| ชื่อ | รหัส | . ภาควิชา | เลขที่นั่งสอบ |
|------|------|-----------|---------------|
| | | | |
| | | | |
| | | | L |

มหาวิทยาลัยเทคโนโลยีพระจอมเกล้าธนบุรี การสอบปลายภาคเรียนที่ 1 ปีการศึกษา 2550

วิชา MEE 234 Thermal Engineering สอบวันอังคารที่ 9 ตุลาคม พ.ศ.2550 ภาควิชา CVE 2, ENV 2, ENV 2(Bil.), CVE 2(inter.) เวลา 13.00 – 16.00 น.

| คำเตือน | 1. | ข้อสอบแบ่งออกเป็น 3 PART มีทั้งหมคมี 4 ข้อ, 14 หน้า (รวมใบปะหน้าค้วย |
|---------|----|--|
| | | (รวม 100 คะแนน) |
| | _ | 9.29.21.4.0 |

- 2. อนุญาตให้ใช้เครื่องคำนวณตามที่มหาวิทยาลัยฯ กำหนดได้
- 3. ไม่อนุญาตให้นำตำราเข้าห้องสอบ
- 4. ให้เขียนชื่อ......(ทุกแผ่น)

เมื่อนักศึกษาทำข้อสอบเสร็จ ต้องยกมือบอกกรรมการคุมสอบ เพื่อขออนุญาตออกนอกห้องสอบ ห้ามนักศึกษานำข้อสอบและกระคาษคำตอบออกนอกห้องสอบ

นักศึกษาซึ่งทุจริตในการสอบ อาจถูกพิจารณาโทษสูงสุดให้พ้นสภาพการเป็นนักศึกษา

| นายสุรชัย | บวรเศรษ ฐ นันท์ |
|---------------|------------------------|
| นายวันชัย | อัศวภูษิตกุล |
| นายเถิศศักดิ์ | เหมยากร |

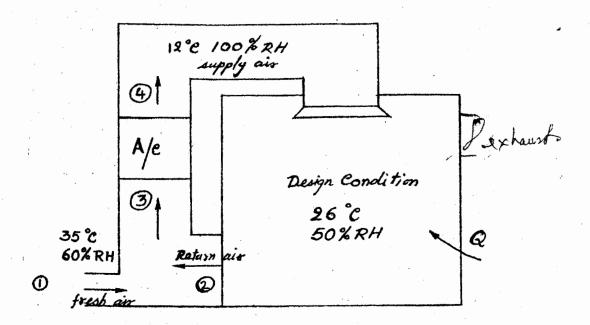
| Name | e Department | ••••• |
|------|---|--------------|
| | (Mr.Surachai Bavorn | serthanan.) |
| | PART I | |
| 1.1 | Draw the schematic and T-s diagram of Rankine cycle | (3 points) |
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| | | |
| 1.2 | Draw the P-h and T-s diagram of the vapor compression refrigo | eration, and |
| | Express the processes that make the cycle. | (3 points) |
| | | |
| | | |
| | | |
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| | | |
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| | | |
| 1.3 | What are the assumptions of air standard cycle in thermodynai | |
| | analysis of internal combustion engine? | (3 points) |
| | | |
| | | |
| | | |

| Name | e Student No | Department |
|-------|--|---------------------------------|
| | | (Mr.Surachai Bavornserthanan.) |
| 1.4 | What are the limitations of the C.O.P. inc | reasing for vapor compression |
| | refrigeration cycle? | (3 points) |
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| | | |
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| | | |
| 1.5 | What is the different of wet bulb tempera | ture and dew point temperature? |
| | | (3 points) |
| | | |
| | | |
| | | |
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| | | |
| | | |
| | | |
| 1 6 V | What is the different between humidity ratio | and relative humidity? |
| 1.0 4 | vilat is the different between numbery ratio | (3 points) |
| | | (o points) |
| | | |
| | | |

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|------|------------|--------------------------------|
| | | (Mr.Surachai Bavornserthanan.) |

