude of 0V .

Draw the frequency domain of the signal.

Sol) The lowest frequency must be at 40 kHz and the highest at 240 kHz

Amplitude



Ex: If a periodic signal is decomposed into five sine waves with frequencies of $100, 300, 500, 700$ and 900 Hz , what is its bandwidth? Draw the spectrum, assuming all components have a maximum amplitude of 10 V .

Sol) Let f_h be the highest frequency, f_l the lowest frequency, and B the bandwidth. Then

The spectrum has only five spikes, at $100, 300, 500, 700, 900\text{ Hz}$.

The bandwidth

$$B = f_h - f_l = 900 - 100 = 800\text{Hz}$$

Energy and Power for Continuous-time signal

$x(t)$ is a signal and it is a function of time.

$x(t)$ is said to be an **energy signal** if the total energy transmitted is finite.

$$\text{The signal Energy} E \text{ in the signal } x(t) \text{ is } E = \int_{-\infty}^{\infty} |x(t)|^2 dt$$

finite duration

The signal power in the signal $x(t)$ is

$$P = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T}^{T} |x(t)|^2 dt \quad \text{Infinite duration}$$

If $0 < E < \infty$, then the signal $x(t)$ is called an **energy signal**.

If $0 < P < \infty$, then the signal is called an **Power signal**.

Note that :-

The power for an energy signal is zero ($P=0$)
 & the energy for a power signal is infinite ($E=\infty$)

- * for power signal the power of signal is finite
 i.e. $0 < P < \infty$, then $E \rightarrow \infty$ $P = \frac{E}{T \rightarrow \infty}$
- * A signal is NENP if both energy and power of the signal is infinite

$$P = \frac{1}{T} \int_{-T}^{T} |x(t)|^2 dt$$

$$P = \frac{dE}{dt} \quad \text{area of } |x(t)|^2 dt$$

$$E = \lim_{T \rightarrow \infty} \int_{-T/2}^{T/2} |x(t)|^2 dt, \quad E = \int_{-\infty}^{\infty} |x(t)|^2 dt$$

$$P = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} |x(t)|^2 dt$$

Energy & power signal

> Finite duration signal is always energy signal with zero power.

> Infinite duration decreasing amplitude signal is also energy signal.

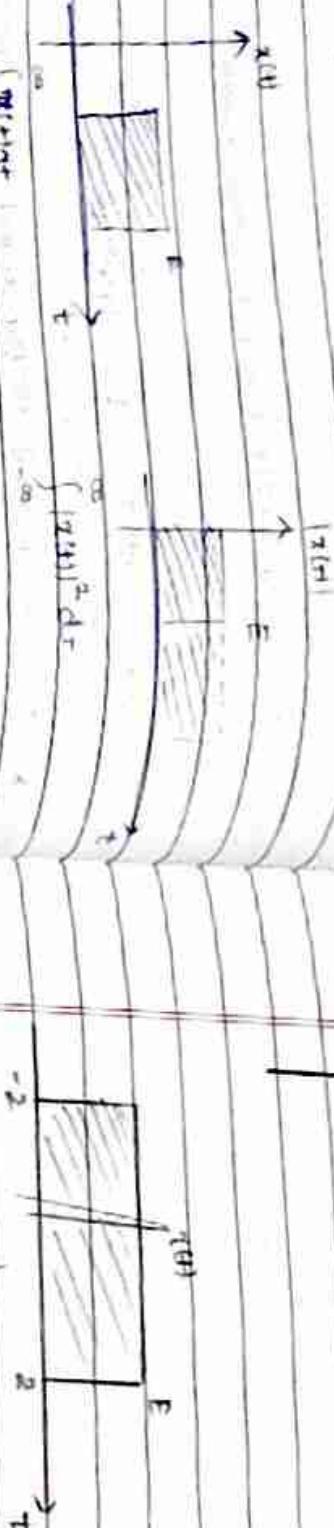
- > Infinite duration decreasing amplitude signal is also power signal.
- > Infinite duration signal is power signal with infinite energy.
- > Any infinite amplitude signal is NEMP signal.



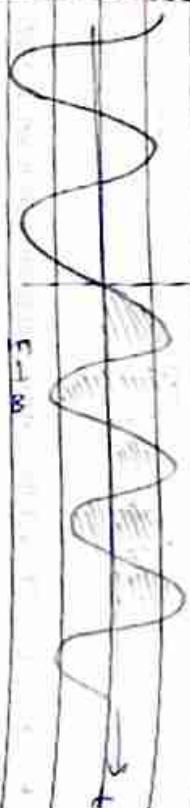
NEMP



NEUT



E



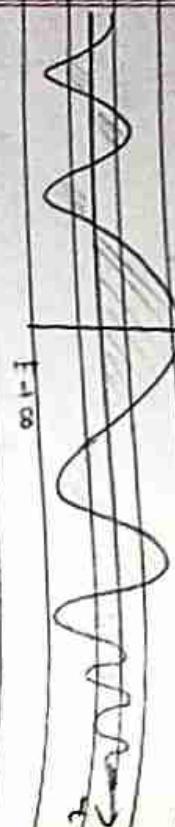
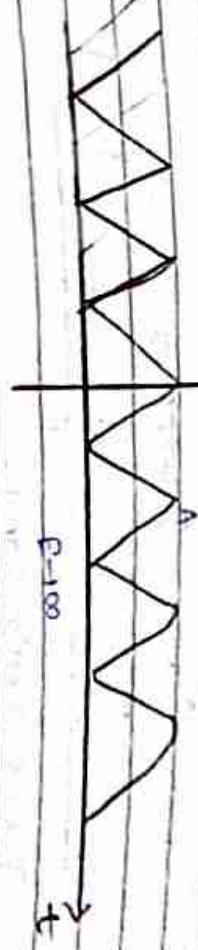
E

P = Power

E = Energy

Energy & power signal

Energy & power signal

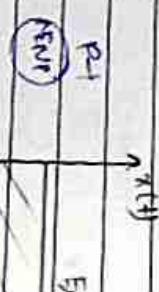
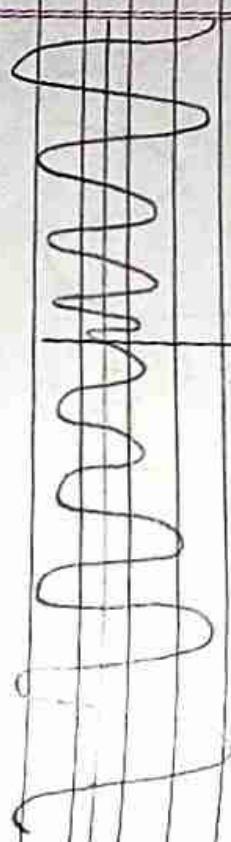


Energy & Power signal

$F = \infty$

$F = \infty$

$P = \text{Power}$



24

$$P = 4 \times 9$$

= 12 units

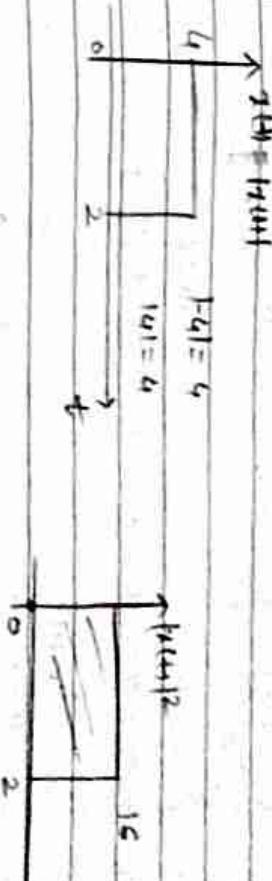
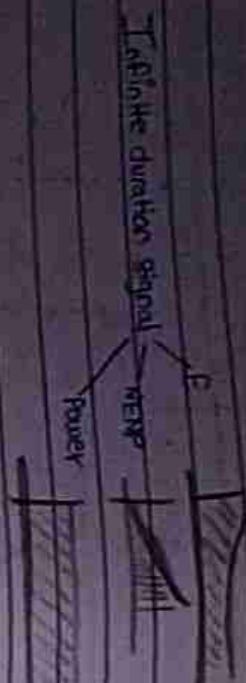
Finite duration signal

NEAR

Cannot be Fourier

$$P=0$$

Q. Calculate the energy of signal



$$\text{Energy} = \int_{-\infty}^{\infty} |x(t)|^2 dt = \text{area of } |x(t)|^2$$

$$E = 16 \times 2$$

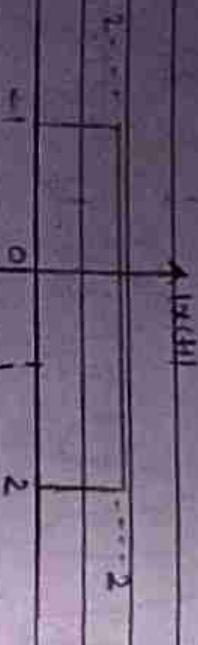
$$= 16 \times 2 = 32 \text{ units}$$

* Check for energy & power of given signal

finite

$x(t)$

$$x(t) = \begin{cases} A & 0 < t < T \\ 0 & \text{else} \end{cases}$$



$$\text{Energy} = \int x^2(t) dt = \int A^2 dt$$

$$= A^2 \int_0^T dt = A^2 [t]_0^T$$

$$= 1 \times 1^2$$

$$= A^2 T = 1^2 \times 2 = 2$$



$$= A^2 T = 1^2 \times 2 = 2$$

Q. Calculate the energy of signal.



$$E_x = \int_{-\infty}^{\infty} |x(t)|^2 dt$$

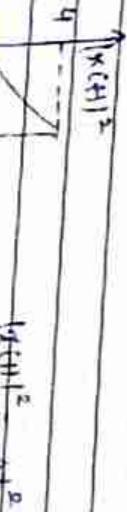
$$= \int_{-\infty}^{\infty} (mt)^2 dt$$

$$= \int_{-\infty}^{\infty} m^2 t^2 dt$$

$$m = 2$$

$$x(t) = 2t$$

Here, the signal energy of signal is finite, E_x is finite, then the signal $x(t)$ is termed as an energy signal.



$$x(t) = \sin(\omega t)$$

$$P_x = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T}^{T} |x(t)|^2 dt$$

$$\text{Energy} = \int_{-\infty}^{\infty} |x(t)|^2 dt = \int_0^{\infty} 4t^2 dt = 4 \left[\frac{t^3}{3} \right]_0^{\infty} \Rightarrow \infty$$

$$\boxed{E = \infty}$$

Ex - Energy of signal from zero to infinity

$$\text{Suppose, } x(t) = \begin{cases} e^{-t} & t \geq 0 \\ 0 & t < 0 \end{cases}$$

e^{-t} unit step function

$$E_x = \int_0^{\infty} |e^{-t}|^2 dt$$

$$= \int_0^{\infty} e^{-2t} dt$$

$$= \lim_{T \rightarrow \infty} \frac{1}{T} \left[\frac{1}{2} \int_0^T dt - \frac{1}{2} \int_0^T e^{-2t} dt \right]$$

$$= \lim_{T \rightarrow \infty} \frac{1}{T} \left[\left(\frac{1}{2} \times \frac{\pi}{2} \right) - \frac{1}{2} \left(\frac{\sin \pi}{2} \right) \right] T^2$$

$$P_x = \lim_{T \rightarrow \infty} \frac{1}{T} \left[\frac{1}{4} - \frac{1}{4} \{ \sin \pi \} \right] T^2$$

$$= \left[\lim_{T \rightarrow \infty} \frac{1}{T} \times \frac{\pi^2}{4} \right] - \left[\lim_{T \rightarrow \infty} \frac{1}{T} \times \sin \pi \right]$$

