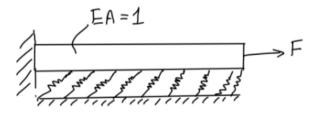
FemAssignments

Assigment 1

Question 1

1. Consider a one-dimensional bar with a distributed spring of stiffness per unit length k as shown in the below figure.



- (a) Derive the governing differential equation and boundary conditions of the bar. (5)
- (b) Write the analytical solution of the above differential equation (no need to derive). (5)
- (c) Write a finite element code in octave to find the displacements and stresses. (10)
- (d) Compare the stresses and displacements from the finite element code with the analytical solution. (5)

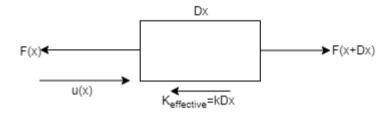
Assume F = 1 and k = 1.

Solution 1

• Code File: Question 1 Mfile

Deriving Governing Equation

Force Balance on an arbitrary element at distance x from bar



$$F(x + \Delta x) - F(x) - k\Delta x u(x) = 0$$

Dividing whole Equation by Δx

$$rac{F(x+\Delta x)-F(\Delta x)}{\Delta x}-ku(x)$$
 = 0

Take limit as $\Delta x o 0$

$$rac{dF}{dx}-ku=0$$
 {Note : Here $u=u(x)$ }

$$\sigma=rac{F}{A}$$
 also $\sigma=Erac{du}{dx}$

E = Elasticity modulus, **A**= Cross Sectional Area Thus,

$$F = EA\frac{du}{dx}$$

Known Boundary Conditions

$$u(0) = 0$$

$$EA\left.\frac{du}{dx}\right|_{x=l} = F$$

and, Finally putting value of **F** in our governing equation

$$\frac{d}{dx}[EA\frac{du}{dx}] - ku = 0$$

Finally Putting values of constants in our equations, questions have asked us to take all constants as unity, so be it.

$$rac{d^2 u}{dx^2} - u = 0$$
 for $x \in (0,1)$

$$u(0) = 0$$

$$\frac{du}{dx} = 1$$
 at $x = 1$

Solving
$$rac{d^2u}{dx^2}-u=0$$
 for $x\in(0,1)$

with Boundary conditions

$$u(0) = 0$$

$$\frac{du}{dx} = 1$$
 at $x = 1$

We get

$$=> u(x) = rac{e^x - e^{-x}}{e + e^{-1}}$$

Finally we get our analytical solution any any x.

$$=> u(x) = \frac{e}{e^2+1}(e^x - e^{-x})$$

Deriving Weak Form

$$\int_{1}^{2} \delta u (\frac{d^{2}u}{dx^{2}} - u) dx = 0$$

 δu is weight function that varies linearly like u since we are going to take linear approximation for our calculations

Evaluating further

$$\int_{1}^{2} \left(\frac{d}{dx} (\delta u \frac{du}{dx}) - \frac{d\delta u}{dx} \frac{du}{dx} - \delta u u \right) dx = 0$$

According to our method our u varies linearly and it will be according to the following equation.

$$u = N_1 u_1 + N_2 u_2$$

$$N_1 = \frac{(x-x_2)}{(x_1-x_2)}$$

$$N_2=rac{(x-x_1)}{(x_2-x_1)}$$

$$\mathbf{N} = egin{bmatrix} N_1 & N_2 \end{bmatrix}$$

$$\mathbf{B}=\mathbf{N}^{'}=egin{bmatrix}N_{1}^{'}&N_{2}^{'}\end{bmatrix}$$

$$\delta u = \mathbf{N} \delta u$$

$$u = \mathbf{N}u$$

$$\frac{du}{dx} = \mathbf{B}u$$

Putting above equations in our integral and simplifying

$$\delta u \frac{du}{dx} \Big|_1^2 = \int \delta u^T \mathbf{B}^T \mathbf{B} u dx + \int \delta u^T \mathbf{N}^T \mathbf{N} u dx$$

$$F^N \delta u^T = \delta u^T u (\int \mathbf{B}^T \mathbf{B} + \mathbf{N}^T \mathbf{N}) dx$$

We can very conveniently compare above expression to F=Kx as we write

$$\mathbf{K} = \int (\mathbf{B}^T \mathbf{B} + \mathbf{N}^T \mathbf{N}) dx$$

there by leading to

$$F^N = \mathbf{K} u$$

For integrating above expression numerically we will be using **Gauss Quadrature** method and we will take **2** gauss points as 2 points will be sufficient to accurately give our answer to polynomial integration.

Analysis Procedure

- We will run This code on octave to get values of displacements and stresses.
- We will also compare numerically calculated stresses and displacement with our analytical solution i.e => $u(x)=\frac{e}{e^2+1}(e^x-e^{-x})$
- We will plot graph of displacement for each node.
- Additionally, we will also see how difference in values of displacements from analytical and numerical solution varies with changing number of elements.

