

Stability Aspects of Scalable delay differential equations

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Introduction

Delay Differential Equations (DDE's):

$$\frac{dx(t)}{dt} = f(x(t), x(t-\tau_1), \dots, x(t-\tau_m)) \quad (1)$$

$$\tau_1, \tau_2, \dots, \tau_m \geq 0$$

$$x(t) = \phi(t), \quad t \leq t_0$$

DDE's are infinite dimensional systems.

$$\frac{dx(t)}{dt} + x(t-\tau) = 0, \quad t \geq 0 \quad (2)$$

Substituting $x(t) = e^{st}$, we get $s + e^{-s\tau} = 0$ — Infinite roots for s .

Scalability:

$$x(t) = f(x, y) \quad (3)$$

$$y(t) = g(x, y) \quad (4)$$

Scalability in $x(t)$

If $x(t)$ and $y(t)$ are the solutions and $ax(t)$ and $y(t)$ are also solutions for $a \geq 0$

Icons: <https://flaticon.com/>

3

Objective and Problem Statement

Hayes DDE with Hysteresis:

$$z(t) = -p z(t) - q z(t-1) - \gamma \theta(t) z(t) \quad (5)$$

$$\theta(t) = \frac{\kappa}{|z(t)| + \epsilon} [\theta_0 + \beta \operatorname{sgn}(z(t) z(t)) - \theta(t)] |z(t)| \quad (6)$$

Where

$$\operatorname{sgn}(x) = \frac{x}{|x|}$$

$$p, q \in \mathbb{R}$$

$$\theta_0, \beta, \kappa > 0$$

$$\epsilon \rightarrow 0^+$$

$$\gamma > 0$$

γ represents the damping of the hysteresis force $\theta(t) z(t)$.

Salient Features :

- Infinite dimensions.
- Non linear and coupled.
- Slope discontinuities at every load reversals.
- Scalable in z (Partially scalable).

If z is a solution, αz is also solution with $\alpha > 0$

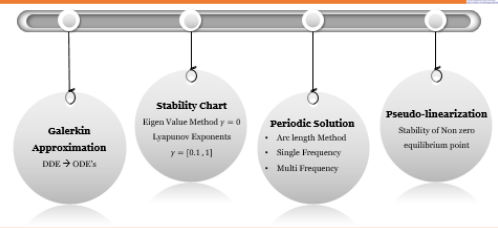
Problem Statement:

Stability analysis of above Hayes equation with Hysteresis for $\gamma \in [0, 0.1, 1]$.

Halju et al., 2018, Stability aspects of the Hayes delay differential equation with scalable hysteresis

4

Methodology



5

Equilibrium zones: Pseudo-linearization

• Equilibrium conditions

$$z(t) = 0, \theta(t) = 0 \text{ \& } z(t-1) = z(t) \quad (22)$$

• We get

$$\gamma \theta = -(p+q) \quad (23)$$

• For the chosen Hysteresis model $\theta \in [0.2, 3.8]$

• The parameter plane containing non zero equilibrium points is $0.2\gamma = -(p+q)$ and $3.8\gamma = -(p+q)$

• Let z_* and θ_* be the non zero equilibrium points, taking small variations

$$\begin{aligned} z(t) &= z_* + \eta(t) \\ \theta(t) &= \theta_* + \phi(t) \end{aligned} \quad (24)$$

• Neglecting higher order terms and using scalability

$$\begin{aligned} \eta(t) &= q(\eta(t) - \eta(t-1)) - \gamma \phi(t) \\ \phi(t) &= \kappa(\theta_* - \theta_*)\eta(t) + \kappa \beta \eta(t) \end{aligned} \quad \text{Non Linear} \quad (25)$$

17

Summary and Conclusions

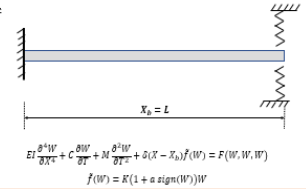
- Studied the stability charts and boundaries of Hayes DDE with hysteresis.
- Scalability of hysteresis force allowed us to use Lyapunov like exponents.
- Numerical difficulties in computing periodic solution through continuation are resolved using Multi-frequency method.
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19

Future Work

Problem Statement:

Stability Analysis of the Heat Exchanger when the cladding just lost initial contact with the tube. Cladding stiffness is asymmetric



20

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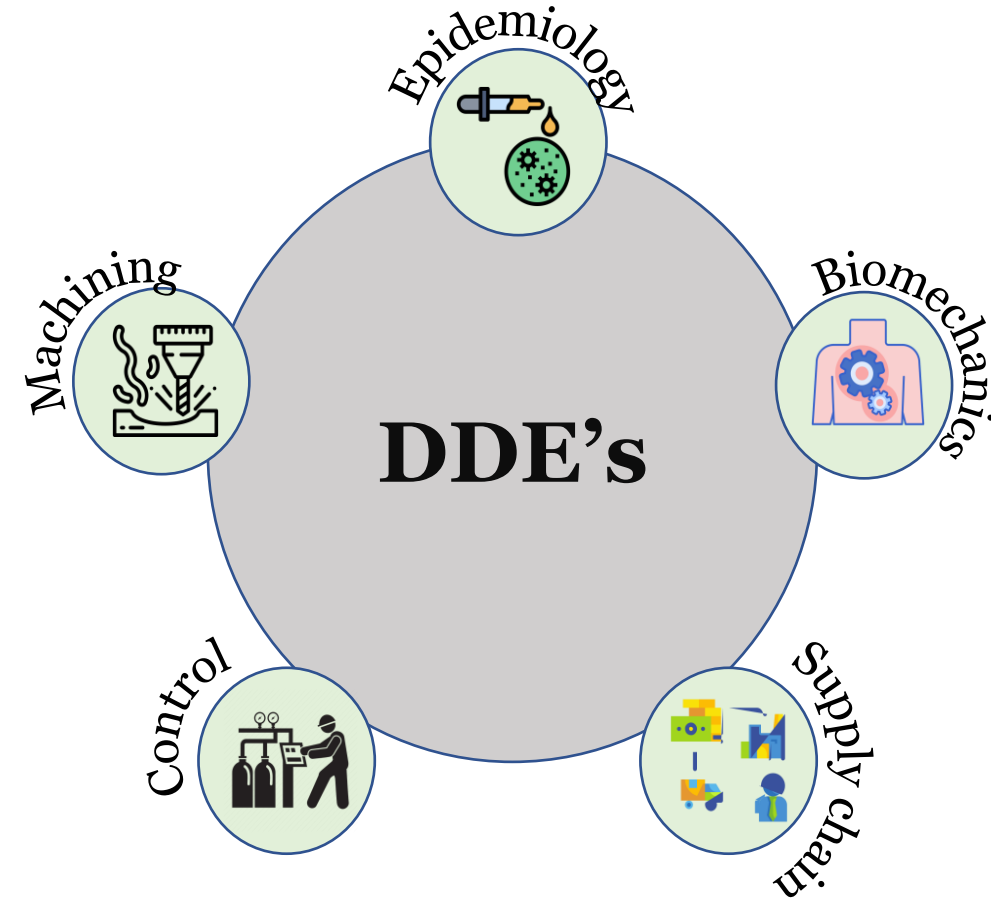
Scalability:

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Scalability in $x(t)$

If $x(t)$ and $y(t)$ are the solutions and $\alpha x(t)$ and $y(t)$ are also solutions for $\alpha \geq 0$



Objective and Problem Statement

Hayes DDE with Hysteresis:

$$\dot{z}(t) = -pz(t) - qz(t-1) - \gamma\theta(t)z(t) \quad (5)$$

$$\dot{\theta}(t) = \frac{\kappa}{|z(t)| + \epsilon} \{ \theta_a + \beta \operatorname{sgn}(z(t)\dot{z}(t)) - \theta(t) \} |\dot{z}(t)| \quad (6)$$

Where

$$\operatorname{sgn}(x) = \frac{x}{|x|}$$

$$p, q \in \mathbb{R}$$

$$\theta_a, \beta, \kappa > 0$$

$$\epsilon \rightarrow 0^+$$

$$\gamma > 0$$

γ represents the damping of the hysteresis force $\theta(t)z(t)$.