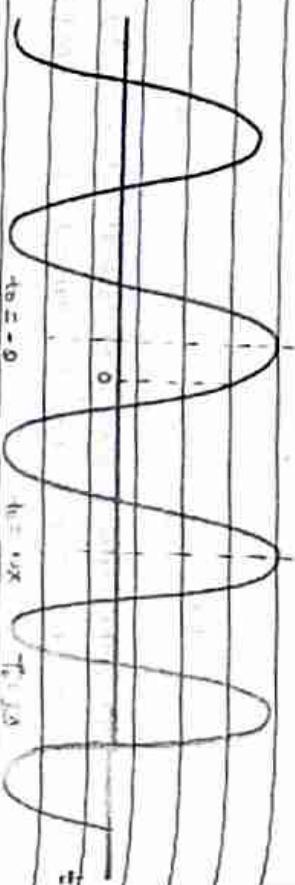
$$\Rightarrow \frac{1}{4} - 0$$

$$\boxed{P_x = \frac{1}{4}} \rightarrow P_x \text{ is a power signal.}$$

Ex.2

Let $x(t) = A \cos(\omega_0 t + \phi)$ Is this a power signal or energy signal?

$$\Rightarrow \frac{1}{T_0} \left[\frac{1}{2} \left(\frac{-\pi + 2\pi}{\omega_0} \right)^2 - \frac{-\phi}{\omega_0} \right]$$



Ex. Consider the signal given below. Is this power or energy type signal?

x_2 is unbounded so

$$P_x = \frac{1}{T_0} \int_{-\infty}^{\infty} A^2 \cos^2(\omega_0 t + \phi) dt$$

$$= \frac{1}{T_0} \int_{-\infty}^{\infty} A^2 \cos^2(\omega_0 t + \phi) dt$$

$$= \frac{A^2}{T_0} \int_{-\infty}^{\infty} \frac{-\Omega + 2\pi}{\omega_0} \frac{1 + \cos(2\omega_0 t + 2\phi)}{2} dt$$

$\frac{-\Omega}{\omega_0}$

$\frac{2\pi}{\omega_0}$

$$= \frac{A^2}{T_0} \left[\frac{1}{2} + \frac{\sin((2\omega_0 t + 2\phi))}{2\omega_0} \right]_{-\infty}^{\infty}$$

$$= \frac{A^2}{T_0} \left[\frac{1}{2} + \frac{\sin((2\omega_0 t + 2\phi))}{2\omega_0} \right]_{-\infty}^{\infty}$$

$$= \frac{A^2}{T_0} \left[\frac{1}{2} \left(\frac{-\Omega + 2\pi}{\omega_0} + \frac{\sin((2\omega_0 t + 2\phi))}{2\omega_0} \right) \right]_{-\infty}^{\infty}$$

$$= \frac{A^2}{T_0} \left[\frac{1}{2} \left(\frac{-\Omega + 2\pi}{\omega_0} + \frac{\sin((2\omega_0 t + 2\phi))}{2\omega_0} \right) \right]$$

$$\Rightarrow \frac{A^2}{T_0} \left[\frac{-\Omega + 2\pi}{2\omega_0} + \frac{\sin(-2\omega_0 t + 4\pi) + 2\pi}{4\omega_0} + \frac{t}{2\omega_0} + \sin(\Omega t - 2\pi) + 2\pi \right]$$

$$= 5 \left[-4 - \frac{9\pi}{24} \right] + 5 \left[4 + \frac{9\pi}{24} - 4 \right] =$$

$$x(t) = \begin{cases} 3\left(1 + \frac{t}{4}\right) & \text{if } 0 \leq t \leq 4 \\ 0 & \text{otherwise} \end{cases}$$

$$x(t) = \begin{cases} |x(t)|^2 dt & \text{if } 0 \leq t \leq 4 \\ 0 & \text{otherwise} \end{cases}$$



$$y = -\frac{3}{4}c - \frac{32x^3}{74} + \frac{x^5}{4} + \frac{32x^7}{74} - \frac{3}{4}c$$

$$E_x = \sum_{n=0}^{\infty} x^2[n] \Rightarrow \sum_{n=0}^{\infty} x^2[n] = \sum_{n=0}^{\infty} \left(\left(\frac{1}{3}\right)^n\right)^2$$

$$\Rightarrow 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^0 \right] + 9 \left[\left(t + \frac{t^3}{48} - \frac{t^5}{4} \right)^0 \right]$$

$$= \sum_{n=0}^{\infty} \left(\frac{1}{3}\right)^{2n} = \sum_{n=0}^{\infty} \left(\frac{1}{9}\right)^n = \frac{1}{1 - \frac{1}{9}}$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^1 \right] + 9 \left[\left(t + \frac{t^3}{48} - \frac{t^5}{4} \right)^1 \right]$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] - \left[-4 + \left(-1 \right)^3 + \left(-1 \right)^5 \right]$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] + 2 \left[4t \left(\frac{t^3}{48} \right) - \left(\frac{t^5}{4} \right)^2 - 4 \right]$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] + 9 \left[4t \cdot \frac{t^3}{48} - \frac{t^5}{4} - 4 \right]$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] + 9 \cdot$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] + 9 \left[4t \cdot \frac{t^3}{48} - \frac{t^5}{4} - 4 \right]$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] + 9 \left[\frac{t^4}{12} - \frac{t^6}{4} - 4 \right]$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] + 9 \cdot$$

$$= 9 \left[\left(t + \frac{t^3}{48} + \frac{t^5}{4} \right)^2 \right] + 9 \cdot$$

$$\alpha[n] = \begin{cases} \left(\frac{1}{3}\right)^n & \text{if } n \geq 0 \\ 0 & \text{otherwise} \end{cases}$$

$$\left| e^{j\omega t} \right| = 1 \quad \forall t \Rightarrow |e^{j\omega nt}| = 1$$

$$= 1$$

Ex: What is the power of the signal $x(t) = e^{j\omega_0 t}$? Where $(T_0 = \frac{2\pi}{\omega_0})$

$$\text{given that } T_0 = \frac{2\pi}{\omega_0} \Rightarrow e^{j\omega_0 \frac{2\pi}{T_0}} = e^{j\omega_0 (t + \frac{2\pi}{\omega_0})}$$

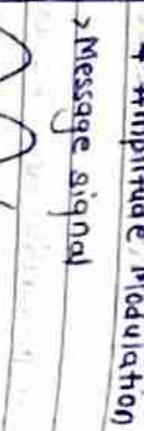
$$= e^{j(\omega_0 t + 2\pi)}$$

We know that $e^{j\omega_0 t} = e^{j(\omega_0 t + 2\pi)} = x(t)$ is periodic with a period of $\frac{2\pi}{\omega_0}$. Therefore,

$$P_x = \frac{1}{T_0} \int_0^{T_0} |e^{j\omega_0 t}|^2 dt = \frac{1}{T_0} \int_0^{T_0} 1 dt$$

Continuous Modulation

- 1) Amplitude Modulation
- 2) Frequency Modulation
- 3) Phase Modulation



* Amplitude Modulation
frequency Modulation
Deviation of freq. Δf



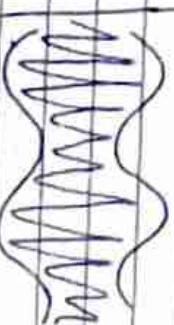
Frequency Modulation

* frequency Modulation

> Message signal



> Modulated signal



> carrier signal



> Carrier signal



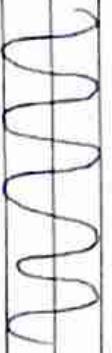
* Phase Modulation

> Message signal

> Modulated signal



> Carrier signal



Amplitude Modulated Signal :-

- It is the process in Amplitude of carrier signal changes w.r.t. message (modulating) signal.

$$\rightarrow m(t) = \text{modulating signal}$$
$$= A_m \sin \omega t$$

Single Tone AM Modulation

AM SIGNAL TRANSMITTER

Long J power, efficiency & Retendency

$$y(t) = -A \sin(\omega t) + \frac{A \omega L}{\pi} \operatorname{Card}(t + \frac{\pi}{\omega})$$

```

graph TD
    CS[Carrier signal] --> USB[USB signal]
    USB -- USB --> USBS[USB signal]
    style USB fill:none,stroke:none
    style USBS fill:none,stroke:none
    
```

→ すま おみやげ

$$P_t = P_c + P_{USA} + P_{i=0} = P_c + P_{USA}$$

$$f(x) = x^2 + 2x - 3$$

ପ୍ରକାଶକ ପତ୍ର

Have information

$$\text{Power of carrier } P_c = \frac{A_i}{2}$$

$$\text{power of USB} = \frac{1}{2} \left(\frac{A_1 - A_2}{2} \right)^2$$

$$= \frac{1}{2} \left(\frac{R_1}{2} \right) = \frac{1}{2} R_1$$

* EFFiciency of the AM modulators & Redundancy

$$\text{Carrier power} = P_c = A c^2 / 2$$

$$= \frac{2\pi}{\Delta t}$$

After Modulations Side band Power

$$(\rho_s) = \frac{m_a}{4}$$

$$\Rightarrow \frac{2+4^2-4L}{2+4^2} = \frac{2}{2+4^2}$$

$$\text{efficiency} = \frac{\text{sideband P}}{\text{total P}}$$

$$n = \frac{P_t}{P_s + P_e} =$$

$$\eta = \frac{P_e}{P_t} = \frac{m_b^2 A_c^2}{\frac{A_c^2}{2} + \frac{m_b^2 A_c^2}{\gamma}}$$

$$\frac{P_0}{P_t} = \frac{\frac{M_0^2}{2}}{1 + \frac{M_0^2}{2}}$$

$$\therefore \quad \left\{ \begin{array}{l} = \frac{P_S}{P_t} \\ = \left[\frac{m_a^2}{2 + m_a^2} \right] \end{array} \right.$$

$$\eta = \frac{m_a^2}{2 + m_a^2}$$

三

where

Modulation

$\mu = \frac{A_m}{A_c}$	where, A_m = Amplitude of modulating signal A_c = Amplitude of carrier signal.
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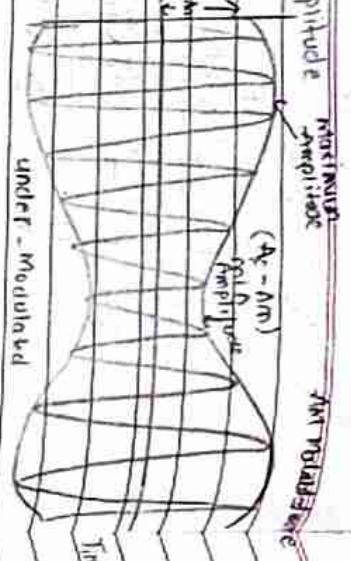
Change in Amplitude of carrier wave

