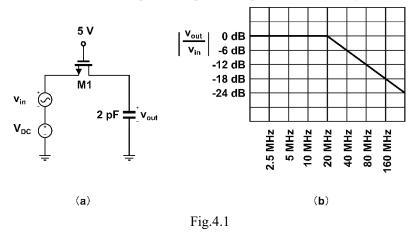
Exercise 4

Table 4.1

| Trained Descent to Value | | | | |
|--------------------------|-----------------------|-------------------------|-----------|----------------|
| | | Typical Parameter Value | | |
| Parameter Symbol | Parameter Description | n-Channel | p-Channel | Units |
| V_{T0} | Threshold | 0.7 | -0.8 | V |
| | voltage(V_{BS} =0) | | | |
| K | Transconductance | 134 | 50 | μ Α /V² |
| | parameter(in | | | |
| | saturation) | | | |
| γ | Bulk threshold | 0.45 | 0.4 | $V^{1/2}$ |
| | parameter | | | |
| λ | Channel length | 0.1 | 0.2 | V-1 |
| | modulation parameter | | | |
| $2 \varphi_{\rm F} $ | Surface potential at | 0.9 | 0.8 | V |
| | strong inversion | | | |

 $[*]K = \mu C_{OX}$

4-1 For the circuit in Fig.4.1(a) assume that there are no capacitance parasitics associated with M1. The voltage source v_{in} is a small-signal value, whereas voltage source V_{DC} has a dc value of 3 V. Design M1 to achieve the asymptotic frequency response shown in Fig.4.1(b).



Answer:

f(-3dB) = 20MHz,thus $\omega = 40\pi$ M rad/s.Note that since no dc current flows through the transistor, the dc value of the drain-source voltage is zero.

$$r_{ON} = \frac{L}{KW(V_{GS} - V_T)}, \text{ then } \frac{1}{RC} = \frac{KW(V_{GS} - V_T)}{LC} \text{ find } \frac{W}{L} = \frac{C \times 40\pi \times 10^6}{K(V_{GS} - V_T)}$$

$$V_T = V_{T0} + \gamma \left(\sqrt{|2\varphi_F| + |v_{bS}|} - \sqrt{|2\varphi_F|} \right) = 0.7 + 0.45 \times \left(\sqrt{0.9 + 3} - \sqrt{0.9} \right) = 1.16$$

$$\frac{W}{L} = \frac{2 \times 10^{-12} \times 40\pi \times 10^6}{134 \times 10^{-6} \times (2 - 1.16)} = 2.23$$

$$Vt=0.7$$
, $w/l=2.88$

- 4-2 Fig.4.2 illustrates a source-degenerated current source. M1 with W/L=2u/1u.
 - (a) Using Table 4.1 model parameters, calculate the output resistance at the given current bias. Ignore the body effect.
 - (b) Calculate the minimum output voltage required to keep the device in saturation.

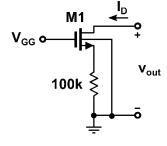


Fig.4.2

Answer:

The small-signal model if this circuit is shown below

$$\begin{array}{c|c}
 & i_{D} \\
 & \downarrow \\
 &$$

(a)
$$V_S = I_D \times r = 1 \text{V}, r_{out} = r + r_{ds} + [(g_m + g_{mb})r_{ds}]r$$
.

$$g_m = \sqrt{2 \times \frac{KW}{L} I_D} = 73.2 \times 10^{-6}$$

$$g_{mb} = g_m \frac{\gamma}{2(2|\Phi_F| + V_{SB})^{\frac{1}{2}}} = 11.9 \times 10^{-6}$$

$$g_{ds} = \lambda I_D = 1 \times 10^{-6}$$

$$r_{ds} = \frac{1}{g_{ds}} = 1 \times 10^6$$

thus
$$r_{out} = 9.61 \times 10^6$$

(b)
$$V_T = V_{T0} + \gamma \left(\sqrt{|2\varphi_F| + |v_{bs}|} - \sqrt{|2\varphi_F|} \right) = 0.89 \ V. V_{GS} = \left(\sqrt{2 \times \frac{L}{KW}} I_D + V_T \right) = 1.16 V. V_{GG} = V_{GS} + V_S = 2.16 \ V. V_{out} > V_{GG} - V_T = 1.27 V$$

4-3 Calculate the output resistance and the minimum output voltage, while maintaining all devices in saturation, for the circuits shown in Fig.4.3. Assume that i_{OUT} is actually $10\mu A$. Use Table 4.1 for device model information. $V_{bs}=0$ V.