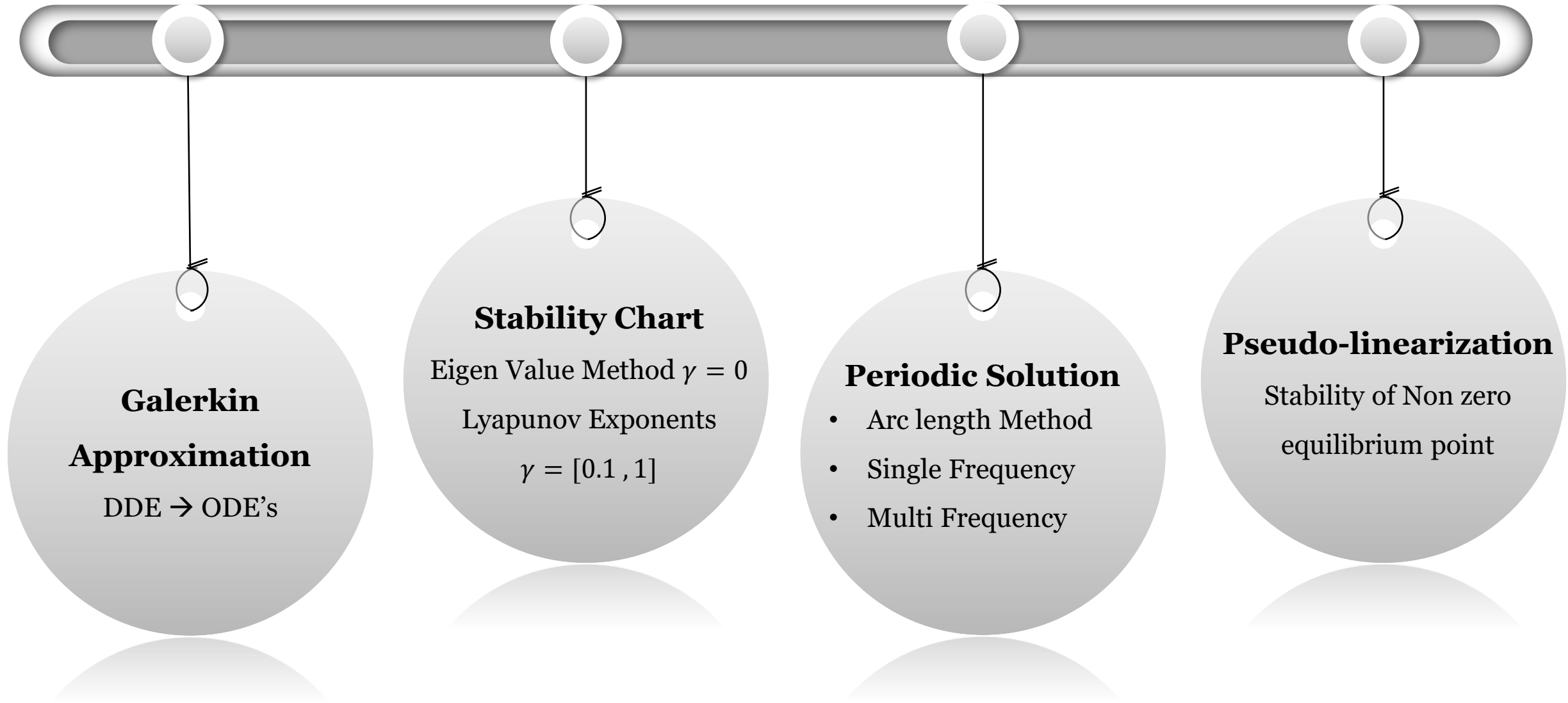
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If z is a solution, αz is also solution with $\alpha > 0$

Problem Statement:

Stability analysis of above Hayes equation with Hysteresis for $\gamma = [0 ; 0.1; 1]$.



Methodology: Galerkin Approximation

Galerkin Approximation:

$$z(t-s) = F(t,s) = a_0(t) + a_1(t)s + \sum_{k=1}^{N-2} a_{k+1}(t)\sin(k\pi s) \quad (7)$$

Where $a_0(t), \dots, a_{N-1}(t)$ are state variables, N : Number of shape functions.

$$\frac{\partial F}{\partial t} + \frac{\partial F}{\partial s} = 0 \quad (8)$$

$$z(t) = F(t,0) = a_0(t) \Rightarrow \dot{z}(t) = \dot{a}_0(t) \quad (9)$$

Residual, $R(t,s)$

$$R(t,s) = \int_0^s \left(\frac{\partial F}{\partial t} + \frac{\partial F}{\partial s} \right) ds \quad (10)$$

Galerkin approximation method

$$\int_0^1 R(t,s) s ds = 0 \quad (11)$$

$$\int_0^1 R(t,s) \sin(k\pi s) ds = 0, k = 1, \dots, N-2 \quad (12)$$

Methodology: Galerkin Approximation

Considering $N=15$, we get 16 system of coupled ODE's of the form

$$\frac{d\mathbf{a}(t)}{dt} = \mathbf{g}(\mathbf{a}(t)) \quad (13)$$

Where

$$\mathbf{a}(t) = [a_0(t), \dots, a_{14}(t), \theta(t)]'$$

$$\mathbf{g}(\mathbf{a}(t)) = [g_1(\mathbf{a}(t)), \dots, g_{16}(\mathbf{a}(t))']'$$

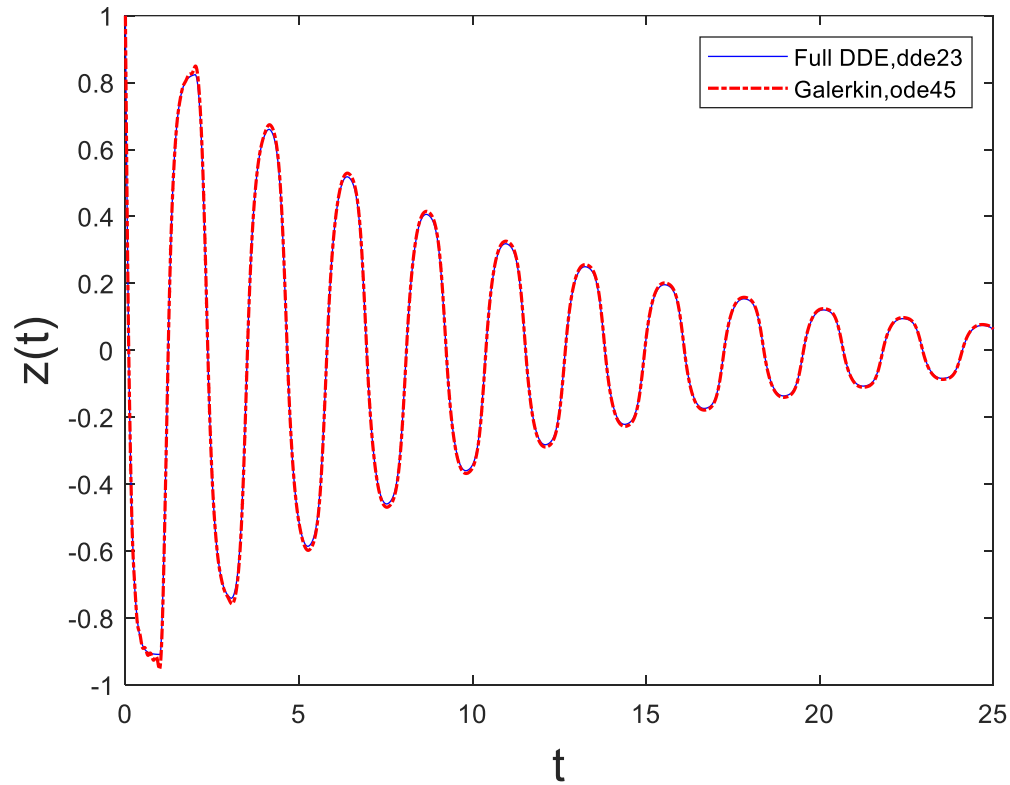
Integrate the above system of ODE's using MATLAB's ode45.

