- The Laplace transform provides a broader characterization of continuoustime LTI systems and their interaction with signals than is possible with Fourier methods. For example, the Laplace transform can be used to analyze a large class of continuous-time problems involving signals that are not absolutely integrable, such as the impulse response of an unstable system. The FT does not exist for signals that are not absolutely integrable, so FT-based methods cannot be employed in this class of problems.

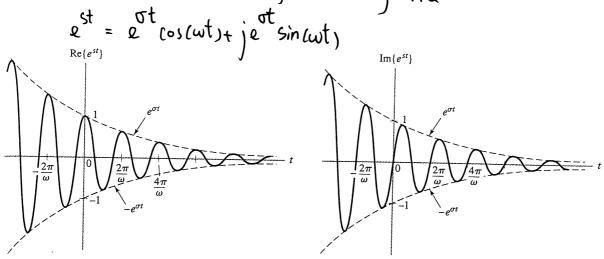
- The Laplace transtorm comes in two varieties: (1) unilateral, or one sided and (2) bilatery, or two sided. The unilateral Laplace transform is a convenient tool for solving differential equations with initial conditions. The bilateral Laplace transform others insight into the nature of system characteristics such as stability, causality and frequency response.

- The primary role of the laplace transform in engineering is the transient and stability analysis of causal LTI systems described by differential equations.

- French mathematician: Pierre-Simon Laplace developed a mathematical method tor solving differential equations by the use of algebraic techniques.

- British physicist Oliver Heaviside is credited with early may of operational methods in circuit analysis.

The Laplace Transform let est be a complex exponential with complex freq S=O+jw. We may write



อง. เอเนอล สาพงเสกับร

- The real part of est is an exponentially damped cosine, and the imaginary part is an exponentially damped sine. (In the figure, it is assumed that Jis negation.)

- The real part of s is the exponential damping factor J, and the imaginary part of s is the frequency of the costne and sine factor, namely, w.

- consider applying an input of the form xct = est to an LTI system with impulse

response het. The system output is given by

 $y(t) = H \left\{ x(t) \right\} = h(t) * x(t) = \int_{-\infty}^{\infty} h(x) x(t-x) dx$ to obtain $\int_{-\infty}^{\infty} (t-x) dx$

We use $x(t) = e^{st}$ to obtain $\int_{-\infty}^{\infty} h(x)e^{-sx} dx = e^{st} \int_{-\infty}^{\infty} h(x)e^{-sx} dx$

we define the transfer function His = 100 hiz = 500 hiz = 500 hiz

50 that we may write yet; H & est 3 = H(5) est

The action of the system on an input est is multiplication by the transfer function H(5). If an eigenfunction is defined as a signal that passes through the system without being modified except for multiplication by a scalar. Hence, we identify est as an eigenfunction of the LTI system and H(5) as the corresponding eigenvalue.

Next, we express the complex-valued transfer function Hiss in polar form as

Hiss= |Hiss= | \$\phi(s)\$ where |Hiss| and \$\phi(s)\$ are the magnitude and phase of Hiss,

respectively. Now we rewrite the LTI system output as

y(t)= |H(s)|e)\(\phi(s)\)_est

we use s=0+jw to obtain
y(t)=|H(0+jw)|e otejwt+d(0+jw)

= $|H(\sigma+j\omega)|e^{\sigma t}\cos(\omega t+\phi(\sigma+j\omega)) + j|H(\sigma+j\omega)|e^{\sigma t}\sin(\omega t+\phi(\sigma+j\omega))$

the system changes the amplitude of the input by /H(o+jw) and shifts the phase of the sinusoidal components by $\phi(\sigma+j\omega)$

- The system does not change I'm damping factor or or the sinusoidal frequency w of the input.