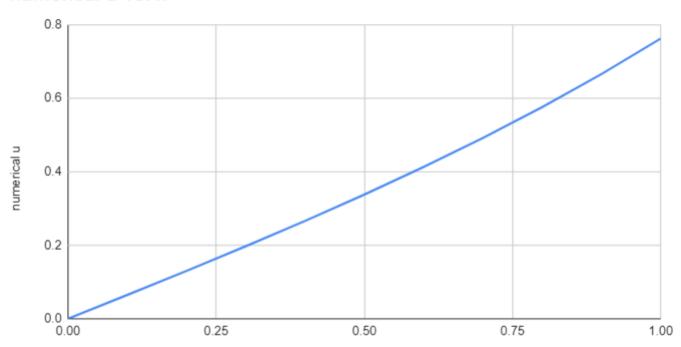
Observations

• Number of Elements: 10

- Root Mean Square Error (Displacements) = $9.8160*10^{-05}$

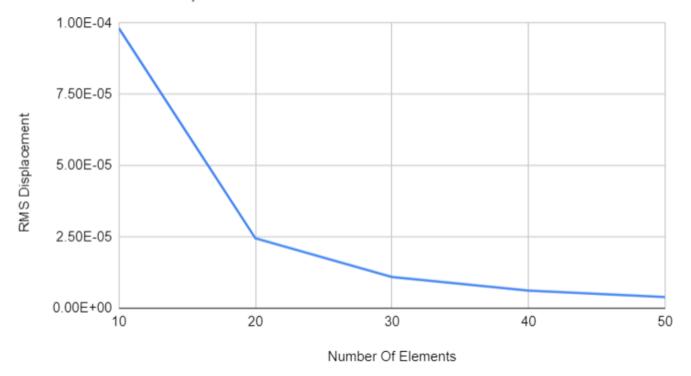
| x | analytical displacement | numerical displacement | numerical stress | analytical stress |
|-----|----------------------------|---------------------------|---------------------|----------------------|
| 0 | 0 | 0 | 0.6489 | 0.6489 |
| 0.1 | 0.0649 | 0.0649 | 0.6554 | 0.6554 |
| 0.2 | 0.1305 | 0.1304 | 0.6685 | 0.6684 |
| 0.3 | 0.1973 | 0.1973 | 0.6883 | 0.6882 |
| 0.4 | 0.2662 | 0.2661 | 0.7149 | 0.7148 |
| 0.5 | 0.3377 | 0.3376 | 0.7487 | 0.7486 |
| 0.6 | 0.4126 | 0.4125 | 0.79 | 0.7898 |
| 0.7 | 0.4916 | 0.4915 | 0.8393 | 0.839 |
| 0.8 | 0.5755 | 0.5754 | 0.8969 | 0.8966 |
| 0.9 | 0.6652 | 0.6651 | 0.9635 | 0.9632 |
| 1 | 0.7616 | 0.7615 | 1 | 1 |





| Number Of Elements | RMS Error in Displacement |
|--------------------|---------------------------|
| 10 | 9.82E-05 |
| 20 | 2.45E-05 |
| 30 | 1.09E-05 |
| 40 | 6.13E-06 |
| 50 | 3.92E-06 |

RMS Error in Displacement vs. Number Of Elements



Question 2

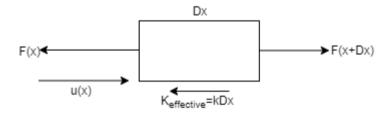
2. Solve the problem 1 when it is subjected to a temperature increase of $\Delta T = 1$. Recall that the stress is given by $\sigma = E(\epsilon - \alpha \Delta T)$, where $\alpha = 1$ is the coefficient of thermal expansion. Assume E = 1. (25)

Solution 2

• Code File: Question 2 Mfile

Deriving Governing Equation

Force Balance on an arbitrary element at distance x from bar



Total Displacement at position x on bar is $(u(x) + \alpha \Delta Tx)$

Total Displacement : $u(x) + \alpha \Delta Tx$ Displacement because of force and spring separately

Also, $\sigma=E(\epsilon)$ note the strain is not due to thermal displacements

$$F(x + \Delta x) - F(x) - k\Delta x(u(x) + x\alpha \Delta T) = 0$$

Dividing whole Equation by Δx

$$rac{(F(x+\Delta x)-F(x))}{\Delta x}-ku(x)-xlpha\Delta T=0$$

Take limit as $\Delta x o 0$

Now;

$$rac{dF}{dx}-ku-x=0$$
 {Note : Here $u=u(x)$ }

$$\sigma = rac{F}{A}$$
 also $\sigma = E(rac{du}{dx})$

E = Elasticity modulus, **A**= Cross Sectional Area

Thus,

$$F = EA(\frac{du}{dx} - \alpha\Delta T)$$

Known Boundary Conditions

$$u(0) = 0$$

$$\frac{du}{dx}\Big|_{x=l} = 1$$

and, Finally putting value of **F** in our governing equation

$$\frac{d}{dx}[EA(\frac{du}{dx} - \alpha\Delta T)] - ku - x = 0$$

Finally Putting values of constants in our equations, questions have asked us to take all constants as unity, so be it.