We used the following parameters:

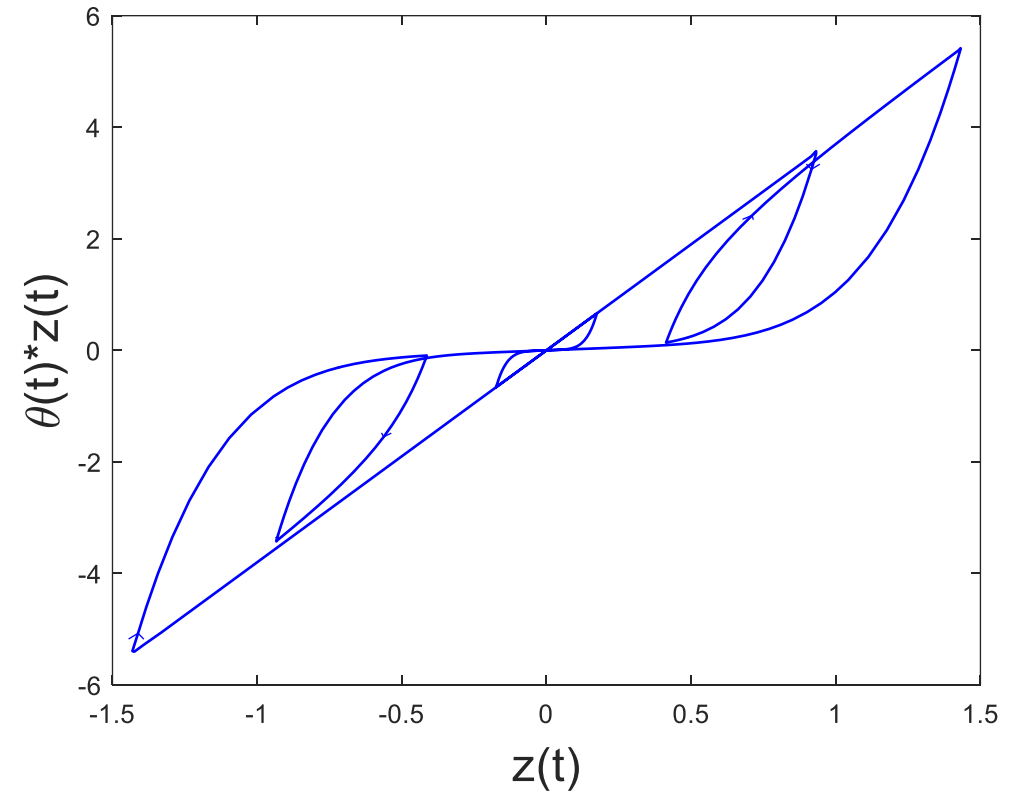
$$p = 5; q = 8; \gamma = 1; \kappa = 4; \theta_a = 2; \beta = 1.8; \epsilon = 10^{-6}$$

ODE: Ordinary differential equations

Methodology: Galerkin Approximation

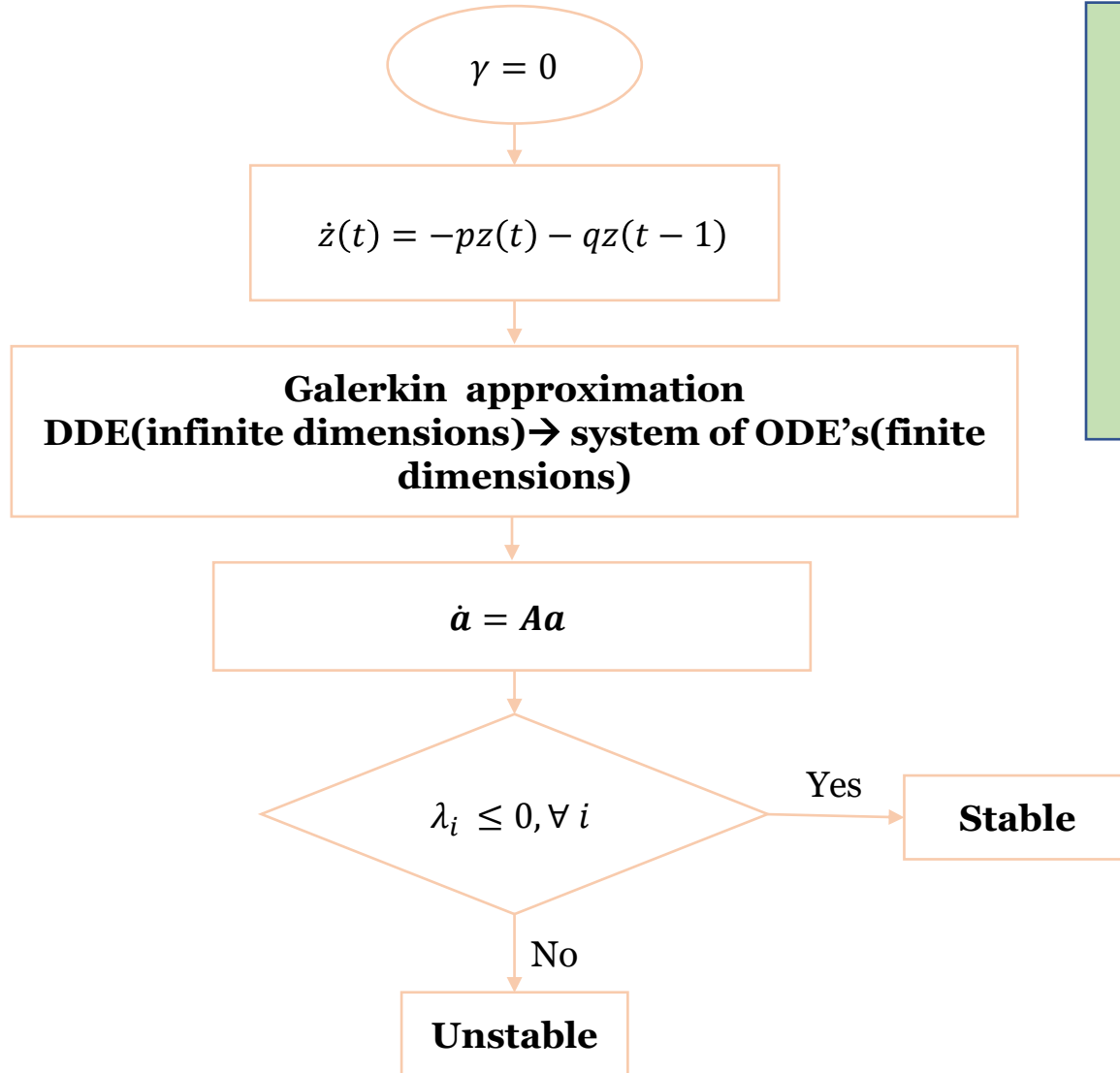


Comparison of solutions obtained from full DDE solution using MATLAB's dde23 and Galerkin approximation



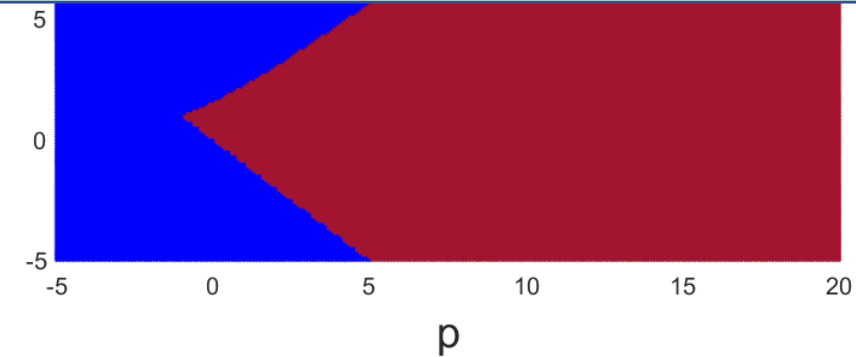
Response of Hysteresis model.