Laplace transform representation

we want to find a representation of arbitrary signals as a weighted superposition of eigenfunctions est. Substituting S = Of jw, and using t as the variable of integration:

100. - (05+)(15+1) 100 1 100 111

H(o+jw) = sont het) = (o+jw) t dt = sont het) = jwt dt

This indicates that $H(\sigma + j\omega)$ is the Fourier transform of hetze there, the inverse Fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be hetze to the fourier transform of $H(\sigma + j\omega)$ must be the fourier transform of $H(\sigma + j\omega)$ the fourier transform of $H(\sigma + j\omega)$ must be the fourier transform of $H(\sigma + j\omega)$ must be the fourier transform of $H(\sigma + j\omega)$ and $H(\sigma + j\omega)$ must be the fourier transform of $H(\sigma + j\omega)$ and $H(\sigma + j\omega)$ must be the fourier transform of $H(\sigma + j\omega)$ and $H(\sigma + j\omega)$ must be the fourier transform of $H(\sigma + j\omega)$ and $H(\sigma + j\omega)$ must be the fourier transform of $H(\sigma + j\omega)$

hetie =
$$\frac{1}{2\pi} \int_{-\infty}^{\infty} H(\sigma + j\omega) e^{j\omega t} d\omega$$

heti = $e^{j\omega} \int_{-\infty}^{\infty} H(\sigma + j\omega) e^{j\omega t} d\omega = \frac{1}{2\pi} \int_{-\infty}^{\infty} H(\sigma + j\omega) e^{j\omega t} d\omega$

Now, substituting S = 0+jw and dw = ds, we get

... The Laplace transform of xets is And the inverse Laplace transform

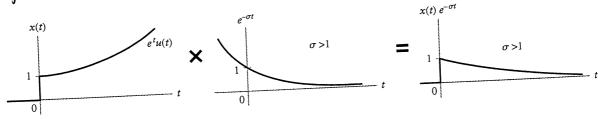
$$X(s) = \int_{-\infty}^{\infty} x(t) e^{-st} dt$$

$$\times (t) = \frac{1}{2\pi i} \int_{\sigma - i\infty}^{\sigma + i\infty} X(s) e^{st} ds$$

[Convergence] A necessary condition for convergence of the Laplace transform is the absolute integrability of xct) etc.

∫on |xitient |dt <∞

The range of or for which the Laplace transform converges is termed the region of convergence (ROC). Note that the Laplace transform exists for signals that do not have a Fourier transform. By limiting ourselves to a certain range of o, we ensure have a Fourier transform. By limiting ourselves to a certain range of o, we ensure that xct e ot is absolutely integrable, even though xct is not absolutely integrable per integrable by itself.



The S-plane It's convenient to represent the complex frequency s graphically in terms of a complex plane termed the s-plane. The horizontal axis represents the real part of s (i.e. the exponential damping factor o), and the vertical axis represents the imaginary part of s (i.e. the sinusoidal frequency).

represents the imaginary part of s (i.e. the sinusoidal freque).

If xets is absolutely integrable, turn we may obtain the Fourier transform from

the Laplace transform by setting 0=0;

In the s-plane, $\sigma=0$ corresponds to the imaginary axis. We thus say that the Fourier transform is given by the Laplace transform evaluated along the imaginary axis

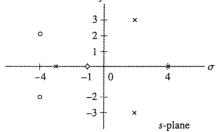


FIGURE 6.3 The s-plane. The horizontal axis is Re $\{s\}$ and the vertical axis is Im $\{s\}$. Zeros are depicted at s=-1 and $s=-4\pm 2j$, and poles are depicted at s=-3, $s=2\pm 3j$, and s=4.

