

22 MAGGIO 2023

STABILITÀ INTERNA (MATRICE A - AUTOV.)

RAGG. OSS.

AUTOV. PARTE COMPL. OSS. E RAGGIUNG. $\begin{pmatrix} \hat{A} \\ \hat{A}_b \end{pmatrix} \rightarrow$ POLI $G(s)$

STABILITÀ BIBO (ESTERNA)

POI $\text{Re} < 0$ DI $G(s)$

SISTEMA INTERNA. AS. STABILE \Rightarrow BIBO STABILE

~~CF~~

PER UN SISTEMA IN FORMA MINIMA (COMPL. OSS E RAGG.)

VALE \Leftrightarrow

LTI

STAB. INTERNA

$$(\delta x_0 \rightarrow \delta x(t))$$

INSTABILE

STABILE

MARGINALM.

ASINTOTICAM

STAB. ESTERNA

(BIBO)

$$u \rightarrow y$$

INSTABILE

STABILE

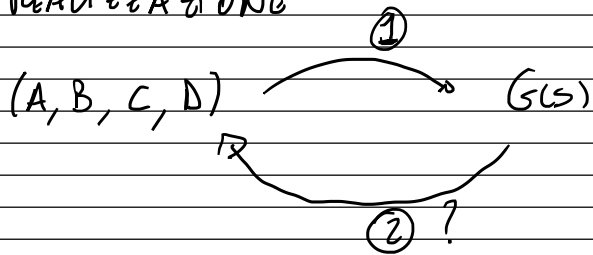
IMPLICA

NON IMPLICA IN
GENERALE

LEMMA PBH ^{PER} MAGG. E OSS.

(SOLO PER SISTEMI
IN
FORMA MINIMA)

REALIZZAZIONE



①

$$G(s) = C(sI - A)^{-1}B + D$$

SOLUZ. UNICA

(LEGAME INGRESSO
USCITA)

② VEDIAMO ADESSO, CI ASPETTIAMO INFINITE POSSIBILITÀ
(INFINITE SCELTE EQ. PER VARABILI DI STATO)

$$G(s) = \frac{N_G(s)}{D_G(s)} = \frac{\beta_n s^n + \beta_{n-1} s^{n-1} + \dots + \beta_1 s + \beta_0}{s^n + \alpha_{n-1} s^{n-1} + \dots + \alpha_1 s + \alpha_0}$$

FORMA PIÙ GENERALE POSSIBILE (grado $N_G(s) \leq$ grado $D_G(s)$)

SISTEMA PROPRIO / STRETTAMENTE PROPRIO

INSEMIANO $G(s)$:

$G(s) =$

$$\beta_n (s^n + \alpha_{n-1} s^{n-1} + \dots + \alpha_1 s + \alpha_0) + \underbrace{(\hat{\beta}_{n-1} - \beta_n \alpha_{n-1})}_{\hat{\beta}_{n-1}} s^{n-1} + \dots + \underbrace{(\beta_1 - \beta_n \alpha_1)}_{\hat{\beta}_1} s + \underbrace{(\beta_0 - \beta_n \alpha_0)}_{\hat{\beta}_0}$$

$$\frac{s^n + \alpha_{n-1} s^{n-1} + \dots + \alpha_1 s + \alpha_0}{s^n + \alpha_{n-1} s^{n-1} + \dots + \alpha_1 s + \alpha_0} + \hat{\beta}_n$$

$$= \frac{\hat{\beta}_{n-1} s^{n-1} + \dots + \hat{\beta}_1 s + \hat{\beta}_0}{s^n + \alpha_{n-1} s^{n-1} + \dots + \alpha_1 s + \alpha_0} + \hat{\beta}_n$$

$$\hat{\beta}_n = \beta_n$$

$$\hat{\beta}_i = \beta_i - \beta_n \alpha_i \quad \forall i \neq n$$

UNA POSSIBILE REALIZZAZIONE

$$A = \begin{bmatrix} 0 & 1 & & 0 \\ 0 & & \ddots & \\ \vdots & & & \\ 0 & 0 & & 1 \\ -\alpha_0 & -\alpha_1 & \dots & -\alpha_{n-1} \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ \vdots \\ 0 \\ 1 \end{bmatrix}$$

FORMA
CANONICA

D

$$C = [\hat{\beta}_0 \quad \dots \quad \hat{\beta}_{n-1}]$$

$$D = \hat{\beta}_n$$

RAGGIUNGIBILITÀ

• PER COSTRUZIONE È SEMPRE COMPLETAMENTE RAGGIUNGIBILE

• LA COMPLETA OSSERVABILITÀ È LEGATA AD EVENTUALI POLINOMI A FATTORE COMUNE TRA $N_G(s)$ E $D_G(s)$ [CANCELLAZIONI]

UNA REALIZZAZIONE ALTERNATIVA

$$A = \left[\begin{array}{c|c} 0 & -\alpha_0 \\ \vdots & \vdots \\ 0 & -\alpha_1 \\ \hline I_{n-1 \times n-1} & \vdots \\ & -\alpha_{n-1} \end{array} \right]$$

$$B = \begin{bmatrix} \hat{\beta}_0 \\ \hat{\beta}_1 \\ \vdots \\ \hat{\beta}_{n-1} \end{bmatrix}$$

COME SOPRA

DI PENDE

DAI SOLI

2n+1 PARAMETRI

α e $\hat{\beta}$

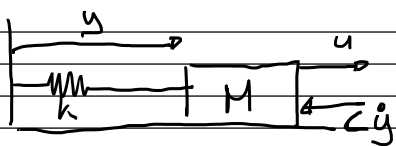
$$C = [0 \dots 0 : 1]$$

$$D = \hat{\beta}_n$$

PER COSTRUZIONE È SEMPRE COMPLETAM. OSS.

