Elettronica Digitale A.A. 2020-2021

Lezione 08/04/2021

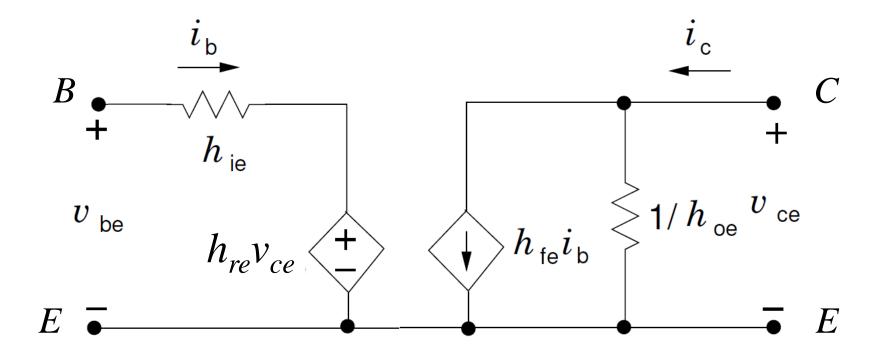
$$\begin{cases} v_{be} = h_{ie}i_b + h_{re}v_{ce} \\ i_c = h_{fe}i_b + h_{oe}v_{ce} \end{cases}$$

$$\left|h_{ie} = \frac{\partial v_{BE}}{\partial i_B}\right|_Q$$

$$\left| h_{re} = \frac{\partial v_{BE}}{\partial v_{CE}} \right|_{Q}$$

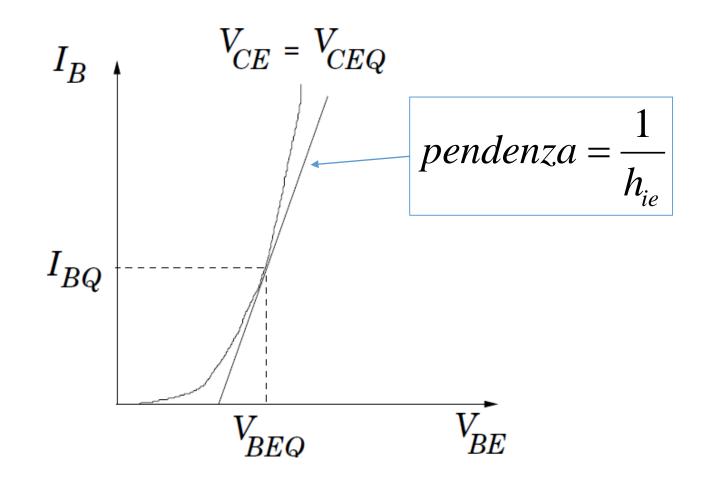
$$\left.h_{fe}=rac{\partial i_C}{\partial i_B}
ight|_Q$$

$$\left| h_{oe} = \frac{\partial i_C}{\partial v_{CE}} \right|_Q$$



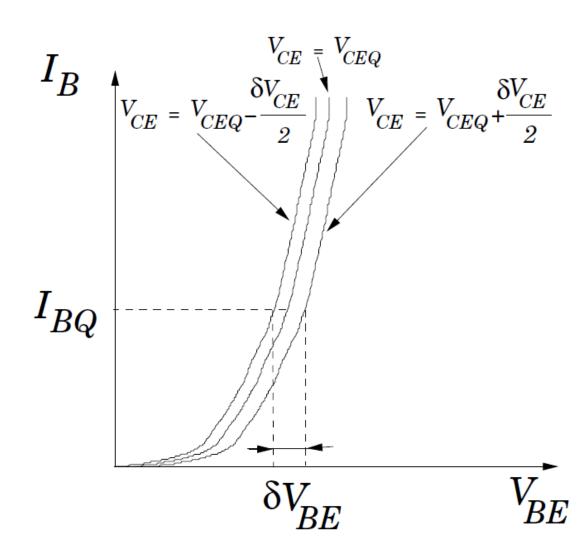
$$\begin{cases} v_{be} = h_{ie}i_b + h_{re}v_{ce} \\ i_c = h_{fe}i_b + h_{oe}v_{ce} \end{cases}$$