But, change is formidable at some

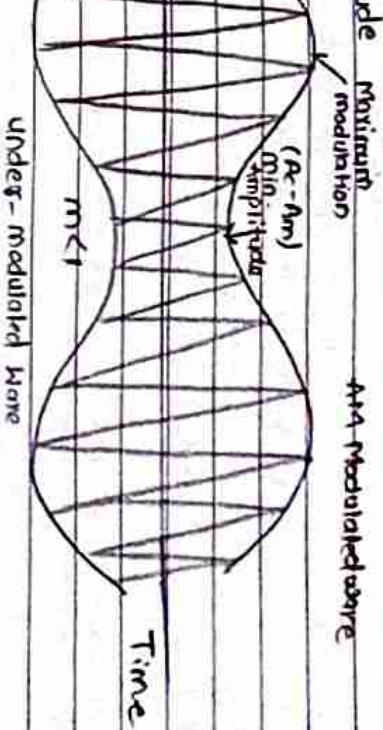
modulating wave (nm)

METHYL BIS(4-BENZYL BORATE)

Where,
Am_{max} and Am_{min} one
Max. and min. voltage of
Am wave, respectively



under-modulated
wave

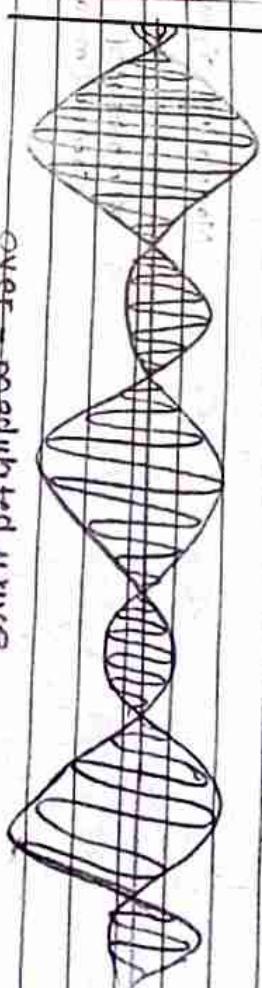


over-modulated wave

$\Delta I = \text{change in amplitude of}$

$$\frac{\Delta I}{I_c} = \frac{A_{\text{max}} - A_{\text{min}}}{A_c} = \frac{A_c + A_m - A_c + A_m}{A_c + A_m}$$

When $m > 1$



over-modulated wave

- * Carrier wave, after being modulated, if the modulated level is calculated, then such an attempt is called as Modulation Index or modulation Depth.
- * It states the level of modulation that an carrier wave undergoes

The maximum and minimum values of the envelope of the modulated wave are represented by Am_{max} and Am_{min} respectively

$$\text{Modulation Index} = \frac{\text{Max. deviation}}{\text{Carrier Amplitude}}$$

(Max. deviation)

carrier

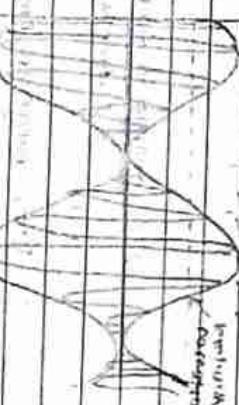
modulation

wave

Time

$m =$

Original Modulation $m=1$



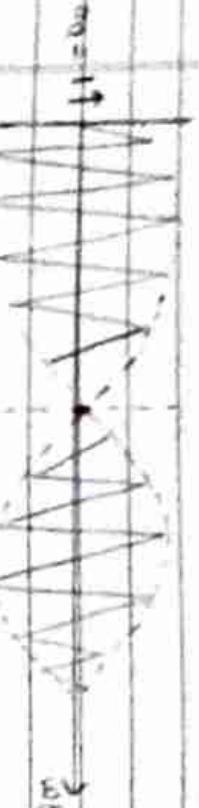
Under-modulated

wave

Time

$$m = \frac{V_{\max} - V_{\min}}{V_{\max} + V_{\min}}$$

$$m = 19$$



* Multiple-tone Amplitude Modulation

Let's have carrier signal, $c(t) = A \sin \omega t$

Multiple tone modulating signal

$$m(t) = A_1 \sin \omega_1 t + A_2 \sin \omega_2 t + A_3 \sin \omega_3 t$$

A_m signal will be

$$y(t) = A \sin \omega t$$

$$= (A_c + m(t)) \sin \omega t$$

Unmodulated carrier ($m=0$)

$$y(t) = A_c \left(1 + \left(\frac{A_1}{A_c} \right) \sin \omega_1 t + \left(\frac{A_2}{A_c} \right) \sin \omega_2 t + \left(\frac{A_3}{A_c} \right) \sin \omega_3 t \right) \sin \omega t$$

$$A_1 = \frac{A_1}{A_c}, A_2 = \frac{A_2}{A_c}, A_3 = \frac{A_3}{A_c}$$

modulated carrier ($m=0.5$)

$$y(t) = A_c (1 + 0.5 \sin \omega_1 t + 0.5 \sin \omega_2 t + 0.5 \sin \omega_3 t) \sin \omega t$$

→ carrier power → sideband power

$$P_c = \frac{A_c^2}{2} \quad P_s = \frac{1}{4} A_1^2 u_1^2 + \frac{1}{4} A_2^2 u_2^2 + \frac{1}{4} A_3^2 u_3^2$$

$$P_c = \frac{1}{2} A_c^2 \left[\frac{1}{2} (u_1^2 + u_2^2 + u_3^2) \right]$$

Carrier turned off here
modulated carrier ($m=0.5$)
on unmodulated

off here

$$\text{where } u_i^2 = u_1^2 + u_2^2 + u_3^2$$

$$P_t = P_c + P_s \cdot P_c + \frac{P_c m u^2}{2} = P_c \left(1 + \frac{m u^2}{2} \right)$$

$$P_t = P_c \left(1 + \frac{1}{2} (m_1^2 + m_2^2 + m_3^2) \right)$$

given, frequency of carrier wave,
 $f_c = 1.5 \text{ MHz} = 1500 \text{ kHz}$

$$\text{Total power } (P_t) = P_c \left(\frac{1 + m_1^2}{2} + \frac{m_2^2}{2} + \frac{m_3^2}{2} \right)$$

$$P_t = P_c \left[1 + \frac{1}{2} \sum_{i=1}^3 m_i^2 \right]$$

Current of single tone AM Wave

$$I_t = I_c^2 R_t$$

$$\text{modulation index, } m = \frac{A_m}{A_c}$$

$$\frac{1}{2} = \frac{A_m}{A_c}$$

$$-A_m = 25 \text{ V}$$

$$\text{Total Power } (P_t) = P_c \left(1 + \frac{m u^2}{2} \right)$$

$$I_t^2 R_t = I_c^2 R_t \left(1 + \frac{m u^2}{2} \right)$$

So, the amplitude of AM wave, $A_m = 25 \text{ V}$

As, we know the sidebands are

$$\text{USB} = f_c + f_m = 1500 + 10 = 1510 \text{ kHz}$$

$$\text{LSB} = f_c - f_m = 1500 - 10 = 1490 \text{ kHz}$$

Q.

The modulating signal $20 \cos(2\pi \times 10^3 t)$ is used to modulate a carrier signal $40 \cos(2\pi \times 10^4 t)$. Find the modulation index, percentage modulation, frequencies of sidebands of the modulated signal?

Soln

The modulating signal is given as

$$E_m = E_{m \text{ constant}}$$

and the given signal is

$$E_c = 20 \cos(2\pi \times 10^4 t)$$

on comparing,

$$f_m = 20, \omega_m = 2\pi \times 10^3$$

$$\therefore f_m = 1000 \text{ Hz} = 1 \text{ kHz}$$

Also, the modulating carrier signal is

$$E_c = E_{c \text{ constant}} t$$

The given signal is, $E_c = 40 \cos(2\pi \times 10^4 t)$

on comparing,

$$E_c = 40, \omega_c = 2\pi \times 10^4$$

$$f_c = 10^4 \Rightarrow 10000 \text{ Hz} = 10 \text{ kHz}$$

The modulation index is given as,

$$m = \frac{E_m}{E_c} = \frac{20}{40} = 0.5$$

$$\therefore m = 0.5 \times 100 = 50 \text{ %.}$$

The frequencies are calculated as,

$$f_{upper} = f_c + f_m = 10 \text{ kHz} + 1 \text{ kHz} = 11 \text{ kHz.}$$

$$f_{lower} = f_c - f_m = 10 \text{ kHz} - 1 \text{ kHz} = 9 \text{ kHz.}$$

The amplitude of each sidebands are

$$\Rightarrow \frac{A_{Ec}}{2} = \frac{0.5 \times 40}{2} = 10 \text{ Volts.}$$

Bandwidth of modulated signal is $\Rightarrow 2 \text{ fm}$

$$\Rightarrow 2(4 \text{ kHz}) = 2 \text{ kHz.}$$

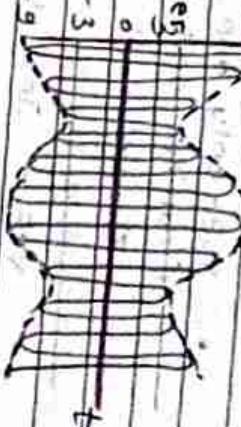
Q.

A sinusoidally modulated ordinary AM waveform is shown below.

a) determine the modulation index.

b) calculate transmission efficiency.

c) determine the amplitude of the carrier which must be added to attain a modulation index of 0.3.



Various amplitude modulation systems

- > Conventional AM,
- > DSB - SC Double side band - suppressed carrier.
- > SSB - single side band.
- > VSB - vestigial side band.

Properties of all

- Conventional AM signal contains carrier and 2 side bands.
- DSB-SC carrier is removed & only side bands are present.
- SSB - only one (single) side band is present.
- Carriers and one sided band is subtracted at transmission.

- VSB - Instead of rejecting one side band completely (like SSB), a gradual cut off of one side is allowed.

- Demodulation / detection of conventional AM is easier in comparison to that of DSB-SC & SSB systems.
- Also demodulation of conventional AM is less expensive comparatively to the others.

- It is easy to produce conventional AM signals at high power levels, therefore, can be used for broadcasting services.

- DSB-SC & SSB systems required lesser power to transmit the same information, so, in conventional AM large power is wasted (i.e. 90%) which contains no information.

Comparison

- DSB-SC & SSB are different efficient but are much more complex & expensive.
- Conventional AM scheme is simplest. Therefore, broadcasting system is very simple & less expensive using conventional AM.