Methodology: Stability Analysis $\gamma = 0$



$$\dot{z}(t) = -pz(t) - qz(t - 1) - \gamma\theta(t)z(t) \quad (5)$$

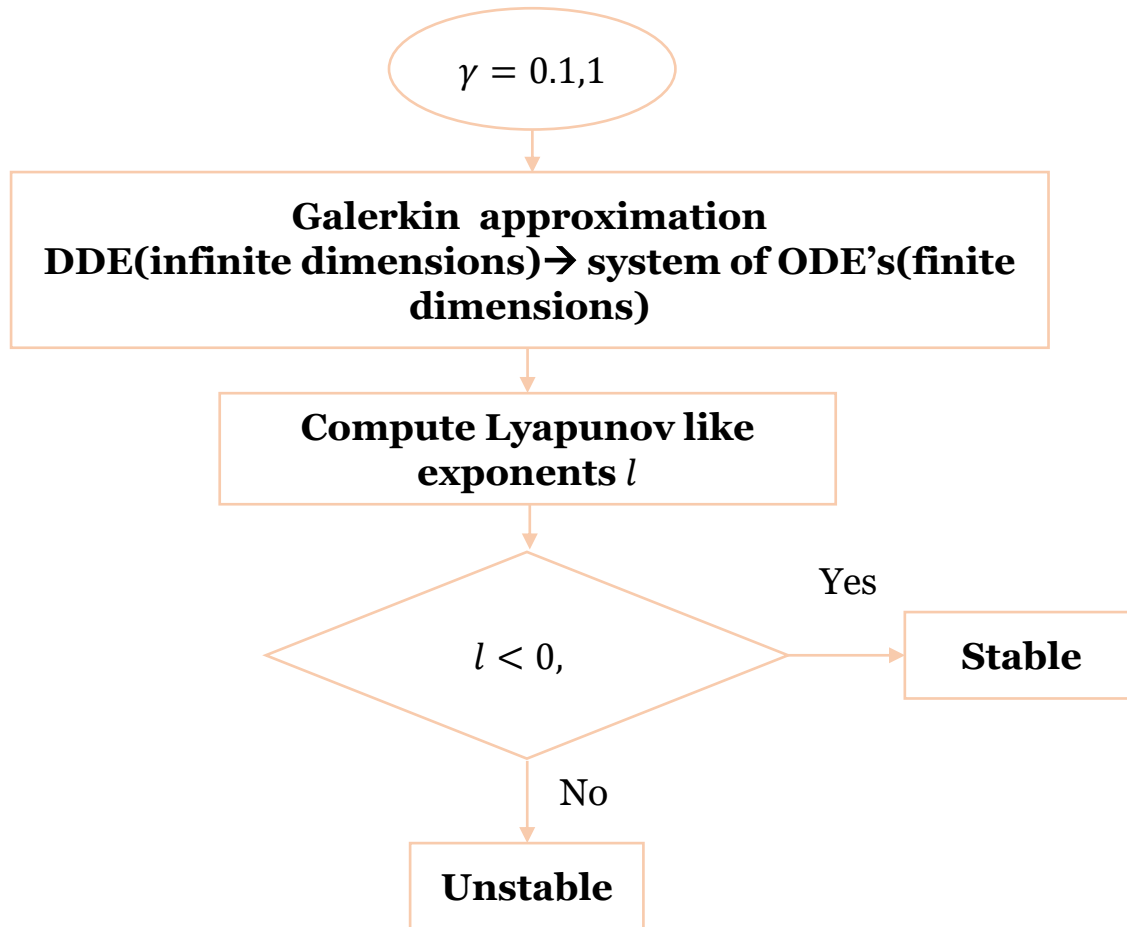
$$\dot{\theta}(t) = \frac{\kappa}{|z(t)| + \epsilon} \{ \theta_a + \beta \operatorname{sgn}(z(t)\dot{z}(t)) - \theta(t) \} |\dot{z}(t)| \quad (6)$$



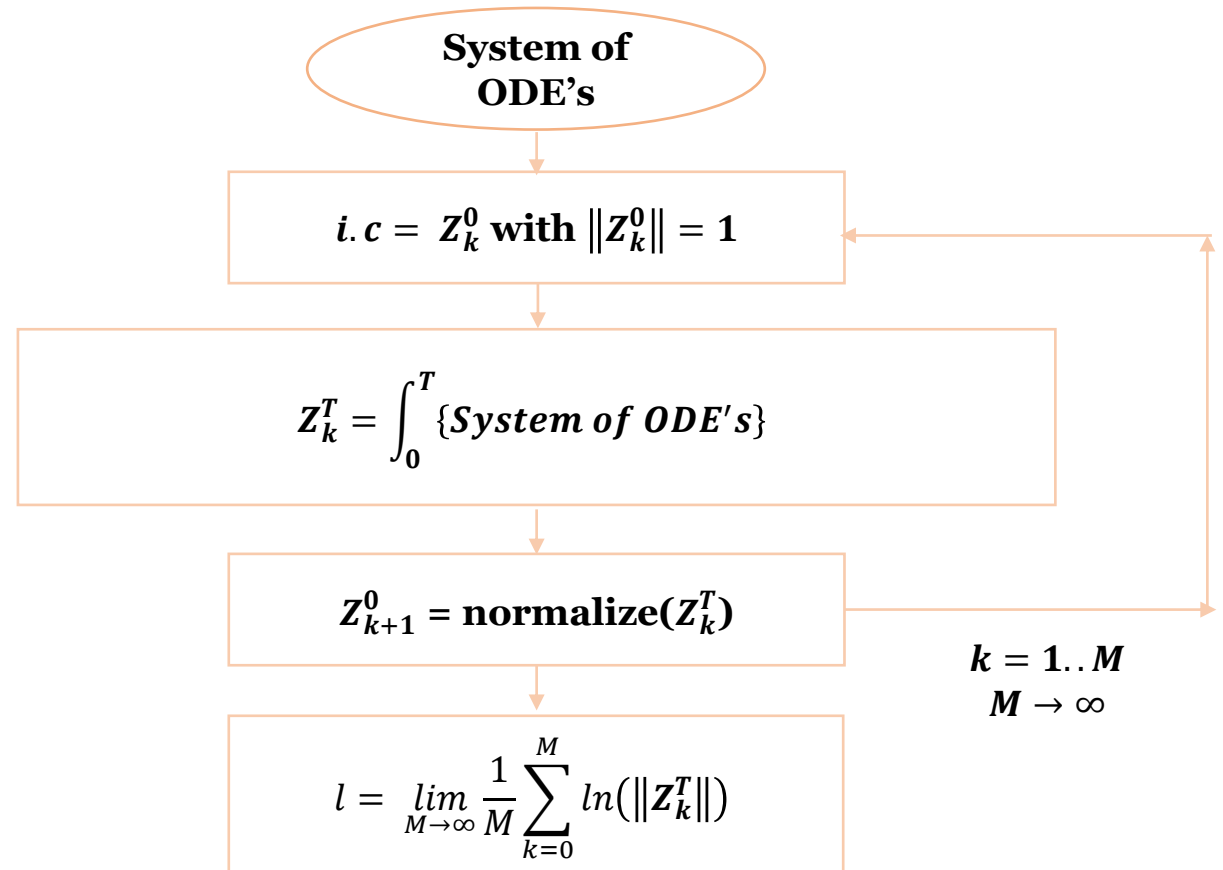
Stability Chart for $\gamma = 0$. Blue is unstable and brown indicates stable regions.