FORMA CANONICA DI OSSERVABILITÀ

LA RAGGIUNGIBILITÀ È LEGATA A EVENTUALI CANCELLAZIONI.



FORMA NORMALE

$$M \ddot{y} = -c \dot{y} - k y + u$$

$$x_1 = y$$

$$x_2 = \dot{y}$$

FORMA IN
STATO

$$\mathcal{L}[\dot{y}(t)] = s F(s) + f(0)$$

$$\begin{cases} \dot{x} = \begin{bmatrix} 0 & 1 \\ -\frac{k}{M} & -\frac{c}{M} \end{bmatrix} x + \begin{bmatrix} 0 \\ 1/M \end{bmatrix} u \\ y = \begin{bmatrix} 1 & 0 \end{bmatrix} x + 0 \cdot u \end{cases}$$

NEL CALCOLO DI f.d.t.

$f(0)$ NON LO CONSIDERO

PERCHÉ È DETERMINANTE

SOLO PER EV. LIBERA

(f.d.t. È LEGATA ALL'EVOLVZ. FORZATA)

$$M \ddot{y} = -c \dot{y} - k y + u$$

$$s^2 M Y(s) + s c Y(s) + k Y(s) = U(s)$$

$$G(s) = \frac{Y(s)}{U(s)} = \frac{1/M}{s^2 + \frac{c}{M}s + \frac{k}{M}}$$

DA f. d. t. \longrightarrow REALIZZAZIONE

FORMA CANONICA DI RAGGIUNGIBILITÀ | FORMA C. DI OSSERV.

$$A = \begin{bmatrix} 0 & 1 \\ -k/M & -c/M \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$A = \begin{bmatrix} 0 & -k/M \\ 1 & -c/M \end{bmatrix}$$

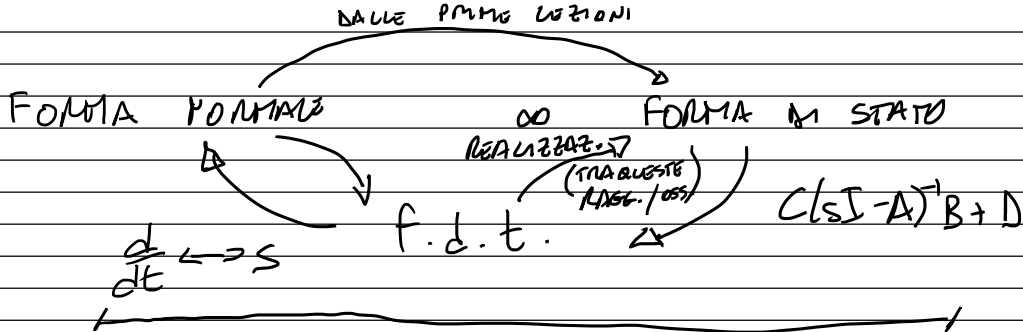
$$B = \begin{bmatrix} 1/M \\ 0 \end{bmatrix}$$

$$C = \begin{bmatrix} 1/M & 0 \end{bmatrix}$$

$$D = 0$$

$$C = \begin{bmatrix} 0 & 1 \end{bmatrix}$$

$$D = 0$$



$$A = \begin{bmatrix} -1 & 1 & 0 \\ 0 & -1 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$B = \begin{bmatrix} 0 \\ -2 \\ 1 \end{bmatrix}$$

STABILITÀ
INTERNA

← ≠ 0

← ≠ 0

$$\begin{aligned} -1 \text{ m.z.} &= 2 \\ \text{m.g.} &= 1 \end{aligned}$$

$$C = \begin{bmatrix} 0 & 1 & 1 \end{bmatrix}$$

$$D = 0$$

$$0 \text{ m.z.} = \text{m.g.} = 1$$

↑ = 0

↑ ≠ 0

RAGGIUNGIBILITÀ

MOM e^{-t} $t e^{-t}$

$$e^{0t} = 1$$

COMPLETAMENTE RAGGIUNGIBILE

MARGINALM. STABILE

OSSERVABILITÀ

• PER f.d.t.

NON COMPL. OSSERVABILE

POLO IN 0

(AUTOV. 0 APPARTIEN-
ALLA PARTE COMPL. REO)

BIBO STABILITÀ
(STABILITÀ ESTERNA)

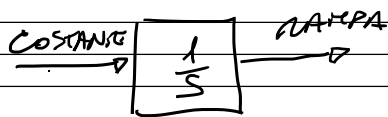
TUTTI I POLI A PARTE $Re < 0$?