Bandwidth Requirements.

- Conventional AM scheme is simplest. Therefore, broadcasting system is very simple & less expensive using conventional AM, DSB-SC & SSB.

Applications :-

- Conventional AM mostly used in public broadcasting services.
- DSB-SC & SSB modulation systems are used in point to point communication.
- SSB is used for the long distance transmission of voice signals.
- VSB is used for the transmission of television signals.

* AM Modulator Square law modulator

voltage

> Non linear :-

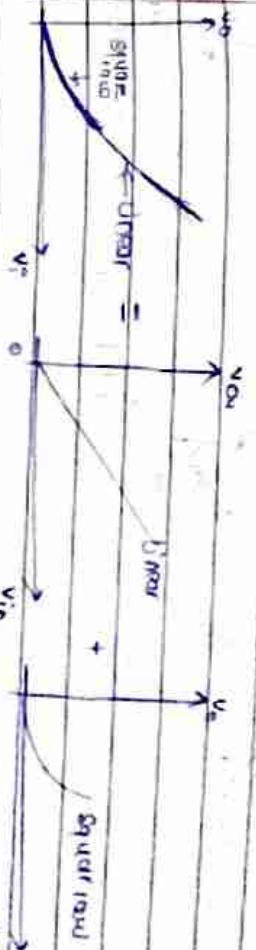
If the output of the device is not directly proportional to the input given to the device then it is called non-linear characteristics of device.



• Diode is used as modulator

It gives :-

- At low voltage Non linear characteristics.
- At high voltage linear characteristics.



* Square law modulator :-

For smaller input voltage, higher order terms are neglected. The output is considered up to the output is considered upto the square of input signal is called as square law device.

The input output relation of the modulating device

can be expressed as

$$V_o = q_1 V_{in} + q_2 V_{in}^2 + q_3 V_{in}^3 + \dots$$

- It consists of linear and non linear characteristics

2 Linear :-

If the output of the device is directly proportional to the input given to the device is called linear characteristics of device.



$$V_o = a_1 [m(t)] + A \cos(2\pi f_c t) + a_2 [m(t)] + A_c \alpha^2 (2\pi f_c t) + A_c \alpha m(t) \cos(2\pi f_c t)$$

(2) $A \cos(2\pi f_c t)$

non oscillating

non linear device

Band Pass filter output will be the final modulated signal

Sum (t)

where α is amplitude generality

$\alpha = \frac{2\pi f_c}{A}$

Not passes through BPF

passes through bandpass (BPF)

$$\text{Sum (t)} = a_1 A_c \left[1 + \frac{2a_2 m(t)}{a_1} \right] \cos(\omega_c t)$$

(BPF) op

Sum (t) = $a_1 A_c \cos(2\pi f_c t) + 2a_2 A_c m(t) \cos(2\pi f_c t)$

• Square law

For smaller voltage slice can be operate in the non linear characteristic region (square law)

$$\text{Sum (t)} = A_c \left[1 + k_a m(t) \right] \cos(\omega_c t)$$

$$A_c = a_1 A_c, \quad k_a = \frac{2a_2}{a_1}$$

where k_a is amplitude generality

modulation index of the output signal is given by

$$m = \frac{2a_2}{a_1} A_m$$

The output of square law device is given as

$$v_i = A_m \cos(\omega_c t) + A \cos(2\pi f_c t)$$

The expression for non linear AM modulator is given by

$$v_o = A_m [m(t) + A \cos(2\pi f_c t) + A \cos(m(t)) + A \cos(2\pi f_c t)]$$



Demodulators :-

Types of Demodulators:

- It is the process of recovering the information signal (baseband) from the incoming modulated signal at the receiver.



fig :- Demodulation of AM using square law device

- Demodulation of AM signals can be performed with the help of following demodulators

1. square law demodulator
 2. Envelope detector or Diode detector
 3. Synchronous detector or coherent detector
- out from any values if complex

- Square law demodulator
- Consider a non-linear demodulator device, modulated AM signal $s_{AM}(t)$ is applied to it.
- When the level of $s_{AM}(t)$ is very small, the output can be considered up to square of an input called square law demodulator

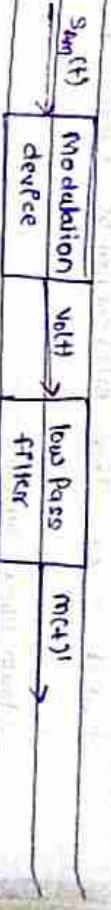


fig - Demodulation of AM using square law device

- If $m(t)$ is the information signal ($\text{0-}1\text{Hz}$)
- Carrier is $c(t) = A \cos(\omega_c t)$
- Amplitude modulated input signal is given to the non-linear

correlations due to

$$S_{\text{MM}}(t) = A_c [1 + k_m(t)] \cos(\omega_m t)$$

$$\begin{aligned} S_{\text{AM}}(t) &= A_c [1 + k_a(t)] \cos(\omega_m t) + \\ &= A_c \cos(\omega_m t) + A_c k_a(t) \cos(\omega_m t) \end{aligned}$$

The output of square law demodulator is

$$y_{\text{SL}} = a_1 S_{\text{MM}}(t) + a_2 S_{\text{AM}}(t)$$

e.g. for $S/I = 10$ and efficiency of demodulator and calculate how much power is wasted

$$\eta \text{ Should be } 0.2$$

$$\eta = 0.1^2$$

$$0.01$$

that means 99% power wasted

$$(APF)_{\text{opt}} = \left[\frac{a_1 A_c k_m^2(t)}{2} \right] + \left[\frac{\partial A_c k_m(t)}{\partial t} \right]$$

$$\downarrow \quad \downarrow$$

noise

signal

\rightarrow if $S \gg 1$, Then $m(t)$ can be completely reconstructed

\rightarrow If $S \ll 1$ then $m(t)$ cannot be completely reconstructed from above equation

$$S = \left[\frac{a_1 A_c k_m(t)}{2} \right] = ?$$

$$\left[\frac{\partial A_c k_m(t)}{2} \right]$$

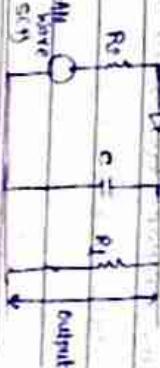
$$N = \sqrt{k_m \cos(2\omega_m t)} = \frac{a}{a}$$

$$\text{for } \cos(\omega_m t) = 1, \quad N = a$$

\rightarrow η should be high for perfect reconstruction that means all should be very low.

• Envelope detector can be

designed with the help of diode & capacitors shown in fig.



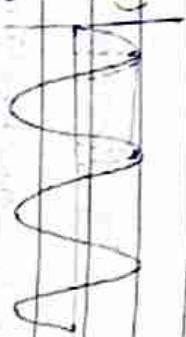
- Assume diode is ideal

→ If capacitor discharges slowly the output signal

$P > N$ \rightarrow F.B. \rightarrow S.C (short circuit)

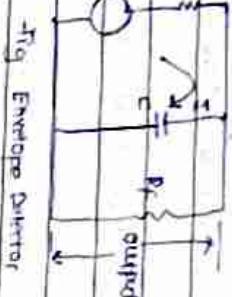
$P < N$ \rightarrow R.B. \rightarrow O.C (open circuit)

Assume the output of envelope detector is a sinusoidal wave as shown in fig



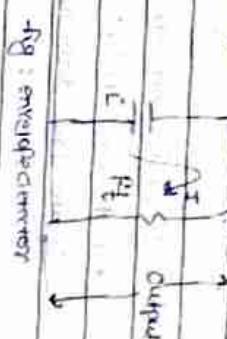
- The working of circuit as follows

- During the +ve half cycles of the input signal, diode D is forward biased and the capacitor C charges up rapidly to the peak of the input signal.



- When the input signal falls below

- Peak value and for -ve half cycle of the input signal diode becomes reverse biased acting as open diode and the capacitor discharges through the load resistor RL



- Case (i) when $t = 0$ to t_1

- time constant R_C should be small, so that capacitor charges rapidly.

- Case (ii) when $t = t_1$ to t_2

- Time constant R_C should be high, so that capacitor discharges slowly.

Some procedure



Γ (reflection coefficient) is a complex number that describes both the magnitude and the phase shift of the reflection.

The simplest cases with Γ measured at the load are:

- $\Gamma = -1$; complete negative reflection, when the line is short-circuited,

- * Short circuit

$$Z_L = 0 \rightarrow$$

- Tolerance between incident and reflected waves along a transmission line.

$$\Gamma = \frac{V_R}{V_I} \quad \Gamma = \frac{Z_L - Z_0}{Z_L + Z_0}$$

$$\begin{aligned} |V_{\text{refl}}| &= |V_I| + |V_R| & |V_{\text{main}}| &= |V_I| - |V_R| \\ &= |V_E| + |\Gamma V_E| & &= |V_E| - |\Gamma V_E| \\ &= (1 + |\Gamma|)|V_E| & &= (1 - |\Gamma|)|V_E| \end{aligned}$$

$$\text{VSWR} = \frac{|V_{\text{refl}}|}{|V_{\text{main}}|}$$

(Voltage Standing Wave Ratio)

$$\text{VSWR} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

$$|\Gamma| = \text{VSWR} - 1$$

$$\text{VSWR} + 1$$

- Stating above -



$N = \text{Holo}$; $A_N = \text{amplitude}$

Input impedance of quarter λ length of Tx line :-



$$Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta L}{Z_0 + jZ_L \tan \beta L} \right]$$

$$\beta L = \frac{2\pi}{\lambda} \times \lambda/4 = \pi/2$$

$$Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta L}{Z_0 + jZ_L \tan \beta L} \right]$$



$$Z_L = \infty$$

$$= Z_0 + jZ_0 \tan \beta L$$

$$\tan(\beta L) = \infty$$

$$Z_{in} = Z_0 \left[1 + jZ_0 \tan \beta L \right]$$

$$Z_{in} = Z_0 \times \frac{Z_L}{Z_L + jZ_0}$$

$$\beta L = \frac{\pi}{2}$$

$$Z_{in} = \frac{Z_L}{Z_L + jZ_0}$$

$$Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta L}{Z_0 + jZ_L \tan \beta L} \right]$$

$$\boxed{\text{Ans}} = \frac{Z_0 \times Z_L}{Z_0 + jZ_L}$$

Voltage standing wave ratio and reflection coefficient :-

The voltage travelled forward towards the load and reflected back, when they are superimposed on each other in a uniform transmission line forms a standing wave (with complex amplitude).

• The voltage is zero at the load and reflected voltage is zero at the source.

(With complex amplitude).

then

• A wave is partly reflected when a transmission line is terminated with impedance which is not equal to its characteristic impedance.