1.7



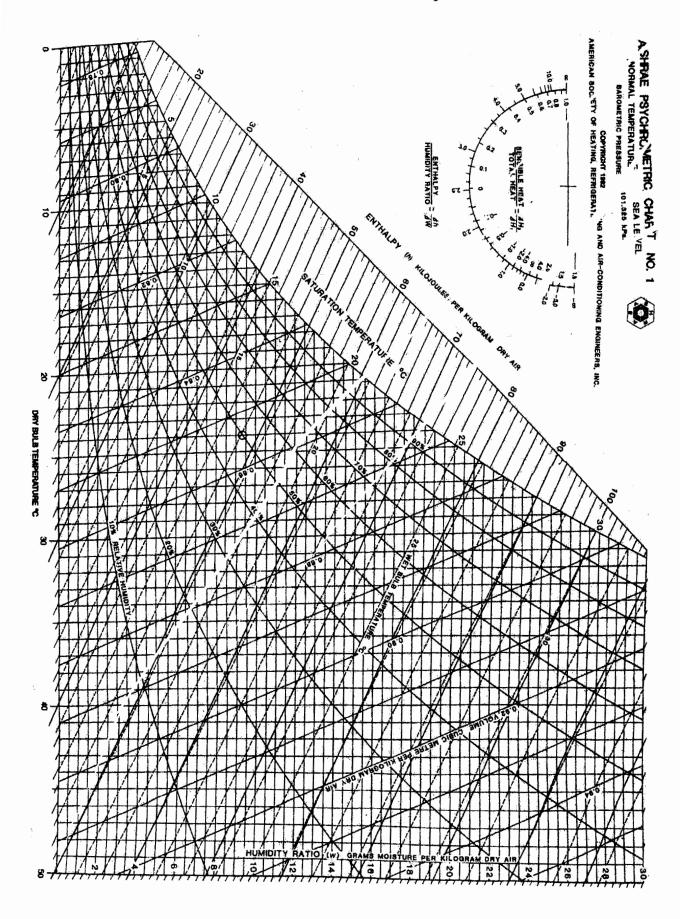
Given:

- Barometric Pressure 101.325 kPa
- State (1) 35°C and 60 % RH
- Air flow rate @ (4) 1 m³/sec

Determire:

- Moist air at state (3)
- Heat that is absorbed at A/C
- Heat load (Q) that enter the room
- Plot state change of air on Psychrometric chart

Name: Student No. Department......



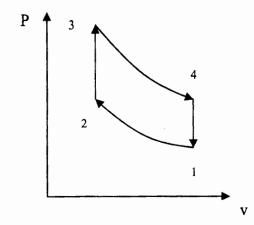
Name...... Student No. Department.....

(Mr.Wanchai Asvaooositkul)

PART II

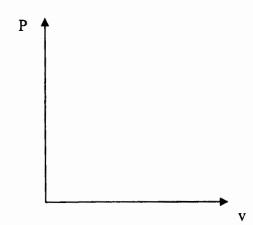
1.1 Draw an air-standard cycle on the P-v and T-s diagrams in the space provided. (10 marks)

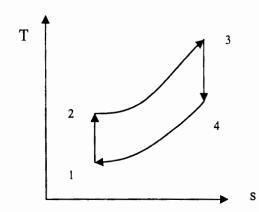
Otto cycle



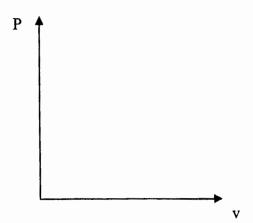
T

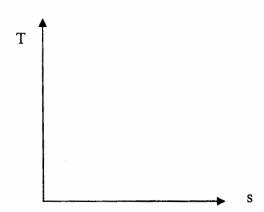
Diesel cycle





Brayton cycle (Gas-turbine engine)





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|------|------------|----------------------------|
| | | (Mr.Wanchai Asvaooositkul) |

2.2 An air-standard Otto cycle has a compression ratio of 8. The minimum and maximum temperatures in the cycle are 300 and 1340 K. Determine (a) the amount of heat transferred to the air during the heat-addition process, (b) the net work output and (c) the thermal efficiency. (10 marks)

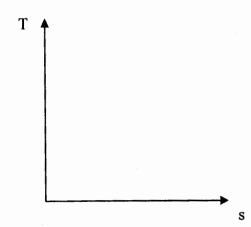
Assumed Air is an ideal gas with constant specific heats. [$c_p = 1.005 \text{ kJ/kg·K}$, $c_v = 0.718 \text{ kJ/kg·K}$, R = 0.287 kJ/kg·K, and k = 1.4]