The jw-axis divides the s-plane in half. The region of the s-plane to the left of the jw-axis is turned the left half of the s-plane, while the region to the right of the jw-axis is termed the right half s-plane. The real part of sis negative in the left half and positive in the right half of the plane.

poles and zeros) The most commonly encountered form of the Laplace transform in engineering is a ratio of two polynomials in s; that is,

$$X(s) = \frac{b_{m}s^{m} + b_{m-1}s^{m-1} + \dots + b_{0}}{s^{n} + a_{n-1}s^{n-1} + \dots + a_{1}s + a_{0}}$$

It is useful to tactor Xis) as a product of turns involving tu roots of the denominator and numerator polynomials:

$$X(s) = \frac{b_m TT_{k=1}^m (s-ck)}{TT_{k=1}^n (s-dk)}$$

when ch are roots of the numerator polynomial, called zeros of X(s), "O"symbol dk are roots of the denominator ", called poles of X(s), "X"symbol

EXAMPLE 6.1 LAPLACE TRANSFORM OF A CAUSAL EXPONENTIAL SIGNAL Determine the Laplace transform of

$$x(t) = e^{at}u(t),$$

and depict the ROC and the locations of poles and zeros in the s-plane. Assume that a is real.

Solution: Substitute x(t) into Eq. (6.5), obtaining

$$X(s) = \int_{-\infty}^{\infty} e^{at} u(t) e^{-st} dt$$
$$= \int_{0}^{\infty} e^{-(s-a)t} dt$$
$$= \frac{-1}{s-a} e^{-(s-a)t} \Big|_{0}^{\infty}.$$

To evaluate $e^{-(s-a)t}$ at the limits, we use $s = \sigma + j\omega$ to write

$$X(s) = \frac{-1}{\sigma + j\omega - a} e^{-(\sigma - a)t} e^{-j\omega t} \bigg|_{0}^{\infty}.$$

Now, if $\sigma > a$, then $e^{-(\sigma - a)t}$ goes to zero as t approaches infinity, and

$$X(s) = \frac{-1}{\sigma + j\omega - a}(0 - 1), \quad \sigma > a,$$

$$= \frac{1}{s - a}, \quad \text{Re}(s) > a.$$
(6.8)

The Laplace transform X(s) does not exist for $\sigma \leq a$, since the integral does not converge. The ROC for this signal is thus $\sigma > a$, or equivalently, Re(s) > a. The ROC is depicted as the shaded region of the s-plane in Fig. 6.4. The pole is located at s = a.

The expression for the Laplace transform does not uniquely correspond to a signal x(t) if the ROC is not specified. That is, two different signals may have identical Laplace transforms, but different ROCs. We demonstrate this property in the next example.

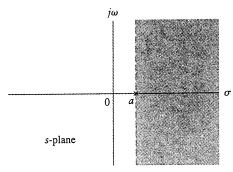


FIGURE 6.4 The ROC for $x(t) = e^{at}u(t)$ is depicted by the shaded region. A pole is located at s = a.

Example 6.2 Laplace Transform of an Anticausal Exponential Signal An anticausal signal is zero for t > 0. Determine the Laplace transform and ROC for the anticausal signal

$$y(t) = -e^{at}u(-t).$$

Solution: Using $y(t) = -e^{at}u(-t)$ in place of x(t) in Eq. (6.5), we obtain

$$Y(s) = \int_{-\infty}^{\infty} -e^{at}u(-t)e^{-st} dt$$

$$= -\int_{-\infty}^{0} e^{-(s-a)t} dt$$

$$= \frac{1}{s-a} e^{-(s-a)t} \Big|_{-\infty}^{0}$$

$$= \frac{1}{s-a}, \quad \text{Re}(s) < a.$$
(6.9)

The ROC and the location of the pole at s=a are depicted in Fig. 6.5.

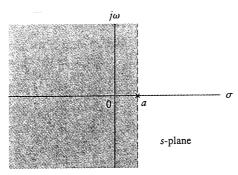


FIGURE 6.5 The ROC for $y(t) = -e^{at}u(-t)$ is depicted by the shaded region. A pole is located at

Examples 6.1 and 6.2 reveal that the Laplace transforms X157 and Y157 are equal, even though the signals xet) and yet) are different. However, the

Rocs of the two signals are different.