NO, SENZ'ALTRO UN POLO IN ZERO

→ INSTABILE

$$A = \begin{bmatrix} -1 & 1 & 1 & 0 \\ 0 & -1 & 1 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$$

• POTREBBE ESSERE
AL PIÙ UN POLO
IN -1



$$C(sI - A)^{-1}B + D$$

$$(sI - A) = \begin{bmatrix} s+1 & -1 & 0 \\ 0 & -s+1 & 0 \\ 0 & 0 & s \end{bmatrix}$$

$$\det(sI - A) = (s+1)^2 s$$

$$\text{cof}(sI - A) = \begin{bmatrix} s(s+1) & 0 & 0 \\ s & s(s+1) & 0 \\ 0 & 0 & (s+1)^2 \end{bmatrix}$$

$$-1 \rightarrow +s$$

$$\text{adj}(sI - A) = \begin{bmatrix} s(s+1) & s & 0 \\ 0 & s(s+1) & 0 \\ 0 & 0 & (s+1)^2 \end{bmatrix}$$

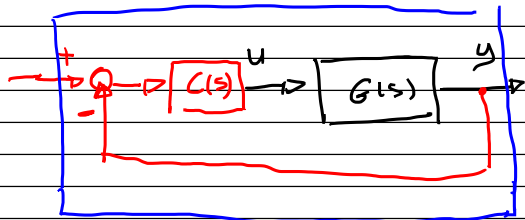
$$(sI - A)^{-1} = \begin{bmatrix} \frac{1}{s+1} & \frac{1}{(s+1)^2} & 0 \\ 0 & \frac{1}{s+1} & 0 \\ 0 & 0 & \frac{1}{s} \end{bmatrix}$$

$$C = [0 \ 1 \ 1]$$

$$B = \begin{bmatrix} 0 \\ -2 \\ 1 \end{bmatrix}$$

$$C(sI - A)^{-1} B = \begin{bmatrix} 0 & \frac{1}{s+1} & 1 \\ \frac{1}{s} \end{bmatrix} \begin{bmatrix} 0 \\ -2 \\ 1 \end{bmatrix} = -\frac{2}{s+1} + \frac{1}{s} =$$

$$G(s) = \frac{-2s + s + 1}{s(s+1)} = \frac{-s + 1}{s(s+1)} = -\frac{s-1}{s(s+1)}$$