Answer:

$$q_{in} =kJ/kg$$
 $Q_{out} =kJ/kg$
 $W_{in} =kJ/kg$
 $W_{out} =kJ/kg$
 $W_{netout} =kJ/kg$
 $n_{th} =\%$

| Name | Student No | . Department |
|------|------------|----------------------------|
| | | (Mr.Wanchai Asvaooositkul) |

3. Consider a 210-MW steam power plant that operates on a simple ideal Rankine cycle. Steam enters the turbine at 10 MPa and 500°C and is cooled in the condenser at a pressure of 10 kPa. Show the cycle on a *T-s* diagram with respect to saturation lines, and determine (a) the quality of the steam at the turbine exit, (b) the thermal efficiency of the cycle, and (c) the mass flow rate of the steam. (20 marks)



Answer:

$$\eta_{th} = \dots\%$$

892 | Thermodynamics

| 32 (| | i illouyilalli | 103 | | | | | | | | | |
|------------------------------------|--|--|---|--|--|--|--|--|--|--|--|----------------------------------|
| TABLE A-5 | | | | | | | | | | | | |
| Saturated water—Pressure table | | | | | | | | | | | | |
| | | | fic volume, m³/kg | Internal energy, kJ/kg | | | <i>Enthalpy,</i> kJ/kg | | | Entropy. kJ/kg · K | | |
| Press., P kPa | Sat. temp., T _{sat} °C | Sat. liquid, v _f | Sat. vapor, v _g | Sat. liquid, <i>u_f</i> | Evap., u _{fg} | Sat. vapor, u _g | Sat. liquid, h, | Evap., h _{fg} | Sat. vapor, h _g | Sat. liquid, s _f | Evap., s _{fg} | Sat. vapor, s _g |
| 1.0 1.5 2.0 2.5 3.0 | 6.97 13.02 17.50 21.08 24.08 | 0.001000 0.001001 0.001001 0.001002 0.001003 | 129.19 87.964 66.990 54.242 45.654 | 29.302 54.686 73.431 88.422 100.98 | 2355.2 2338.1 2325.5 2315.4 2306.9 | 2384.5 2392.8 2398.9 2403.8 2407.9 | 29.303 54.688 73.433 88.424 100.98 | 2484.4 2470.1 2459.5 2451.0 2443.9 | 2513.7 2524.7 2532.9 2539.4 2544.8 | 0.1956 0.2606 | 8.6314 8.4621 8.3302 | 8.8270 8.7227 8.6421 |
| 4.0 5.0 7.5 10 15 | 28.96 32.87 40.29 45.81 53.97 | 0.001004 0.001005 0.001008 0.001010 0.001014 | 34.791 28.185 19.233 14.670 10.020 | 121.39 137.75 168.74 191.79 225.93 | 2293.1 2282.1 2261.1 2245.4 2222.1 | 2414.5 2419.8 2429.8 2437.2 2448.0 | 121.39 137.75 168.75 191.81 225.94 | 2432.3 2423.0 2405.3 2392.1 2372.3 | | 0.5763 | 8.0510 7.9176 7.6738 7.4996 7.2522 | 8.3938 8.2501 8.1488 |
| 20 25 30 40 50 | 60.06 64.96 69.09 75.86 81.32 | 0.001017 0.001020 0.001022 0.001026 0.001030 | 7.6481 6.2034 5.2287 3.9933 3.2403 | 251.40 271.93 289.24 317.58 340.49 | 2204.6 2190.4 2178.5 2158.8 2142.7 | 2456.0 2462.4 2467.7 2476.3 2483.2 | 251.42 271.96 289.27 317.62 340.54 | 2357.5 2345.5 2335.3 2318.4 2304.7 | 2617.5 | 0.8320 0.8932 0.9441 1.0261 1.0912 | | 7.8302 |
| 75 100 101.325 125 150 | 91.76 99.61 99.97 105.97 111.35 | 0.001037 0.001043 0.001043 0.001048 0.001053 | 2.2172 1.6941 1.6734 1.3750 1.1594 | 384.36 417.40 418.95 444.23 466.97 | 2111.8 2088.2 2087.0 2068.8 2052.3 | 2496.1 2505.6 2506.0 2513.0 2519.2 | 384.44 417.51 419.06 444.36 467.13 | 2278.0 2257.5 2256.5 2240.6 2226.0 | 2662.4 2675.0 2675.6 2684.9 2693.1 | 1.2132 1.3028 1.3069 1.3741 1.4337 | 6.2426 6.0562 6.0476 5.9100 5.7894 | 7.3589 7.3549 |
| 175 200 225 250 275 | 116.04 120.21 123.97 127.41 130.58 | 0.001057 0.001061 0.001064 0.001067 0.001070 | 1.0037 0.88578 0.79329 0.71873 0.65732 | 486.82 504.50 520.47 535.08 548.57 | 2037.7 2024.6 2012.7 2001.8 1991.6 | 2524.5 2529.1 2533.2 2536.8 2540.1 | 487.01 504.71 520.71 535.35 548.86 | 2213.1 2201.6 2191.0 2181.2 2172.0 | 2700.2 2706.3 2711.7 2716.5 2720.9 | 1.4850 1.5302 1.5706 1.6072 1.6408 | 5.6865 5.5968 5.5171 5.4453 5.3800 | 7.1270 7.087 7.052 |
| 300 325 350 375 400 | 133.52 136.27 138.86 141.30 143.61 | 0.001073 0.001076 0.001079 0.001081 0.001084 | 0.60582 0.56199 0.52422 0.49133 0.46242 | 583.89 594.32 | 1982.1 1973.1 1964.6 1956.6 1948.9 | 2543.2 2545.9 2548.5 2550.9 2553.1 | 561.43 573.19 584.26 594.73 604.66 | 2163.5 2155.4 2147.7 2140.4 2133.4 | 2724.9 2728.6 2732.0 2735.1 2738.1 | 1.6717 1.7005 1.7274 1.7526 1.7765 | 5.3200 5.2645 5.2128 5.1645 5.1191 | 6.9656 6.940 6.917 |
| 450 500 550 600 650 | 147.90 151.83 155.46 158.83 161.98 | 0.001088 0.001093 0.001097 0.001101 0.001104 | 0.41392 0.37483 0.34261 0.31560 0.29260 | 639.54 655.16 669.72 | 1934.5 1921.2 1908.8 1897.1 1886.1 | 2557.1 2560.7 2563.9 2566.8 2569.4 | 623.14 640.09 655.77 670.38 684.08 | 2120.3 2108.0 2096.6 2085.8 2075.5 | 2743.4 2748.1 2752.4 2756.2 2759.6 | 1.8205 1.8604 1.8970 1.9308 1.9623 | 5.0356 4.9603 4.8916 4.8285 4.7699 | 6.820 6.788 6.759 |
| 700 750 | 164.95 167.75 | 0.001108 0.001111 | 0.27278 0.25552 | | 1875.6 1865.6 | 2571.8 2574.0 | 697.00 709.24 | 2065.8 2056.4 | 2762.8 2765.7 | 1.9918 2.0195 | 4.7153 4.6642 | |

