

# نظم القياس الإلكترونية

# Electronic Measurement Systems

## (EMS)

كلية الهندسة الكهربائية والالكترونية - جامعة حلب  
د. أسعد كعدان

المحاضرين 2-1 – مقدمة في القياسات ونظم القياس  
الإلكترونية

## مصادر المحاضرة

- Electronic Instrumentation, Prof. Dr. Kofi Makinwa  
<https://ocw.tudelft.nl/courses/electronic-instrumentation/>
  - Lecture 1 - Measurement Science & Electronic Instrumentation
- Measurement Science, Dr. ir. Michiel Pertijns  
<https://ocw.tudelft.nl/courses/measurement-science/>
  - Lecture 1 - Introduction to Measurements and Measurement Systems

# Mobile measurement system



# Measurement science is everywhere!



# The importance of measurements

- The numbers tell the tale!
- For scientists, measuring is *the way to test a theory*
- For engineers, measuring is *the way to validate a design*
- Measurement systems and sensors are the senses of the computer
- Measuring also implies: knowing what you *don't* know



*"We have lots of information technology.  
We just don't have any information."*

## Measurement Science:

Analyzing whether information on a parameter of interest (the *measurand*) has been (can be) obtained with sufficient quality, when considering interfering conditions and *specifications*.

### Interfering with the measurand:

- Source loading by the measurement
- (Cross) sensitivity to undesired signals
- Electro-magnetic interference
- Many more.....

## Electronic Instrumentation:

Designing a measurement instrument according to specifications

### Specifications:

Imposed by measurement problem (= *problem specification*)  
vs.

Offered by instrument (= *instrument specification*)

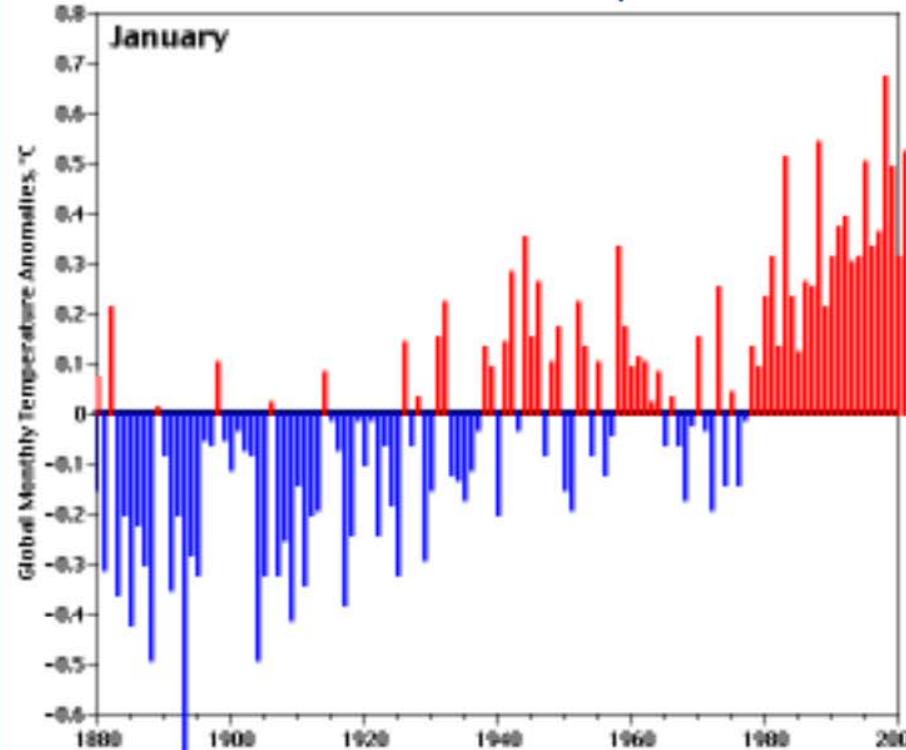
But there will be a ***Detection limit*** set by technology or by nature!

# Application to real-world measurement problems

Starts with a measurement problem.

Is there global warming ?

“Of course, *everyone* knows that !  
Just look at the *measured* temperatures”

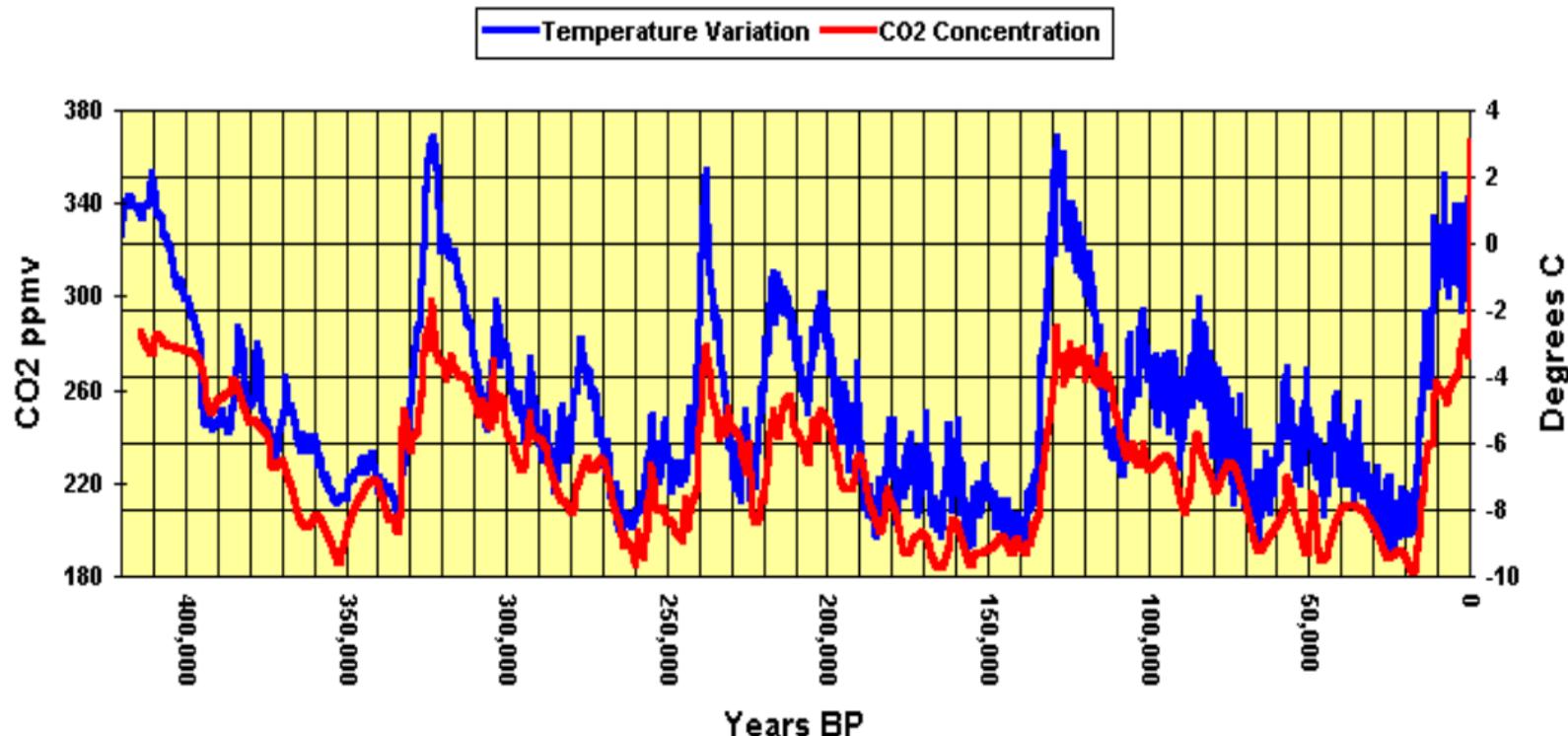


“Act now, or would you like this  
to happen.....”

Drilling down to 3623 m in the Antarctic ice at Vostoc (equivalent to about 420 kyr BP with 4-6 kyr delay). Samples analyzed for:

- CO<sub>2</sub> by gas chromatography
- Temperature by measuring <sup>18</sup>O and Deuterium concentration
- Dust particle concentration.

## Antarctic Ice Core Data 1



## Medical application

### Platonic ideals

Location of specific object-recognition areas on the hemispheres of the cerebral cortex

Left hemisphere

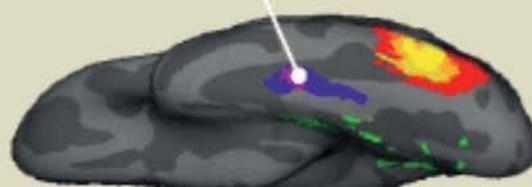


Right hemisphere



Side view

Faces



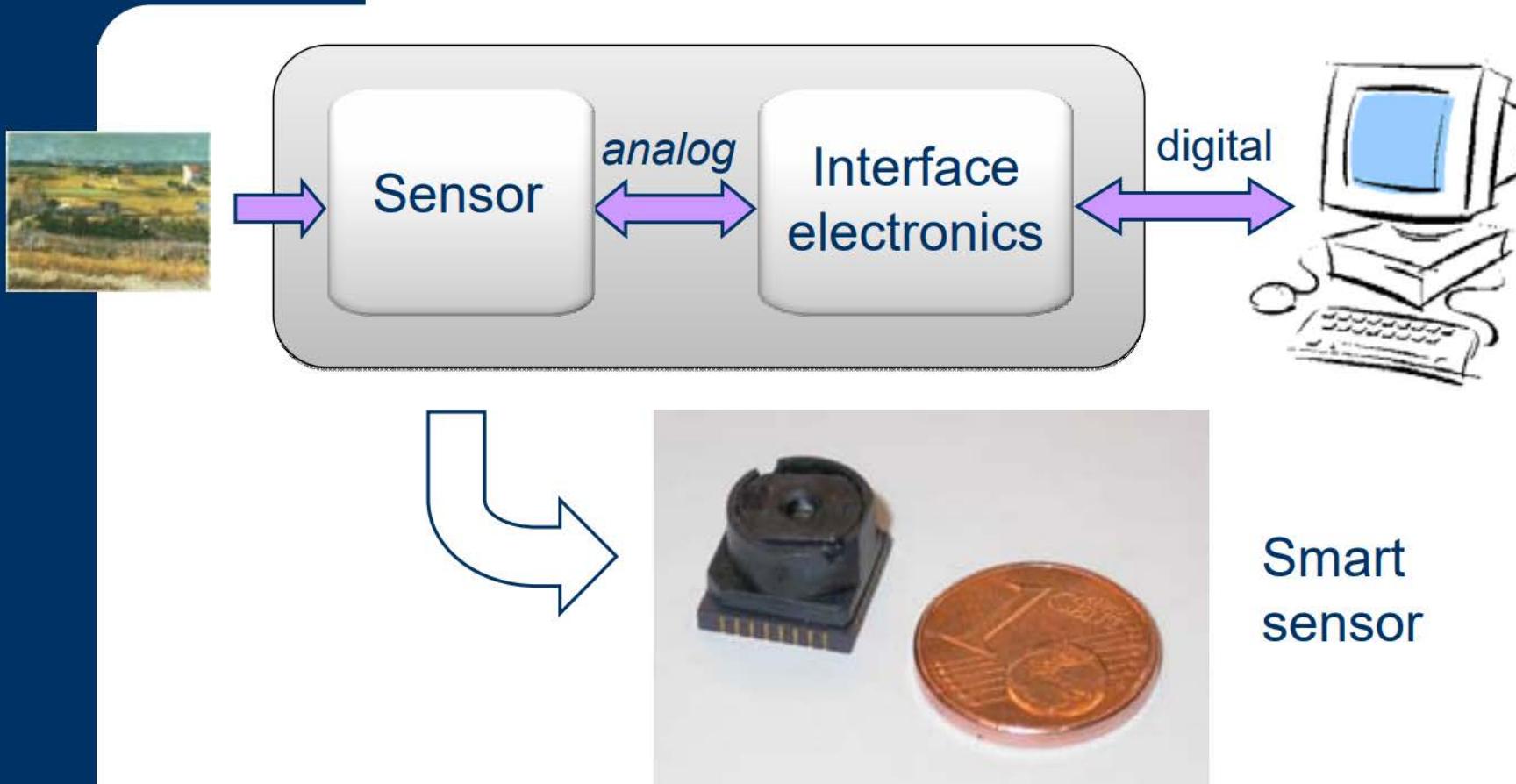
Places

Bottom view

Source: Mona Spiridon, Bruce Fischl, Nancy Kanwisher

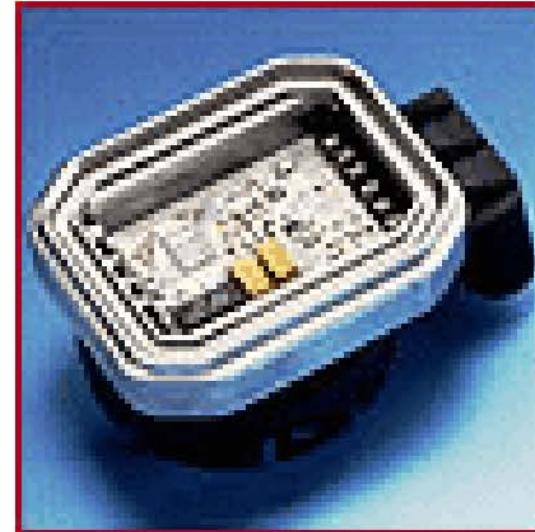
# We need (smart) sensors!

