

Kane's Method: Finding Constraint Equations

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Kane's Equation

Recall Kane's equation in matrix form:

$$\Omega^T (T - I \alpha - \omega \times H) + V^T (F - ma) = 0$$

We've said that the matrices Ω and V project Euler's and Newton's equations into the state space spanned by the generalized speeds.

Let's step back and look at the bigger picture.

Rigid Bodies and Joints

- A system of rigid bodies has a total of $6N_b$ DOF
- Assign 6DOF to the root body
- Examine each joint
 - The outer body motion is dictated by the inner body motion and the joint DOFs
- A joint introduces 0-6 constraints (typically 1-5)
 - Example: a simple hinge introduces 3 translational constraints and 2 rotational constraints, leaving 1 DOF
- So each of the $6N_b$ potential DOFs either becomes a DOF or a constraint: $N_u + N_c = 6N_b$

Doing It the Hard Way

- Typical Newton-Euler formulations (ref Haug, etc) adjoin the constraint equations to the equations of motion and solve them together
- Introduces constraint forces (and torques) as additional unknowns to be solved for
 - These are obtained “for free”, in the sense that you have no choice but to obtain them
- Size of system to be solved is then $6N_b + N_c$
 - Solution time grows like $(6N_b + N_c)^3$
- Due to roundoff, constraints may not be perfectly satisfied
 - This can also degrade the accuracy of the overall solution

Kane's Method is Faster and More Accurate

- Constraints are identically satisfied
 - Numerical issues related to augmented systems are avoided entirely
- Size of system to solve is $6N_b - N_c$
 - Solution time grows like $(6N_b - N_c)^3$
 - Example: $N_b = 2$, $N_c = 5$ (a 1DOF hinge)
 - $6N_b + N_c = 17$, $6N_b - N_c = 7$
 - $7^3/17^3 = 0.07$
 - So Kane's Method is much faster
 - This system is solved 4x per time step for RK4
- Computation of constraint forces/torques is optional, not compulsory
 - 1x per time step (not 4x), and with no matrix inversion

Assigning DOFs and Constraints

- Every system starts out with $6N_b$ potential DOFs
- Give the root body (B_1) 6 DOFs
- Examine each joint in turn
 - Assign each potential DOF to an actual DOF or a constraint
 - For a tree topology, all potential DOFs will be accounted for
 - Non-tree topologies are a topic for another day

An Example Joint Definition

```
0 1          ! Inner, outer body indices
1  213  GIMBAL ! RotDOF, Seq, GIMBAL or SPHERICAL
0  123          ! TrnDOF, Seq
```

- Identify number of rotational, translational DOFs
- Give 3-element sequences in all cases
 - Ex: Rotational axis 2 is free, and axes 1 and 3 are constrained (in that order!)
- Spherical joints are distinguished from 3-DOF gimbal joints by additional keyword

Theory

Imagine the dynamical system with all potential DOFs.

We write Kane's equation:

$$\Omega_P^T [T - I(\Omega \dot{u} + \alpha_r) - \omega \times H] + V_P^T [F - m(V \dot{u} + a_r)] = 0$$

where Ω_P , V_P project into all $6 N_b$ dimensions of the state space.

Now partition Ω_P , V_P :

$$\Omega_P = [\Omega \quad \Omega_c], \quad V_P = [V \quad V_c]$$

where Ω , V project into the permissible motion subspace, and Ω_c , V_c project into the constrained subspace.

Equations of Motion

$$\Omega^T [T - I(\Omega \dot{u} + \alpha_r) - \omega \times H] + V^T [F - m(V \dot{u} + a_r)] = 0$$

Rearrange to solve for \dot{u} :

$$(\Omega^T I \Omega + V^T m V) \dot{u} = \Omega^T (T - I \alpha_r - \omega \times H) + V^T (F - m a_r)$$

- An $N_u \times N_u$ system of equations to solve by Gaussian elimination (or similar)
- Propagate using RK4
 - Requires system to be solved four times per timestep
- If constraints are unwanted, this gives the complete solution

Equations of Constraint

$$\Omega_c^T [T - I(\Omega \dot{u} + \alpha_r) - \omega \times H] + V_c^T [F - m(V \dot{u} + a_r)] = 0$$