$$\frac{C(s) \cdot G(s)}{1 + C(s) \cdot G(s)}$$

IL PRODOTTO

$$C(s) \cdot G(s)$$

DEVE AVERE
ALMENO UN
POLO NELL'ORIGINI

CONTROLLARE IN
MODO CHE
IL SISTEMA
CONTROLLATO
ABBI A CARICA
DI INSEGUIMENTO
PER MF. A GRADIN
NULLO

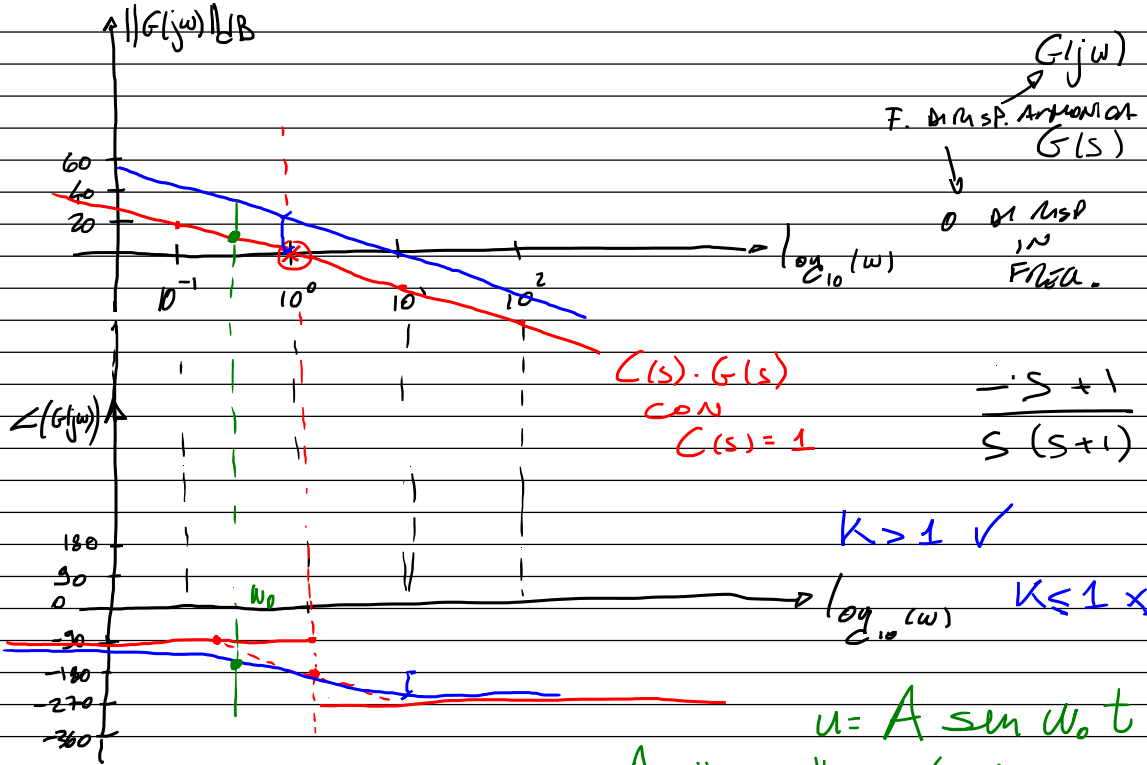
A REGIME

$G(s)$ HA GIÀ UN POLO NELL'ORIGINE

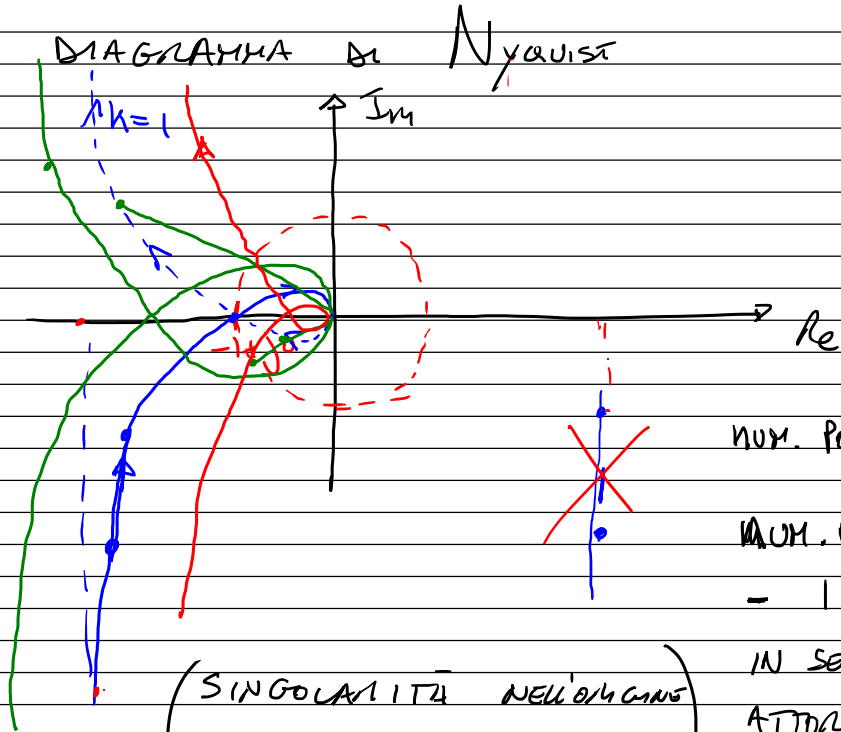
QUAL È LA FORMA PIÙ SEMPLICE PER $C(s)$
PER "SPERARE" CHE LA SPECIFICARE CHE LA
SPECIFICA SIA GARANTITA?

$$C(s) = K$$

• ~~GARANTEE~~ STABILITÀ DI $\frac{C(s) G(s)}{1 + C(s) G(s)}$



$u = A \sin \omega_0 t$
 $y = A \cdot |G(j\omega_0)| \sin(\omega_0 t + \angle G(j\omega_0))$



NUM. POLI $Re > 0$ A.C.

NUM. POLI $Re > 0$ A.A.

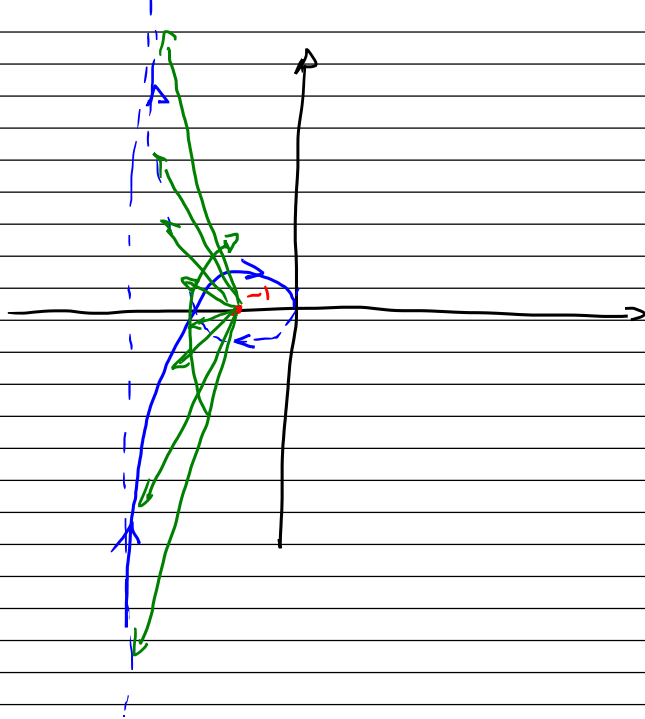
- 1 CIRCONVANTO

IN SENSO ANTICLOCKWISE

ATTORNO A $-1+j0$

DEL DIAGRAMMA COMPLETO

(SINGOLARITÀ NELL'ORGANISMO)
(CONTANO PER MEZZO
GIRO)