ET8.017  
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- Analog-to-digital conversion ⇒ Interface electronics
- Smart sensor = Sensor system in a package

Automotive application – airbag crash detection



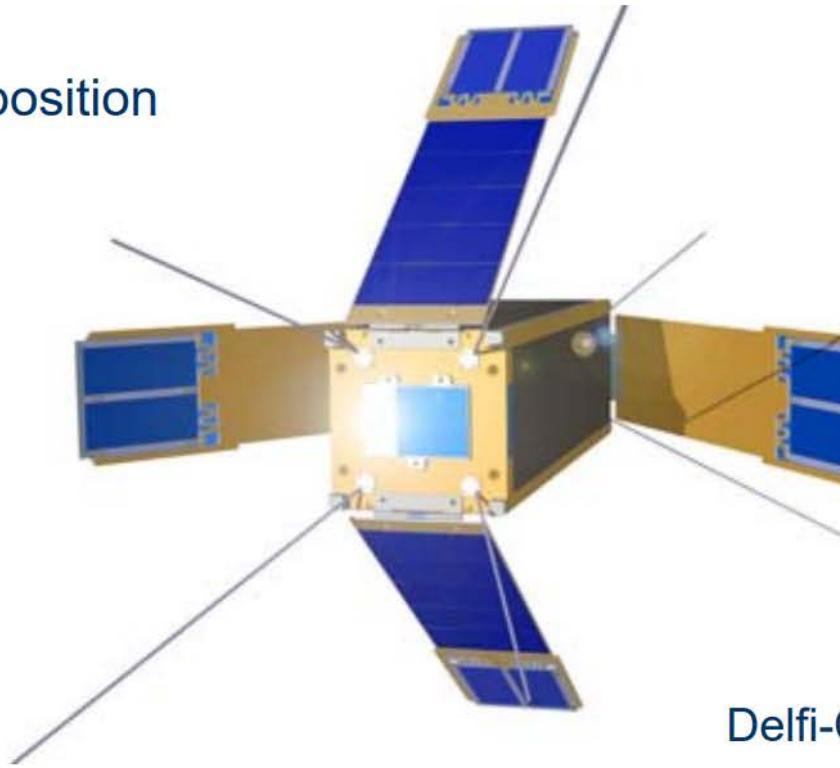
Airbag should only operate  
when needed ⇒ crash sensor

Also for:

- side impact
- Non-passengers



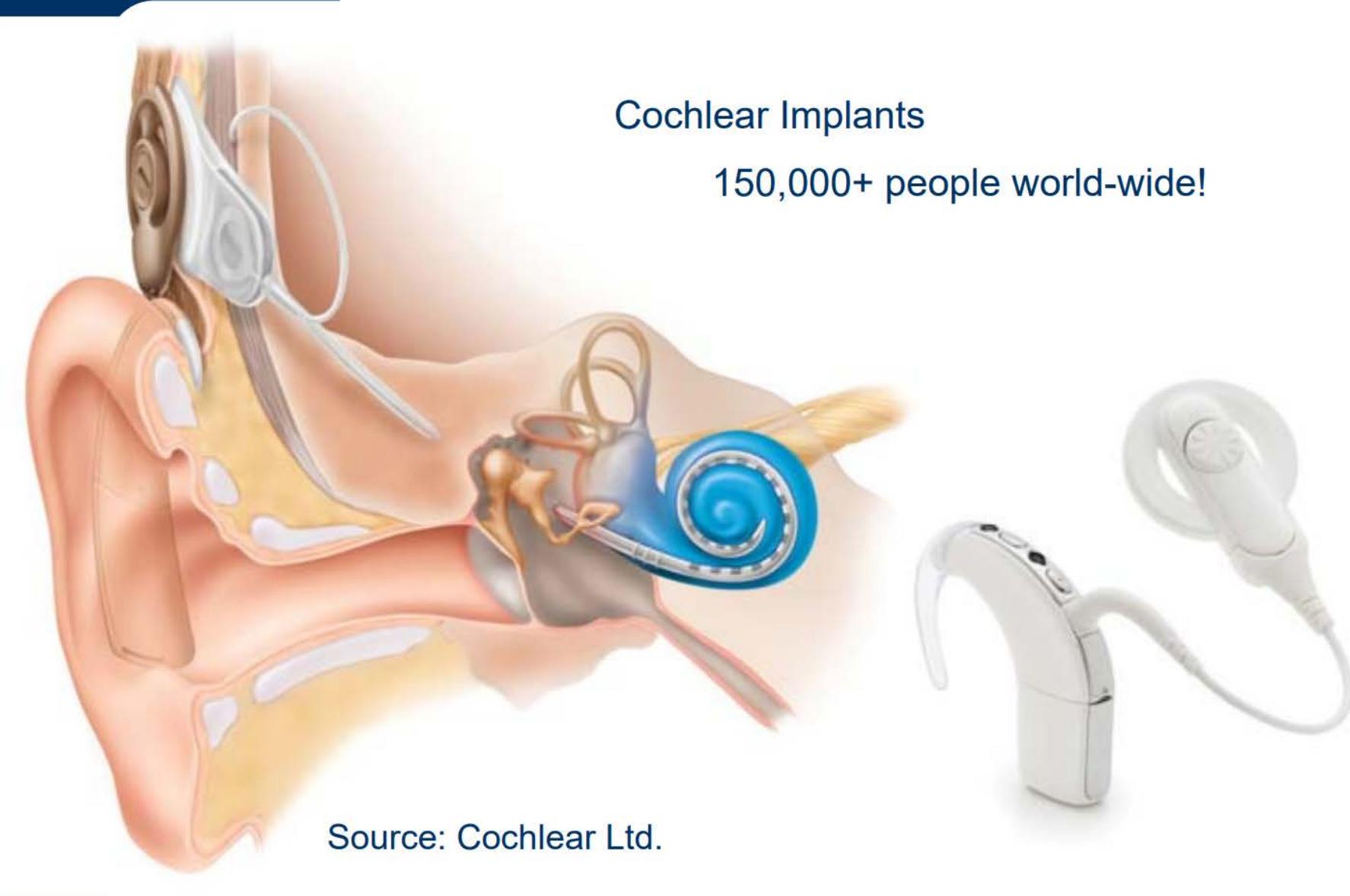
Measuring satellite position



Delfi-C3/MISAT

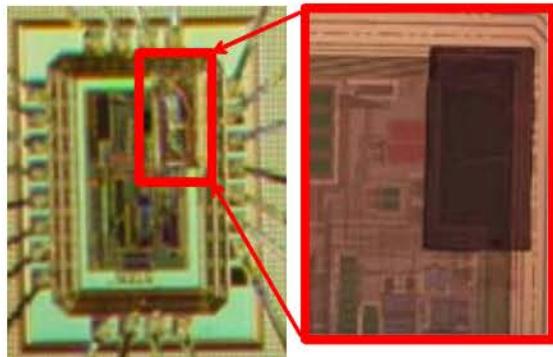
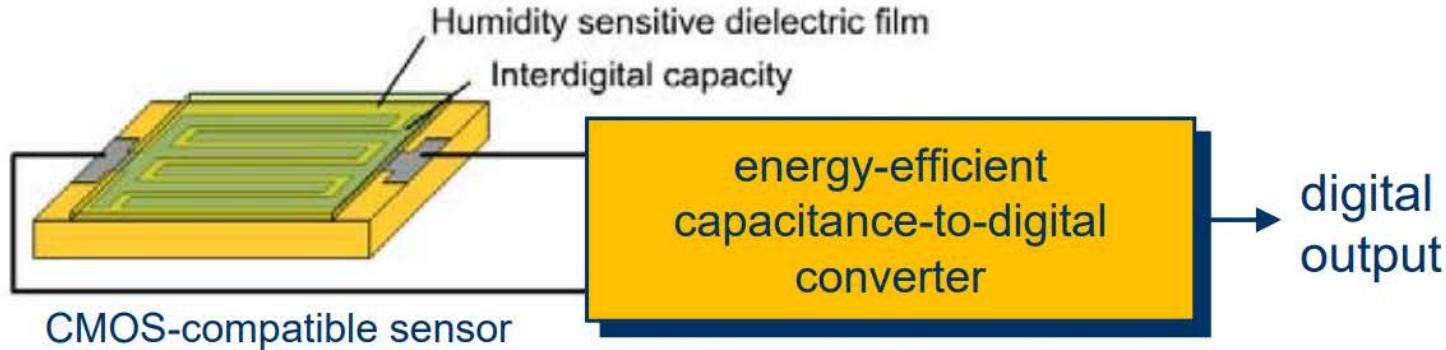
Purpose:

- Solar panel position control
- Antenna directional control
- Satellite attitude control



# Smart Humidity Sensor

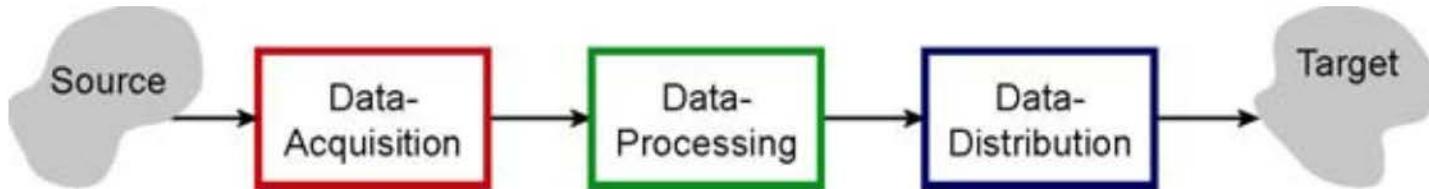
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El. Instr.



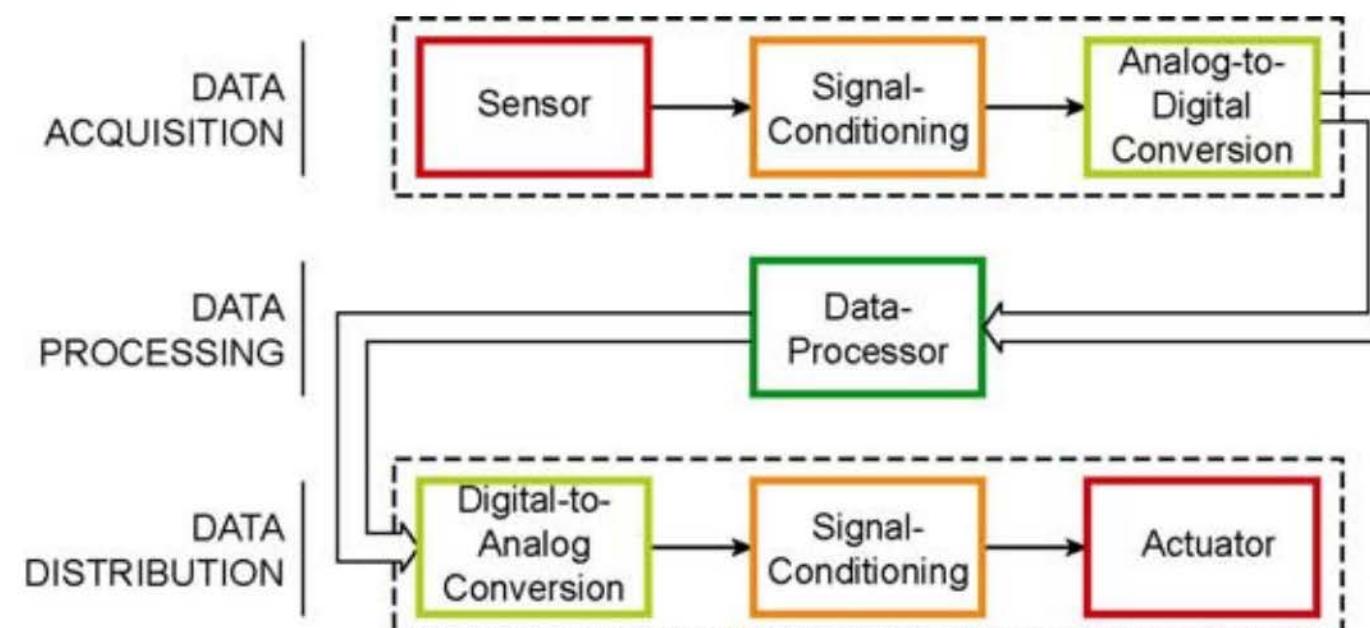
**smart humidity sensor**  
(0.16 $\mu$ m CMOS)

- Humidity sensitive dielectric (NXP) causes capacitance changes
- These are digitized by a capacitance-to-digital converter (delta-sigma converter)
- Achieves resolution of 0.1%RH while consuming only 8.3nJ / meas

## General structure of an instrument



## Components in an instrument



# Learning objectives of this course

- Analyzing **measurement problems**:
  - you'll be able to
    - identify and describe a measurement problem
    - translate a measurement problem to measurable quantities
    - estimate whether a quantity is measurable under certain conditions
- Analyzing and interpreting **measurement results**:
  - you'll be able to
    - identify and describe sources of error

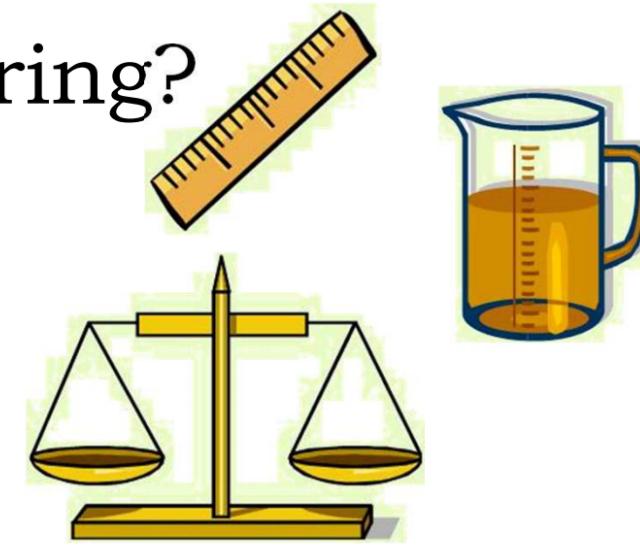


# Learning objectives of this course

- Realization of simple measurement set-ups:
  - you'll be able to
    - apply **sensors** to measure non-electric quantities
    - apply simple **signal processing circuits** for sensor read-out
- Skillful use of **measurement instruments**:
  - you'll be able to
    - describe the operating principle of common instruments for electrical measurements
    - compare available instruments based on quality and accuracy



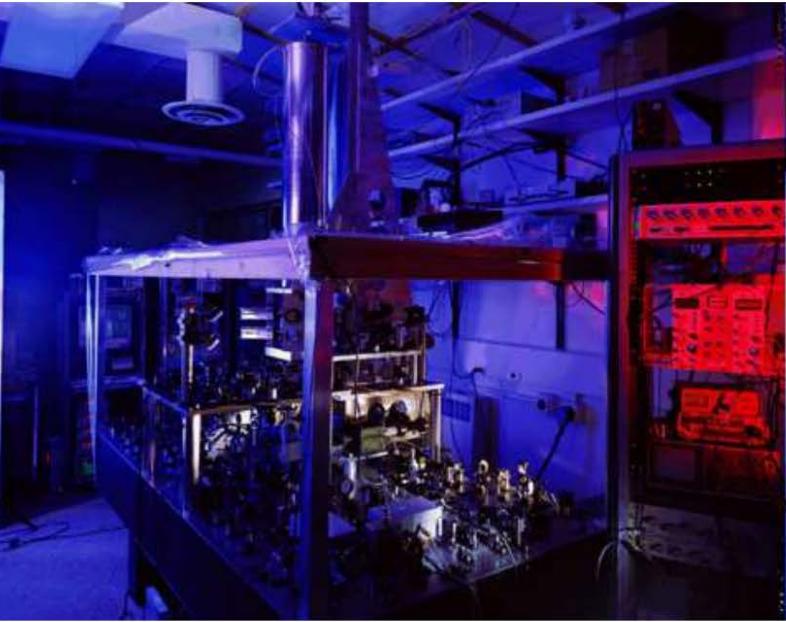
# What exactly is measuring?