Methodology: Stability Analysis damped

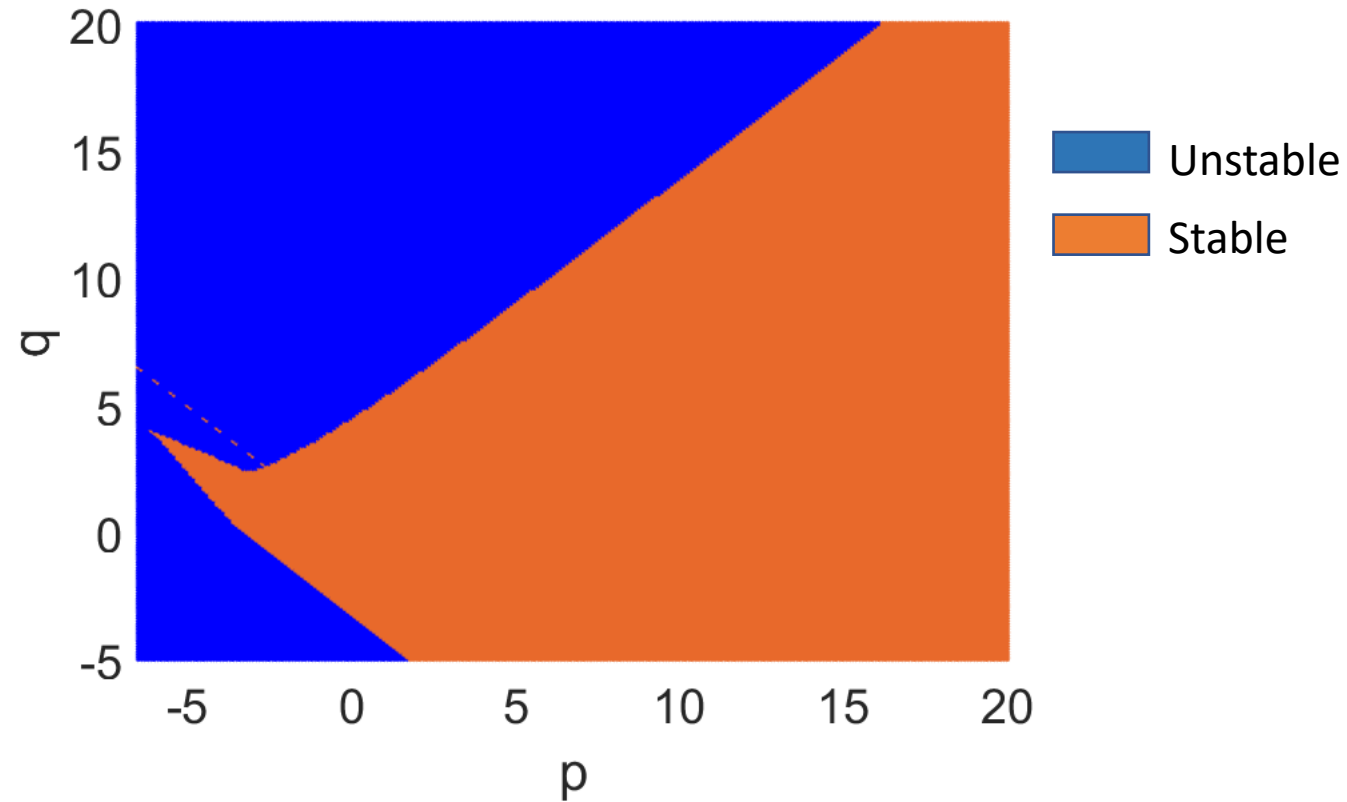
Stability Analysis



Calculation of Lyapunov like exponents



Methodology: Stability Analysis damped



Stability Chart for $\gamma = 1$. Blue is unstable and orange indicates stable regions.

Methodology: Periodic Solution-Arc length method

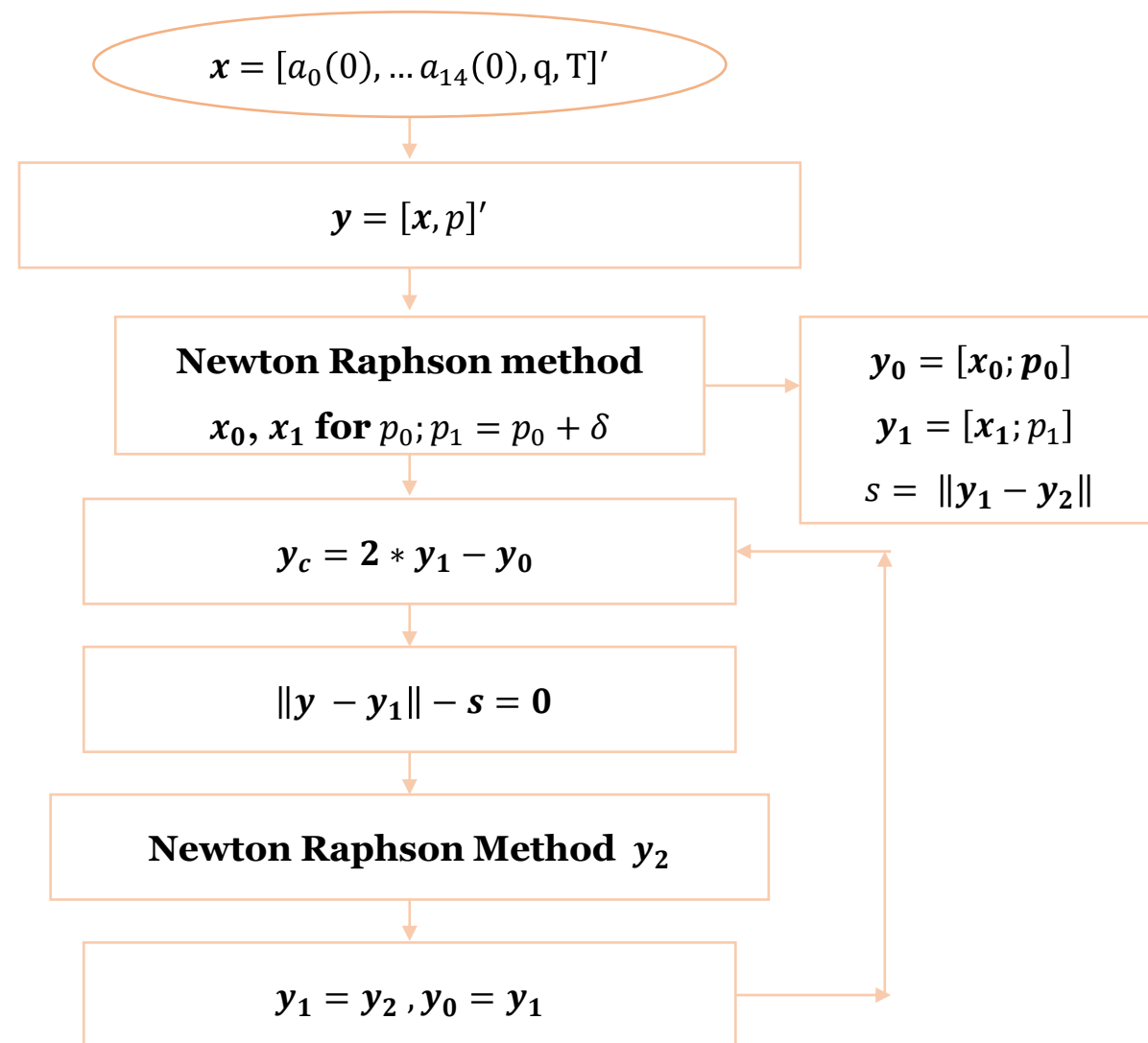
Arc length based numerical continuation method :

$$\text{Periodicity} \left\{ \begin{array}{l} a_0(T) - a_0(0) = 0, \\ a_1(T) - a_1(0) = 0, \\ \cdot \\ \cdot \\ \cdot \\ a_{N-1}(T) - a_{N-1}(0) = 0, \\ \theta(T) - \theta(0) = 0 \\ \psi(T) - T = 0 \end{array} \right. \quad (14)$$

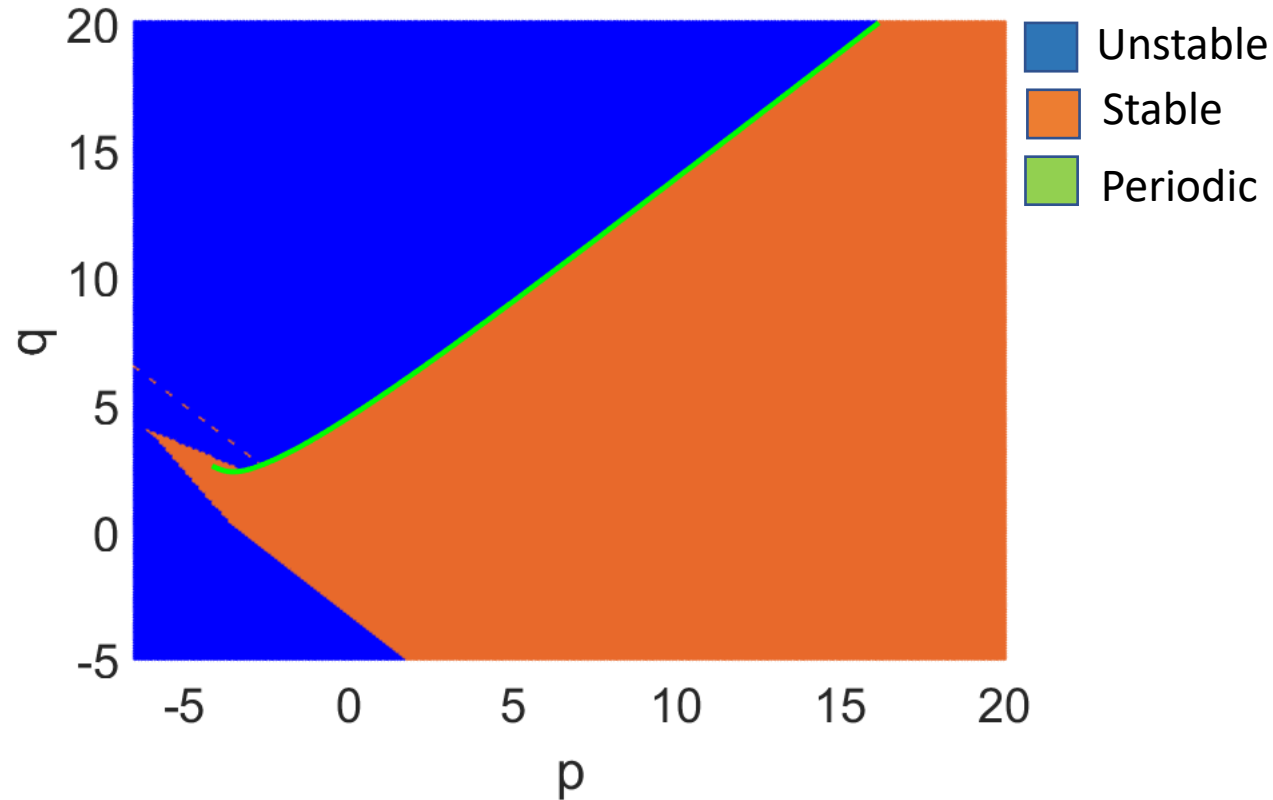
Setting RMS value of $a_0(t) = 1$; $\dot{\psi} = a_0(t)^2$, $\psi(0) = 0$;