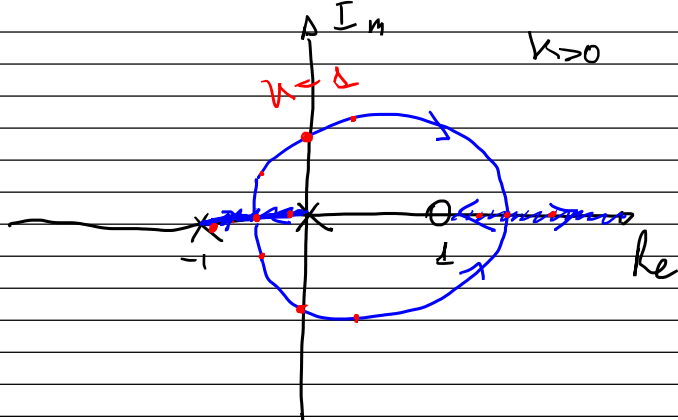


1 GIRO E MEZZO
IN
SENSO ORARIO

$$\frac{1}{2} + \frac{3}{2} = \frac{4}{2}$$

ZPOLL $Re > 0$
PER

$$K > 1$$



LUOGO DELLE
RADICI
DEL DEN. DI

$$\frac{C(s) \cdot G(s)}{1 + C(s)G(s)}$$

AL VARIARE DI
 K

$$- \frac{s-1}{s(s+1)}$$

$$1 + k \left(- \frac{s-1}{s(s+1)} \right) = 0$$

$$s(s+1) - k(s-1) = 0$$

$$s^2 + s - ks + k = 0$$

$$s^2 + s(1-k) + k = 0$$

TUTTE ILLA MA CON $\operatorname{Re} s < 0$

$$1 - k > 0$$

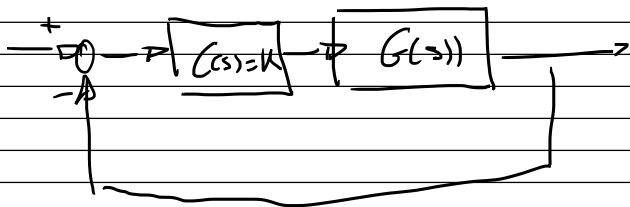
$$k < 1$$

$$0 < k < 1$$

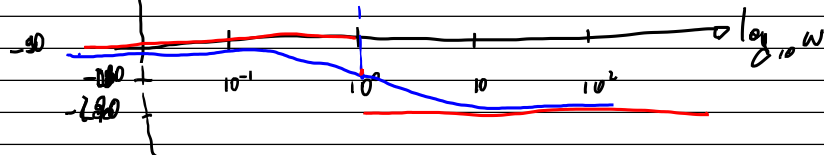
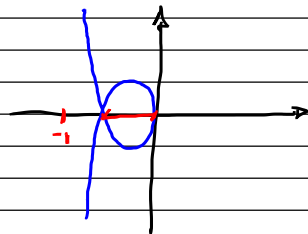
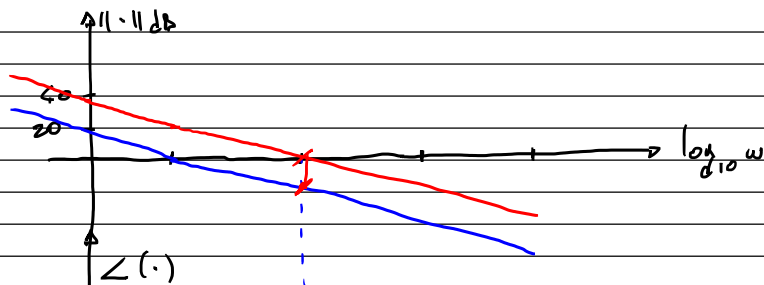
$$k > 0$$

$$k > 0$$

$$G(s) = \frac{-s + 1}{s(s+1)}$$



$$k = 0, 1$$



$K < 1$ ✓
 $K > 1$ ✗

$$\xrightarrow{6 \text{ sent}} \boxed{G_C(s)} \longrightarrow$$

$$G_C(s) = \frac{C(s) G(s)}{1 + C(s) G(s)}$$

$$G_C(s) = \frac{0,1 (-s+1)}{\cancel{s(s+1)} + \frac{0,1(-s+1)}{\cancel{s(s+1)}}} \cdot \frac{1}{\cancel{s(s+1)}}$$

$$= \frac{0,1 (-s+1)}{s^2 + s - 0,1s + 0,1} =$$

$$G_C(s) = \frac{0,1 (-s+1)}{s^2 + 0,9s + 0,1} = \frac{\cancel{0,1} (-s+1)}{\cancel{0,1} (10s^2 + 9s + 1)}$$

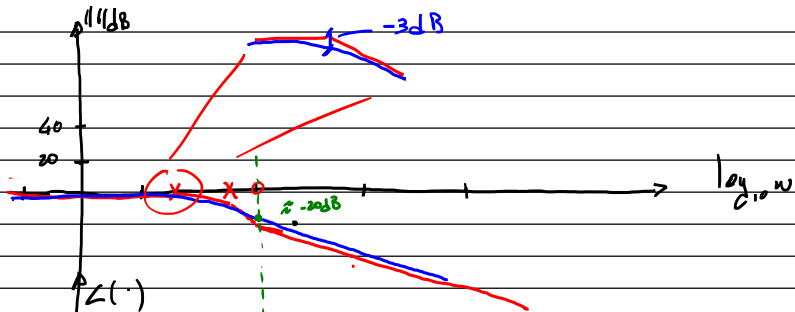
$$\begin{array}{l} z \quad 1 \\ p \quad -0,775 \\ p \quad -0,125 \end{array}$$

$$\Delta = 0,81 - 0,4 = 0,41$$

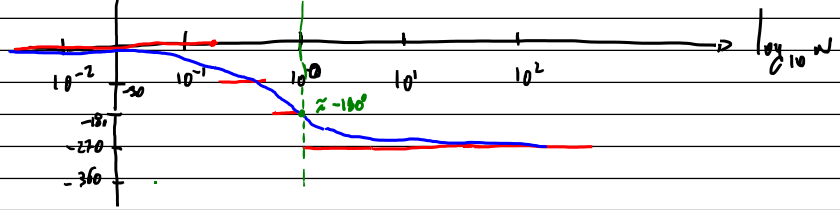
$$\frac{-0,9 \pm \sqrt{0,41}}{2}$$

$$\begin{array}{l} \frac{-1,55}{2} = -0,775 \\ \frac{-0,25}{2} = -0,125 \end{array} \quad \sqrt{0,41} \sim 0,65$$