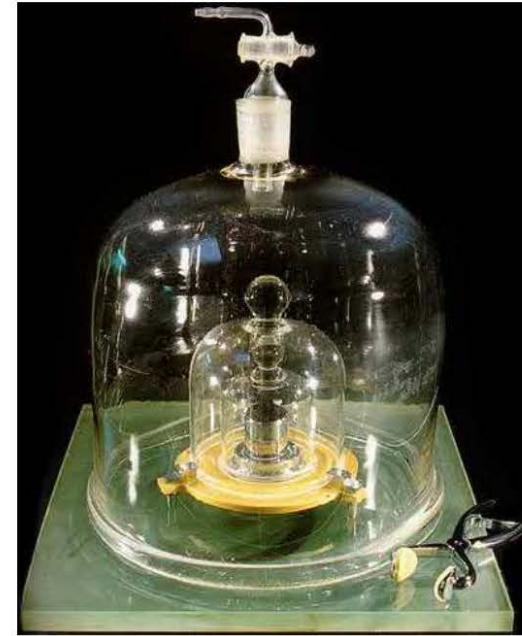
- measuring = determining the value of a quantity
- quantity = property of a phenomenon or object that can be qualitatively distinguished, and quantitatively determined
  - length, time, mass, temperature, electrical resistance

# Standards

- Objective, comparable measurements require **standards**

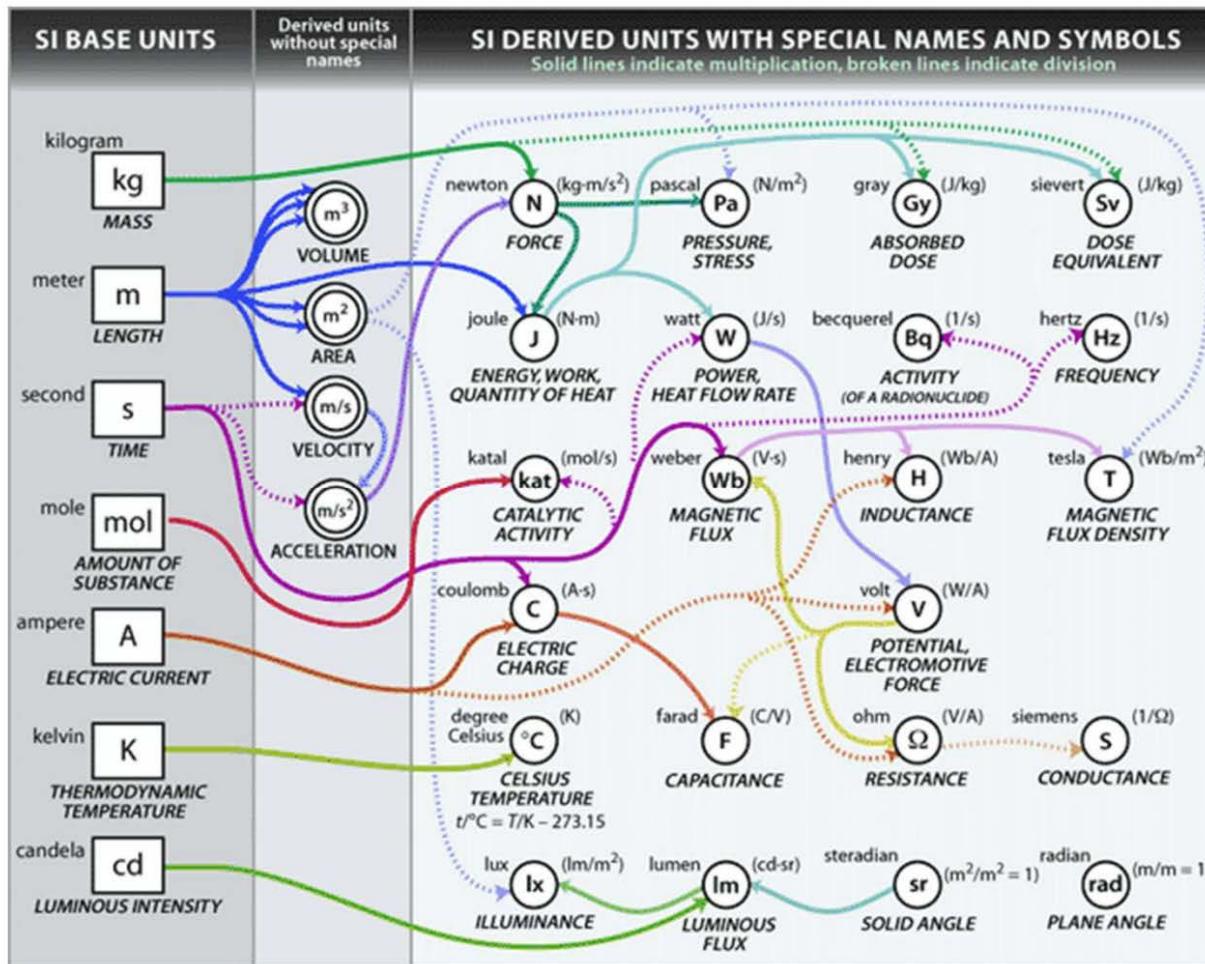


NIST-F1 time- and frequency standards:  
 $1\text{s} = 9.191.631.770$  periods of the resonance  
frequency of a Cs-133 atom



Copy of the *international prototype kilogram*  
(cylinder of 90% platinum and 10% iridium)

# International System of Units (SI)



# Kilograms vs. pounds: “The Gimli Glider”

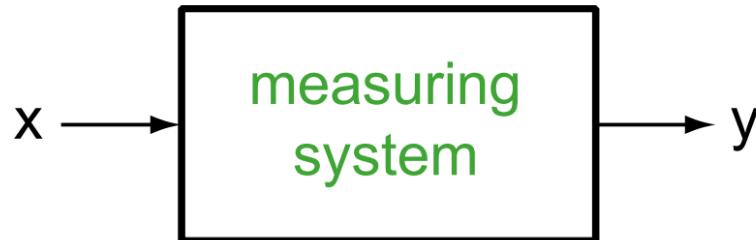
<http://www.youtube.com/watch?v=4yvUi7OAOL4>

- 1983: Canada switches from imperial units to metric
- Air Canada flight 143: mistake with the fuel transfer...
  - 22.300 kg needed for the flight
  - 7.682 l left in the tank
    - how many kg is that?
  - the crew use 1.77 lb/l instead of 0.8 kg/l
  - consequence: only 4916 l transferred instead of the required 20088 l
  - emergency landing!!



July 23, 1983: Air Canada flight 143 lands at a closed air force base in Gimli, Canada

# Measurement Uncertainty



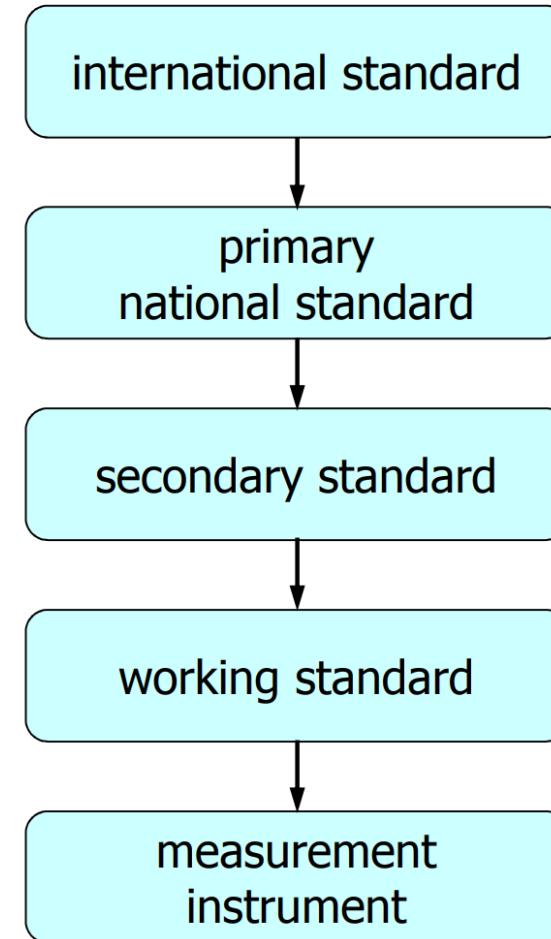
- Every measurement  $y$  of a quantity  $x$  is subject to measurement uncertainty
- Many causes:
  - random variations in the measurement value
  - varying measurement conditions
  - finite resolution / incorrect reading
  - deviations in the transfer of the measurement system
  - poorly defined definition of the quantity to be measured
  - ...

# Uncertainty vs. error

- Measurement uncertainty  $\neq$  measurement error
  - Error: difference between measured value and the 'true' value
  - Uncertainty: quantification of the doubt about the measurement
- Measurement uncertainty can be quantified by
  - a standard deviation:  
"the mass is 100.02147 g with a standard deviation of 0.35 mg"
  - a confidence interval:  
"the mass is  $(100.02147 \pm 0.00079)$  g, at a confidence level of 95%"
- Unknown measurement errors contribute to the measurement uncertainty
- Some measurement errors can be determined, by means of calibration, and be corrected for afterwards.

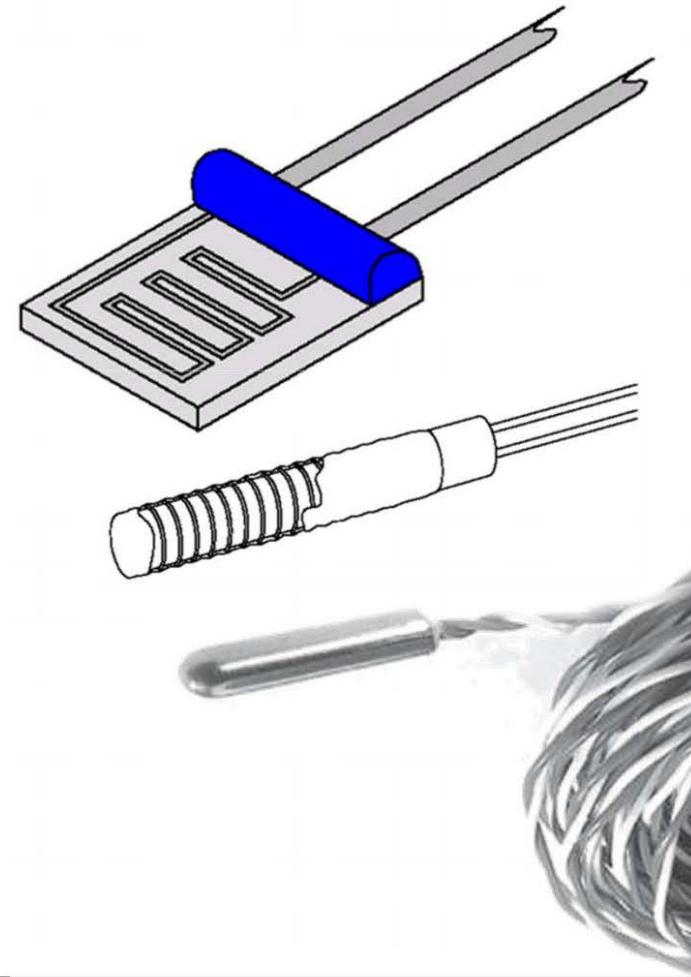
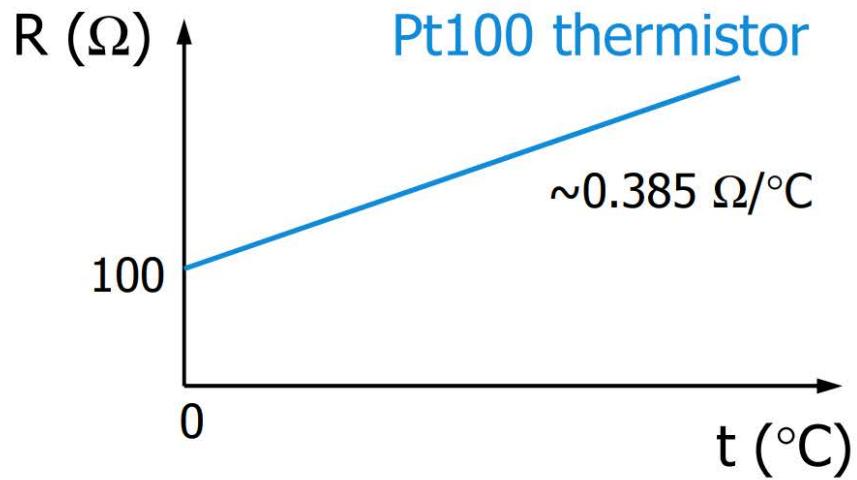
# Calibration

- **Calibration** makes a connection between
  - measurement values produced by a measurement instrument
  - corresponding values realized by standards
- **Calibration procedure:** comparison of an instrument with a (more accurate) measurement standard
- Calibration enables measurements which are **traceable** to standards
  - through an unbroken chain of comparisons
  - with associated specified uncertainties !



