

With the *unsteady-state method*, air is then introduced and the change in dissolved oxygen (DO) is monitored until the solution is nearly saturated. In this case,

$$\frac{dC_L}{dt} = k_L a (C^* - C_L) \quad (10.4a)$$

or

$$\frac{-d(C^* - C_L)}{dt/(C^* - C_L)} = k_L a \quad (10.4b)$$

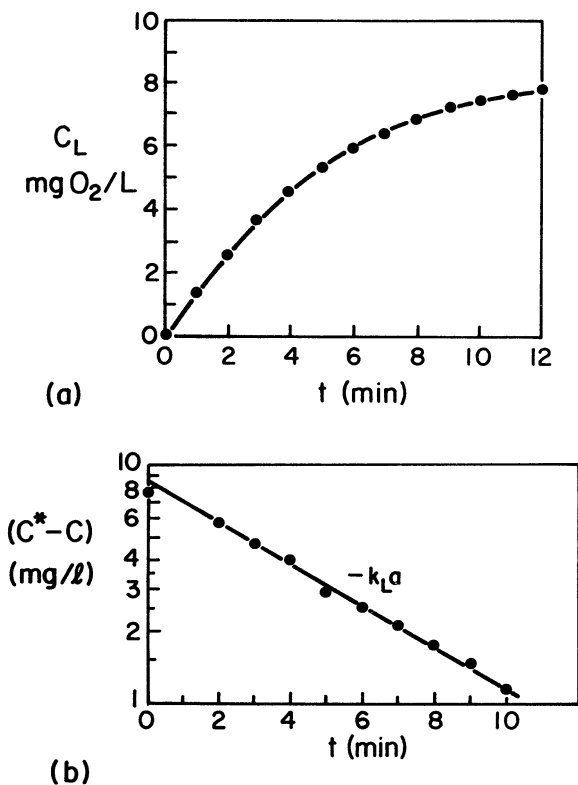
or

$$\ln(C^* - C_L) = -k_L a t \quad (10.5)$$

As shown in Fig. 10.4, a plot of  $\log(C^* - C_L)$  versus time will give an estimate of  $k_L a$ .

Another approach is the *sulfite method*. In the presence of  $\text{Cu}^{2+}$ , the sulfur in sulfite ( $\text{SO}_3^{2-}$ ) is oxidized to sulfate ( $\text{SO}_4^{2-}$ ) in a zero-order reaction. This reaction is very rapid, and consequently  $C_L$  approaches zero.

The rate of sulfate formation is monitored and is proportional to the rate of oxygen consumption ( $\frac{1}{2}$  mol of  $\text{O}_2$  is consumed to produce 1 mol of  $\text{SO}_4^{2-}$ ). Thus,



**Figure 10.4.** (a) Typical data for unsteady-state accumulation of oxygen in a large stirred tank. (b) Assuming  $C^* = 8.65 \text{ mg O}_2/\text{l}$ , a value of  $k_L a = 11.5 \text{ h}^{-1}$  is determined. (With permission, from D. W. Sundstrom and H. E. Klei, *Wastewater Treatment*, Pearson Education, Upper Saddle River, NJ, 1979, p. 53.)