$$G_C(s) = \frac{-s+1}{\left(\frac{s}{0,775} + 1\right) \left(\frac{s}{0,125} + 1\right)}$$



$$G_C(s) = \frac{-s+1}{\left(\frac{s}{0,775}+1\right)\left(\frac{s}{0,125}+1\right)}$$



$$u = 6 \sin t$$

$$y \approx 0,6 \sin(t - \pi)$$

$$0,1 \approx \|G_C(j\omega)\|$$

$$G_C(s) = \frac{(-s+1)}{(10s^2 + 9s + 1)}$$

$$G_c(j\omega) = \frac{1-j}{-10+9j+1} = \frac{1-j}{-9+j} = \frac{1-j}{-9(1-j)} = -\frac{1}{9}$$

$$\|G_c(j\omega)\| = \frac{\sqrt{2}}{9\sqrt{2}} = \frac{1}{9} \quad \angle(G_c(j\omega)) = -180^\circ = -\pi$$

$$A = \begin{bmatrix} 1 & 2 & 0 \\ -2 & 1 & 0 \\ 0 & 0 & -1 \end{bmatrix} \quad B = \begin{bmatrix} 2 \\ 0 \\ 1 \end{bmatrix}$$

STABILITÀ INTERNA

INSTABILE

AUTOV: $1+j2$
 $1-j2$

$$C = \begin{bmatrix} 0 & 1 & 1 \end{bmatrix} \quad D = 0$$

MODI: $e^{st} \sin \omega t$
 $e^{st} \cos \omega t$

e^{-t}
 $e^t \sin ct$
 $e^t \cos ct$

RAGGIUNGIBILITÀ:

$$M_r \quad [1I - A : B]$$

$$M_r = \begin{bmatrix} 2 & 2 & -6 \\ 0 & -4 & -8 \\ 1 & -1 & 1 \end{bmatrix}$$

COMPLETAM. RAGGIUNGIBILE

$$\det(M_r) = -64$$

$$\rho(M_r) = 3$$

OSSERVABILITÀ:

$$M_o = \begin{bmatrix} 0 & 1 & 1 \\ -2 & 1 & -1 \\ -4 & -3 & 1 \end{bmatrix}$$

$$\det(M_o) = 16 \neq 0$$

$$\rho(M_o) = 3$$

COMPLETAMENTE OSSERVABILE

STABILITÀ ESTERNA: INSTABILE

f.l.t. den: $(s+1) \underbrace{(s-1+j2)(s-1-j2)}$

$\frac{\text{GRADO} < 3 \quad (\Delta=0 \text{ STRETT. PROPRIO})}{(s+1)(s^2-2s+5)} (s-1)^2 - (j2)^2 = (s-1)^2 + 4$
 $s^2 - 2s + 1 + 4$

$G(s) = C(sI - A)^{-1}B + \cancel{D} \rightarrow = 0$

$$(sI - A) = \begin{bmatrix} s-1 & -2 & 0 \\ 2 & s-1 & 0 \\ 0 & 0 & s+1 \end{bmatrix}$$

$$\det(sI - A) = (s+1)((s-1)^2 + 4)$$

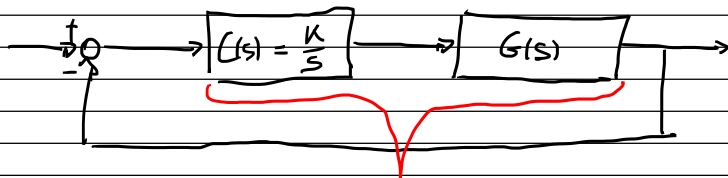
$$\text{cof}(sI - A) = \begin{bmatrix} s^2 - 1 & -2(s+1) & 0 \\ 2(s+1) & s^2 - 1 & 0 \\ 0 & 0 & (s-1)^2 + 4 \end{bmatrix} \quad C =$$

$$(sI - A)^{-1} = \begin{bmatrix} \frac{s-1}{(s-1)^2 + 4} & + \frac{2}{(s-1)^2 + 4} & 0 \\ -\frac{2}{(s-1)^2 + 4} & \frac{s-1}{(s-1)^2 + 4} & 0 \\ 0 & 0 & \frac{1}{s+1} \end{bmatrix} \quad \begin{bmatrix} 0 & 1 & 1 \end{bmatrix}$$

$$G(s) = C (sI - A)^{-1} B = \begin{bmatrix} -\frac{2}{(s-1)^2 + 4} & \frac{s-1}{(s-1)^2 + 4} & \frac{1}{s+1} \end{bmatrix} \begin{bmatrix} 2 \\ 0 \\ 1 \end{bmatrix}$$

$$-\frac{4}{(s-1)^2 + 4} + \frac{1}{s+1} = \frac{-4s - 4 + s^2 - 2s + 1 + 4}{(s+1)(s^2 - 2s + 5)}$$