$$h_{ie} = \frac{\partial v_{BE}}{\partial i_B} \bigg|_{Q}$$



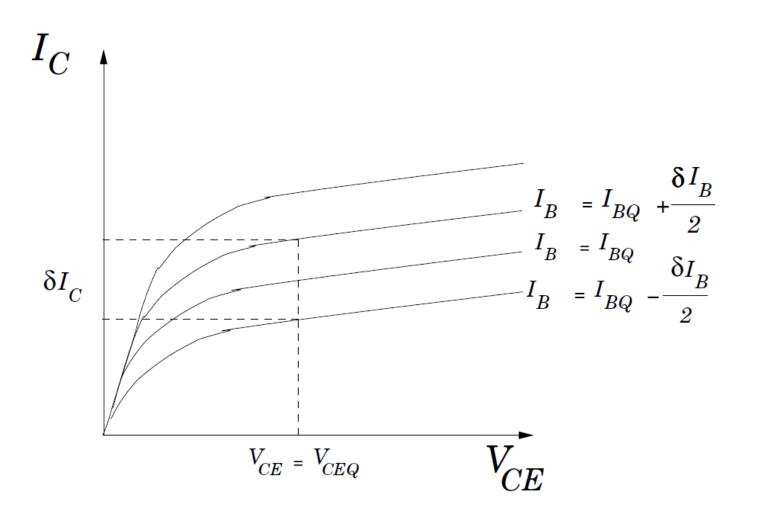
$$\begin{cases} v_{be} = h_{ie}i_b + h_{re}v_{ce} \\ i_c = h_{fe}i_b + h_{oe}v_{ce} \end{cases}$$

$$h_{re} = \frac{\partial v_{BE}}{\partial v_{CE}} \bigg|_{Q} = \lim_{\delta v_{CE} \to 0} \frac{\delta v_{BE}}{\delta v_{CE}} \bigg|_{i_{B} = I_{BQ}}$$



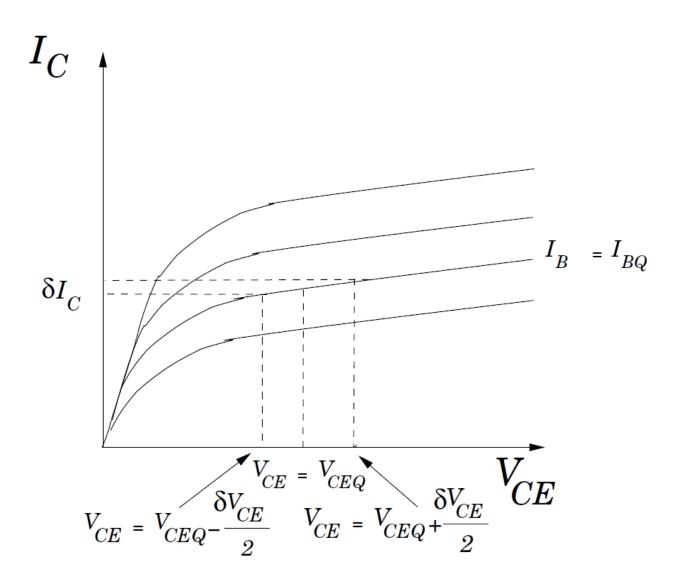
$$\begin{cases} v_{be} = h_{ie}i_b + h_{re}v_{ce} \\ i_c = h_{fe}i_b + h_{oe}v_{ce} \end{cases}$$

$$\left| h_{fe} = \frac{\partial i_C}{\partial i_B} \right|_{Q} = \lim_{\delta i_B \to 0} \frac{\delta i_C}{\delta i_B} \bigg|_{v_{CE} = V_{CEQ}}$$



$$\begin{cases} v_{be} = h_{ie}i_b + h_{re}v_{ce} \\ i_c = h_{fe}i_b + h_{oe}v_{ce} \end{cases}$$