Rearrange to isolate generalized constraint forces:

$$F_c = \Omega_c^T T + V_c^T F = \Omega_c^T [I(\Omega \dot{u} + \alpha_r) + \omega \times H] + V_c^T [m(V \dot{u} + a_r)]$$

- All terms on RHS are known from solution of equations of motion
- No simultaneous solution needed (no matrix inverse!)
 - Simply matrix multiplication and addition
- Evaluated once per timestep (not four times, as would be if it were solved along with equations of motion)
- Completely optional
 - Find all, some, or none as desired

Conclusion

- Kane's method provides a straightforward way to obtain constraint forces and torques
- Accuracy of equations of motion is not compromised as happens when EOM are augmented with constraint equations
- Computational complexity of Kane's method is much less than for augmented formulation
- Addition of constraint equations is much less burdensome by using Kane's method
 - Constraint equations do not “perturb” equations of motion
 - No matrix inversion
 - Solve once per timestep, not four times (for RK4)
 - Can restrict attention to those constraints of interest

Appendix: Example from OSIRIS-REX

Example from OSIRIS-REX

- To study the dynamics of the Touch-And-Go (TAG) maneuver, we built a model of O-Rex in 42 with:
 - Main Body: 6 DOF
 - Shoulder and Elbow Joints: All DOF constrained
 - To find constraint forces and torques
 - Pogo Joint: 1DOF Translation
 - Wrist: 2DOF Gimballed
- Following slides show part of output file Tree00.42
 - Documents partition of potential DOFs into DOFs and constraints

Main Body has 6DOF

```
*****
Body 00:   RotSeq = 123   TrnSeq = 123
              Col in      Col in      Col in
Axis       F/C      u[ ]   x[ ]      u00.42   x00.42   Constraint00.42
-----
Rot1        F        00    00          01      01          --
Rot2        F        01    01          02      02          --
Rot3        F        02    02          03      03          --
(Sph)       -        --    03          --      04          --

Trn1        F        06    07          07      08          --
Trn2        F        07    08          08      09          --
Trn3        F        08    09          09      10          --
```

Shoulder and Elbow are Constrained

```

*****
Joint 00:    RotSeq = 213    TrnSeq = 123
              Col in      Col in      Col in
Axis         F/C      u[ ]  x[ ]      u00.42  x00.42  Constraint00.42
-----
Rot1          C        --   --        --      --          01
Rot2          C        --   --        --      --          02
Rot3          C        --   --        --      --          03

Trn1          C        --   --        --      --          04
Trn2          C        --   --        --      --          05
Trn3          C        --   --        --      --          06
*****
Joint 01:    RotSeq = 213    TrnSeq = 123
              Col in      Col in      Col in
Axis         F/C      u[ ]  x[ ]      u00.42  x00.42  Constraint00.42
-----
Rot1          C        --   --        --      --          07
Rot2          C        --   --        --      --          08
Rot3          C        --   --        --      --          09

Trn1          C        --   --        --      --          10
Trn2          C        --   --        --      --          11
Trn3          C        --   --        --      --          12

```

Pogo and Wrist Joints

```

*****
Joint 02:   RotSeq = 213   TrnSeq = 312
              Col in      Col in      Col in
Axis        F/C      u[ ]  x[ ]      u00.42  x00.42  Constraint00.42
-----
Rot1         C        --   --        --      --      13
Rot2         C        --   --        --      --      14
Rot3         C        --   --        --      --      15

Trn1         F        03   04        04      05      --
Trn2         C        --   --        --      --      16
Trn3         C        --   --        --      --      17
*****
Joint 03:   RotSeq = 213   TrnSeq = 123
              Col in      Col in      Col in
Axis        F/C      u[ ]  x[ ]      u00.42  x00.42  Constraint00.42
-----
Rot1         F        04   05        05      06      --
Rot2         F        05   06        06      07      --
Rot3         C        --   --        --      --      18

Trn1         C        --   --        --      --      19
Trn2         C        --   --        --      --      20
Trn3         C        --   --        --      --      21

```