The Unitational Laplace Transform There are many applications of Laplace transforms in which it is reasonable to assume that the signals involved are causal. that is zero for time t < 0. In such problems, it is advantageous to define the unitational or one-sided Laplace transform, which is based on the nonnegativetime (t >> 0) portion of a signal.

| X(s) = \int \int \text{x(t)} \overline{e}^{st} dt |

The lower limit of o- implies That un do include discontinuities and impulses that occur at t=0 in the integral. By working with causal signals, we remove the ambiguity inherent in the bilateral transform and thus do not need to consider the ROC

Proporties of the Laplace transform

Linearity
$$a_1x_1(t) + a_2x_2(t) \qquad \qquad a_1X_1(s) + a_2X_2(s)$$

$$SX(s) - x(0^-)$$

$$SX(s) - x(0^-)$$

$$S^2X(s) - sx(0^-) - x^{(1)}(0^-)$$

$$S^2X(s) - sx(0^-) - x^{(1)}(0^-)$$

$$S^3X(s) - sx(0^-) - x^{(1)}(0^-)$$

$$S^3X(s) - sx(0^-) - x^{(1)}(0^-)$$

$$S^3X(s) - s^{n-1}x(0^-) - s^{n-2}x^{(1)}(0^-) - \cdots - x^{(n-1)}(0^-)$$

$$S^3X(s) - s^{n-1}x(0^-) - s^{n-2}x^{(1)}(0^-) - \cdots - x^{(n-1)}(0^-)$$

$$S^3X(s) - s^{n-1}x(0^-) - s^{n-2}x^{(1)}(0^-) - \cdots - x^{(n-1)}(0^-)$$

$$S^3X(s) - s^{n-1}x(0^-) - s^{n-2}x^{(1)}(0^-) - \cdots - x^{(n-1)}(0^-)$$

$$S^3X(s) - sx(0^-) - x^{(1)}(0^-)$$

$$S^3X(s) - sx(0^-)$$

$$S^3X(s) -$$

Table 6CT.1Laplace Transform Properties

The region of convergence of the Laplace transform of $\delta(t)$ is the entire s-plane. The region of convergence of every other entry is the half plane to the right of the rightmost pole.

	Waveform	Transform
6CT.LT1	$\delta(t)$	1
6CT.LT2	1	<u>-</u> s
6CT.LT3	t	$\frac{1}{s^2}$
6CT.LT4	$\frac{1}{(n-1)!}t^{(n-1)}$	$\frac{\frac{s}{s^2}}{\frac{1}{s^n}}$ $\frac{1}{\frac{s-s_0}{1}}$ $\frac{1}{(s-s_0)^2}$ $\frac{1}{(s-s_0)^n}$ $\frac{1}{s-j\Omega_0}$
6CT.LT5	e^{s_0t}	$\frac{1}{s-s_0}$
6CT.LT6	te ^{sot}	$\frac{1}{(s-s_0)^2}$
6CT.LT7	$\frac{1}{(n-1)!}t^{(n-1)}e^{s_0t}$	$\frac{1}{(s-s_0)^n}$
6CT.LT8	$e^{j\Omega_0 t}$	$\frac{1}{s-j\Omega_0}$
6CT.LT9	$e^{\sigma_0 t}$	$\frac{\frac{1}{s-\sigma_0}}{\frac{s}{s^2+\Omega_0^2}} =$
6CT.LT10	$\cos(\Omega_0 t)$	$\frac{s}{s^2 + \Omega_0^2} =$
		$\frac{s}{(s-j\Omega_0)(s+j\Omega_0)} = \frac{\frac{1}{2}}{s-j\Omega_0} + \frac{\frac{1}{2}}{s+j\Omega_0}$ $\frac{\Omega_0}{(s-j\Omega_0)(s+j\Omega_0)}$
6CT.LT11	$\sin(\Omega_0 t)$	$\frac{\Omega_0}{(s-j\Omega_0)(s+j\Omega_0)}$
6CT.LT12	$Ae^{\sigma_0 t}\cos(\Omega_0 t + \phi) = \mathcal{R}\{2Xe^{s_0 t}\}$	$\frac{X}{s - s_0} + \frac{X^*}{s - s_0^*} X = \frac{1}{2} A e^{j\phi}, s_0 = \sigma_0 + j\Omega_0$
6CT.LT13	$\frac{\frac{1}{(n-1)!}t^{(n-1)}Ae^{\sigma_0 t}\cos(\Omega_0 t + \phi)}{=\frac{1}{(n-1)!}t^{(n-1)}\mathcal{R}\{2Xe^{s_0 t}\}$	$\frac{X}{(s-s_0)^n} + \frac{X^*}{(s-s_0^*)^n} X = \frac{1}{2} A e^{j\phi}, s_0 = \sigma_0 + j\Omega_0$