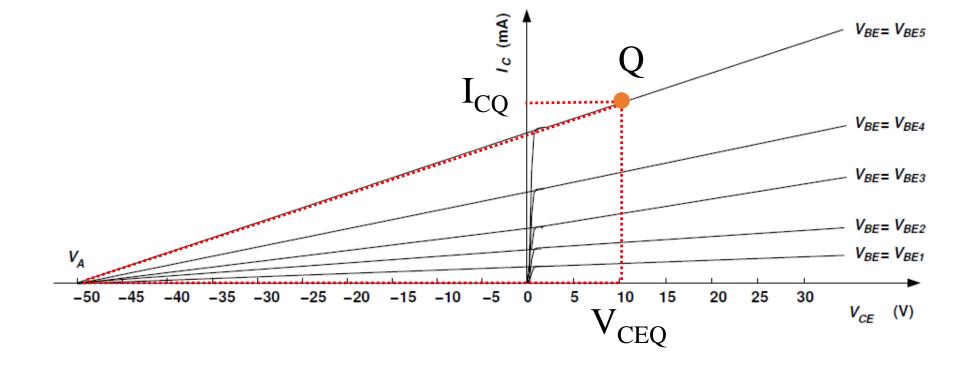
$$\left| h_{oe} = \frac{\partial i_C}{\partial v_{CE}} \right|_{Q} = \lim_{\delta v_{CE} \to 0} \frac{\delta i_C}{\delta v_{CE}} \Big|_{i_B = I_{BQ}}$$



$$h_{re} = \frac{\partial v_{BE}}{\partial v_{CE}} \bigg|_{Q} \approx 0$$

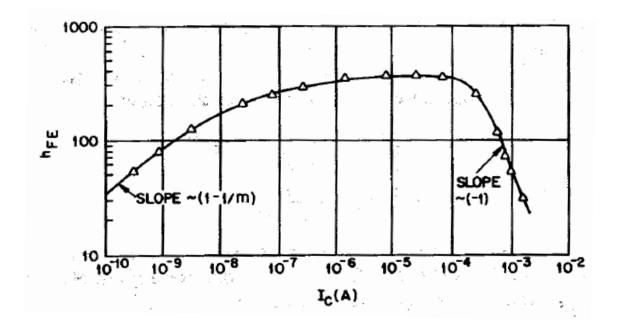
$$h_{oe} = \frac{\partial i_C}{\partial v_{CE}} \bigg|_{Q}$$

$$h_{oe} \approx \frac{I_{CQ}}{V_A + V_{CEQ}}$$



$$h_{fe} = \frac{\partial i_C}{\partial i_B} \bigg|_{Q}$$
 $i_C = \beta_F i_B$ $\beta_F = f(i_C)$

$$\frac{\partial i_C}{\partial i_B} = \beta_F + i_B \frac{\partial \beta_F}{\partial i_B} = \beta_F + i_B \frac{\partial \beta_F}{\partial i_C} \frac{\partial i_C}{\partial i_B}$$

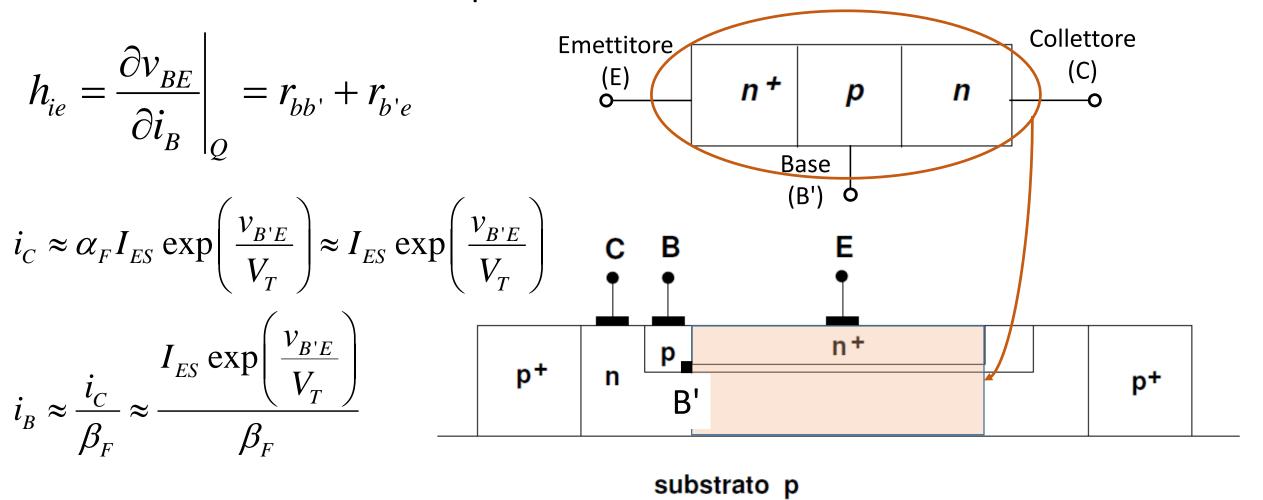


$$\frac{\partial i_C}{\partial i_B} = \frac{\beta_F}{1 - i_B \frac{\partial \beta_F}{\partial i_C}}$$