Input impedance of open circuit :-



$$Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta L}{Z_0 + jZ_L \tan \beta L} \right]$$

$$Z_L = \infty$$

$$Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta L}{Z_0 + jZ_L \tan \beta L} \right]$$

$$\tan(\beta L) = \infty$$

$$Z_{in} = Z_0 \left[1 + jZ_0 \tan \beta L \right]$$

$$Z_{in} = \frac{Z_L}{Z_L + jZ_0}$$

$$Z_{in} = Z_0 \left[\frac{Z_L + jZ_0 \tan \beta L}{Z_0 + jZ_L \tan \beta L} \right]$$

$$\boxed{\text{Ans}} = \frac{Z_0 \times Z_L}{Z_0 + jZ_L}$$

$$Z_{in} = -jZ_0 \cot \beta L$$

βL = length of transmission

Input impedance of short circuit :-

Put $Z_L = 0$

$$Z_{in} = Z_0 \left[\frac{Z_0 + jZ_0 \tan \beta L}{Z_0 + jZ_0} \right]$$

$$Z_{in} = Z_0 \left[1 + jZ_0 \tan \beta L \right]$$

$$Z_{in} = Z_0 \left[\frac{Z_0 + jZ_0 \tan \beta L}{Z_0 + jZ_0} \right]$$

$$Z_{in} = Z_0$$

$$Z_{in} = Z_0$$

3) Distortion less transmission line :-

$$\boxed{\frac{R}{L} = \frac{G}{C}}$$

$$\gamma = \sqrt{(R+j\omega L)(G+j\omega C)} \Rightarrow \sqrt{\frac{R(1+j\omega L)}{R}} \frac{G}{R} \left(1 + j\frac{\omega C}{G}\right)$$

$$\gamma = \sqrt{RG} \left(1 + j\frac{\omega C}{G}\right)^2$$

$$= \sqrt{RG} \left(1 + j\frac{\omega C}{G}\right)$$

$$\text{Put } \gamma = \alpha + j\beta.$$

$$\therefore \alpha + j\beta = \sqrt{RG} \left(1 + j\frac{\omega C}{G}\right)$$

$$\therefore \alpha = \sqrt{RG} \quad \& \quad \beta = \sqrt{RG} \frac{\omega C}{G} \quad (\text{on comparing})$$

$$Z_0 = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = \sqrt{\frac{R(1+j\omega L/R)}{G(1+j\omega C/G)}} = \sqrt{\frac{R}{G}}$$

$$\text{where } \frac{R}{L} = \frac{G}{C}$$

$$\boxed{Z_0 = \sqrt{\frac{R}{G}} = \sqrt{\frac{L}{C}}}$$

Different types of transmission line

Date _____
Page _____

1) load loss Tr. Line

R < R₀, G > G₀

$\Delta = \sqrt{R^2 + G^2} \cdot Z_0$

$$\Delta = \sqrt{Z_0^2 \left(\frac{R}{Z_0} + \frac{G}{Z_0} \right)^2 + \left(\frac{R}{Z_0} - \frac{G}{Z_0} \right)^2}$$

$$= \sqrt{Z_0^2 \left(1 - \frac{R}{Z_0} \right)^2 + \left(\frac{G}{Z_0} \right)^2}$$

$$= \sqrt{Z_0^2 \left[1 - \left(\frac{R}{Z_0} \right)^2 + \left(\frac{G}{Z_0} \right)^2 \right]}$$

R = 0, G = 0

2) lossless Tr. Line

R = 0, G = 0

$\Delta = \sqrt{Z_0^2 \left(R_0 + jG_0 \right)}$



doubt

$\Delta = jw\sqrt{LC} \sqrt{1 - \frac{jG}{jw} - j\frac{R}{Z_0} + j\frac{R}{Z_0}}$

$\Delta = jw\sqrt{LC} \sqrt{1 - \frac{j(G + R)}{jw + Z_0}}$

$$= jw\sqrt{LC} \sqrt{1 - j\left(\frac{G}{wL} + \frac{R}{Z_0}\right)} = \frac{R}{Z_0} jw\sqrt{LC}$$

$$\sqrt{R^2 + G^2} = \frac{R}{Z_0} \sqrt{Z_0^2 - \frac{R^2}{Z_0^2}}$$

$$\Delta \equiv jw\sqrt{LC} \sqrt{1 - \frac{j}{\frac{1}{2}} \left[\left(\frac{R}{Z_0} + \frac{G}{Z_0} \right) \right]}$$

$$a \equiv \frac{1}{2} \left[R \sqrt{\frac{C}{L}} + G \sqrt{\frac{1}{C}} \right]$$

$$B \equiv w\sqrt{LC}$$

$$z_0 = \sqrt{R + jwL}$$

Q6. A carrier wave of frequency 91 MHz is frequency modulated by a sine wave of amplitude 10 volts and 15 kHz. The frequency sensitivity of the modulator is 3 kHz/v. Determine the bandwidth by transmitting only those side frequencies with amplitudes that exceed 1% of the unmodulated carrier wave amplitude. Use universal curve for this calculation.

$f_c = 91 \text{ MHz} ; A_m = 10 \text{ V} \text{ & } f_m = 15 \text{ kHz}$

$k_f = 3 \text{ kHz/V.}$

Q7. An FM wave is defined below.

$$s(t) = 12 \sin(6 \times 10^8 \pi t + 5 \sin 1250 \pi t)$$

Find carriers & modulating frequencies, the modulating index, and the maximum deviation of the FM wave. Also find the bandwidth of FM wave, what power will the FM wave dissipate in a 10 ohm resistor?

(c) Repeat part (a) assuming frequency at modulated wave is doubled.

$$\rightarrow f_c = 91 \text{ MHz}, A_m = 10V, f_m = 90 \text{ kHz}$$

$$V_F = 3 \text{ mV}.$$

$$B = 2(\beta + 1)f_m$$

$$\Delta f = k_F A_m \approx 3 \times 10^2 \times 10 = 30 \text{ kHz}$$

$$k_F = 3 \text{ kHz}^{-1}$$

$$f_c = 91 \text{ MHz}; f_m = 10 \text{ V} \rightarrow f_m = 15 \text{ kHz}$$

$$B = \frac{\Delta F}{f_m} = \frac{30 \times 10^3}{30 \times 10^3} = 1$$

$$B_m = 3 \text{ kHz}$$

Q.5

Find the bandwidth of a single-tone-modulated FM signal described by

frequency deviation Δf is fixed at

maximum value of frequency deviation ΔF is fixed at 75 kHz. For commercial FM broadcasting by radio and modulation frequency is $\alpha = 15 \text{ kHz}$.

(b) Repeat part (a) assuming that the amplitude of modulating wave is doubled.

$$\Delta f = 75 \text{ kHz}$$

$$A_m = 20 \text{ V}$$

$$\text{Bandwidth } B = 2(\beta + 1)f_m$$

$$B = \frac{\Delta F}{f_m} = \frac{75}{15} = 5 \text{ kHz}$$

$$\Delta F = k_F A_m \approx 3 \times 10^2 \times 20 = 60 \times 10^3 \text{ kHz}$$

$$B = \frac{\Delta F}{f_m} = \frac{60 \times 10^3}{15 \times 10^3} = 4$$

$$B = 0 (\beta + 1)f_m \approx 0(5 + 1) \cdot 15 \times 10^3$$

$$= 0(5) \cdot 15 \times 10^3$$

$$= 150 \text{ kHz}$$

A carrier wave of frequency 91 MHz is frequency modulated by a sine wave of amplitude 10 V. The frequency sensitivity of the modulator is 3 kHz. The

(a) Determine the appropriate bandwidth of the modulator using Carson's rule.

$$B = \frac{\Delta F}{f_m}$$

$$\Delta F = k_F A_m$$

$$\Delta F = 3 \text{ kHz} \times 10$$

$$\boxed{\Delta F = 30 \times 10^3}$$

$$B = 2 \text{ kHz}$$

$$\therefore B = 0(5) \cdot 15 \times 10^3$$

$$= 0(5) \cdot 15 \times 10^3$$

$$= 150 \text{ kHz}$$

If amplifying will be a standard tuned amplifier

Q.1 A sinusoidal wave of amplitude 10 volts & freq of 1 kHz is applied to an fm generator that has a frequency sensitivity constant of 40 Hz / mV determine the frequency deviation and modulation index.

→ Message signal $m(t) = 10 \cos(1000\pi t)$, freq $f_m = 1000 \text{ Hz}$
line freq. dev. const. $b_f = 40 \text{ Hz/mV}$

$$\text{Freq. deviation } \Delta f = b_f \cdot m = 40 \times 10 = 400 \text{ Hz}$$

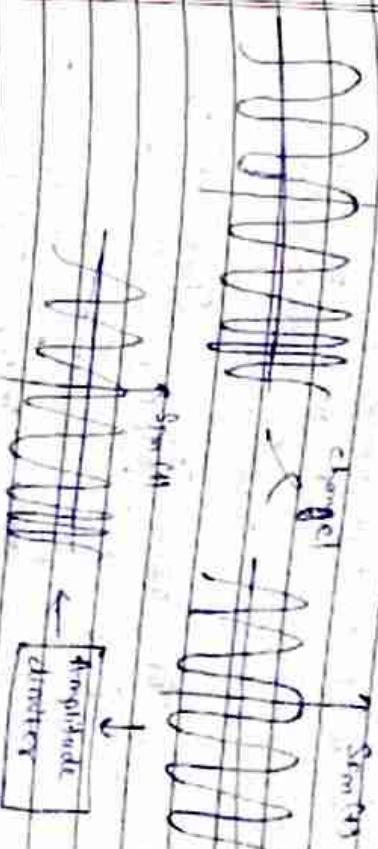
$$\text{Modulation index } \mu = \Delta f / f_m = 400 = 0.4$$

Q.2 A modulating signal $m(t) = 10 \cos(1000\pi t)$ modulated a carrier signal $A_c \cos(\omega_c t)$. find the frequency deviation and modulation index of the resulting fm signal $\text{Us}(t) = 5 \sin(\omega_c t + \Delta \phi)$

→ Mod. signal $m(t) = 10 \cos(1000\pi t)$, freq. $f_m = 5000 \text{ Hz}$

freq. sensitivity $b_f = 40 \text{ Hz/mV}$

freq. deviation $\Delta f = b_f \cdot m = 5 \times 10 = 500 \text{ Hz}$
modulation index $\mu = \Delta f / f_m = 500 \times 10^{-3} = 0.5$



→ The operation of fast recovery detectors (FRD) is highly sensitive to peak voltage fluctuations of fm signal. Therefore, amplitude limiter is essential.

→ Ratio Detectors provide high stabilization to wideband amplitude fluctuations of fm signal so

Q.3. find the bandwidth of single tone modulated fm signal described by $s(t) = 10 \cos[2\pi 10^6 t + 8 \sin(2\pi 10^3 t)]$.

$$f_m \text{ signal } S(t) = A_m \cos[\omega_f t + \theta_m \sin(2\pi f_m t)]$$

$$f_m = 6 \quad f_m = 1000 \text{ Hz}$$

by Carson's rule

$$\text{Transmission bandwidth } B_T = 2(f_m + \Delta f_m) = 2(6 + 1000) = 2006 \text{ Hz}$$

* FM RECEIVERS :-

→ FM receiver is used for receiving frequency modulated signal.