$$rac{d^2u}{dx^2}-u-x=0$$
 for $x\in(0,1)$

$$u(0) = 0$$

$$\frac{du}{dx} = 1$$
 at $x = 1$

Solving
$$rac{d^2u}{dx^2}-u-x=0$$
 for $x\in(0,1)$

with Boundary conditions

$$u(0) = 0$$

$$rac{du}{dx}=1$$
 at $x=1$

We get

$$=>u(x)=-rac{e^2x+x+2e^{1-x}-2e^{x+1}}{1+e^2}$$

Finally we get our analytical solution any any x.

$$=>$$
 $=> u(x) = -rac{e^2x + x + 2e^{1-x} - 2e^{x+1}}{1 + e^2}$

Deriving Weak Form

$$\int_1^2 \delta u \left(\frac{d^2 u}{dx^2} - u - x \right) dx = 0$$

 δu is weight function that varies linearly like u since we are going to take linear approximation for our calculations

Evaluating further

$$\int_{1}^{2} \left(\frac{d}{dx} (\delta u \frac{du}{dx}) - \frac{d\delta u}{dx} \frac{du}{dx} - \delta u u - \delta u x \right) dx = 0$$

According to our method our u varies linearly and it will be according to the following equation.

$$u = N_1 u_1 + N_2 u_2$$

$$N_1 = \frac{(x-x_2)}{(x_1-x_2)}$$

$$N_2 = rac{(x-x_1)}{(x_2-x_1)}$$

$$\mathbf{N} = egin{bmatrix} N_1 & N_2 \end{bmatrix}$$

$$\mathbf{B} = \mathbf{N}^{'} = egin{bmatrix} N_1^{'} & N_2^{'} \end{bmatrix}$$

$$\delta u = \mathbf{N} \delta u$$

$$u = \mathbf{N}u$$

$$\frac{du}{dx} = \mathbf{B}u$$

Putting above equations in our integral and simplifying

$$=\left.\delta urac{du}{dx}
ight|_{1}^{2}=\int\delta u^{T}\mathbf{B}^{T}\mathbf{B}udx+\int\delta u^{T}\mathbf{N}^{T}\mathbf{N}udx+\int\delta u^{T}\mathbf{N}^{T}xdx$$

$$=>F^N\delta u^T=\delta u^Tu(\int \mathbf{B}^T\mathbf{B}+\mathbf{N}^T\mathbf{N})dx+\int \delta u^T\mathbf{N}^Txdx$$

We can very conveniently compare above expression to F=Kx as we write

$$\mathbf{K} = \int (\mathbf{B}^T \mathbf{B} + \mathbf{N}^T \mathbf{N}) dx$$

and

$$F^B = \int \delta u^T \mathbf{N}^T x dx$$

there by leading to

$$F^N - F^B = \mathbf{K}u$$

For integrating above expression numerically we will be using **Gauss Quadrature** method and we will take **2** gauss points as 2 points will be sufficient to accurately give our answer to polynomial

integration.

Analysis Procedure

- We will run This code on octave to get values of displacements and stresses.
- We will also compare numerically calculated stresses and displacement with our analytical solution i.e => => $u(x)=-\frac{e^2x+x+2e^{1-x}-2e^{x+1}}{1+e^2}$
- We will plot graph of displacement for each node.

Observations

• Number of Elements: 10

- Root Mean Square Error (Displacements) = $1.994*10^{-04}$

| x | analytical displacement | numerical displacement | stress | analytical stress |
|-----|-------------------------|------------------------|--------|-------------------|
| 0 | 0 | 0 | 0.2979 | 0.2977 |
| 0.1 | 0.1298 | 0.1298 | 0.3109 | 0.3107 |
| 0.2 | 0.261 | 0.2609 | 0.337 | 0.3368 |
| 0.3 | 0.3947 | 0.3946 | 0.3765 | 0.3763 |
| 0.4 | 0.5324 | 0.5322 | 0.4298 | 0.4296 |
| 0.5 | 0.6754 | 0.6752 | 0.4975 | 0.4971 |
| 0.6 | 0.8252 | 0.825 | 0.5801 | 0.5797 |
| 0.7 | 0.9832 | 0.983 | 0.6786 | 0.6781 |
| 0.8 | 1.1511 | 1.1508 | 0.7938 | 0.7932 |
| 0.9 | 1.3305 | 1.3302 | 0.9271 | 0.9263 |
| 1 | 1.5232 | 1.5229 | 1 | 1 |

• Graph of Displacement vs x