For $N = 15$, Unknown $x = [a_0(0), \dots a_{14}(0), q, T]'$

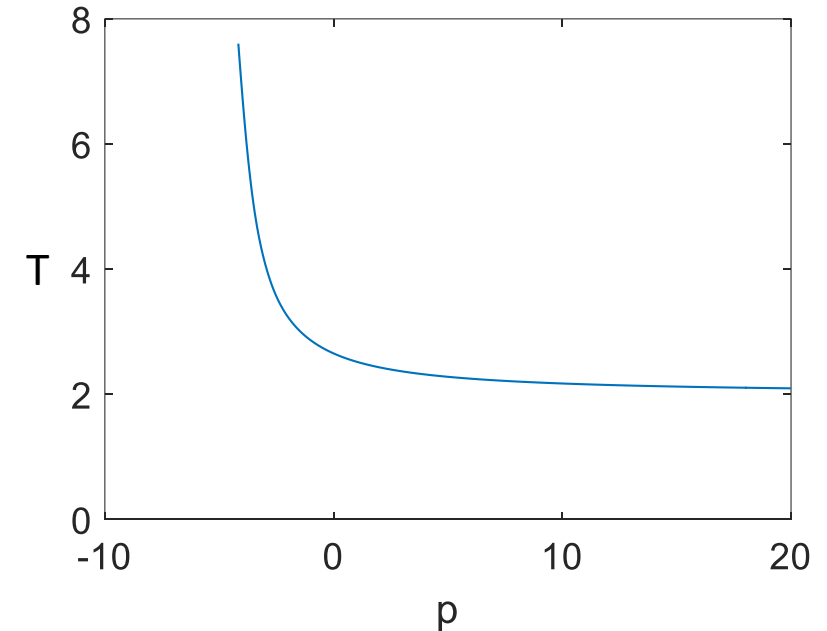
p is the independent variable



Methodology: Periodic Solution-Arc length method



Stability Chart for $\gamma = 1$. Blue is unstable and orange indicates stable regions. Periodic solution obtained using Arc length denoted by green curve



Arc length method: Plot of P vs T

Methodology: Periodic Solution – Single Frequency

- Assume $z(t) = \sin(\omega t)$ (15)

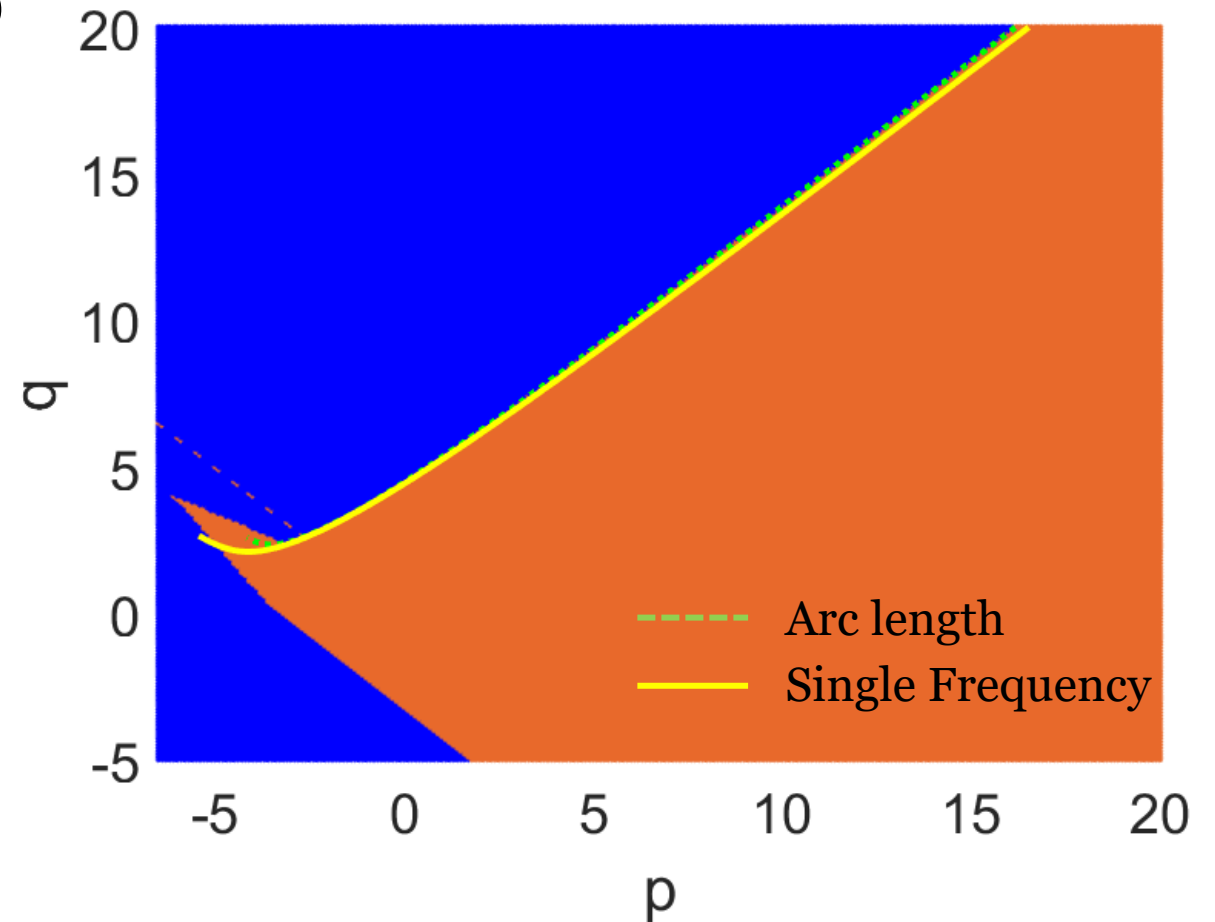
- By fitting the solution using hysteresis model

$$\theta(t)z(t) \approx \alpha_0 \sin(\omega t) + \alpha_1 \cos(\omega t) \quad (16)$$

- Substituting the above two into eq.(5) and eq.(6)

- Set the coefficients of cos and sin to zero

$$\left. \begin{aligned} p + q \cos(\omega) + \gamma \alpha_0 &= 0 \\ \omega - q \sin(\omega) + \gamma \alpha_1 &= 0 \end{aligned} \right\} \quad (17)$$



Periodic solution obtained using Single frequency
Harmonic Balance method denoted by yellow curve

Methodology: Periodic Solution – Multi Frequency method

- Define distorted time scale

$$\tau = \omega t + \sum_{k=1}^n [A_k \sin(k\omega t) + B_k (\cos(k\omega t) - 1)] \quad (18)$$