$$G(s) = \frac{s^2 - 6s + 1}{(s+1)(s^2 - 2s + 5)}$$



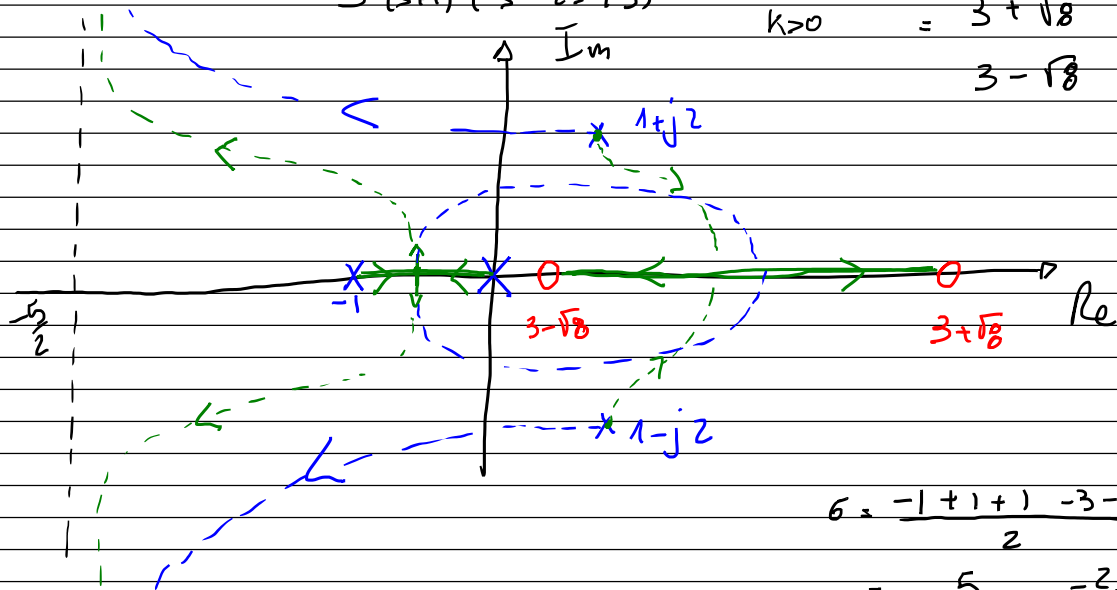
ALMENO UN TIPO 1

ALMENO UN POLO IN 0

$K = ?$

ERRORE
INSEG.
A GRADINO
NULLO A
REGIME

$$C(s) G(s) = \frac{k (s^2 - 6s + 1)}{s (s+1) (s^2 - 2s + 5)}$$



$$3 \pm \sqrt{9-1} =$$

$$k > 0 \quad = \quad 3 + \sqrt{8} \\ 3 - \sqrt{8}$$

$$\sigma = \frac{-1 + 1 + 1 - 3 - 3}{2} \\ = -\frac{5}{2} = -2.5$$

$$G_C(s) = \frac{C(s) G(s)}{1 + C(s) G(s)}$$

$$1 + C(s) G(s)$$

$$1 + \frac{k(s^2 - 6s + 1)}{s(s+1)(s^2 - 2s + 5)}$$

$$s(s+1)(s^2 - 2s + 5) + k(s^2 - 6s + 1) = 0$$

$$G(s) = \frac{s - 1000}{(s+1)(s^2 + s + 100)}$$

Bode

STABILITÀ ESTERNA (BIBO) : $s_1!$

FORMA DI BODE:

$$\frac{\cancel{-1000}}{\cancel{100}} \frac{\left(-\frac{s}{1000} + 1\right)}{(s+1)\left(\frac{s^2}{100} + \frac{s}{100} + 1\right)} = -10 \frac{\left(-\frac{s}{1000} + 1\right)}{(s+1)\left(\frac{s^2}{100} + \frac{s}{100} + 1\right)}$$