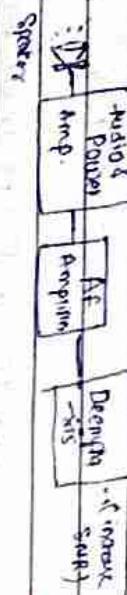
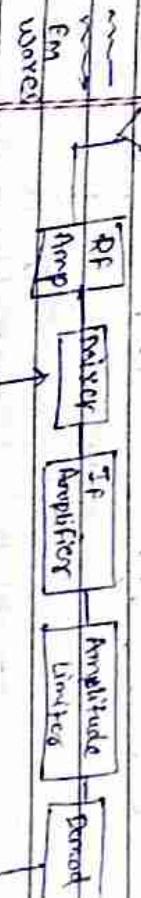
→ In FM, message signal is stored in the form of frequency variations and these frequency variations are little affected by channel noise therefore FM transmission is very much of noise free.

→ For FM: Carrier Frequency: 88 MHz - 108 MHz.

Bandwidth: 200 kHz

$f_{IF} = 10.7 \text{ MHz}$

(Intermodulation)



Rejection of image frequency

$$f_{IM} = f_{RF} + \frac{f_{IF}}{2f_{IF}}$$

$$f_{LO} > f_{RF}$$

$$f_{LO} < f_{RF}$$

$$f_{IM} = f_{RF} - 2f_{IF}$$

$$f_{IM} = f_{RF} - 2f_{IF}$$

> circuit having higher quality factor with lower frequency signal. Cross talk takes place there.

> Then faces selectivity problem therefore,

> Superheterodyne receiver is designed, which is having fixed frequency signal.

- Block diagram of FM receiver.

Quality factor for FM receiver within low range for

$$\approx \frac{82 \times 1000}{200} = 100 \text{ kHz}$$

$$Q.F = \frac{108 \times 1000}{200} = 540 \text{ kHz}$$



• Antenna :-

1. Receive the different frequency stations.
2. Convert it in to electric wave.

Why Intermediate frequency?

> Sensitivity depends on the gain, gain is more, sensitivity is more. Sensitivity is more, sensitivity is more, but gain increases signal is unstable. To generate stable signal, frequency should be constant, it is 655 kHz intermediate frequency.

> To design high freq. signal circuit is very difficult.

- 1. Reject unwanted & image frequency signals and select desired carrier frequency.
- 2. RF Amplifier (Tuned at desired frequency)

$$f_i = f_{c1} - f_{c2}$$

* TRF Receiver having quality factor issue:

Sensitivity depends on quality factor.

Freq. Range of AM TRF receiver is 550 - 1600 kHz and BW (bandwidth) : 10 kHz

Sensitivity :

$$\text{Sensitivity} = \frac{f_c}{\text{BW}} \left(\frac{\text{Center Freq.}}{\text{Bandwidth}} \right)$$

Sensitivity depends on quality factor.

Sensitivity depends on Gain

i.e. gain of receiver or gain of amplifying.

> So having wide quality factor range

> To design circuit having higher quality factor is very difficult. The circuit is very complex.



$f_{IF} > f_{c1}$	$f_{IF} = f_{c1} + f_{c2}$
$f_{IF} < f_{c1}$	$f_{IF} = f_{c1} + f_{c2}$ (local oscillator freq. = Radio + Intermediate freq.)

$f_{IF} < f_{c1}$	$f_{IF} = f_{c1} + f_{c2}$ (local oscillator freq. = Radio + Intermediate freq.)
-------------------	---

fidelity-

- Tank circuit used for tuning purpose. Variable capacitor and variable inductor forms part of tank circuit.
- * Class C amplifier - its efficiency is high while linearity is poor.
- * giving efficient high performance and reduces noise effect. Active element conduct for less than one half cycle of the input signal.

* Re Coupled Amplifier

In it is used in multistage amplifier for coupling.

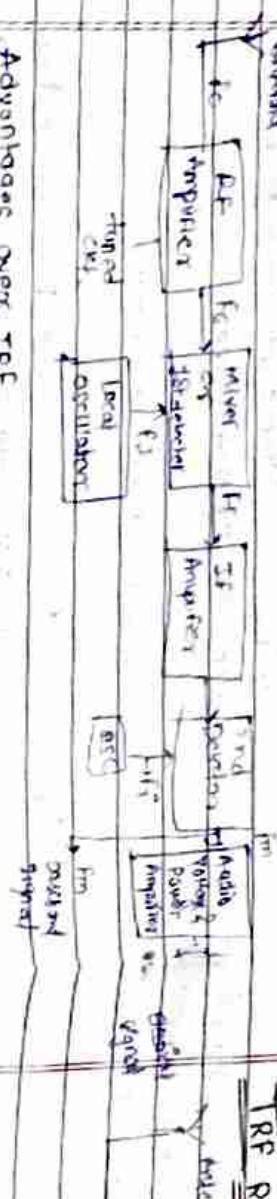
it is also compact, excellent frequency response and having constant gain.

Push pull class B amplifier

+ enhance both the load capacity and switching speed.

Speaker: Convert electrical signal into desired message signal.

* Superheterodyne Receiver



TRF Receiver

Unmodulated antenna and receiver for maximum fidelity.

Tuned Radio Frequency

(TRF) Receiver

Superheterodyne

Modulated antenna and receiver for maximum fidelity.

TRF Receiver

Unmodulated antenna and receiver for maximum fidelity.

Types of AM Receivers

Coherent Receiver

(Synchronous Receiver)

The frequency generated in the receiver is synchronized to the carrier frequency in the transmitter.

The frequency generated in the receiver is completely independent from the transmitter's carrier frequency.

Non-coherent Receiver

(Heterodyne receiver)

- Antenna - is a conductor, it receives EM waves and convert it into electrical signal.
- > it selects desired carrier frequency and reject all other frequency.
- Advantages over TRF
 1. Good Sensitivity
 2. Good Selectivity
 3. Good Fidelity

Now, recall Euler's equations:

$$e^{+j\theta} = \cos\theta + j\sin\theta$$

$$e^{-j\theta} = \cos\theta - j\sin\theta$$

A Radio receiver is an electronic system that receives a desired modulated signal and recovers the original message signal from it.

functions of receiver :-

> Process to demodulate the incoming modulated signals.

> Carrier frequency tuning to select the desired freq signal

> "filtering" To separate the desired frequency signal from noisy modulated signal.

> Amplification To compensate the loss of signal during transmission

Hence proved.

$$\begin{aligned} Z_{in} &= Z_0 \left[\frac{Z_1 \cos\theta_1 + jZ_1 \sin\theta_1}{Z_0 \cos\theta_1 + jZ_0 \sin\theta_1} \right] \\ &= Z_0 \left[\frac{Z_1 + jZ_0 \tan\theta_1}{Z_0 + jZ_1 \tan\theta_1} \right] \end{aligned}$$

Performance characteristics -

Selectivity :-

Ability of the receiver to select desired frequency signal & reject all others. e.g. 93.5 MHz (tuned circuit) reject adjacent frequency signal. Filter quality factor (sharpness of frequency response).

Sensitivity :-

> Ability of a receiver to detect the weakest possible received signal.

> Gain of receiver proportional its sensitivity of receiver for desired signal.

Q. Prove that input impedance of transmission line is

$$Z_{in} = Z_0 \left[\frac{Z_0 \cos \beta L + j Z_0 \sin \beta L}{Z_0 \cos \beta L + j Z_0 \sin \beta L} \right]$$

- The input impedance is simply the line impedance seen at the beginning ($z = -\lambda$) of the transmission line, i.e.

$$Z_{in} = Z_0(z = -\lambda) = \frac{V(z = -\lambda)}{I(z = -\lambda)}$$

Z_{in} equal to neither the load impedance Z_L nor the characteristic impedance Z_0 !

To determine exactly Z_{in} , we

$$Z_{in} \neq Z_L \text{ & } Z_{in} \neq Z_0$$

We know that

$$V(z = -\lambda) = V_0 \left[e^{j\beta z} + T e^{-j\beta z} \right]$$

$$I(z = -\lambda) = \frac{V_0}{Z_0} \left[e^{j\beta z} - T e^{-j\beta z} \right]$$

Therefore,

$$Z_{in} = \frac{V(z = -\lambda)}{I(z = -\lambda)} = \frac{Z_0 (e^{j\beta z} + T e^{-j\beta z})}{(e^{j\beta z} - T e^{-j\beta z})}$$

We can explicitly write Z_{in} in terms of load Z_L using the previously determined relationship:

$$T = \frac{Z_L - Z_0}{Z_L + Z_0}$$

Combining those two expression, we get :

$$Z_{in} = Z_0 \left[\frac{(Z_L + Z_0)e^{j\beta z} + (Z_L - Z_0)e^{-j\beta z}}{(Z_L + Z_0)e^{j\beta z} - (Z_L - Z_0)e^{-j\beta z}} \right]$$

$$= Z_0 \left[\frac{Z_L (e^{j\beta z} + e^{-j\beta z}) + Z_0 (e^{j\beta z} - e^{-j\beta z})}{Z_L (e^{j\beta z} + e^{-j\beta z}) - Z_0 (e^{j\beta z} - e^{-j\beta z})} \right]$$

Note :-

Z_{in} equal to neither the load impedance Z_L nor the characteristic impedance Z_0 !

To determine exactly what Z_{in} is, we first must determine the voltage and current at the beginning ($x = -\lambda$)

$$V(x = -\lambda) = V_0 \left[e^{j\beta x} + T e^{-j\beta x} \right]$$

$$I(x = -\lambda) = \frac{V_0}{Z_0} \left[e^{j\beta x} - T e^{-j\beta x} \right]$$

Therefore,

$$Z_{in} = \frac{V(x = -\lambda)}{I(x = -\lambda)} = \frac{Z_0 \left[e^{j\beta x} + T e^{-j\beta x} \right]}{\left[e^{j\beta x} - T e^{-j\beta x} \right]}$$

Q. Prove input impedance of transmission line is

$$Z_{in} = Z_0 \left[\frac{Z_0 \cos \beta L + j Z_0 \sin \beta L}{Z_0 \cos \beta L + j Z_0 \sin \beta L} \right]$$

(using formula)

$$J(z,t) = \frac{v^2 e^{-izt}}{z_0} - \frac{v^2 e^{izt}}{z_0}$$

卷之三

D. 160

$$Z_1 = \frac{I(1)}{V(1)} = \frac{V_0 - V_1}{V_0 + V_1 - 2V_1}$$

$$\gamma = \sqrt{(p + \rho u_1)(q + \rho u_2)}$$

卷之三

$$2 \left\{ \frac{2}{N} + 1 \right\}, N$$

$\frac{V_i}{V_f} \rightarrow$ Retention coefficient, denoted by F

三

V_o is voltage of wave travelling back, load to generator and
V_o is source to load, ratio is the reflection coefficient.

$$z_1 = \frac{1 + \Gamma \cdot z_0}{1 - \Gamma}, \quad \Gamma = \frac{z_1 - z_0}{z_1 + z_0}$$

5. Input impedance

卷之三

Consider a lossless line, length L , terminated so that a load Z_L

The input impedance is simply the line impedance.

seen at the beginning ($x = -1$) of the transmission line

$$z_0 = z(x=-\infty) = \frac{v(x=-\infty)}{I(x=-\infty)}$$

When characteristic impedance = z_0

$$N = \sqrt{p} (\text{max role})^k \quad \text{and} \quad N^k = \omega$$

$$\frac{J \cdot 2\pi}{\lambda} = \sqrt{(R + j\omega L)(G + j\omega C)}$$

$$\frac{j\omega}{-V_P} = \sqrt{(R+j\omega L)(G+j\omega C)}$$

load Impairment & 4. Reflection coefficient

$$y(0,t) = v^+ e^{-\lambda_1 t} + v^- e^{\lambda_2 t}$$

2
11
4
-2
11
12,
17

\rightarrow distance travelled

$$V(x,t) = \underbrace{V^+ \cos(\omega t - \beta x)}_{\text{Travelling in +ve direction}} + \underbrace{V^- \cos(\omega t + \beta x)}_{\text{Travelling in -ve direction}}$$



Parameters of Transmission lines

Characteristic Impedance.