# Example: calibration of a platinum thermometer

- PRT: platinum resistance thermometer
- typical **transfer**:

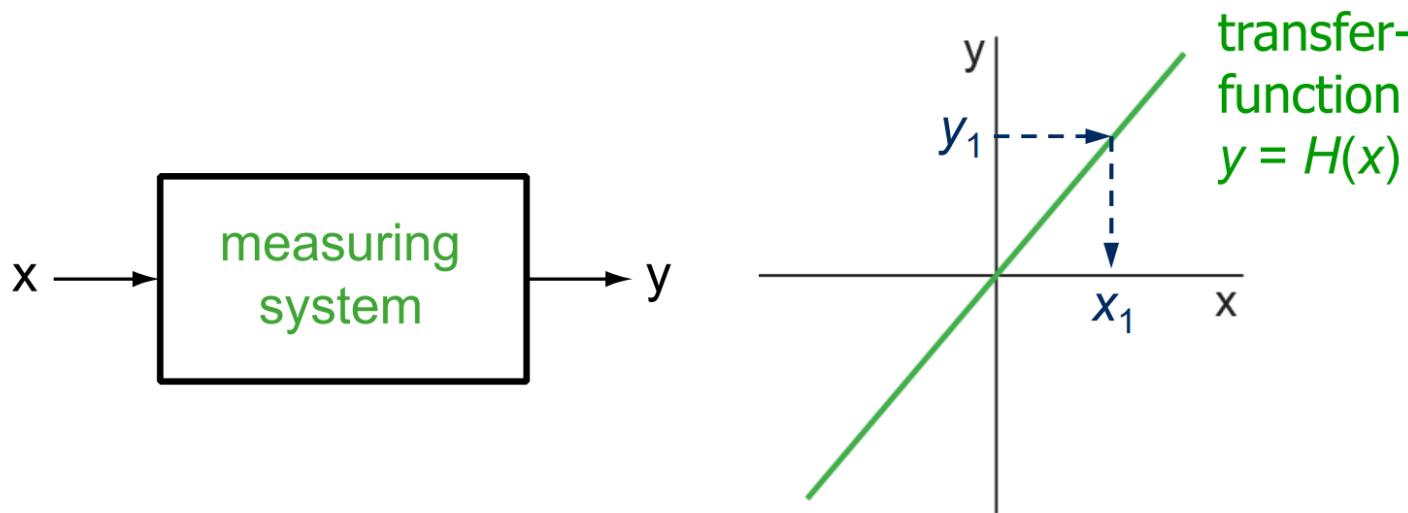


# Example: calibration of a platinum thermometer



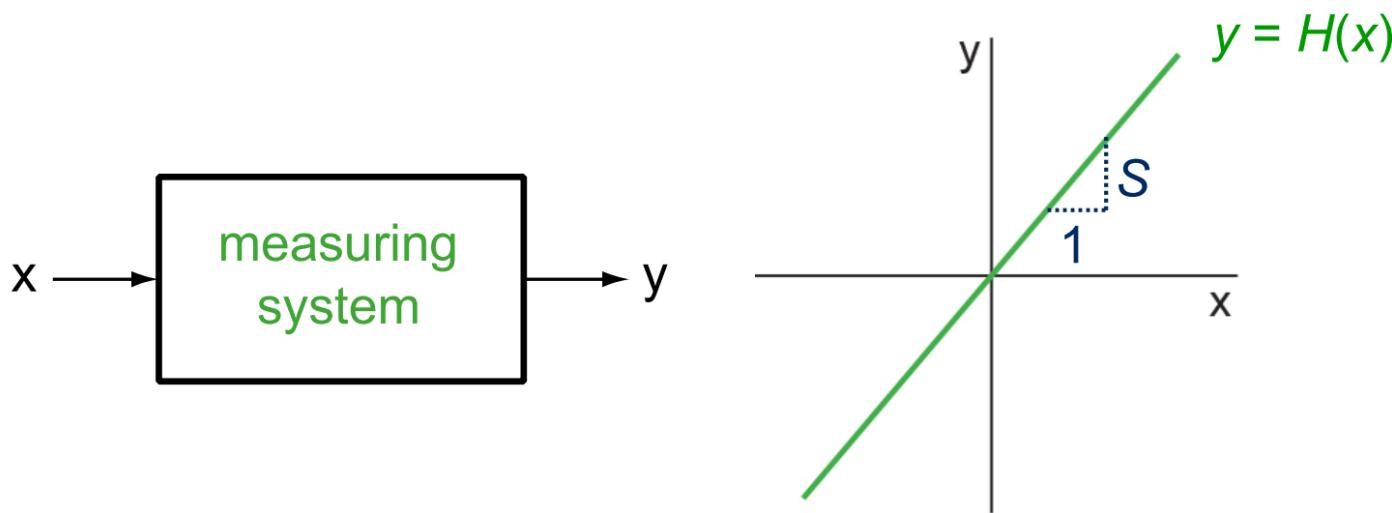
- Calibration procedure:
  - comparison to a more accurate reference thermometer (the working standard) at various calibration temperatures  
⇒ list of measured temperatures and resistance values with measurement uncertainty
  - determination of the coefficients of a formula that relates measured resistance to temperature  
 $\Rightarrow R(t) = R_0 ( 1 + A \cdot t + B \cdot t^2 )$
  - determination of the corresponding measurement uncertainty
- Next, when using the thermometer, this formula will be used to translate a measured resistance into temperature

# Transfer of a measurement system



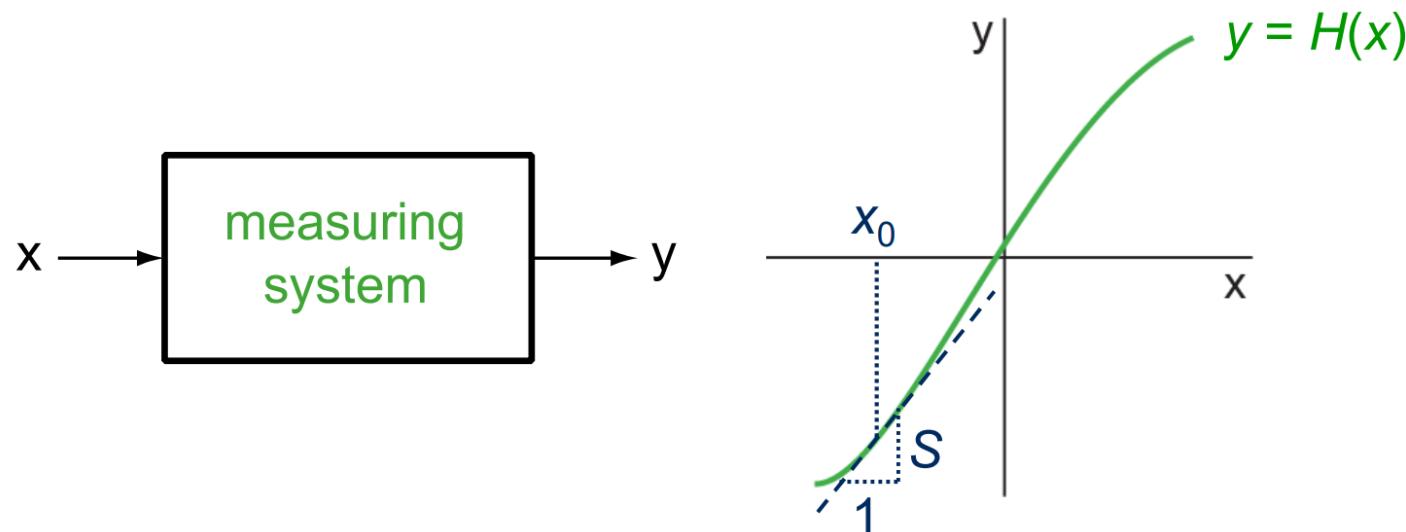
- Using the transfer function  $H$ , output signal (indication)  $y_1$  can be translated back to a measurement value  $x_1$

# Sensitivity



- **Sensitivity:**  $S = \Delta y / \Delta x$
- Ideal linear transfer: sensitivity  $S = y / x$

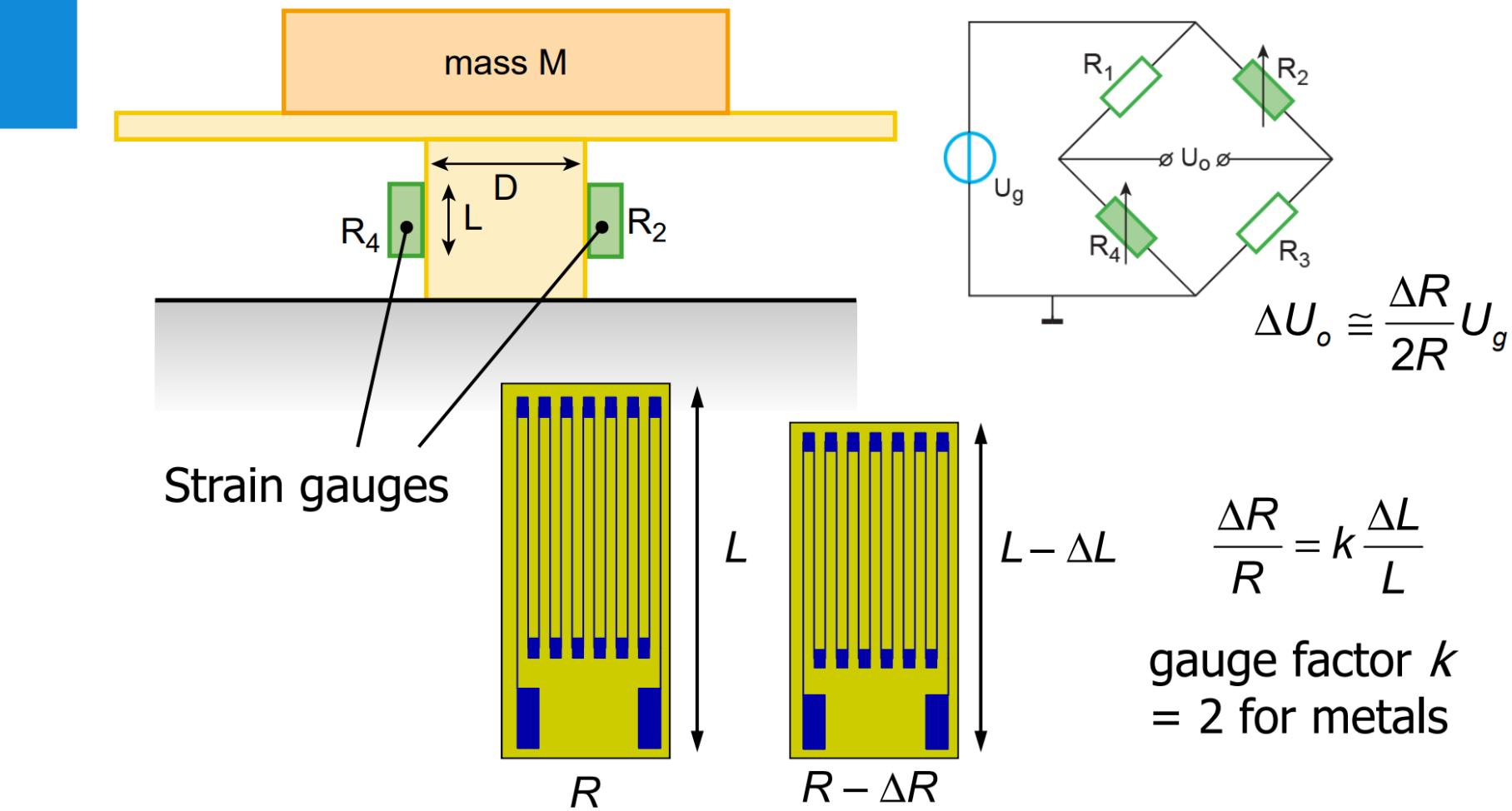
# Differential Sensitivity



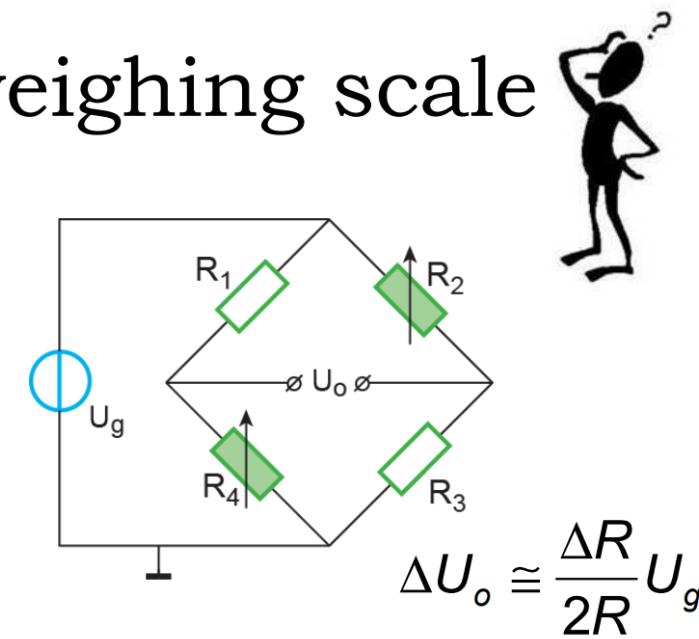
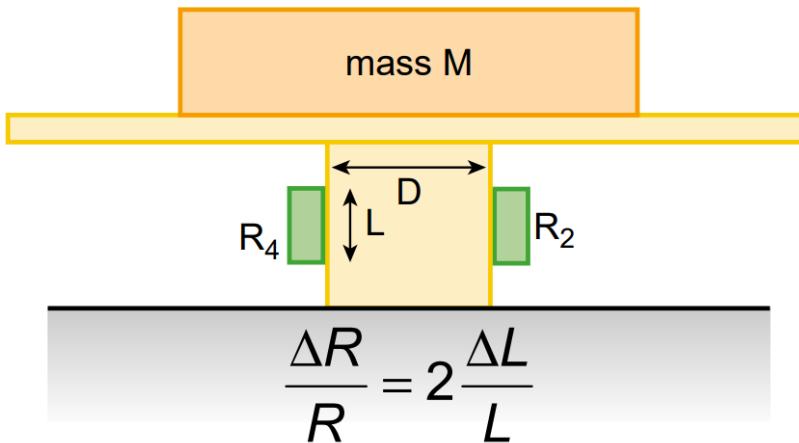
- Non-linear transfer  
⇒ **differential** sensitivity round  $x_0$ :