GUADAGNO DI BODE -10

$$\frac{s^2}{\omega_n^2} + \frac{2\zeta}{\omega_n}s + 1$$

z 1000 $\text{Re} > 0$

p -1 $\text{Re} < 0$

z p $\omega_n = 10$ $\text{Re} < 0$

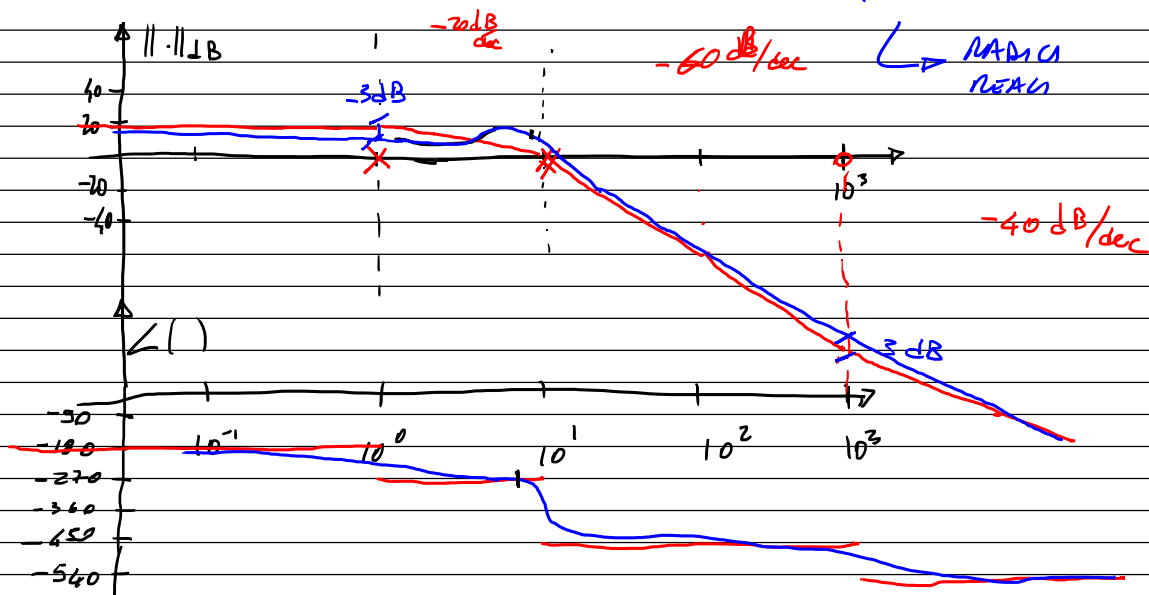
$$\zeta = \frac{1}{20}$$

$$\frac{2}{\cancel{10}} \zeta = \frac{1}{100} = \frac{1}{20}$$

$$[s^2 + 8s + 1]$$

$$\omega_n = 1$$

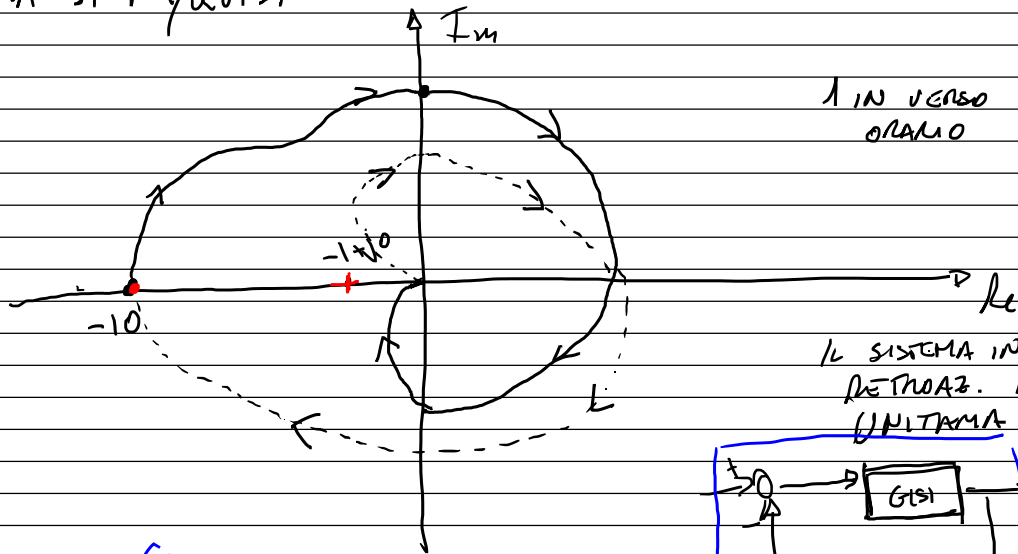
$$\frac{2\zeta}{\omega_n} = 8 \quad \zeta = 4$$



$$20 \log_{10} |10|$$

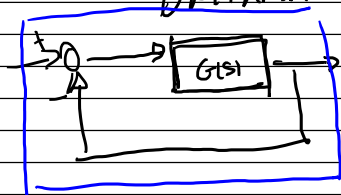
$$20 \log_{10} 10 = 20 \text{ dB}$$

DIAGRAMMA DI Nyquist



1 IN VERSO
ORARIO

IL SISTEMA IN
RETROAZ. NEG.
UNITARIA

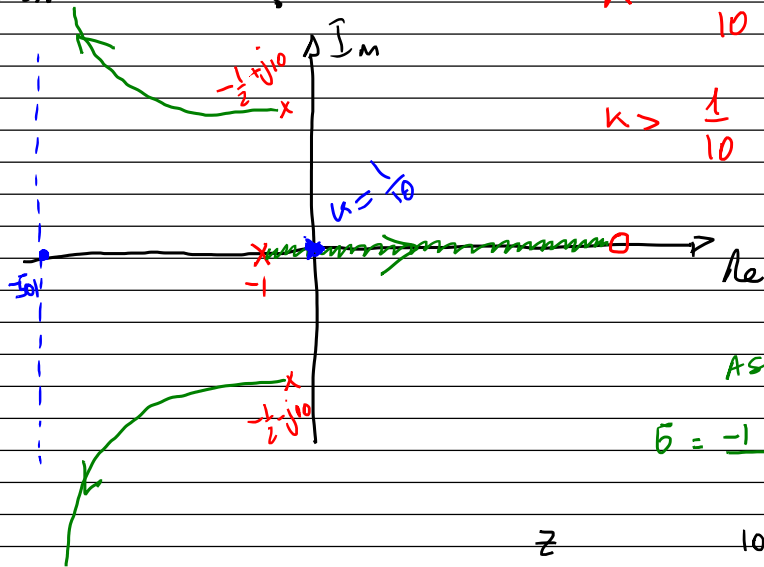


$$G_c(s) = \frac{1 G(s)}{1 + G(s)}$$

3 POLI DI CU1

1 con $\text{Re} > 0$
2 con $\text{Re} < 0$

AL VARIARE DI K ?



$K < \frac{1}{10}$ 0 POLO $Re > 0$
SISTEMA STABILE

$K > \frac{1}{10}$ 1 POLO $Re > 0$
SIST. INSTAB.

ASINTOTI $3 - 1 = 2$

$$\sigma = \frac{-1 - \frac{1}{2} - \frac{1}{2} - 1000}{2} = -501$$

$$s^2 + s + 100$$

$$\frac{-1 \pm \sqrt{1 - 400}}{2} \approx \begin{cases} -\frac{1}{2} + j10 \\ -\frac{1}{2} - j10 \end{cases}$$

z	1000	$Re > 0$
p	-1	$Re < 0$
2p	$\omega_n = 10$	$Re < 0$