Table 6CT.2

Laplace Transform Pairs

D.1 Basic Laplace Transforms

Transform L [∞]	
$X(s) = \int_{-\infty} x(t)e^{-st} dt$	ROC
$\frac{1}{s}$	$Re\{s\} > 0$
$\frac{1}{s^2}$	$Re\{s\} > 0$
e ^{-sτ}	for all s
$\frac{1}{s+a}$	$Re\{s\} > -a$
$\frac{1}{(s+a)^2}$	$Re\{s\} > -a$
$\frac{s}{s^2 + \omega_1^2}$	$Re\{s\} > 0$
$\frac{\omega_1}{s^2 + \omega_1^2}$	$Re\{s\} > 0$
$\frac{s+a}{(s+a)^2+\omega_1^2}$	$Re\{s\} > -a$
$\frac{\omega_1}{(s+a)^2+\omega_1^2}$	$Re\{s\} > -a$
	$X(s) = \int_{-\infty}^{\infty} x(t)e^{-st} dt$ $\frac{1}{s}$ $\frac{1}{s^2}$ $e^{-s\tau}$ $\frac{1}{s+a}$ $\frac{1}{(s+a)^2}$ $\frac{s}{s^2 + \omega_1^2}$ $\frac{\omega_1}{s^2 + \omega_1^2}$ $\frac{s+a}{(s+a)^2 + \omega_1^2}$ ω_1

$m extbf{B}$ D.1.1 Bilateral Laplace Transforms for Signals That Are Nonzero for t < 0

Signal	Bilateral Transform	ROC
$\delta(t-\tau), \tau < 0$	$e^{-s au}$	for all s
-u(-t)	$\frac{1}{s}$	$Re\{s\} < 0$
-tu(-t)	$\frac{1}{s^2}$	$Re\{s\} < 0$
$-e^{-at}u(-t)$	$\frac{1}{s+a}$	$Re\{s\} < -a$
$-te^{-at}u(-t)$	$\frac{1}{(s+a)^2}$	$Re\{s\} < -a$

D.2 Laplace Transform Properties

Signal	Unilateral Transform $x(t) \xleftarrow{\mathcal{L}_u} X(s)$ $y(t) \xleftarrow{\mathcal{L}_u} Y(s)$	Bilateral Transform $x(t) \stackrel{\mathcal{L}}{\longleftrightarrow} X(s)$ $y(t) \stackrel{\mathcal{L}}{\longleftrightarrow} Y(s)$	ROC $s \in R_x$ $s \in R_y$
$\frac{1}{ax(t) + by(t)}$	aX(s) + bY(s)	aX(s) + bY(s)	At least $R_x \cap R_y$
x(t- au)	$e^{-s\tau}X(s)$ if $x(t-\tau)u(t) = x(t-\tau)u(t-\tau)$	$e^{-s\tau}X(s)$	R _x
	$X(s-s_o)$	$X(s-s_o)$	$R_x + \text{Re}\{s_o\}$
x(at)	$\frac{1}{a}X\left(\frac{s}{a}\right), a > 0$	$\frac{1}{ a }X\left(\frac{s}{a}\right)$	$\frac{R_x}{ a }$
x(t) * y(t)	X(s)Y(s) if $x(t) = y(t) = 0$ for $t < 0$	X(s)Y(s)	At least $R_x \cap R_y$
-tx(t)	$\frac{d}{ds}X(s)$	$\frac{d}{ds}X(s)$	R_x
$\frac{d}{dt}x(t)$	$sX(s)-x(0^-)$	sX(s)	At least R _x
$\int_{-\infty}^t x(\tau) d\tau$	$\frac{1}{s}\int_{-\infty}^{0^{-}}x(\tau)d\tau+\frac{X(s)}{s}$	$\frac{X(s)}{s}$	At least $R_x \cap \{\text{Re}\{s\} > 0\}$