- > Phase velocity
- > Load Impedance
- > Reflection Coefficient
- > Input impedance
 - For open circuit
 - For short circuit
 - For quarter wavelength

Characteristic Impedance

$$\frac{d^2 V}{dx^2} = \gamma^2 V$$

$$\boxed{\gamma = \alpha + j\beta}$$

$$\frac{dV}{dx} = -(R+j\omega L)I$$

$$\frac{d}{dx}(V^+ e^{-j\alpha x} + V^- e^{+j\alpha x}) = -(R+j\omega L)[I^+ e^{-j\alpha x} + I^- e^{+j\alpha x}]$$

$$\boxed{V^+ e^{-j\alpha x} + V^- e^{+j\alpha x} = -(R+j\omega L)[I^+ e^{-j\alpha x} + I^- e^{+j\alpha x}]} \quad \begin{matrix} \text{approximate} \\ \text{at propagation} \\ \text{medium} \\ \text{surface} \end{matrix}$$

On comparing

$$V^+ e^{-j\alpha x} = -(R+j\omega L) I^+ e^{-j\alpha x}$$

$$\frac{V^+}{I^+} = \frac{-(R+j\omega L)}{j\alpha} = R + j\omega L$$

We know that $\gamma = \sqrt{(R+j\omega L)(G+j\omega C)}$

$$\frac{V^+}{I^+} = \frac{\sqrt{R+j\omega L}, \sqrt{G+j\omega C}}{\sqrt{(R+j\omega L)(G+j\omega C)}} = \frac{R+j\omega L}{G+j\omega C}$$

Solution of Transmission line equation :-

$$\frac{d^2 V}{dx^2} = \gamma^2 V$$



Solution of transmission line equation:

$$\boxed{\frac{d^2 E}{dx^2} = -\gamma^2 E}$$

Solution of wave equation

$$E = E_0 e^{-j\gamma x} \quad \textcircled{C}$$

Now eq is in phase form; how to convert it into time varying,
take a real part and multiply by $e^{j\omega t}$

$$E(x,t) = \operatorname{Re}(E_0 e^{-j\gamma x}) e^{j\omega t}$$

$$\boxed{\frac{d^2 E}{dx^2} = \gamma^2 E} \quad \text{from } \textcircled{C}$$

$$\boxed{\frac{d^2 E}{dx^2} = -\gamma^2 E}$$

$$\boxed{\frac{dE}{dx} = -\gamma e^{-j\gamma x}}$$

$$\boxed{\frac{dE}{dx} = -\gamma^2 e^{-j\gamma x} E_0}$$

$$\boxed{\frac{dE}{dx} = \gamma^2 e^{-j\gamma x} E_0}$$

$$\boxed{\frac{dE}{dx} = \gamma^2 e^{-j\gamma x} E_0}$$

Solution of transmission line equation

$$V(x,t) = (V^+ e^{-j\alpha x} + V^- e^{+j\alpha x}) e^{j\omega t}$$

$$= V_o e^{j(\omega t - \beta x)} + V^- e^{j(\omega t + \beta x)}$$

Primary constants of transmission line

$$I = \left[\frac{1}{X_C} + \frac{1}{X_R} \right] V$$

$$X_C = \frac{1}{j\omega C}; X_R = \frac{1}{G}$$

$$\Delta I = j\omega C (Measured in m)$$

$$J = [j\omega C + G] V$$

$$\Delta I = -(\bar{g}_{dR} + j\omega C \bar{g}_d) V$$

$$J_{out} + \frac{\Delta I}{\alpha - j\omega \Delta I} = -(\bar{g}_d + j\omega C) V$$

$$\frac{dI}{dx} = -(\bar{g}_d + j\omega C) V \quad \text{--- (2)}$$

from eq (1)

$$\Delta V = -(R_d V + j\omega L_d) I$$

$$\frac{dV}{dx} = -(R_d + j\omega L_d) I \quad \text{--- (1)}$$

voltage
along wire

After diff.

$$\frac{d^2V}{dx^2} = -(R_d + j\omega L_d) \frac{dI}{dx}$$

$$\frac{d^2V}{dx^2} = (R_d + j\omega L_d)(G_d + j\omega C) V$$

$$Y^2 \cancel{R^2} = (R_d + j\omega L_d)(G_d + j\omega C); Y = \sqrt{(R_d + j\omega L_d)(G_d + j\omega C)}$$

$$\frac{d^2V}{dx^2} = \boxed{Y^2 + \frac{d^2V}{dx^2}}$$

gamma

primary constants of transmission line



$\Delta I \rightarrow 0$ (Measured in m)



ΔI measured at m

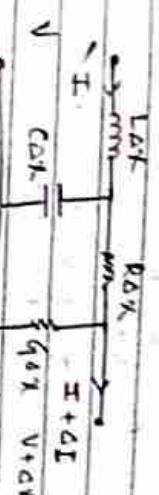
measured in henry/meter H/m

$C \rightarrow F/m$

$R_d \rightarrow \Omega/m$

$G_d \rightarrow -U/m$

Equivalent circuit & Equation of Transmission Line



where output is $I + \Delta I$ (out ΔI is -ve).

$$T_{out} = I + \Delta I \quad R_d \ll \Delta I \approx -V$$

$$V_{out} = V + \Delta V \quad \Delta V \text{ is } \Delta I \cdot R_d; \Delta V = -(R_d V + j\omega L_d) \Delta I$$

Apply ohm's law

$$V = I R$$

$$V = I \left[\frac{X_C X_R}{X_C + X_R} \right]$$

importance of admittance
importance of admittance



Transmission Lines

Date: 4/5/02

$$t_2 = \frac{d}{v}$$

where d = length,
 v = velocity.

t_2 = transit time.

$$T > t_2$$

$$T > d \cdot \frac{1}{f} \gg \frac{1}{v} \cdot \frac{1}{f} \gg d \cdot \lambda \gg d$$

(transit time is very less, i.e. it can be negligible)

- $T \gg d \cdot \frac{1}{f}$ → transit time effect is negligible at the load
- $T \ll d \rightarrow$ then transit time effect is present in the output and effects the output.
- $T = d \rightarrow$ Transit time effect is zero.

* Block diagram of Tx line.

$A \rightarrow B$



$$240 \text{ m} \quad \frac{1}{R} \gg \frac{1}{L} \quad \frac{1}{C} \gg \frac{1}{Z_0}$$

$$T = \frac{1}{f} = \frac{1}{10^9} = 10^{-9} \text{ sec}$$

$$T = \frac{1}{f} = \frac{1}{10^9} = 10^{-9} \text{ sec}$$

Transit time

Required time to travel the voltage from one point to another point on Tx. lines

- smaller the frequency of signal, \Rightarrow wavelength is longer than slow change in potential, \therefore transit time effect is less.

But there is,

Transit time effect is proportional to the length of Tx. lines and frequency used.

- Use : transfers the power from one place to another
- Tx. lines made up of conductor.
- Designed to carry an electrical signal for long distance.
- Losses and distortion are minimum in Tx. lines.

* Types of transmission lines

- > Parallel line
- > Coaxial line
- > Micro strip line

Noise

uncorrelated noise

External Noise

It is a static disturbance.
Such as lightning, frequency of signal, such as affect the generally less than 30 MHz.

Atmospheric Noise

- extraterrestrial noise
- internally in the circuit
- electronic components such as resistors, diodes, & transistors produce this noise.
- The noise power is directly proportional to generated temperature in the circuit.

Internal Noise

- Thermal noise
- shot noise
- low freq. or flicker noise
- excess resistor noise
- burst noise or popcorn noise

presence of frequency component in the output waveform which is not in the input waveform (Phase change noise)

- Two or more signals are amplified in nonlinear device, then some unwanted sum and difference frequencies are generated.

Distortion off those frequencies called Inter-modulation distortion.

- > Uncorrelated Noise \Rightarrow Present all the time, whether signal is present or not.
- > Correlated Noise \Rightarrow Present only when signal is present.
- > External noise:- this noise generated from variety of sources. It is natural and man made noise. This generated noise is external, to receiving system.
- > Extraterrestrial Noise-
Gen- Solar & cosmic noise i.e. space noise
 - Solar \rightarrow Sun reradiates broad band frequency of noise, and it varies with time. The sun cycle repeats after 11 years.
 - Cosmic \rightarrow Noise generated by stars.