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| TABLE | A-6 | | | | | | | | | | | |
|--------------|--------------------|----------------------|------------------|------------------|----------------------|------------------|------------------|------------------|---------------------------------|------------------|---------|------------------|
| Superh | eated wat | er (<i>Conti</i> | nued) | | | | | | | | | |
| T | V | U | h | S | V 3.0 | U | h | S | V | u | h | s |
| °C | m ³ /kg | kJ/kg | kJ/kg | kJ/kg · K | m ³ /kg | kJ/kg | kJ/kg | kJ/kg · K | m ³ /kg | kJ/kg | kJ/kg | kJ/kg · K |
| | Р | = 4.() MF | Pa (250.35 | °C) | Р | = 4.5 MP | a (257.44° | C) | P - | 5.0 MPa | (263.94 | C) |
| Sat. | 0.04978 | | 2800.8 | 6.0696 | 0.04406 | 2599.7 | 2798.0 | 6.0198 | 0.03945 | 2597.0 | | 5.9737 |
| 275 | 0.05461 | | 2887.3 | 6.2312 | 0.04733 | 2651.4 | 2864.4 | 6.1429 | 0.04144 | 2632.3 | | 6.0571 |
| 300 350 | 0.05887 0.06647 | | 2961.7 3093.3 | 6.3639 6.5843 | 0.05138 0.05842 | 2713.0 2818.6 | 2944.2 3081.5 | 6.2854 6.5153 | 0.04535 0.05197 | 2699.0 2809.5 | | 6.2111 6.4516 |
| 400 | 0.00047 | | 3214.5 | 6.7714 | 0.05642 | 2914.2 | 3205.7 | 6.7071 | 0.05784 | 2907.5 | | 6.6483 |
| 450 | 0.08004 | | 3331.2 | 6.9386 | 0.07076 | 3005.8 | 3324.2 | 6.8770 | 0.06332 | 3000.6 | | 6.8210 |
| 500 | 0.08644 | 3100.3 | 3446.0 | 7.0922 | 0.07652 | 3096.0 | 3440.4 | 7.0323 | 0.06858 | 3091.8 | | 6.9781 |
| 600 | 0.09886 | | 3674.9 | 7.3706 | 0.08766 | 3276.4 | 3670.9 | 7.3127 | 0.07870 | 3273.3 | | 7.2605 |
| 700 | 0.11098 | | 3906.3 | 7.6214 | 0.09850 | 3460.0 | 3903.3 | 7.5647 | 0.08852 | 3457.7 | | 7.5136 |
| 800 | 0.12292 | | 4142.3 | 7.8523 | 0.10916 | 3648.8 | 4140.0 | 7.7962 | 0.09816 | 3646.9 | | 7.7458 |
| 900 1000 | 0.13476 | | 4383.9 | 8.0675 | 0.11972 0.13020 | 3843.3 | 4382.1 | 8.0118 | 0.10769 | 3841.8 | | 7.9619 |
| 1100 | 0.14653 0.15824 | | 4631.2 4884.4 | 8.2698 8.4612 | 0.13020 | 4043.9 4250.4 | 4629.8 4883.2 | 8.2144 8.4060 | 0.11715 0.12655 | 4042.6 4249.3 | 4628.3 | 8.3566 |
| 1200 | 0.16992 | | 5143.2 | 8.6430 | 0.15103 | 4462.6 | 5142.2 | 8.5880 | 0.12533 | | 5141.3 | |
| 1300 | 0.18157 | | 5407.2 | 8.8164 | 0.16140 | 4680.1 | 5406.5 | 8.7616 | 0.14527 | 4679.3 | | 8.7124 |
| | Р | = 6.0 MF | Pa (275.59 | l°C) | Ρ | 7.0 M P | a (285.83 | C) | P = | 8.0 MPa | (295.01 | C) |
| Sat. | 0.03245 | 2589.9 | 2784.6 | 5.8902 | 0.027378 | 2581.0 | 2772.6 | 5.8148 | 0.023525 | | 2758.7 | 5.7450 |
| 300 | 0.03619 | 2668.4 | 2885.6 | 6.0703 | 0.029492 | 2633.5 | 2839.9 | 5.9337 | 0.024279 | 2592.3 | 2786.5 | 5.7937 |
| 350 | 0.04225 | | 3043.9 | 6.3357 | 0.035262 | | 3016.9 | 6.2305 | 0.029975 | | | 6.1321 |