- Assume $z(\tau) = \sin(\tau)$ (19)
- Hysteresis response

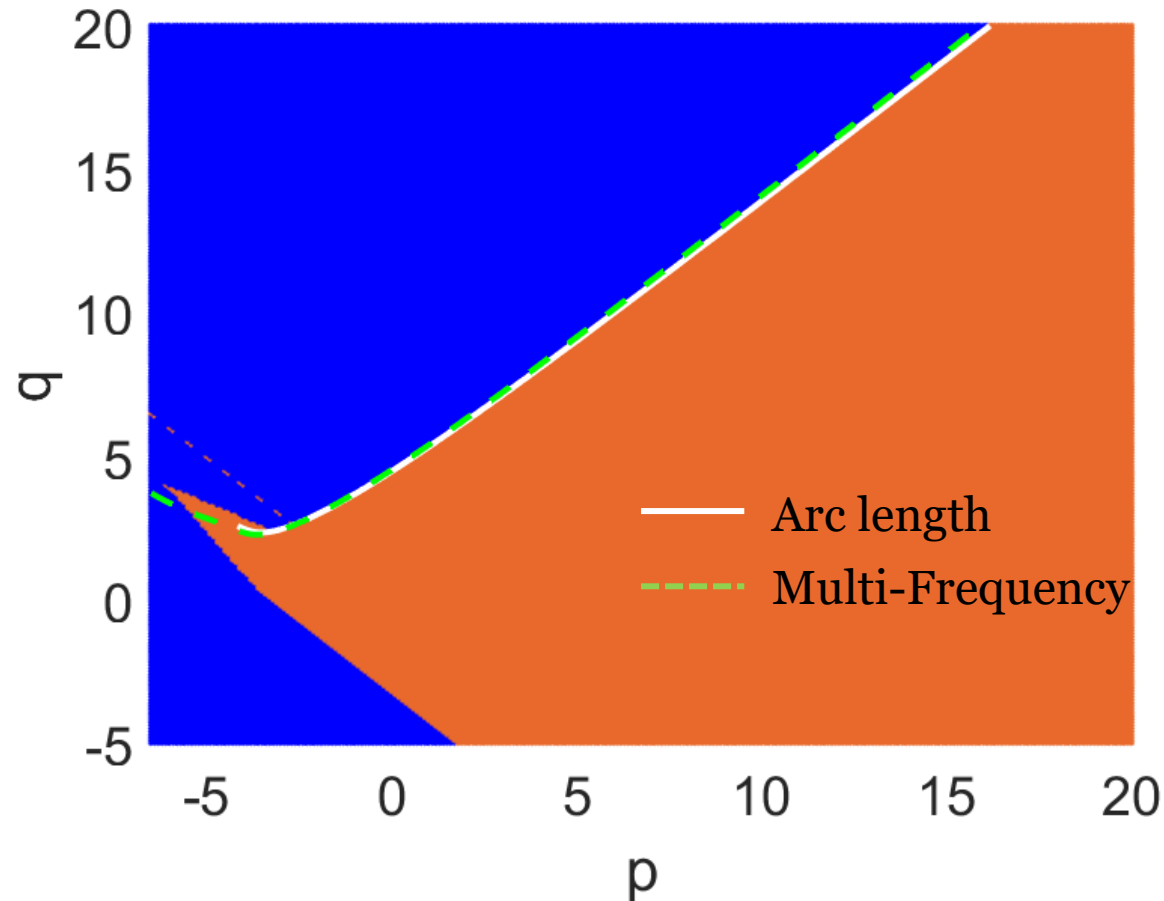
$$\theta(\tau)z(\tau) \approx \alpha_0 \sin(\tau) + \alpha_1 \cos(\tau) + \alpha_2 \sin(3\tau) + \alpha_3 \cos(3\tau) \quad (20)$$

- Numerically fitting we get $\alpha_0 = 3.125, \alpha_1 = 0.7638, \alpha_2 = -0.5625, \alpha_3 = -0.3829$
- Define Residual $R(p, q, \mathbf{A}, \mathbf{B}, \omega, t)$
- Minimizing R in least square sense, we get $2n+2$ equations.

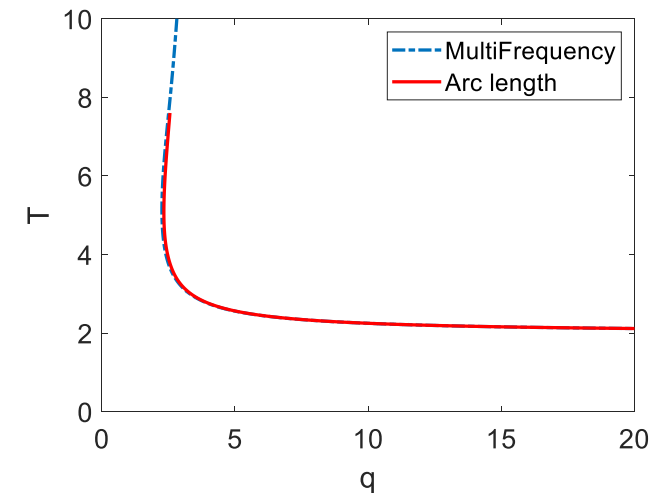
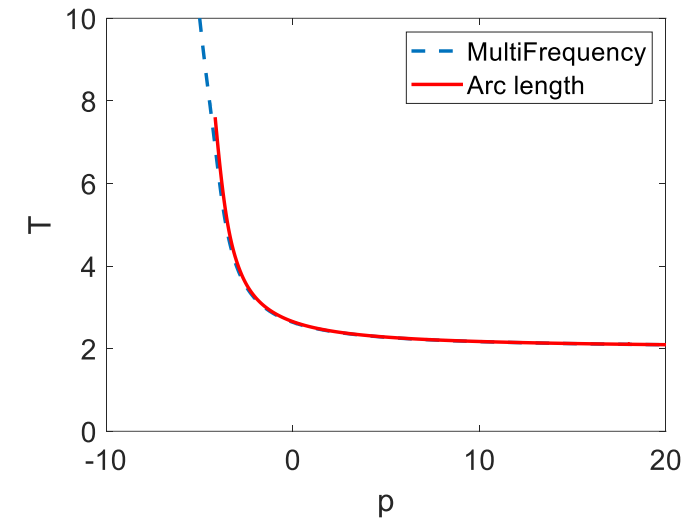
$$\frac{\partial}{\partial p} \int_0^{\frac{2\pi}{\omega}} R^2 dt = 0, \frac{\partial}{\partial q} \int_0^{\frac{2\pi}{\omega}} R^2 dt = 0, \frac{\partial}{\partial A_i} \int_0^{\frac{2\pi}{\omega}} R^2 dt = 0, \frac{\partial}{\partial B_i} \int_0^{\frac{2\pi}{\omega}} R^2 dt = 0 \quad (21)$$

- Keeping ω as a independent variable , we can solve for p, q, A_i, B_i

Methodology: Periodic Solution – Multi Frequency method



Periodic solution obtained using Multi- frequency method
denoted by dotted green curve