For comparison with the Fourier transform

A Short Table of Fourier Transforms

	f(t)	$F(\omega)$	
1	$e^{-at}u(t)$	$rac{1}{a+j\omega}$	<i>a</i> > 0
2	$e^{at}u(-t)$	$rac{1}{a-j\omega}$	<i>a</i> > 0
3	$e^{-a t }$	$\frac{2a}{a^2+\omega^2}$	<i>a</i> > 0
4	$te^{-at}u(t)$	$\frac{1}{(a+j\omega)^2}$	<i>a</i> > 0
5	$t^n e^{-at} u(t)$	$\frac{n!}{(a+j\omega)^{n+1}}$	<i>a</i> > 0
6	$\delta(t)$	1	
7	1	$2\pi\delta(\omega)$	
8	$e^{j\omega_0t}$	$2\pi\delta(\omega-\omega_0)$:
9	$\cos \omega_0 t$	$\pi[\delta(\omega-\omega_0)+\delta(\omega+\omega_0)]$	
10	$\sin\omega_0 t$	$j\pi[\delta(\omega+\omega_0)-\delta(\omega-\omega_0)]$	
11	u(t)	$\pi\delta(\omega)+rac{1}{j\omega}$	
12	$\operatorname{sgn} t$	$rac{2}{j\omega}$	
13	$\cos\omega_0 tu(t)$	$\frac{\pi}{2}[\delta(\omega-\omega_0)+\delta(\omega+\omega_0)]+\frac{j\omega}{\omega_0^2-\omega^2}$	
14	$\sin \omega_0 t u(t)$	$\frac{\pi}{2j}[\delta(\omega-\omega_0)-\delta(\omega+\omega_0)]+\frac{\omega_0}{\omega_0^2-\omega^2}$	
15	$e^{-at}\sin\omega_0 tu(t)$	$rac{\omega_0}{(a+j\omega)^2+\omega_0^2}$	a > 0
16	$e^{-at}\cos\omega_0 tu(t)$	$\frac{a+j\omega}{(a+j\omega)^2+\omega_0^2}$	a > 0
17	$\mathrm{rect}\left(\frac{t}{\tau}\right)$	$ au \operatorname{sinc} \left(rac{\omega au}{2} ight)$	
18	$\frac{W}{\pi}\operatorname{sinc}(Wt)$	$\mathrm{rect}\left(rac{\omega}{2W} ight)$	
19	$\Delta\left(\frac{t}{\tau}\right)$	$\frac{\tau}{2}\operatorname{sinc}^2\left(\frac{\omega\tau}{4}\right)$	
20	$\frac{W}{2\pi}\operatorname{sinc}^2\left(\frac{Wt}{2}\right)$	$\Delta\left(rac{\omega}{2W} ight)$	
21	$\sum_{n=-\infty}^{\infty} \delta(t - nT)$	$\omega_0 \sum_{n=-\infty}^{\infty} \delta(\omega - n\omega_0)$	$\omega_0 = \frac{2\pi}{T}$
22	$e^{-t^2/2\sigma^2}$	$\sigma\sqrt{2\pi}e^{-\sigma^2\omega^2/2}$	

more about properties...