$$S = \left. \frac{dy}{dx} \right|_{x=x_0} = H'(x_0)$$

# Sensitivity example: weighing scale



# Sensitivity example: weighing scale

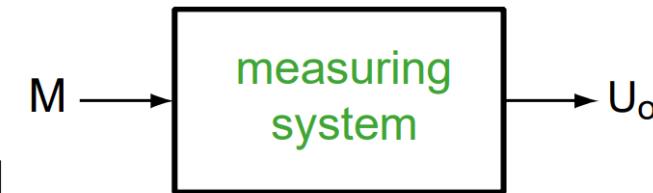


Given: the source voltage  $U_g = 10 \text{ V}$

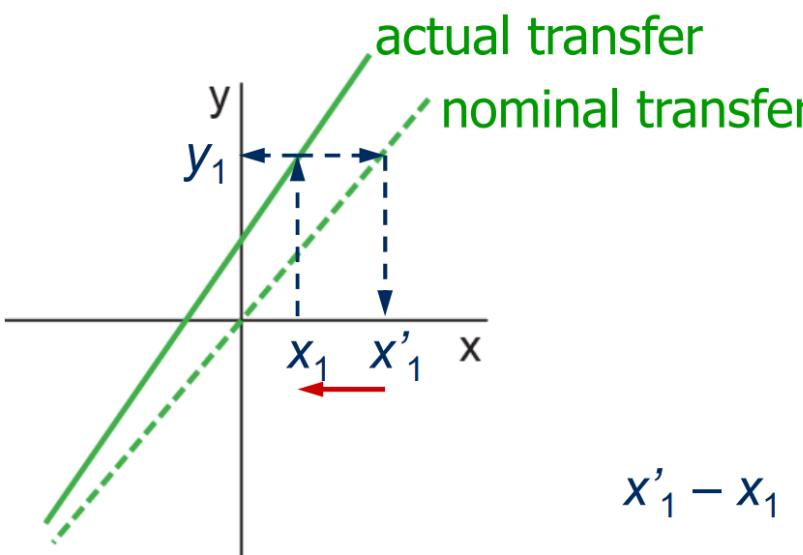
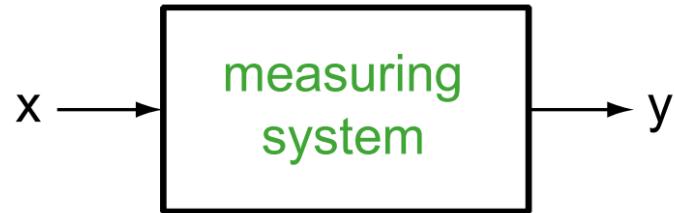
the relative sensitivity of the length change is

$$\frac{\Delta L / L}{\Delta M} = 6.2 \cdot 10^{-7} \text{ kg}^{-1}$$

Determine the sensitivity  $S = \Delta U_o / \Delta M$  [V/kg] of the measurement system



# Measurement errors due to deviations in the transfer

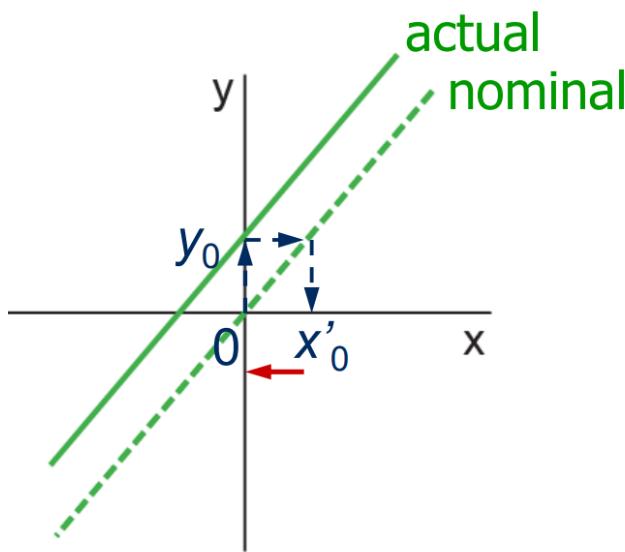


- $x_1$  actual value of quantity to be measured
- $y_1$  output signal of measurement system
- $x'_1$  measured value determined based on nominal transfer

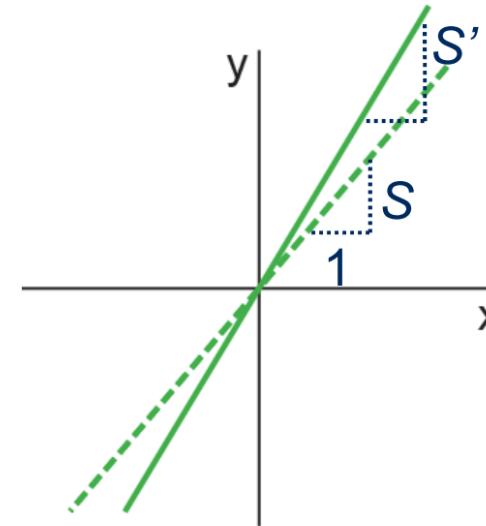
$x'_1 - x_1$  **measurement error**

# Deviation in linear transfer

**Offset error**

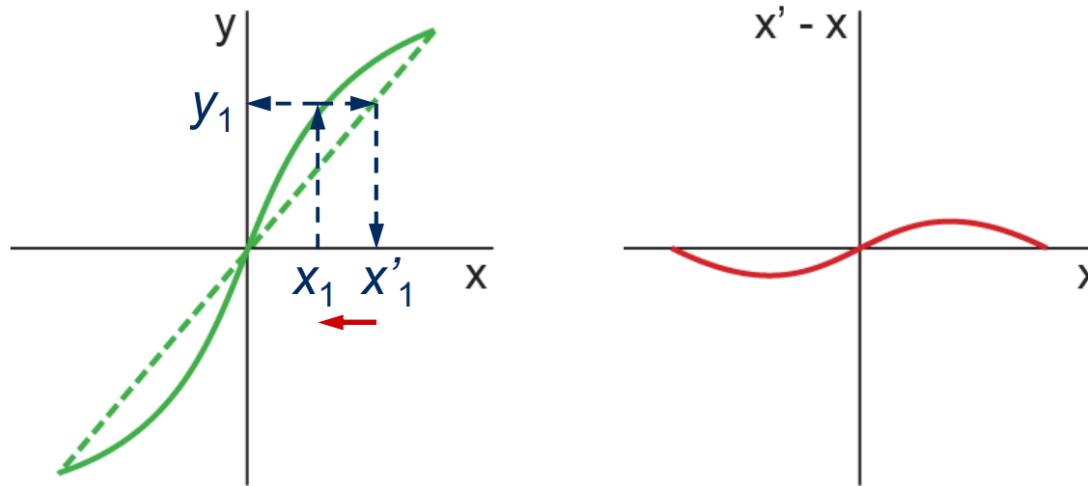


**Gain error (sensitivity error)**



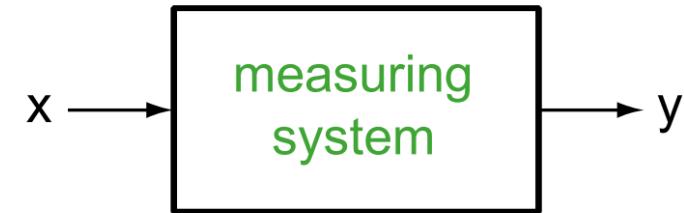
# Non-linearity

- A non-linear transfer will give measurement errors if the nominal transfer is assumed to be linear
- Integral non-linearity:

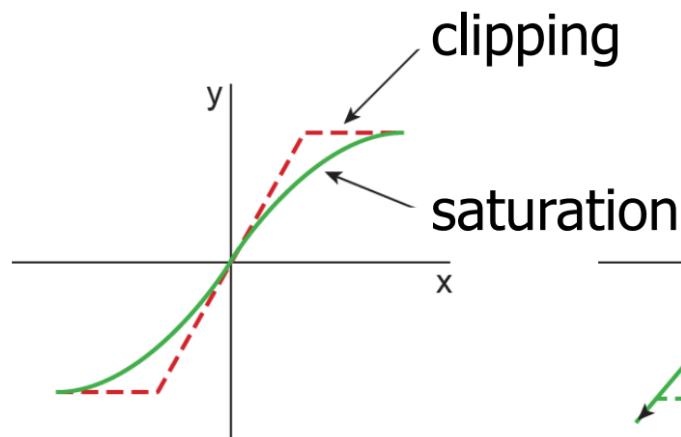


# Ambiguity

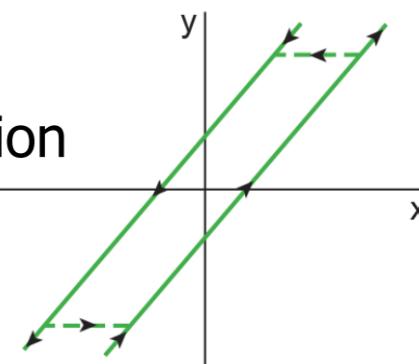
- No one-to-one relation between the quantity to be measured  $x$  and the output signal  $y$



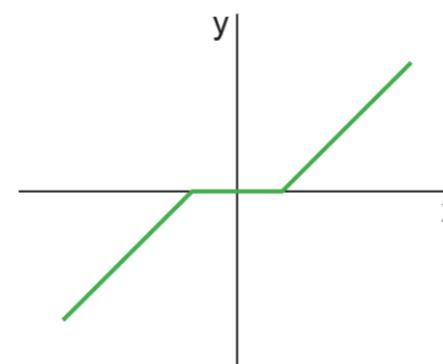
**saturation**



**hysteresis**



**dead zone**



# Ambiguity

saturation  
hysteresis  
dead zone



- Moving coil meter with friction

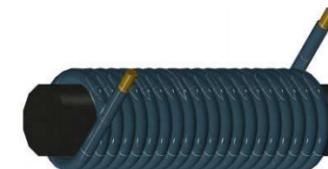
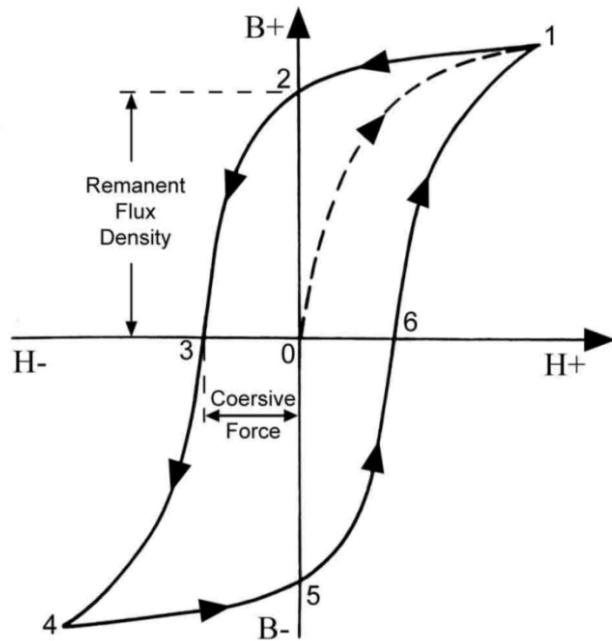


# Ambiguity

saturation  
hysteresis  
dead zone



- Magnetisation of a ferromagnetic core

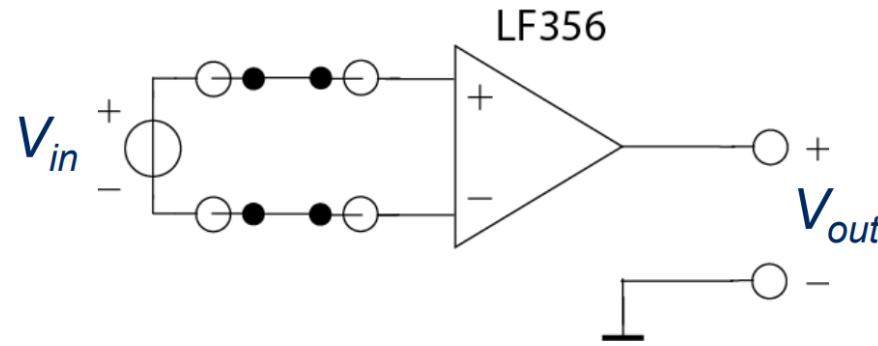


# Ambiguity

saturation  
hysteresis  
dead zone

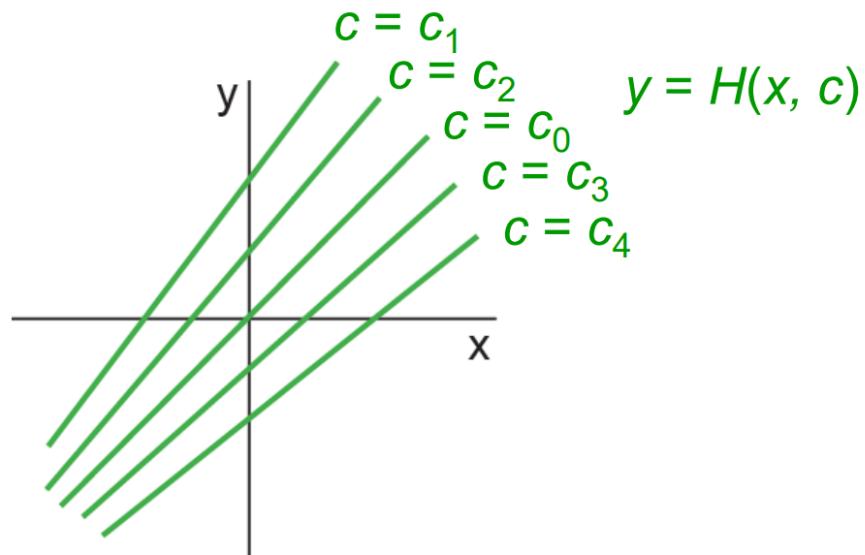
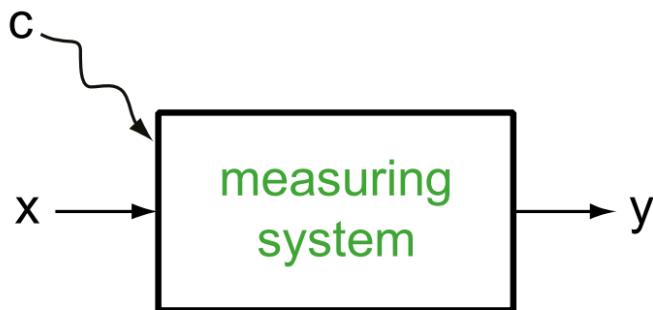