$$\frac{\partial i_{C}}{\partial i_{B}} = \frac{\beta_{F}}{1 - i_{B}} \frac{\partial \beta_{F}}{\partial i_{C}} \qquad h_{fe} = \frac{\partial i_{C}}{\partial i_{B}} \Big|_{Q} = \frac{\beta_{F}|_{Q}}{1 - i_{B}} \frac{\partial \beta_{F}}{\partial i_{C}} \Big|_{Q} = \frac{\beta_{F}|_{Q}}{1 - \frac{i_{C}}{\beta_{F}}} \frac{\partial \beta_{F}}{\partial i_{C}} \Big|_{Q} \qquad \Longrightarrow \boxed{h_{fe} \approx \beta_{F}}$$







$$h_{ie} = \frac{\partial v_{BE}}{\partial i_B} \bigg|_{Q} = r_{bb'} + r_{b'e}$$
 $i_B \approx \frac{i_C}{\beta_F} \approx \frac{I_{ES} \exp\left(\frac{v_{B'E}}{V_T}\right)}{\beta_F}$

$$\frac{1}{r_{b'e}} = \frac{\partial i_B}{\partial v_{B'E}} \bigg|_{O} = \frac{1}{V_T} \frac{I_{ES} \exp\left(\frac{v_{B'E}}{V_T}\right)}{\beta_F} - \frac{1}{\beta_F^2} \frac{\partial \beta_F}{\partial v_{B'E}} I_{ES} \exp\left(\frac{v_{B'E}}{V_T}\right)$$

$$\frac{1}{r_{b'e}} = \frac{1}{V_T} \frac{i_C}{\beta_F} - \frac{1}{\beta_F^2} \frac{\partial \beta_F}{\partial i_C} \frac{\partial i_C}{\partial v_{B'E}} i_C = \frac{1}{V_T} \frac{i_C}{\beta_F} - \frac{i_C}{\beta_F^2} \frac{i_C}{V_T} \frac{\partial \beta_F}{\partial i_C}$$

$$h_{ie} = \frac{\partial v_{BE}}{\partial i_B} \bigg|_{Q} = r_{bb'} + r_{b'e} \qquad i_B \approx \frac{i_C}{\beta_F} \approx \frac{I_{ES} \exp\left(\frac{v_{B'E}}{V_T}\right)}{\beta_F}$$

$$\frac{1}{r_{b'e}} = \frac{1}{V_T} \frac{i_C}{\beta_F} - \frac{i_C}{\beta_F^2} \frac{i_C}{V_T} \frac{\partial \beta_F}{\partial i_C} = \frac{1}{V_T} \frac{i_C}{\beta_F} \left(1 - \frac{i_C}{\beta_F} \frac{\partial \beta_F}{\partial i_C} \right) \qquad h_{fe} = \frac{\beta_F |_Q}{1 - \frac{i_C}{\beta_F} \frac{\partial \beta_F}{\partial i_C}|_Q}$$

$$h_{fe} = \frac{\left. \beta_F \right|_Q}{1 - \frac{i_C}{\beta_F} \frac{\partial \beta_F}{\partial i_C} \right|_O}$$

$$\frac{1}{r_{b'e}} = \frac{1}{V_T} \frac{i_C}{\beta_F} \frac{\beta_F}{h_{fe}} \Big|_{O} = \frac{1}{V_T} \frac{i_C}{h_{fe}} \Big|_{O}$$
 $r_{b'e} = \frac{V_T}{I_{CO}} h_{fe}$