Differentiation in the s-Domain

Initial and Final value Theorem:

-The initial value theorem does not apply to rational functions X(s) in which the order of the numerator polynomial is greater them or equal to that of the

denominator. polynomial order.

lim \$X(s) = x(\omega)

s-\omega

The final-value theorem applies only if all the poles of X(s) are in the left half of the s-plane, with at most a single pole at s=0

Example 6.6 Applying the Initial- and Final-Value Theorems Determine the initial and final values of a signal x(t) whose unilateral Laplace transform is

$$X(s) = \frac{7s+10}{s(s+2)}.$$

Solution: We may apply the initial-value theorem, Eq. (6.21), to obtain

$$x(0^{+}) = \lim_{s \to \infty} s \frac{7s + 10}{s(s + 2)}$$
$$= \lim_{s \to \infty} \frac{7s + 10}{s + 2}$$
$$= 7.$$

The final value theorem, Eq. (6.22), is applicable also, since X(s) has only a single pole at s=0 and the remaining poles are in the left half of the s-plane. We have

$$x(\infty) = \lim_{s \to 0} s \frac{7s + 10}{s(s+2)}$$
$$= \lim_{s \to 0} \frac{7s + 10}{s+2}$$
$$= 5$$

The reader may verify these results by showing that X(s) is the Laplace transform of $x(t) = 5u(t) + 2e^{-2t}u(t).$

A Ramp **EXAMPLE 6CT.9**

Figure 6CT.5

Consider

Pole-zero plot for the unit ramp.

 $j\Omega$

$$x(t) = r(t) = tu(t)$$

We showed earlier that

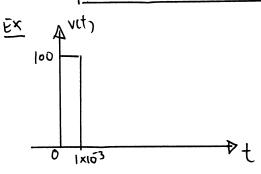
$$u(t) \stackrel{\text{LT}}{\longleftrightarrow} \frac{1}{s} \quad \mathcal{R}\{s\} > 0$$

The "multiply by t" property yields

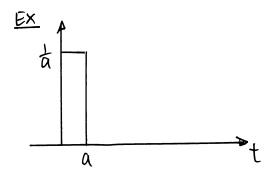
$$r(t) \stackrel{\text{LT}}{\longleftrightarrow} -\frac{d}{ds} \frac{1}{s} = \frac{1}{s^2} \quad \mathcal{R}\{s\} > 0$$
 (46)

The pole-zero plot is shown in Figure 6CT.5, where the pole is indicated by overlapping crosses. This pole is called a second-order pole because the degree of the denominator s^2 is 2.

Laplace transform by using table



The area of the pulse is 100 Vx 10-3 = 0.1 V.5 -- we may approximate vct) as vct) ~ 0.1 Sct) :. Visi = Z[viti] = Z[0.1 &cti] = 0.1 L[Sity]= 0.1



$$f(t) = \frac{1}{4}[u(t) - u(t-a)]$$

$$F(s) = \mathcal{L}[f(t)]$$

$$\mathcal{L}[u(t)] = \frac{1}{5}; \mathcal{L}[u(t-a)] = \frac{1}{5}e^{as}$$

$$F(s) = \frac{1}{4}[\frac{1}{5} - \frac{1}{5}e^{as}]$$

Ex Find I (s) when i(t) = 10(0s(20t+30°)

First, we decompose ict, into the sum of a sine function and a costre function

i(t) = [0[(0520t(0530-5)n20ts)n30] = 5√3 (0520t-5)sin20t

(00 (0,+02) = (050, (0502-5170,51762)

_. I(s) = 5/3 Z[ws 20t] -5 Z[sin 20t]

$$= \frac{5\sqrt{3}}{5^2 + 400} - \frac{100}{5^2 + 400}$$

= 5/35 - 100 52+400 52+400

Inverse Laplace transform by using table

Ex given I(s) = 5 [1-2e35+2065-20+20-125], find i(t)

since Z'[1] = tuct, and Z[f(t-a)uct-a)] = easfis)

- it)= Z'[]()]= 5[tut)-2(t-3)u(t-3)+2(t-6)u(t-6) -2(t-9)u(t-9)+2(t-12)u(t-12)-...]