- Opamp



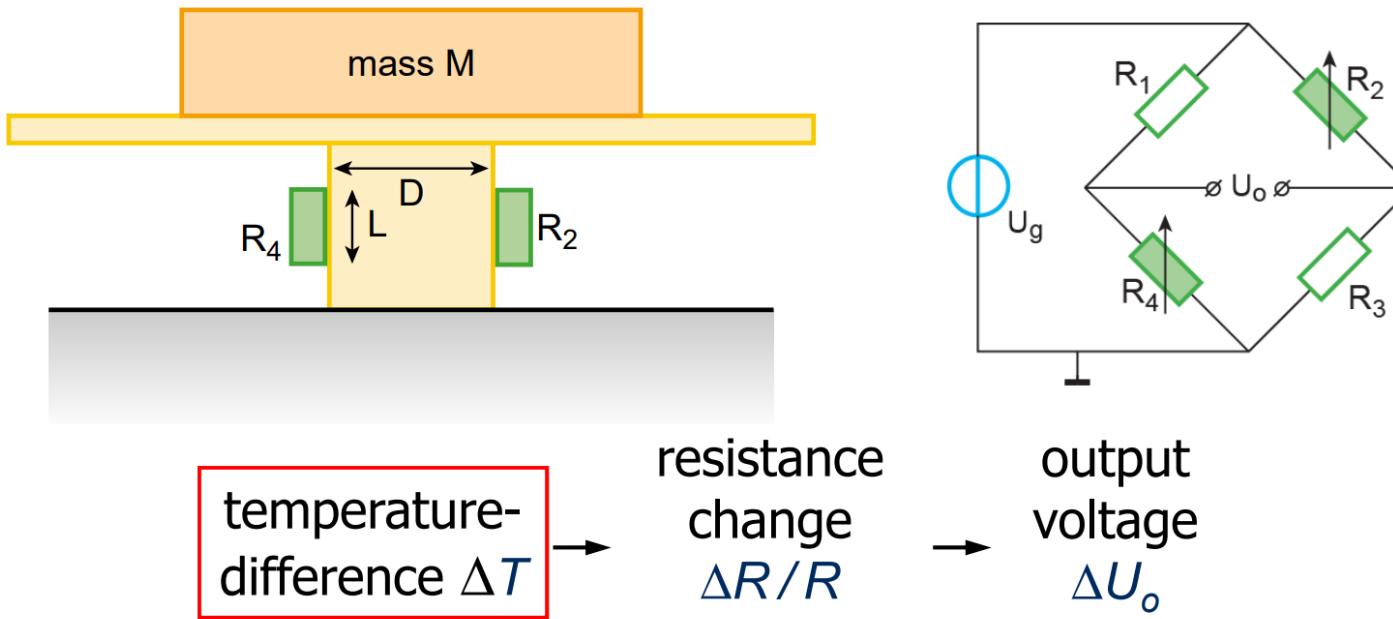
# Cross-sensitivity

- Unwanted sensitivity to an **influence quantity  $c$**



- Ideally:  $S_c^y = 0$

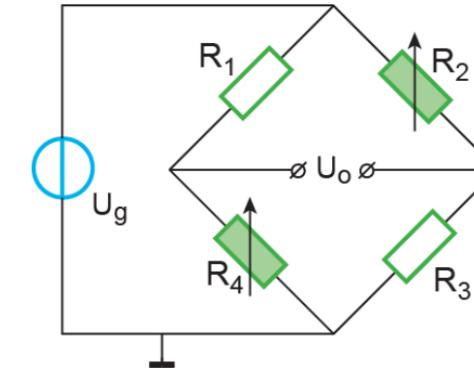
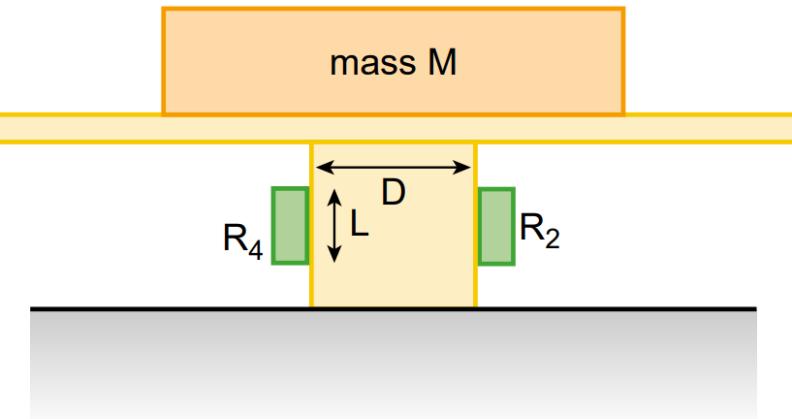
# Cross-sensitivity ex.: weighing scale



- Temperature sensitivity resistors typically expressed as

$$\text{temperature coefficient: } \alpha = \frac{1}{R} \cdot \frac{dR}{dT} [\text{K}^{-1}] \quad \Rightarrow \frac{\Delta R}{R} = \alpha \cdot \Delta T$$

# Cross-sensitivity ex.: weighing scale



temperature-difference  $\Delta T$

resistance change  $\Delta R/R$

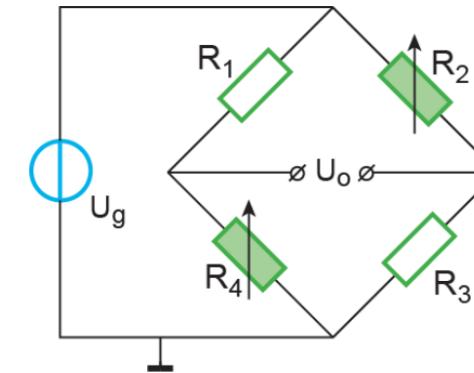
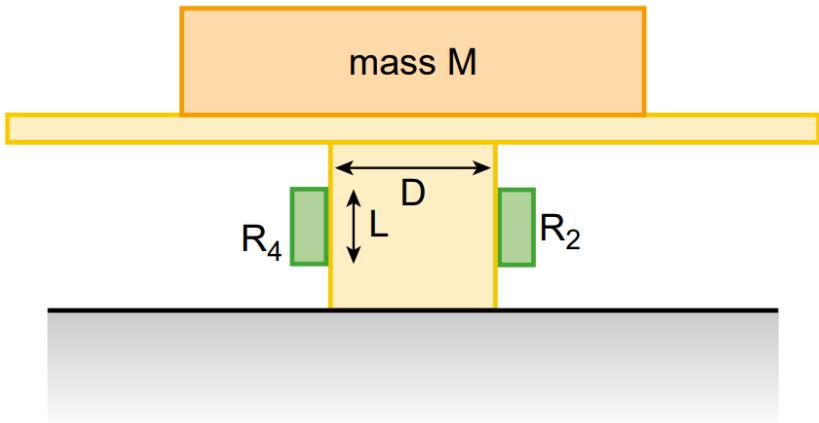
output voltage  $\Delta U_o$

$$\frac{\Delta R}{R} = \alpha \cdot \Delta T$$

$$\Delta U_o \approx \frac{\Delta R}{2R} U_g$$

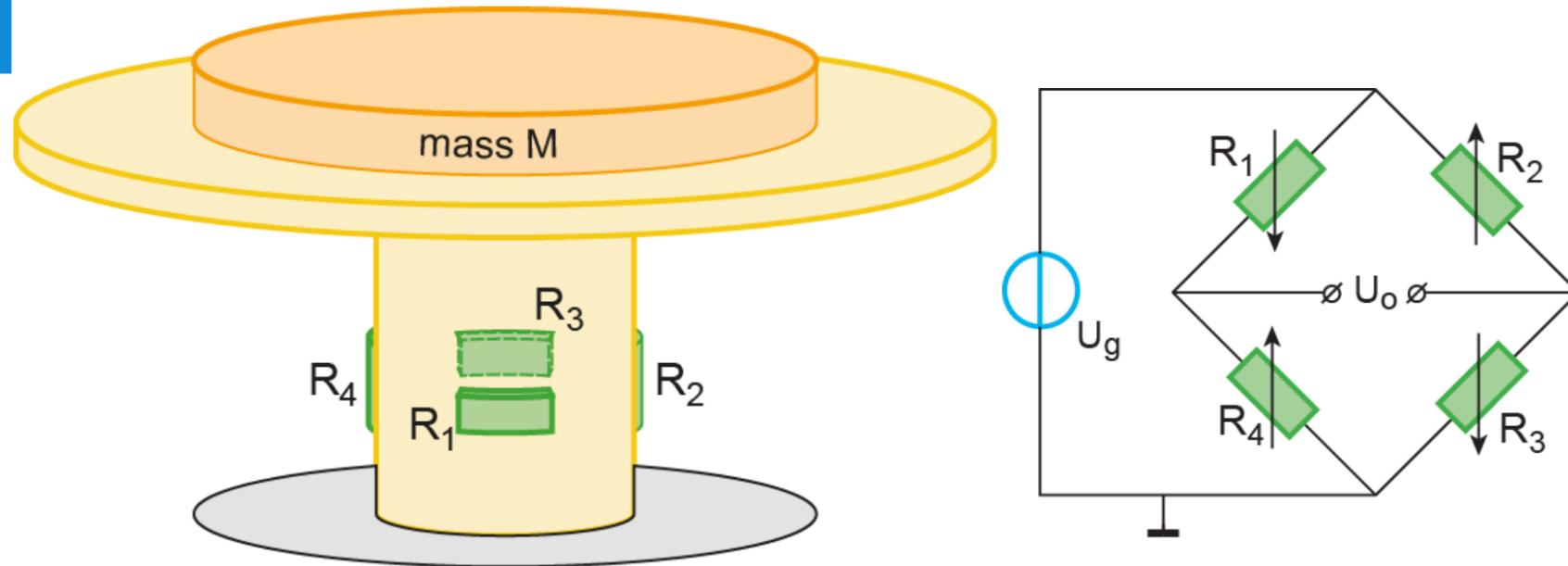
- Cross sensitivity:  $S_{temp} = \frac{\Delta U_o}{\Delta T} = \frac{\alpha \cdot U_g}{2}$

# Cross-sensitivity ex.: weighing scale



- Cross-sensitivity:  $S_{temp} = \frac{\Delta U_o}{\Delta T} = \frac{\alpha \cdot U_g}{2}$
  - Let:  $\alpha = 2,0 \cdot 10^{-5} K^{-1}$ ,  $U_g = 10 V \Rightarrow S_{temp} = 0,10 mV/K$
  - Compare to earlier found  $S_{massa} = 6,2 \mu V / kg$
- } error:  
16 kg / K !!

# Cross-sensitivity ex.: weighing scale



- **Compensation** for temperature differences:  
4 strain gauges mounted to the base  $\Rightarrow$  small  $\Delta T$

# Measurement errors due to aging

- Measurement systems change over time  
⇒ uncertainty increases  
⇒ frequent calibration is needed



**Accuracy Specifications**  $\pm$  (% of reading + % of range)

Function	Range <sup>3</sup>	24 Hour <sup>2</sup> $23^{\circ}\text{C} \pm 1^{\circ}\text{C}$	90 Day $23^{\circ}\text{C} \pm 5^{\circ}\text{C}$	1 Year $23^{\circ}\text{C} \pm 5^{\circ}\text{C}$
<b>DC voltage</b>	100.0000 mV	0.0030 + 0.0030	0.0040 + 0.0035	0.0050 + 0.0035
	1.000000 V	0.0020 + 0.0006	0.0030 + 0.0007	0.0040 + 0.0007
	<b>10.00000 V</b>	<b>0.0015 + 0.0004</b>	<b>0.0020 + 0.0005</b>	<b>0.0035 + 0.0005</b>
	100.0000 V	0.0020 + 0.0006	0.0035 + 0.0006	0.0045 + 0.0006
	1000.000 V	0.0020 + 0.0006	0.0035 + 0.0010	0.0045 + 0.0010

# Resolution



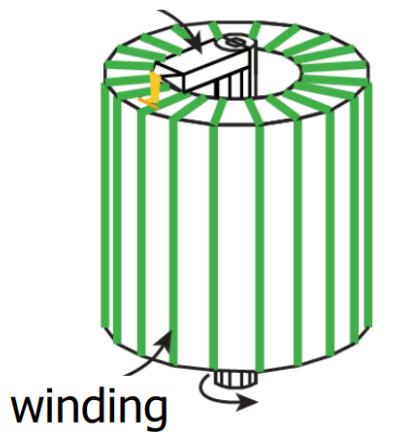
- **Resolution:** smallest change in x that causes a noticeable change in y
- Expressed in two ways:
  - absolute:  $\Delta x$
  - relative to the full scale:  $\Delta x / x_{max}$   
often in bits:  $-2\log(\Delta x / x_{max})$
- Example: 4½-digit display, 200V range
  - $\Delta x = 0.01 \text{ V}$
  - $\Delta x / x_{max} = 0.01 \text{ V} / 199.99 \text{ V} = 5 \cdot 10^{-5}$   
in bits:  $-2\log(5 \cdot 10^{-5}) = 14.3 \text{ bits}$





# Resolution examples

- Resolution determined by sensor: wirewound potentiometer  
sliding contact (wiper)

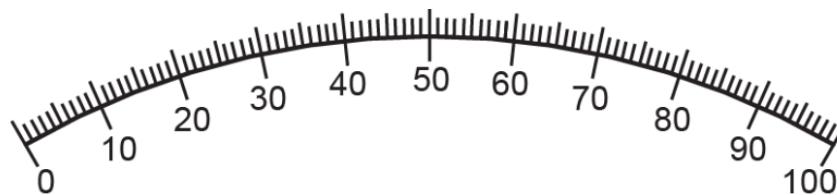


1000 windings



# Resolution examples

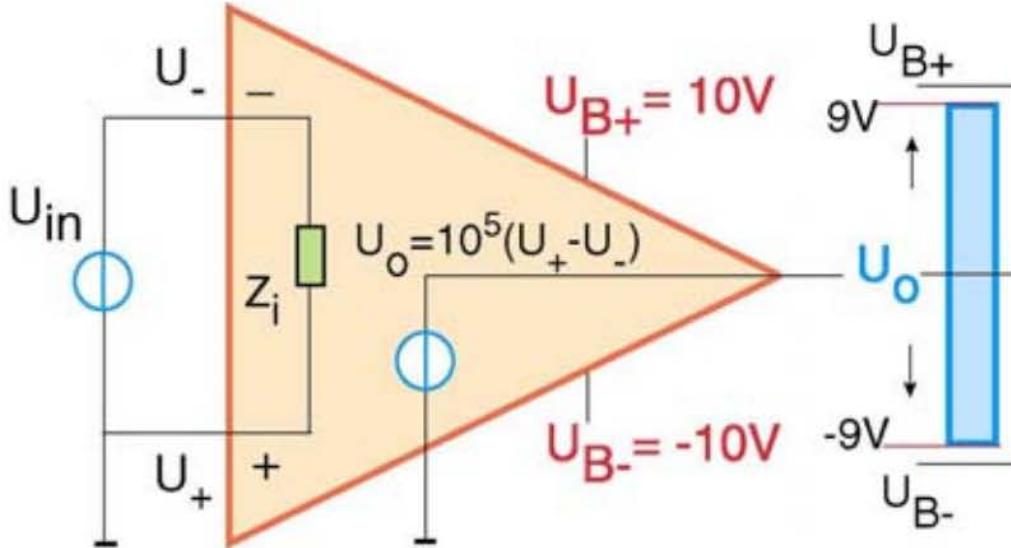
- Resolution determined by display:



# Summary

- Measuring = determining the value of a quantity
  - measurement requires international standards
  - calibration is needed for traceable, comparable measurements
  - every measurement is subject to measurement uncertainty
- Measurement system: converts quantity to be measured  $x$  into usable output signal  $y$  (often electrical, digital)
  - Data acquisition:  $x \rightarrow$  sensor  $\rightarrow$  signal conditioning  $\rightarrow$  ADC  $\rightarrow y$
  - Characterized by transfer  $y = H(x)$  with sensitivity  $H'(x)$
  - Deviations in the transfer can lead to measurement errors:  
non-linearity, ambiguity, cross sensitivity, finite resolution

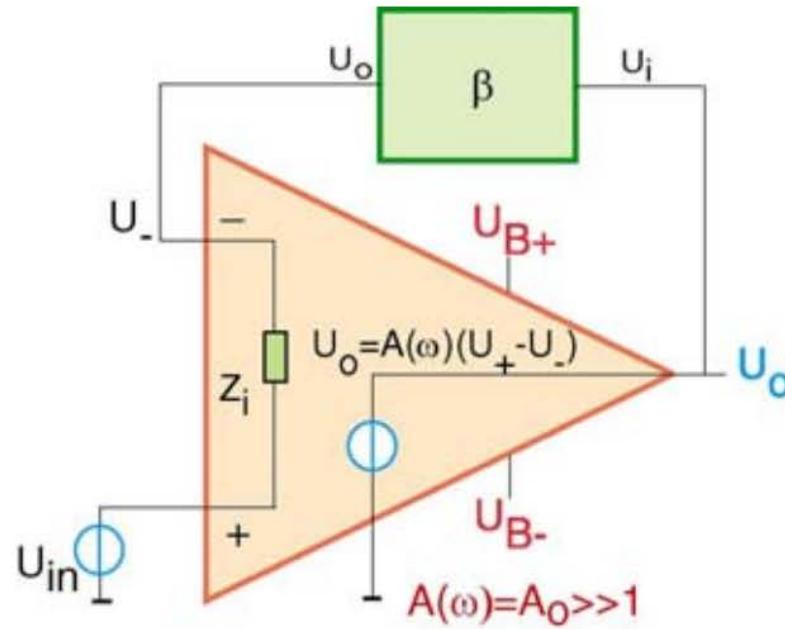
## Using the open-loop gain



$$U_{in,max} = U_{o,max}/10^5 = 9/10^5 = 90 \mu V \ll U_{offset}$$

⇒ Should be used in a feedback configuration

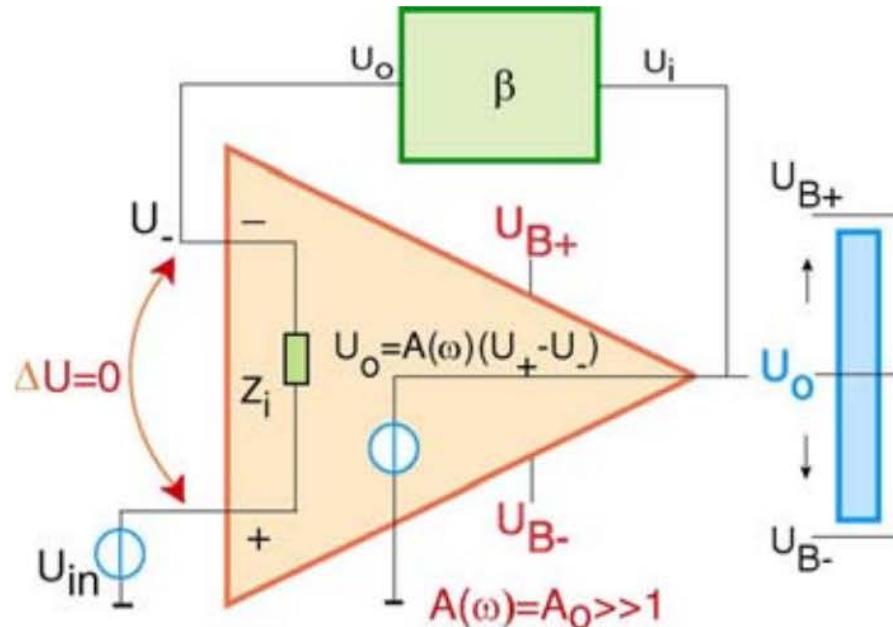
Opamp in feedback - Principle



Stability concerns !

## Read-out using Operational Amplifiers

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A finite value for  $U_o$  and a very high open-loop gain implies:  $U_+ - U_- = 0$ .

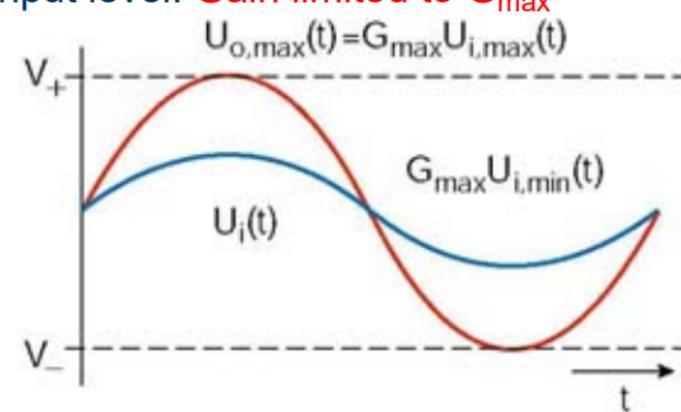
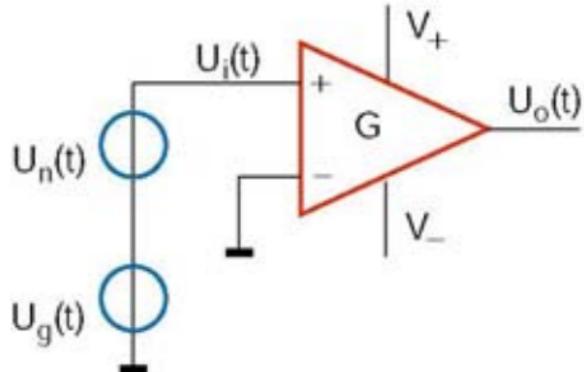
The feedback loop ensures that the value of  $U_o$  is such that:  $U_- = U_+$

This implies that the potential at the opamp's non-inverting input is **virtually copied** to the inverting input

**Definition: The minimum level of the input quantity that can be reproducibly measured at specified inaccuray/SNR (default: SNR= 0 dB).**

A practical signal is specified by its dynamic range: ratio between minimum and maximum signal level occurring within inaccuracy specification

Constraint due to maximum possible input level: **Gain limited to  $G_{max}$**

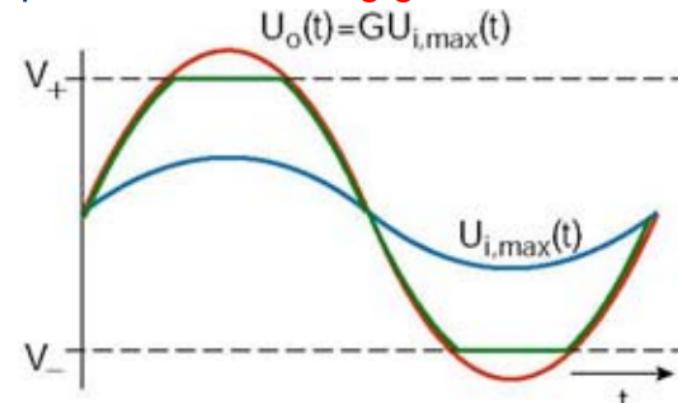
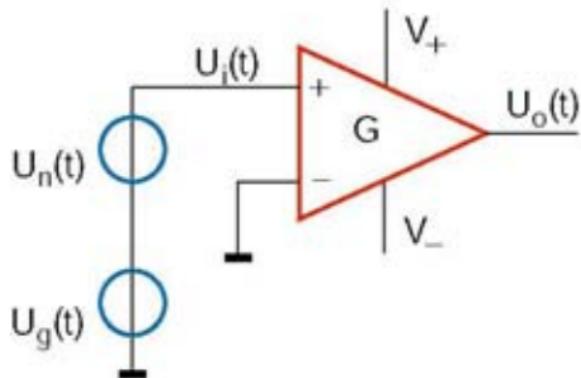


The maximum level of the input signal sets the maximum gain. However, the lower end of the input signal also results in a constraint.

**Definition:** The minimum level of the input quantity that can be reproducibly measured at specified inaccuracy/SNR (default: SNR= 0 dB).

A practical signal is specified by its dynamic range: ratio between minimum and maximum signal level occurring within inaccuracy specification

Constraint due to maximum possible input level: **Increasing gain G**

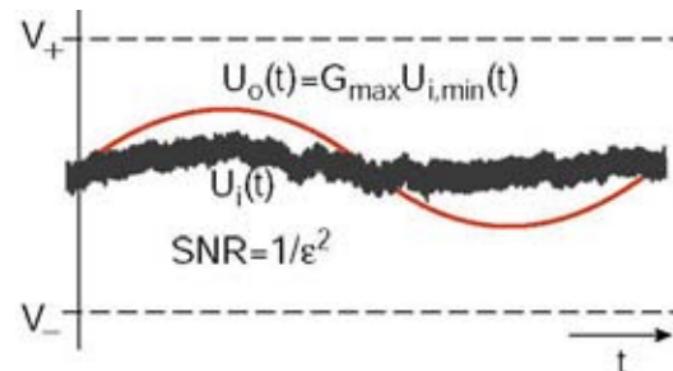
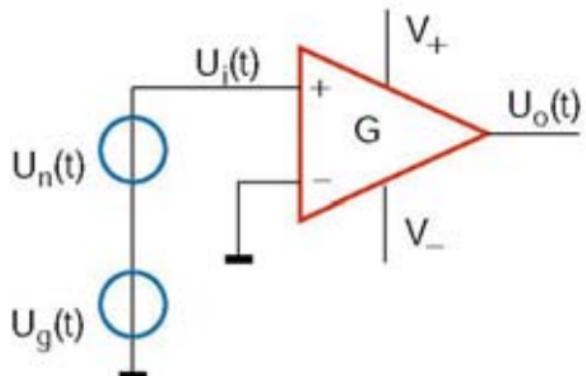


Maximum output voltage would be higher than system can deliver  $\Rightarrow$  saturation at maximum possible output level: **Gain limited to  $G_{max}$**

**Definition:** The minimum level of the input quantity that can be reproducibly measured at specified inaccuracy/SNR (default: SNR= 0 dB).

However, the minimum input signal is also limited at given inaccuracy (or Signal-to-Noise Ratio-SNR) specification when considering noise and interference

At  $G_{\max}$  and specified inaccuracy,  $\varepsilon$ :



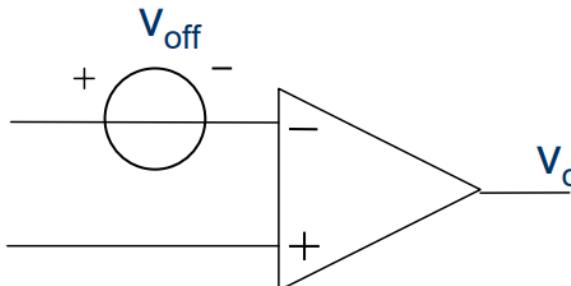
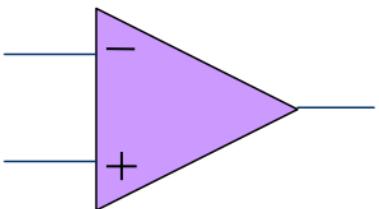
Note: output (red line) is drawn WITHOUT noise

System sensitivity is not limited by the gain one can implement in the signal conditioning, but rather by the detection limit.