$$r_{b'e} = \frac{V_T}{I_{CQ}} h_{fe}$$

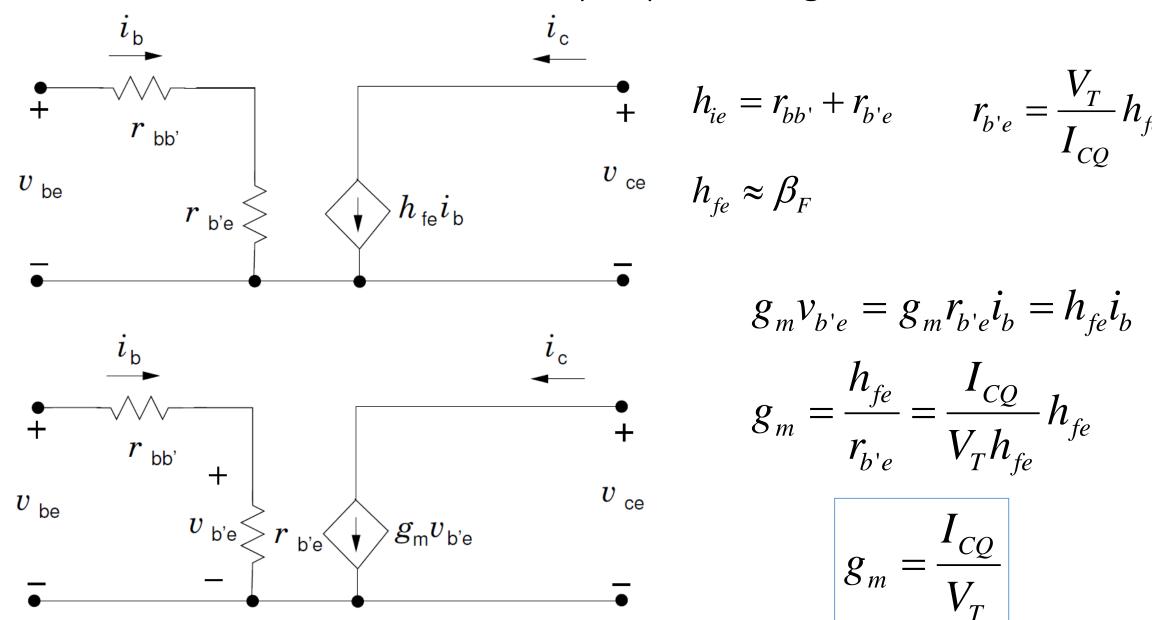
Determinazione dei valori dei parametri

$$h_{ie} = \frac{\partial v_{BE}}{\partial i_B} \bigg|_{Q} = r_{bb'} + r_{b'e}$$
 $r_{b'e} = \frac{V_T}{I_{CQ}} h_{fe}$

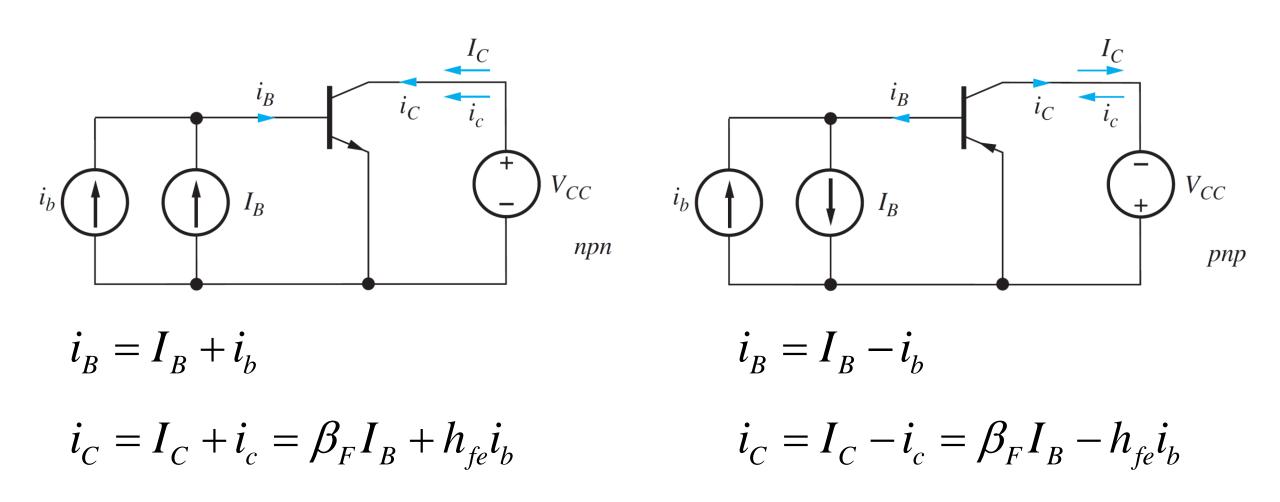
Se il costruttore fornisce i parametri per un particolare punto di riposo si può determinare il valore di $r_{bb'}$ considerando che tale resistenza è indipendente dal punto di riposo

$$h_{ie}^* = r_{bb'}^* + r_{b'e}^*$$
 $r_{bb'}^* = h_{ie}^* - r_{b'e}^* = r_{bb'}^*$