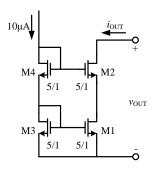
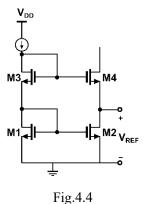


Fig .4.3

Answer:

$$\begin{split} V_{GS3} &= V_{GS4} = \left(\sqrt{2 \times \frac{L}{KW} I_D} + V_T\right) = 0.17 + 0.7 \, V = 0.87 \, \text{V}. \\ g_{m2} &= g_{m4} = \sqrt{2 \times \frac{KW}{L} I_D} = 115.8 \times 10^{-6} \\ r_{out} &= r_{ds1} + r_{ds2} + g_{m2} r_{ds1} r_{ds2}. \\ r_{ds1} &= r_{ds2} = \frac{1}{\lambda I_D} = 1 \times 10^6 \\ r_{out} &= 117.8 \times 10^6 \\ v_{out} &= V_{GS3} + V_{GS4} - V_{T2} = 1.04 \, V \end{split}$$

4-4 A reference circuit is shown in Fig.4.4, assume that $(W/L)_1=(W/L)_2=(W/L)_3=4$, $(W/L)_4=1$, please derive a symbolic expression of V_{REF} . (已知各管处于饱和区且各管阈值电压为 V_{Ti})



Answer:

$$\begin{split} V_{REF} &= V_{GS1} + V_{GS3} - V_{GS4} \\ V_{REF} &= V_{ON1} + V_{T1} + V_{ON3} + V_{T3} - V_{ON4} - V_{T4} \\ V_{T3} &= V_{T4} \\ V_{ON4} &= 2 \times V_{ON1} = 2 \times V_{ON3} \\ V_{REF} &= V_{T1} \end{split}$$

4-5 As the circuits shown in Fig.4.5, I_{REF} =0.3mA and γ =0. Using the model parameters in Table 4.1,

- (a) Calculate the voltage V_b when $V_X=V_Y$;
- (b) If V_b is 100mV smaller than the value in (a), calculate the deviation of I_{out} from 300 μА.

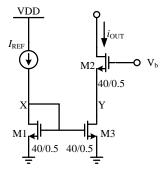


Fig.4.5

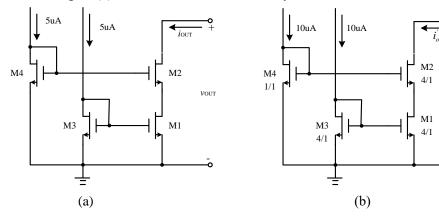
Answer:

(a)
$$V_{GS1} = \left(\sqrt{2 \times \frac{L}{KW} I_{REF}} + V_T\right) = 0.24 + 0.7 = 0.94 \, V. V_b = 2 \times V_{GS1} = 1.88 \, V.$$

(b)
$$\lambda(L=0.5u) = 2 \times \lambda(L=1u) = 0.2V^{-1}$$

$$I_{out} = I_{REF} \frac{1 + \lambda(V_{GS1} + \Delta V_b)}{1 + \lambda V_{GS1}}, \ \Delta I_{out} = I_{REF} \frac{\lambda \Delta V_b}{1 + \lambda V_{GS1}} = -5.05 \times 10^{-6}$$

4-6 Design M3 and M4 of Fig.4.6(a) so that the output characteristics are identical to the circuit shown in Fig.4.6(b). It is desired that i_{OUT} is ideally 10uA.



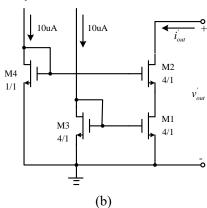


Fig.4.6

(a)
$$V_{GS1} = V_{GS3}, V_{GS2} = V_{GS4}, I_3 = I_4 = 5uA$$
, $I_{out} = 10uA$, we must have $(\frac{W}{L})_{1} = 2 \times (\frac{W}{L})_{3}$, $(\frac{W}{L})_{3} = 2/1$.

In (b)
$$i_3 = i_4 = 10uA = i_1$$
, $(\frac{W}{L})_4 \times V_{Dsat4}^2 = (\frac{W}{L})_1 \times V_{Dsat1}^2$, $V_{Dsat4} = 2 \times V_{Dsat1}$, $V_{GS4} = V_T + V_{Dsat4}$, $V_{GS2} = V_T + V_{Dsat4}$, $V_{out} > V_{GS2} - V_T = V_{Dsat4} = 2 \times V_{Dsat1}$
In (a) $I_3 = I_4 = 5uA = 2 \times I_1$, $(\frac{W}{L})_4 \times V_{Dsat4}^2 = \frac{1}{2} (\frac{W}{L})_1 \times V_{Dsat1}^2$

because,
$$\frac{V_{Dsat4}}{V_{Dsat1}} = \sqrt{\frac{1}{2} \times \left(\frac{W}{L}\right)_{1} / \left(\frac{W}{L}\right)_{4}} = 2$$
, $\left(\frac{W}{L}\right)_{4} = \frac{1}{8} \times \left(\frac{W}{L}\right)_{1} = 1/2$