1. Thermal Noise

> thermal noise power is given by $P = V^2/R = 4kTB - \text{Watts}$

> For thermal noise, its spectral density given by $N_0 = kT$

(k = Boltzmann's const)



2. Shot Noise

(c) Noise voltage across parallel combination is given by

$$\frac{1}{R_{\text{eq}}} = \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3}$$

$$\frac{1}{R_{\text{eq}}} = 1 \cdot \frac{1}{5} + \frac{1}{5} + \frac{1}{5} = \frac{3}{5}$$

$$R_{\text{eq}} = \frac{5}{3} = 1.6666 \approx 1.67 \text{ k}\Omega$$

$$E_A = \sqrt{4 \times 4 \times 10^{-21} \times 1 \times 10^6 \times 1.67 \times 10^3}$$

$$= \sqrt{16 \times 1.67 \times 10^{-21} \times 10^9} = \sqrt{16 \times 1.67 \times 10^{-12}}$$

$$= 0.0000051691$$

$$= 5.169 \approx 5.17 \mu\text{V}$$

* general Comments

- 5) Three five kohm resistors are connected in series. for room temperature. $f = 1\text{ MHz}$ ($\tau = 4.8 \times 10^{-11} \text{ s}$) and an effective noise bandwidth of 1 MHz, determine

- The noise voltage appearing across series combination
- The noise voltage appearing across each resistor
- What is the rms noise voltage which appears across some three resistors connected in parallel under the same condition

\rightarrow (b) Noise voltage across series combination is given by

$$R_{eq} = R_1 + R_2 + R_3$$

$$= 5 \text{ k}\Omega + 5 \text{ k}\Omega + 5 \text{ k}\Omega = 15 \text{ k}\Omega$$

$$E_n = \sqrt{4kTBW}$$

$$\text{equivalent noise temp.}$$

$$T_{eq} = T_0(f-1)$$

$$T_{eq} = 290 \text{ (} 1533-1 \text{)}$$

$$T_{eq} = 154.457 \text{ K}$$

$$f = 1 + \frac{R_{eq}}{R_T} = 1 + \frac{15}{75} = 1.533$$

$$f = 1.533 \text{ dB}$$

$$\text{equiv. noise resistance at } f = R_{eq} = 40 \text{ }\Omega$$

4) A receiver connected to an antenna has an equivalent noise resistance whose magnitude is 75Ω . The receiver's noise figure is 4.8 dB . Calculate the receiver's noise figure in decibels and its equivalent temperature.

$$R_{eq}$$

$$= 75 \Omega$$

$$\text{noise figure of receiver} = 4.8 \text{ dB}$$

$$\text{noise voltage across } R_{eq} = V_{eq} = 40 \text{ }\Omega$$

Some condition

\rightarrow (c) Noise voltage across each resistor is given by

$$R_{eq} = R_1 + R_2 + R_3$$

$$= 5 \text{ k}\Omega + 5 \text{ k}\Omega + 5 \text{ k}\Omega = 15 \text{ k}\Omega$$

$$E_n = \sqrt{4kTBW}$$

$$\text{equivalent noise temp.}$$

$$T_{eq} = T_0(f-1)$$

$$T_{eq} = 290 \text{ (} 1533-1 \text{)}$$

$$T_{eq} = 154.457 \text{ K}$$

5) Determining the internal noise power of a microwave amplifier operating with a bandwidth of 500 MHz & a specified noise figure of 2.5 dB .

$$\begin{aligned} \text{value of } R_{eq} &= \sqrt{80 \times 10^{-11} \times 10^9} = \sqrt{8 \times 10^{-11} \times 10^9} \\ &= \sqrt{8 \times 10^{-11}} = 2.83 \sqrt{10^{-11}} = 0.00000283 \end{aligned}$$

$$B = 500 \text{ dB},$$

$$\begin{aligned} f &= 2.5 \text{ dB} = 10^{1.25} \times 10^{-3} \\ &= 10^{0.25} = 1.778 \end{aligned}$$

(b) Noise voltage across series combination is given by

$$R_{eq} = R_1 + R_2 + R_3 = 5 \text{ k}\Omega + 5 \text{ k}\Omega + 5 \text{ k}\Omega = 15 \text{ k}\Omega$$

$$\begin{aligned} \text{Here } E_n &= \sqrt{4 \times 4 \times 10^{-11} \times 1 \times 10^6 \times 15 \times 10^3} \\ &= \sqrt{16 \times 15 \times 10^{-12}} = \sqrt{240 \times 10^{-12}} = 0.000494 \text{ V} \end{aligned}$$

$$\begin{aligned} \text{value of } R_{eq} &= \sqrt{16 \times 15 \times 10^{-12}} = \sqrt{240 \times 10^{-12}} = 0.000494 \text{ V} \\ &= 1.552 \text{ mV} / 15.4 \text{ mV} \end{aligned}$$

- Q. A noise figure with resolution had a noise figure grade
Ans: Noise figure required at the input
to achieve an overall system input SNR of 30dB.

Q. 4

Ans:

$$P_{out} = kTB - \text{noise}$$

$$t = \frac{P_{in}}{P_{out}}$$

$$\text{noise fig} = \frac{P_{out}}{P_{in}}$$

$$20 = 10 \log \left[\frac{P_{out}}{P_{in}} \right]$$

$$P_{in} = \text{noise power at input}$$

$$= kTB_{in}$$

$$= 1000 \times 1.39 \times 10^{-23} \times (223 + 27) \times 10 \times 10^3$$

$$= 4.14 \times 10^{-14} \text{ W}$$

$$P_{in}^2 = 4.14 \times 10^{-14} \text{ W}$$

$$\text{SNR}_{AB} = 10 \log \left(\frac{P_{in}}{P_{out}} \right)$$

$$\frac{P_{in}}{P_{out}} = T_i$$

$$30 = 10 \log \left(\frac{P_{in}}{P_{out}} \right) = 10 \log \left(\frac{T_i}{T_o} \right) = 10 \log \left(\frac{273 + 27}{273 + 20} \right) = 4.01 \times 10^{-2} \text{ dB}$$

$$30 = 10 \log \left(\frac{P_{in}}{P_{out}} \right)$$

for $T_o = C$

$$S = \log \left(\frac{P_{in}}{4.14 \times 10^{-14}} \right)$$

$$10^3 \times 4.14 \times 10^{-14} = P_{in}$$

$$P_{in} = 4.14 \times 10^{-11}$$

$$= 4.14 \times 10^{-11} \text{ W}$$

- Q. Q. of the following noise factors in dB.
a) 1.0 ; b) 1.15 ; c) 3.0 ; d) 10.0

$$N_{FdB} = 10 \log (1.0) = 0 \text{ dB}$$

$$N_{FdB} = 10 \log (1.15) = 0.602 \text{ dB}$$

$$N_{FdB} = 10 \log (3.0) = 4.771 \text{ dB}$$

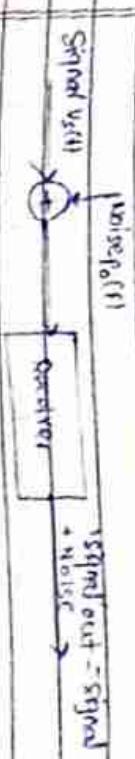
$$N_{FdB} = 10 \log (10.0) = 10 \text{ dB}$$

Types of noise

- > Additive
- > White
- > Gaussian noise

Additive

Noise is usually additive in that it adds to the information bearing signal. A model of the received signal with additive noise is shown below.



White

$$\text{Noise} \left[\begin{array}{l} \text{uniform} \\ \text{white noise} = P_0(F) = \text{constant} \end{array} \right]$$

freq.f

freq.f

decibels :-

Unit	Reference Power	Application
dBW	1W	Absolute Power
dBM	1mW	Amplifier Power
dBmV	1mV	Positive voltage is typically at input terminals of a project.

$$P_{\text{dBW}} = \text{Power}_{\text{dBW}}$$

$$= 10 \log_{10} \left(\frac{P}{P_{\text{ref}}} \right)$$

$P_{\text{dBW}} = P_{\text{dBM}} - 30$

Positive voltage is typically at input terminals of a project.

dB	any	Gain or loss of network
dBmV/m	1mV/m	Electric field strength.

dB	any	Power radiated by antenna
dB	Power radiated by antenna	Gain of an antenna

dB	any	Gain of an antenna
dB	Power radiated by antenna	Gain of an antenna

$$C(t) = \text{Actual current}, \quad n(t) = \text{Accidental current}$$

General exp. of DSB. i.e. on frequency DSB is given by

$$S_{\text{DSB}}(t) = m(t) + n(t)$$

$$S_{\text{DSB}}(t) = \text{Actual current} + \text{Accidental current}$$

$$\Rightarrow \frac{\text{Actual current}}{2} \cos(2\pi f_m t + 2\pi f_c t) + \text{Accidental current}$$

$$S_{\text{DSB}}(t) = \frac{1}{2} [\text{const. constant} t + \text{const. const. t}]$$

$$\text{Power} = \frac{1}{2} \log_{10} \left(\frac{P}{P_{\text{ref}}} \right)$$

$$\text{Power} = \text{Gain} \times \text{Antenna Gain}$$

$$\text{Power} = 2.15 \text{ dB}$$

②

NDM :-

In this many data streams of different wavelengths are transmitted in the light spectrum. If wavelength increases, the frequency of signal decreases.

or - optical fibre communications

Digital multiplexing:-

Digital represents the discrete bit of info.

TDM :-

This technique is used to transmit a signal over a single communication channel, with allowing one slot for each message.

1. Synchronous TDM :-

In this the sampling rate is common to each sample and hence same clock input is given.

2. Asynchronous TDM :-

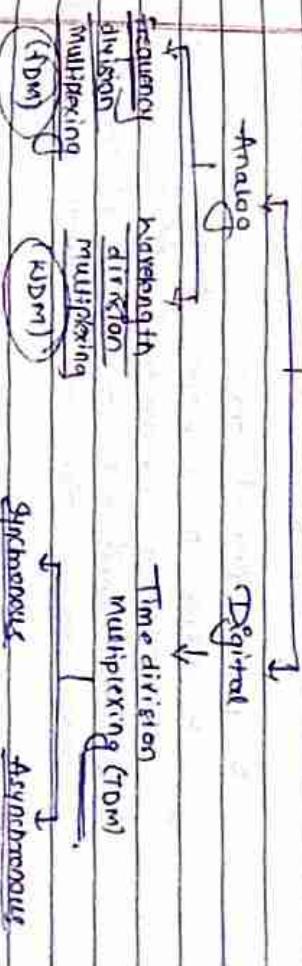
The sampling rate is different for each of the signals and the clock signal is also not common.

Multiplexing & its Types

→ Multiplexing is the process of combining multiple signals into one signal over a shared medium. If analog signals are multiplexed it's analog multiplexing and if digital signal is multiplexed it's digital multiplexing.

Types of multiplexors:-

Multiplexes



e] Improves quality of reception :-

With FM and digital communications techniques like PSK, the effect of noise is reduced to great extent.

1. FDM -

This technique uses various frequencies to combine stream of data, for sending them on a communication medium, as a single signal.

2. Television Transmitter

• Why modulation is required?

Modulation is required because

i) Baseband signals can be transmitted directly.

but these signals have many limitations which can be overcome using modulation.

ii) In process of modulation, the baseband signals are translated i.e. shifted from low to high frequency carrier.

iii) Advantages of modulation :-

a) Reduction in the height of antenna -

When the transmission occurs over free space the antenna radiate the signal out and receiver receives it. In order to operate efficiently antenna need to be in order of magnitude of increment of transmitted signal.

b) Avoid mixing of signals :-

By using different waves of high frequencies and allowing a have kind of frequencies to each message, there is no mixing up of signals and the received signal are obviously perfect.

c) Increase the range of communication

Technique of modulation helped human to use wireless equipment in a very way in their life.

d) Multiplexing is possible -

Multiplexing allows the same channel to be used by many signals.

Baseband signal

Passband signal

1. All sources of information generates baseband signal.
e.g. Audio, video, image
2. It is high frequency modulated
e.g. Landline
3. (0 to 20 kHz) audio signal
4. (0 to 55 MHz) video signal
5. (550 kHz - 1600 kHz) for AM
(88 MHz - 108 MHz) for FM

1. Frequency domain
e.g. Satellite signals
2. Frequency domain
e.g. FM
3. Frequency domain
e.g. AM
4. Frequency domain
e.g. FM