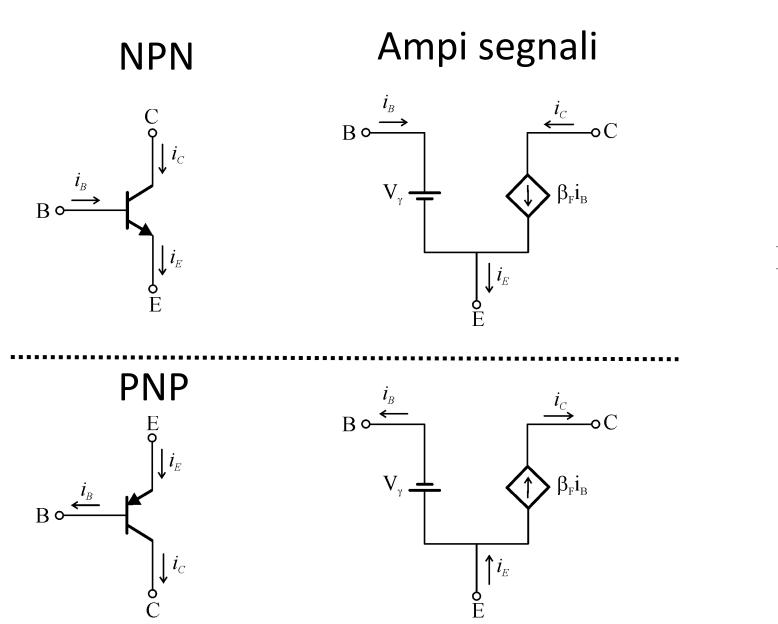
$$h_{ie} = r_{bb'} + r_{b'e} = \left(h_{ie}^* - r_{b'e}^*\right) + \frac{V_T}{I_{CQ}} h_{fe}$$



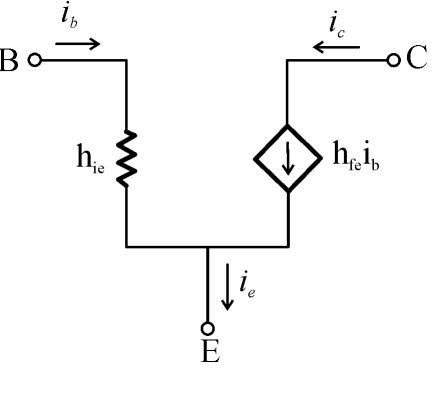
Transistore BJT– Equivalenza modello linearizzato per piccoli segnali NPN e PNP



Transistore BJT- Modelli NPN e PNP in zona attiva diretta



Piccoli segnali semplificato



Transistore MOSFET— Modelli linearizzato per piccoli segnali in saturazione

$$i_D = k \frac{W}{L} \left(v_{GS} - V_T \right)^2 \left(1 + \lambda v_{DS} \right) = f \left(v_{GS}, v_{DS} \right)$$

$$i_{D} = I_{DQ} + i_{d}(t) = f\left(V_{GSQ} + v_{gs}, V_{DSQ} + v_{ds}\right) = f\left(V_{GSQ}, V_{DSQ}\right) + \frac{\partial f}{\partial v_{GS}}\bigg|_{Q} v_{gs} + \frac{\partial f}{\partial v_{DS}}\bigg|_{Q} v_{ds} + \dots$$

$$i_{d} = \frac{\partial i_{D}}{\partial v_{GS}} \Big|_{Q} v_{gs} + \frac{\partial i_{D}}{\partial v_{DS}} \Big|_{Q} v_{ds}$$