Equilibrium zones: Pseudo-linearization

- Equilibrium conditions

$$\dot{z}(t) = 0, \dot{\theta}(t) = 0 \text{ \& } z(t - 1) = z(t) \quad (22)$$

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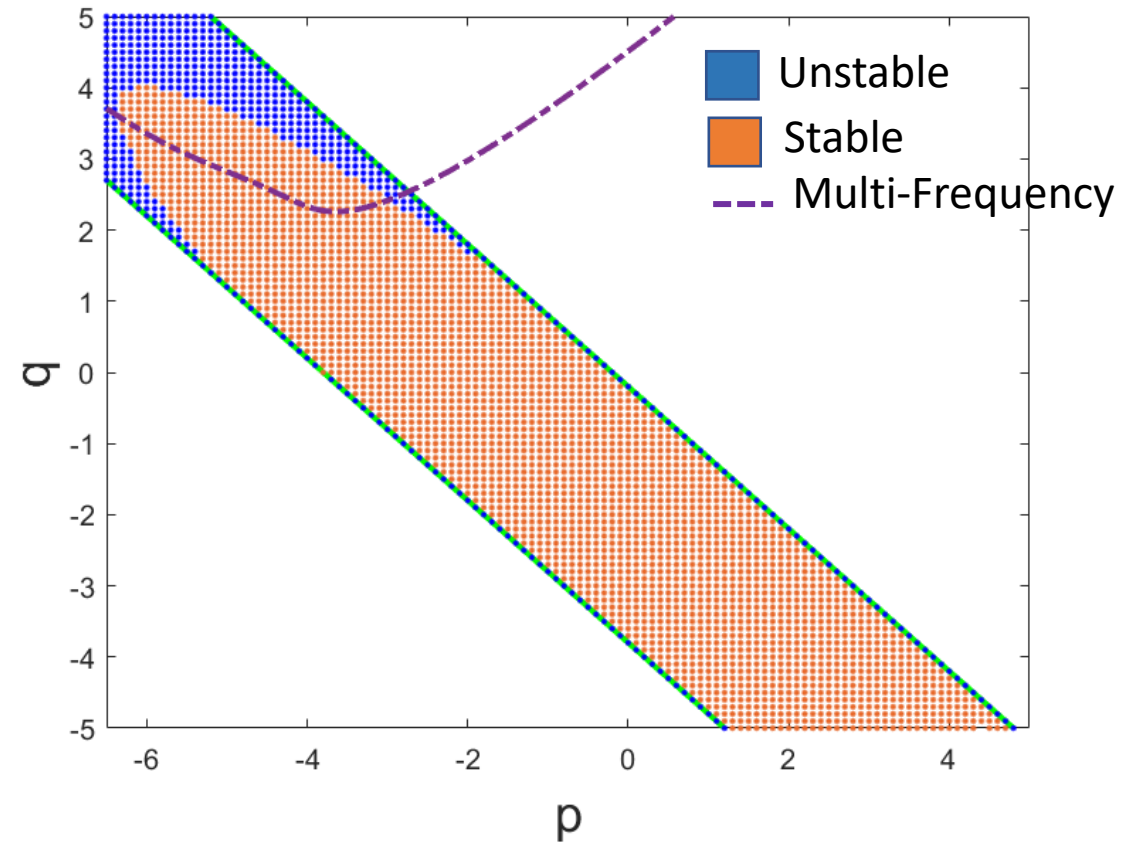
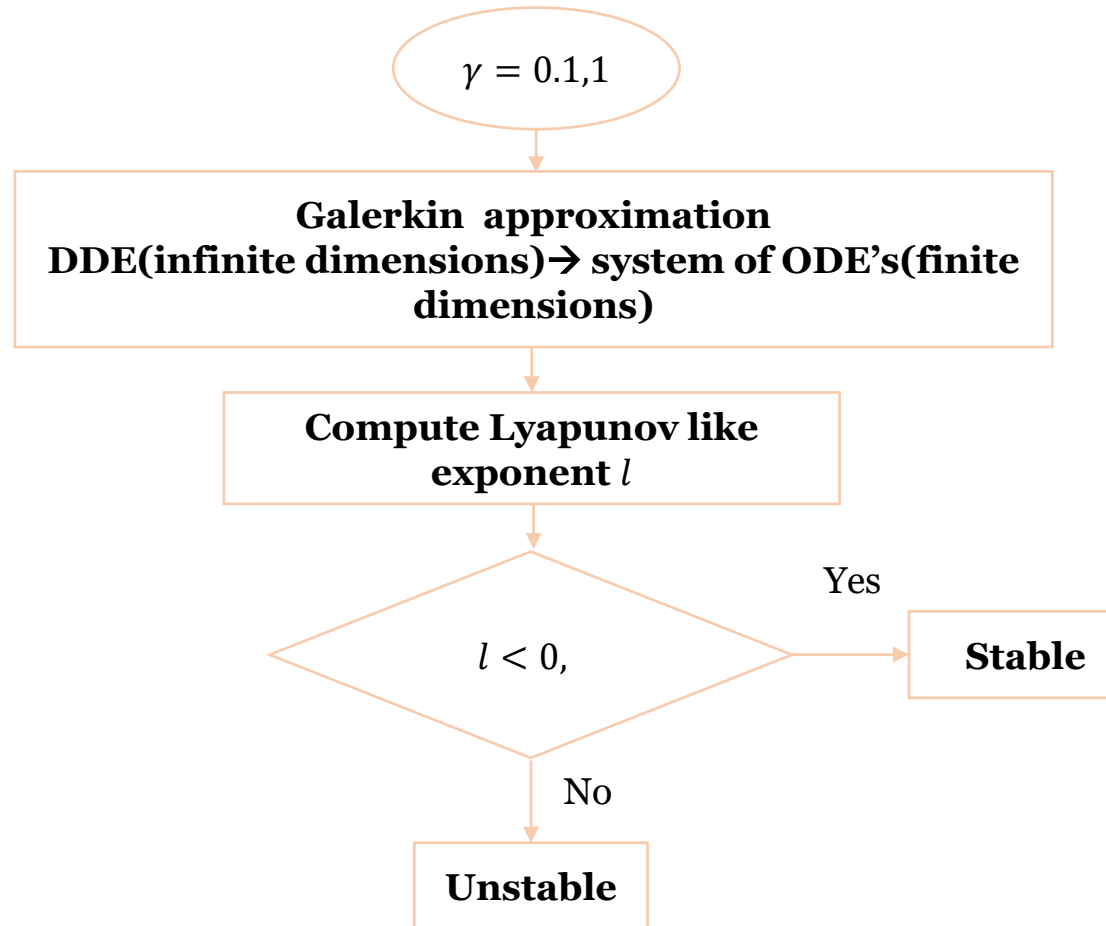
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$$\left. \begin{aligned} \dot{\eta}(t) &= q(\eta(t) - \eta(t - 1)) - \gamma\phi(t) \\ \dot{\phi}(t) &= \kappa(\theta_a - \theta_c)|\dot{\eta}(t)| + \kappa\beta\dot{\eta}(t) \end{aligned} \right\} \text{ Non Linear} \quad (25)$$

Equilibrium zones: Pseudo-linearization



Periodic solution obtained using pseudo-linearization.
Parametric zone with non zero equilibrium points are represented using green lines

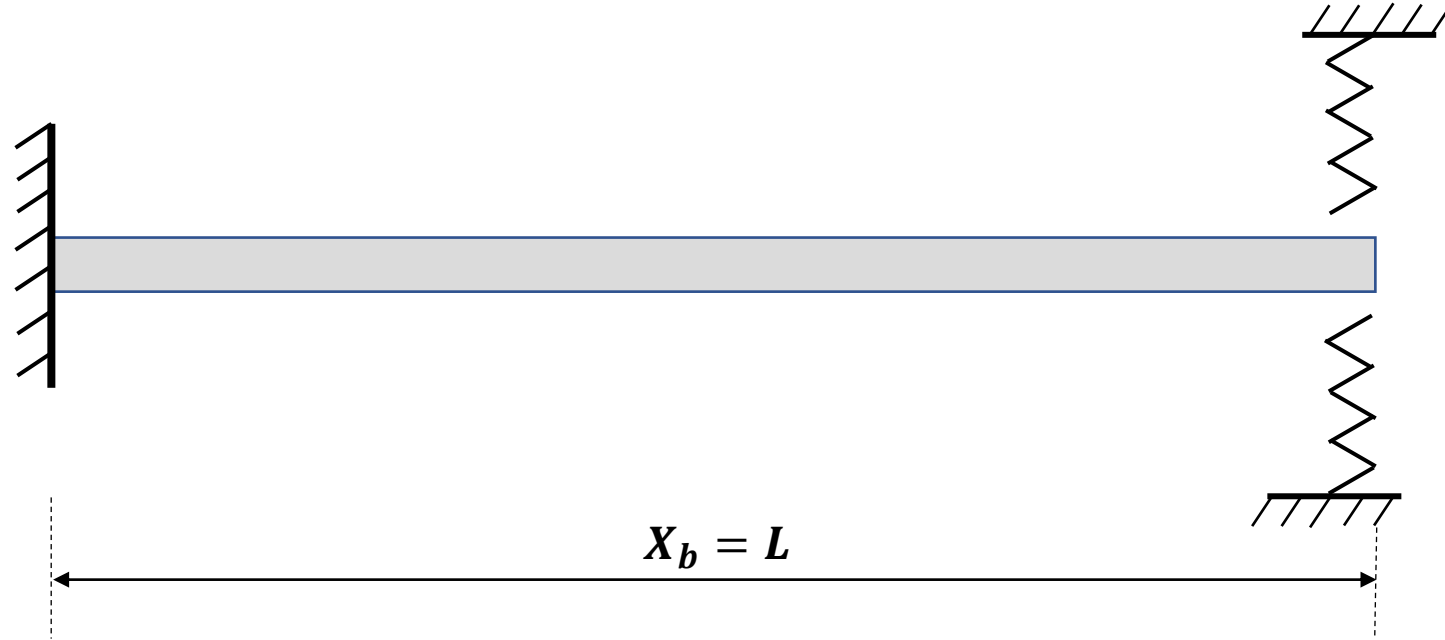
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Future Work

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Stability Analysis of the Heat Exchanger when the cladding just lost initial contact with the tube. Cladding stiffness is asymmetric



$$EI \frac{\partial^4 W}{\partial X^4} + C \frac{\partial W}{\partial T} + M \frac{\partial^2 W}{\partial T^2} + \delta(X - X_b) \tilde{f}(W) = F(W, \dot{W}, \ddot{W})$$

$$\tilde{f}(W) = K(1 + a \operatorname{sign}(W))W$$

Acknowledgement

I thank my supervisor Dr. C.P. Vyasarayani for guiding me through difficulties in the problem, and my lab mate Balaji, Junaid for their suggestions.