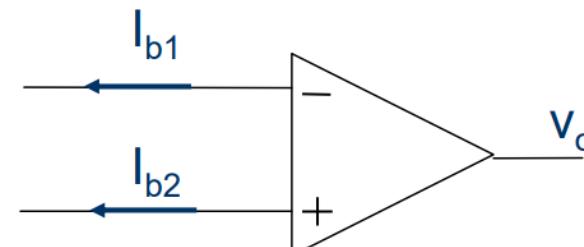
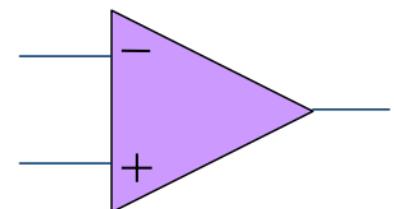
Procedure for finding the detection limit:

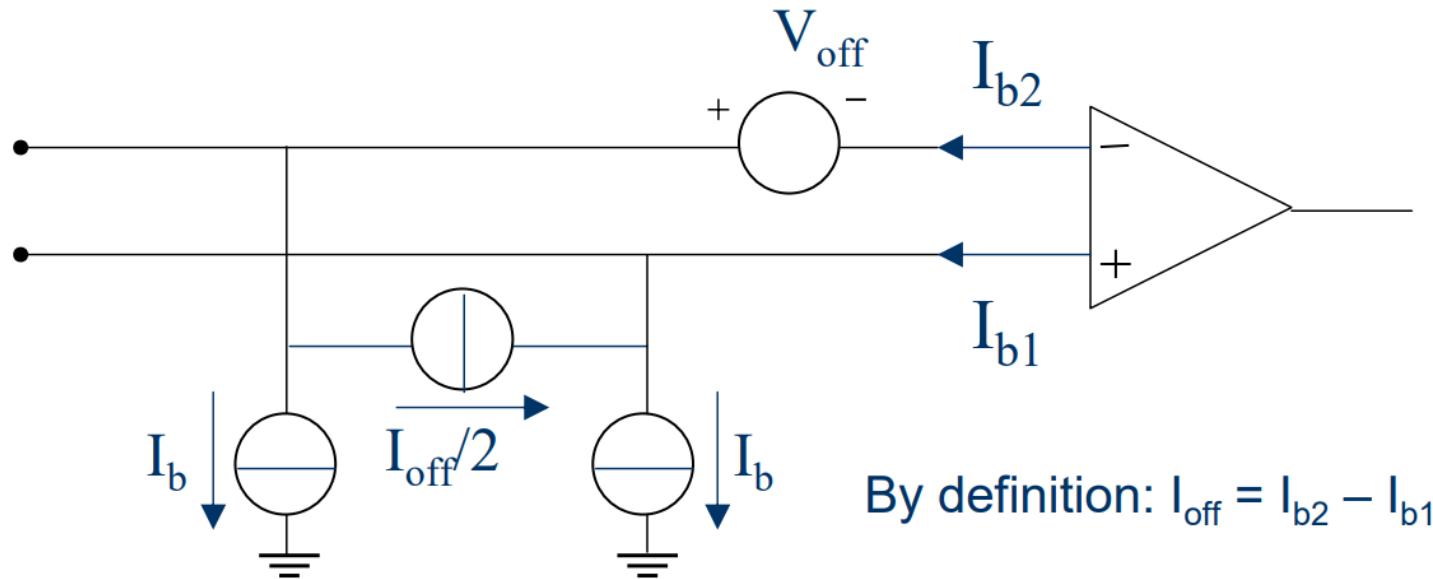
1. Determine the various error sources within the instrument and calculate the combined effect on the output.
2. Identify the dominating source of uncertainty
  - a. Source loading
  - b. offset
  - c. Finite CMRR in a differential measurement
  - d. Noise or interference
3. Calculate the input-referred equivalent sources of uncertainty.

- For a REAL amplifier,  $v_o \neq 0$  when  $v_{in} = 0$ ,  
actually  $v_o = 0$  when  $v_{in} = v_{off}$
- We call  $v_{off}$  the input offset voltage



- Input bias currents  $I_{b1}, I_{b2}$
- Input offset current  $I_{off} = I_{b2} - I_{b1}$





By definition:  $I_{off} = I_{b2} - I_{b1}$

- Non-ideal opamp = error sources + ideal opamp
- The polarities of  $V_{off}$  en  $I_{off}$  are usually unknown!
- So the numbers in data-sheets are **absolute** values

# **LM324, LM324A, LM324E, LM224, LM2902, LM2902E, LM2902V, NCV2902**

## **Single Supply Quad Operational Amplifiers**

The LM324 series are low-cost, quad operational amplifiers with true differential inputs. They have several distinct advantages over standard operational amplifier types in single supply applications. The quad amplifier can operate at supply voltages as low as 3.0 V or as high as 32 V with quiescent currents about one-fifth of those associated with the MC1741 (on a per amplifier basis). The common mode input range includes the negative supply, thereby eliminating the necessity for external biasing components in many applications. The output voltage range also includes the negative power supply voltage.

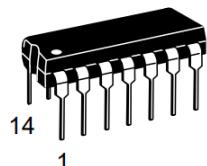
### **Features**

- Short Circuited Protected Outputs
- True Differential Input Stage
- Single Supply Operation: 3.0 V to 32 V
- Low Input Bias Currents: 100 nA Maximum (LM324A)
- Four Amplifiers Per Package
- Internally Compensated
- Common Mode Range Extends to Negative Supply
- Industry Standard Pinouts
- ESD Clamps on the Inputs Increase Ruggedness without Affecting Device Operation
- NCV Prefix for Automotive and Other Applications Requiring Unique Site and Control Change Requirements; AEC-Q100 Qualified and PPAP Capable
- These Devices are Pb-Free, Halogen Free/BFR Free and are RoHS Compliant



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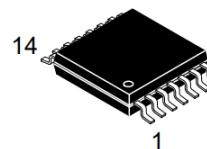
[www.onsemi.com](http://www.onsemi.com)



**PDIP-14  
N SUFFIX  
CASE 646**

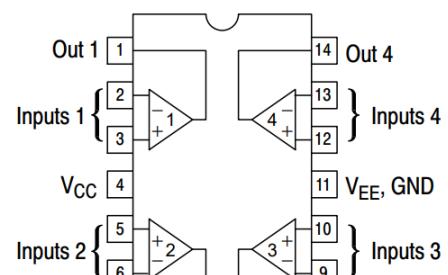


**SOIC-14  
D SUFFIX  
CASE 751A**

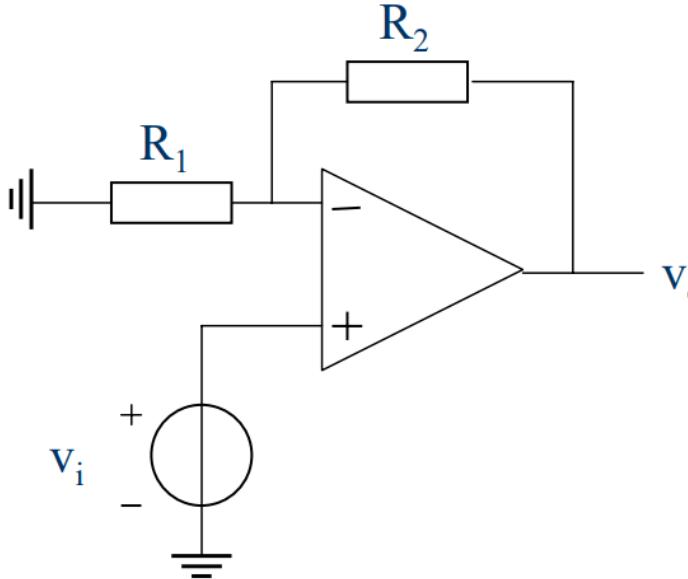


**TSSOP-14  
DTB SUFFIX  
CASE 948G**

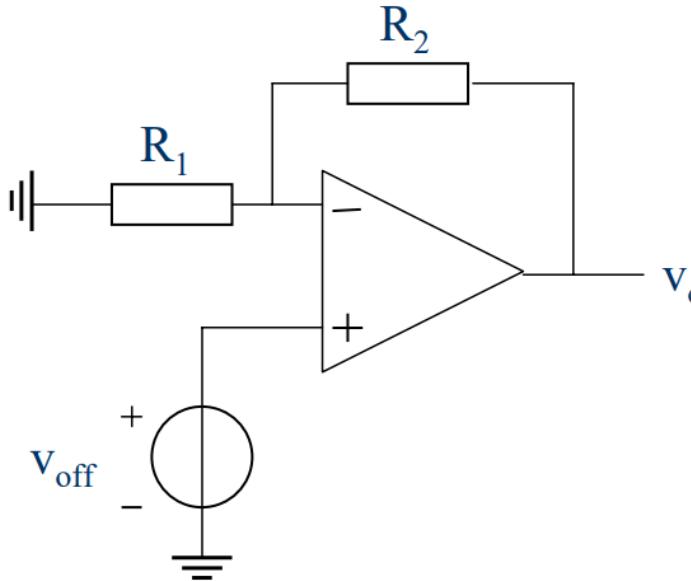
### **PIN CONNECTIONS**



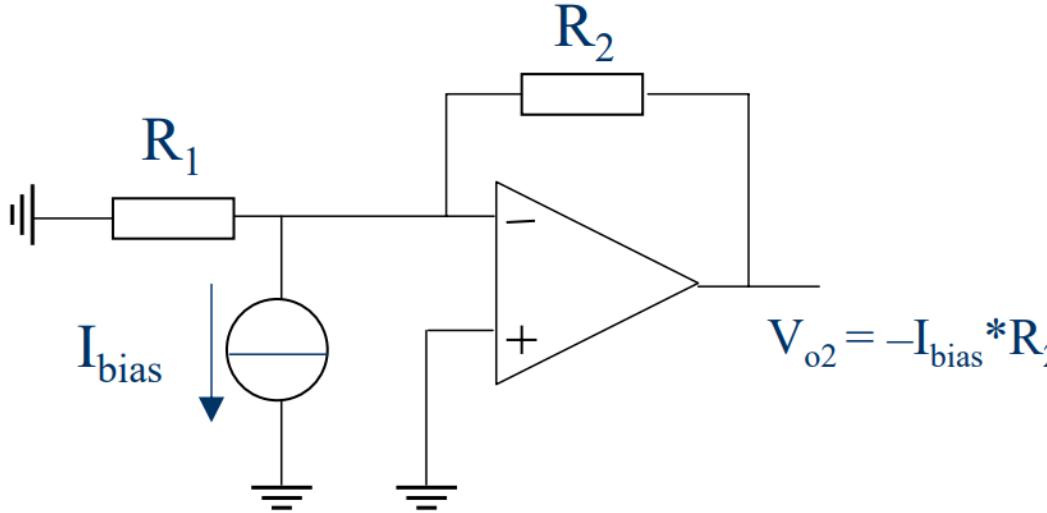
**ELECTRICAL CHARACTERISTICS** ( $V_{CC} = 5.0\text{ V}$ ,  $V_{EE} = \text{GND}$ ,  $T_A = 25^\circ\text{C}$ , unless otherwise noted.)



- If the opamp has finite offset and bias current, calculate the input-referred offset of this amplifier?



- **Use superposition, since this an LTI system!**
- So the effect of every DC source can be independently determined and then summed
- Contribution of  $V_{off} \Rightarrow V_{o1} = V_{off}(1 + R_2/R_1)$



- Why doesn't any current flow through  $R_1$ ?

- The two results can be added

$$V_o = V_{o1} + V_{o2}$$

$$V_o = V_{off} (1 + R_2/R_1) - I_{bias} * R_2$$

- Input-referred offset  $V_{in,off} = V_o / A_{CL}$

$$\text{So } V_{in,off} = V_{off} - I_{bias} * R_1 || R_2$$

- How is this a detection limit?
- Can you name other DC detection limits?

1.3 An experiment results in the following empirical relation:

$$f = \frac{1}{2Lr} \sqrt{\frac{F}{\rho}} \quad (1-5)$$

With the following quantities:  $f$ : frequency,  $F$ : Force,  $L$ : length,  $\rho$ : specific mass and  $r$ : radius. Can this empirical relation be correct?

Select the correct answer:

- a. Yes, because the units match
- b. No, because the units do not match
- c. Yes, because a resonance frequency is always described by a square root function
- d. No answer possible due to insufficient specification

1.3 Insertion of SI basic units yields:

$$[s]^{-1} = [m]^2([N]/\{[kg][m]^{-3}\})^{1/2} = [m]^2([kg][m/s^2]/\{[kg][m]^{-3}\})^{1/2} = [s]^{-1}.$$

The unit expression would be correct in case the SI-units would be specified. Since the units are NOT specified, this is not necessarily the case (length could e.g. be given in inches). Therefore, the correct answer is D.

## تمارين

1.4 Express the unit of electrostatic capacitance,  $C$  [F], in SI- units. Capacitance is related to charge and voltage via the expression:  $Q = C \times V$ ,  $[C] = [F][V]$ . Moreover, electric charge buildup is equal to the product of charging current and time:

$Q = I.t$ ,  $[C] = [A][s]$ . Finally, the unit of mechanical power is equal to that of electrical power:  $[V][A] = [N][m][s]^{-1}$ .

$$1.4 \quad C = Q/V = I.t/V: [F] = [A][s]/[V], [V] = [kg][m]^2/([A][s]^3) \rightarrow [F] = [A][s]\{[A][s]^3/([kg][m]^2\} = [A]^2[s]^4[kg]^{-1}[m]^{-2}$$

Note: The Volt [V] is NOT a basic SI unit.

2.2 The following specifications are listed for an instrument:

- ↳ Temperature drift:  $0.01\%/\text{°C}$
- Time stability:  $0.1\%/\text{month}$
- Operating temperature range between  $-10\text{ °C}$  and  $60\text{ °C}$ .

Calculate the reproducibility of a measurement if only once every three months a calibration is performed at  $20\text{ °C}$  (the calibration is assumed to be perfectly accurate and the time elapsed since the last calibration is assumed to be unknown).

2.2 Largest deviation from calibration temperature is:  $\max\{60-20, 20-(-10)\}=40\text{ °C} \rightarrow$   
Repr. =  $0.01\%/\text{°C} \times 40\text{ °C} + 0.1\%/\text{month} \times 3\text{ months} = 0.7\%$ .

An instrument is used to measure a voltage of about 7.2 V. It is composed of a 4-digit indicator with 9.999 full-scale. The inaccuracy is specified at 0.2% full scale + 0.5% indication.

2.3 Calculate the resolution of this instrument.

2.4 Also calculate the inaccuracy of this instrument.

2.3 Display with 4 digits and 10 V full scale → Resolution =  $10^{-4} \times 10 \text{ V} = 1 \text{ mV}$ .

2.4 Inaccuracy =  $0.002 \times 10 \text{ V} + 0.005 \times 7.2 \text{ V} = 56 \text{ mV}$ .

The following specifications are listed for an instrument:

- Temperature drift:  $0.04\%/\text{ }^{\circ}\text{C}$
- Time stability:  $0.1\%/\text{month}$
- Operating temperature range between  $0\text{ }^{\circ}\text{C}$  and  $30\text{ }^{\circ}\text{C}$ .

2.5 Select the most convenient calibration temperature and calculate the maximum calibration interval for a reproducibility specification at 1%.

2.5 Calibration temperature preferably at mid-range:  $T_{\text{cal}} = 15\text{ }^{\circ}\text{C}$ . The maximum temperature deviation from the calibration temperature is then  $\Delta T_{\text{max}} = 15\text{ }^{\circ}\text{C}$ . To obtain a reproducibility of 1%, we need  $\Delta T_{\text{max}} \times 0.04\%/\text{ }^{\circ}\text{C} + t_{\text{max}} \times 0.1\%/\text{month} = 1\%$ . Therefore, the maximum time  $t_{\text{max}}$  before re-calibration is  $t_{\text{max}} = 4$  months.