| 400 | 0.04742 | | 3178.3 | 6.5432 | 0.039958 | | 3159.2 | 6.4502 | 0.034344 | | | 6.3658 |
| 450 | 0.05217 | | 3302.9 | 6.7219 | 0.044187 | | 3288.3 | 6.6353 | 0.038194 | | | 6.5579 |
| 500 | 0.05667 0.06102 | | 3423.1 3541.3 | 6.8826 7.0308 | 0.048157 0.051966 | | 3411.4 3531.6 | 6.8000 6.9507 | 0.041767 0.045172 | | | 6.7266 6.8800 |
| 550 600 | 0.06527 | | 3658.8 | 7.1693 | 0.051966 | | 3650.6 | 7.0910 | 0.043172 | | | 7.0221 |
| 700 | 0.00327 | | 3894.3 | 7.4247 | 0.062850 | | 3888.3 | 7.3487 | 0.054829 | | | 7.2822 |
| 800 | 0.08165 | | 4133.1 | 7.6582 | 0.069856 | | 4128.5 | 7.5836 | 0.061011 | | | |
| 900 | 0.08964 | | 4376.6 | 7.8751 | 0.076750 | | 4373.0 | 7.8014 | 0.067082 | | | |
| 1000 | 0.09756 | 4040.1 | 4625.4 | 8.0786 | 0.083571 | 4037.5 | 4622.5 | 8.0055 | 0.073079 | 4035.0 | 4619.6 | 7.9419 |
| 1100 | 0.10543 | | 4879.7 | 8.2709 | 0.090341 | | 4877.4 | 8.1982 | 0.079025 | | | 8.1350 |
| 1200 | 0.11326 | | 5139.4 | 8.4534 | 0.097075 | | 5137.4 | 8.3810 | 0.084934 | | | 8.3181 |
| 1300 | 0.12107 | 4677.7 | 5404.1 | 8.6273 | 0.103781 | 4676.1 | 5402.6 | 8.5551 | 0.090817 | 4674.5 | 5401.0 | 8.4925 |
| | | | Pa (303,35 | | | | Pa (311.00 | | making the second second second | 12.5 MP | | |
| Sat. | 0.020489 | | 2742.9 | 5.6791 | 0.018028 | | 2725.5 | 5.6159 | 0.013496 | 2505.6 | 2674.3 | 5.4638 |
| 325 | 0.023284 | | 2857.1 | 5.8738 | 0.019877 0.022440 | | 2810.3 | 5.7596 | 0.016120 | 2624.0 | 2026.6 | E 7120 |
| 350 400 | 0.025816 | | 2957.3 3118.8 | 6.0380 6.2876 | 0.022440 | | 2924.0 3097.5 | 5.9460 6.2141 | 0.016138 | | | 5.7130 6.0433 |
| 450 | 0.023360 | | 3258.0 | 6.4872 | 0.020430 | | 3242.4 | 6.4219 | 0.023019 | | | 6.2749 |
| 500 | | 3056.3 | | 6.6603 | 0.032811 | | 3375.1 | 6.5995 | 0.025630 | | | 6.4651 |
| 550 | | 3153.0 | | 6.8164 | 0.035655 | | 3502.0 | 6.7585 | 0.028033 | | | 6.6317 |
| 600 | | | 3634.1 | | 0.038378 | | | 6.9045 | 0.030306 | | | |
| 650 | 0.04575 | 5 3343.4 | 3755.2 | 7.0954 | 0.041018 | 3338.0 | 3748.1 | 7.0408 | 0.032491 | 3324.1 | 3730.2 | 6.9227 |
| 700 | | 3438.8 | | 7.2229 | 0.043597 | | 3870.0 | 7.1693 | 0.034612 | | | |
| 800 | | 2 3632.0 | | 7.4606 | 0.048629 | | 4114.5 | 7.4085 | 0.038724 | | | |
| 900 | | 2 3829.6 | | 7.6802 | 0.053547 | | 4362.0 | 7.6290 | 0.042720 | | | |
| 1000 1100 | | 9 4032.4 4 4240.7 | | 7.8855 8.0791 | 0.058391 | | 4613.8 4870.3 | 7.8349 8.0289 | 0.046641 | | | |
| 1200 | | 2 4454.2 | | 8.2625 | 0.063183 | | 5131.7 | 8.2126 | 0.054342 | | | |
| 1300 | | 3 4672.9 | | 8.4371 | 0.072667 | | 5398.0 | 8.3874 | 0.058147 | | | |
| | | | | | L | | | | | | | |