$$i_{d} = g_{m} v_{gs} + \frac{v_{ds}}{r_{d}}$$

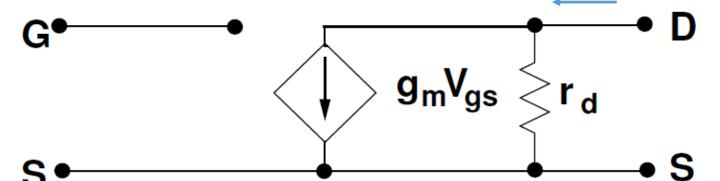
$$\mathbf{g_{m}} \mathbf{v_{gs}} + \mathbf{v_{ds}}$$

$$\mathbf{s} \bullet \mathbf{s}$$

Transistore MOSFET- Modelli linearizzato per piccoli segnali in

saturazione

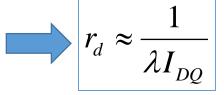
$$i_d = g_m v_{gs} + \frac{v_{ds}}{r_d}$$



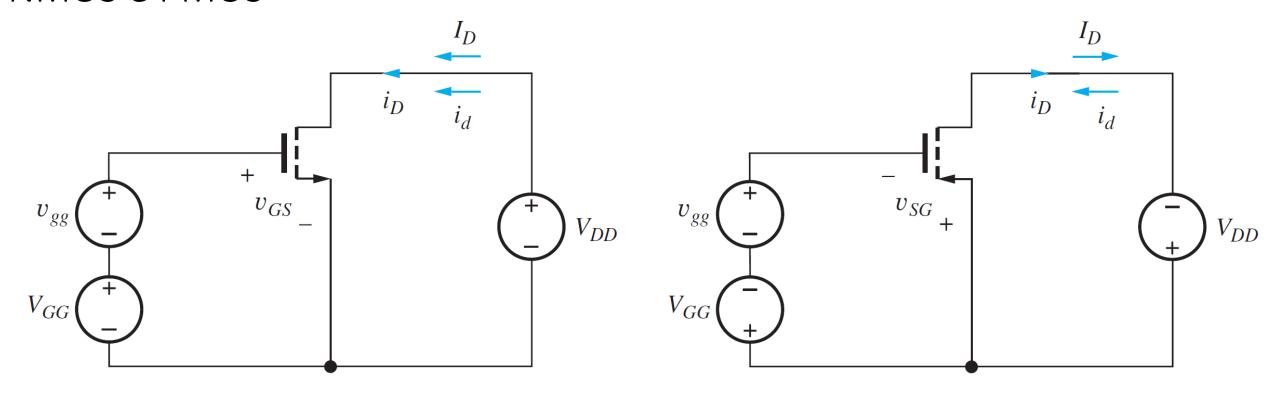
$$i_D = k \frac{W}{L} \left(v_{GS} - V_T \right)^2 \left(1 + \lambda v_{DS} \right)$$

$$\left|g_{m} = \frac{\partial i_{D}}{\partial v_{GS}}\right|_{Q} = 2k \frac{W}{L} (v_{GS} - V_{T}) (1 + \lambda v_{DS}) \Big|_{Q} = \frac{2I_{DQ}}{(V_{GSQ} - V_{T})}$$

$$\frac{1}{r_d} = \frac{\partial i_D}{\partial v_{DS}} \bigg|_{Q} = k \frac{W}{L} \left(v_{GS} - V_T \right)^2 \lambda \bigg|_{Q} = \frac{I_{DQ} \lambda}{\left(1 + \lambda V_{DSQ} \right)} = \frac{I_{DQ}}{\left(\frac{1}{\lambda} + V_{DSQ} \right)} \approx I_{DQ} \lambda$$



Transistore MOSFET – Equivalenza modello linearizzato per piccoli segnali NMOS e PMOS



$$\begin{aligned} v_{GS} &= V_{GG} + v_{gg} \\ i_D &= I_{DQ} + i_d = k \frac{W}{I} \left(V_{GG} - V_T \right)^2 + g_m v_{gg} \end{aligned}$$

$$v_{SG} = V_{GG} - v_{gg}$$

$$i_D = I_{DQ} - i_d = k \frac{W}{L} (-V_{GG} - V_T)^2 - g_m v_{gg}$$

Transistore MOSFET- Modelli NMOS e PMOS in zona di saturazione

Ampi segnali Canale N $k\frac{W}{L}(V_{GS}-V_T)^2$ Canale P $k \frac{W}{L} (V_{GS} - V_T)^2$

Piccoli segnali semplificato