| | Student No | _ | <u>jarn.Lertsak Hemyakorn)</u> |
|------------|---|----------------------------|--------------------------------|
| | PART II | <u>u</u> | |
| Problem 4. | (20 marks) | | |
| | gerator uses refrigerant-134a as the compression refrigeration cycle as t Condensing pressure | _ | g. 1.4 MPa.(abs) |
| a. | Evaporating temperature State of refrigerant at the of State of refrigerant at the of | - | - |
| Given | At the inlet of compressor At the outlet of compressor At the inlet of expansion v At the inlet of evaporator | or is state valve is st | (2) tate (3) |
| Determ | | | |
| | Show that the state and protection the P-h chart R-134a. | ocesses of | f the refrigeration cycle on |
| Pressu | | n | - MDa (aha |
| Tomn | Evaporating; | P_{E} | =MPa.(abs |
| rempe | erature : | • | =°C |
| | At the condenser; | t _c | |
| | At inlet of the compressor | | 0 |
| | At outlet of the compresso | | 0 |
| | At inlet of the compressor | | 0 |
| | At outlet of the compresso | or. t_4 | =°C |
| Enthal | ру: | | |
| | At inlet of the compressor | , h ₁ | = kJ/kg |
| | Density at the inlet of con | npressor; | $\rho_1 = \dots kg/m^3$ |
| | At outlet of the compresso | r; h ₂ | = kJ/kg |
| | At outlet of the condenser | , h ₃ | = kJ/kg |
| | At inlet of the evaporator, | . h ₄ | = kJ/kg |
| | Refrigerating effect | | = kJ/kg |
| | Condensing load | | = kJ/kg |
| | Compressor work | | = kJ/kg |
| | COP. of the refrigeration | | = kJ/kg |
| If the | refrigeration capacity 100 kW cal Mass flow rate of refriger | | |

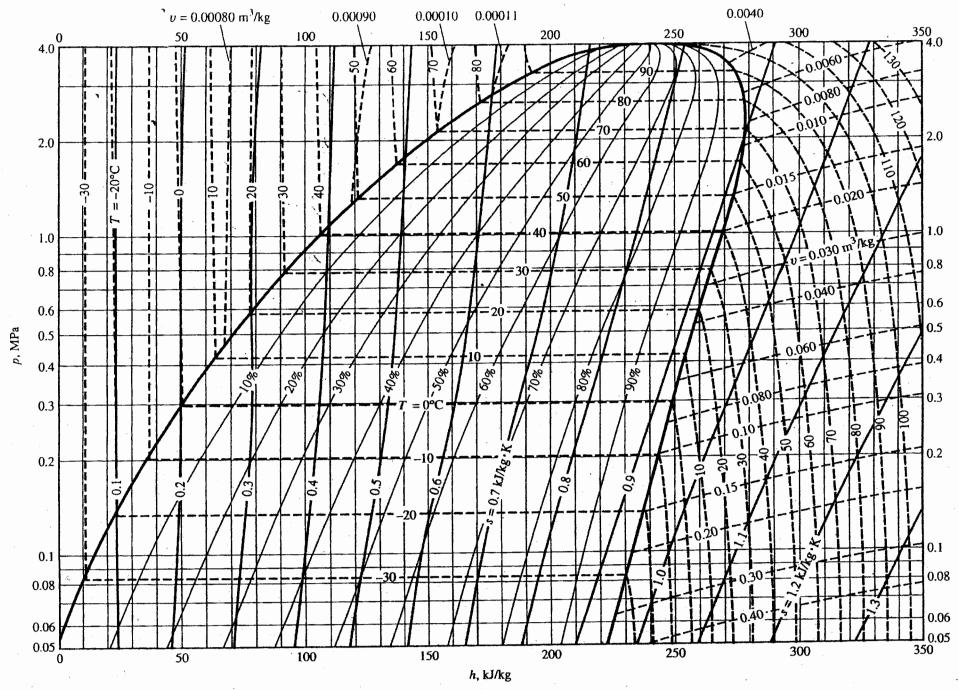


Chart A-11 R134a nh diagram (Source: Rased on Thermodynamic December of the 124-1111 2

Key concepts and formulas

1. Gas Law
$$p v = R T$$

2. Clausius inequality
$$\oint \left(\frac{dQ}{T}\right) \le 0$$

3. Entropy
$$dS = \left(\frac{dQ}{T}\right)_{int re}$$

4. T ds relation
$$T ds = du + p dv$$
$$T ds = dh - v dp$$

5. Isentropic process
$$p v^k = const, k = \frac{c_p}{c_v}$$

6. Enthalpy
$$h = u + p v$$

$$du = c_v dT, \qquad dh = c_p dT$$

7. Work -for control mass,
$$w = \int p \, dv$$

- for control volume, $w = -\int v \, dp$

8. Steady flow energy equation
$$q - w = \Delta h + \Delta ke + \Delta pe$$

9. Compression ratio
$$r = \frac{V_{max}}{V_{min}} = \frac{V_{BDC}}{V_{TDC}}$$

10. MEP
$$MEP = \frac{w_{\text{net}}}{v_{\text{max}} - v_{\text{min}}}$$

11. Adiabatic mixing
$$\frac{m_{a1}}{m_{a2}} = \frac{\omega_2 - \omega_3}{\omega_3 - \omega_1} = \frac{h_2 - h_3}{h_3 - h_1}$$
 subscript 1, 2 = inlet, 3 = mixed