
ENE 104

Electric Circuit Theory



Lecture 12:
Two-Port Networks

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Objectives include:

- Learning the distinction between one-port and two-port network
- Techniques for characterizing networks by y , z , h , and t parameters
- Transformation methods between y , z , h , and t parameters
- Performing circuit analysis using network parameters, including cascaded networks

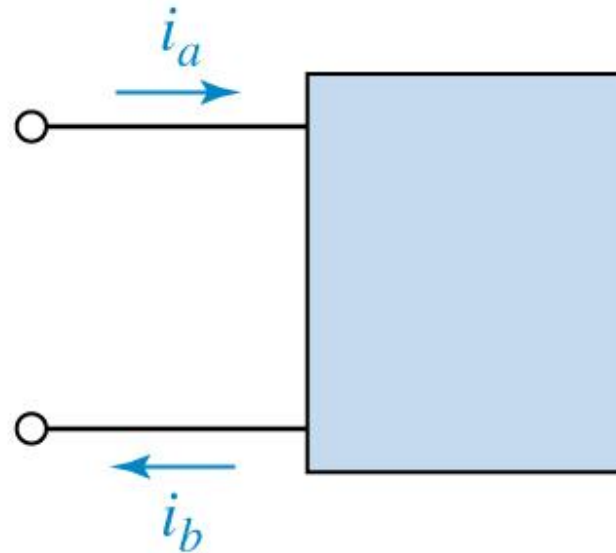
The circuit is **linear**, and the ability to measure voltages and currents:

It is possible to characterize such a network with a set of **parameters** that allow us to predict how the network will interact with other networks.

A multiport Network:

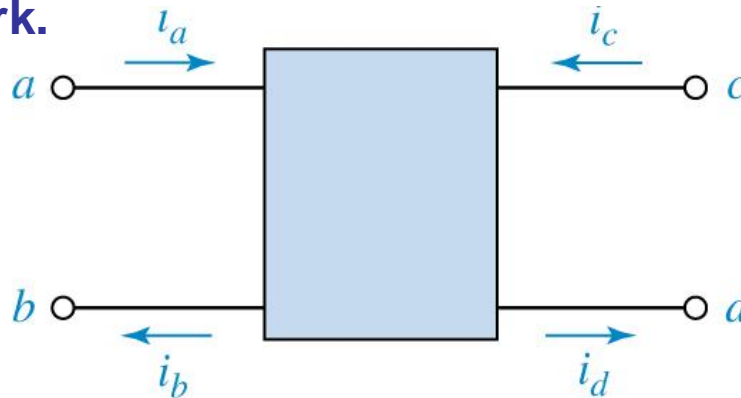
A one-port network.

i_a must be equal i_b



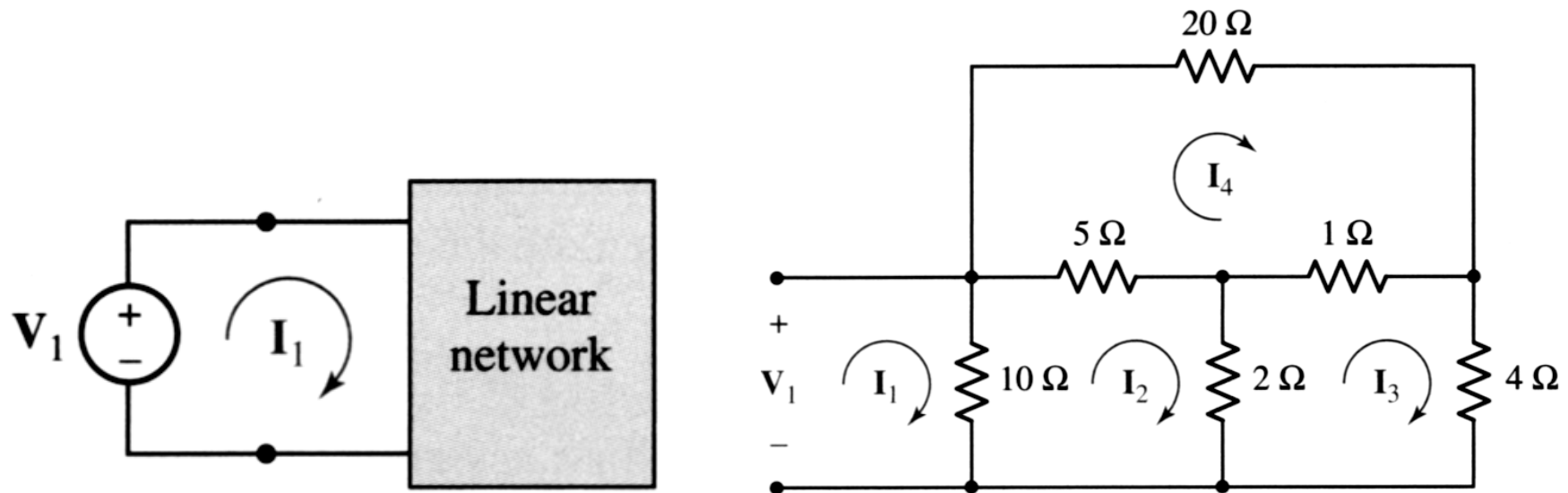
A two-port network.

$$i_a = i_b$$



$$i_c = i_d$$

A multiport Network:



$$\mathbf{Z}_{11}\mathbf{I}_1 + \mathbf{Z}_{12}\mathbf{I}_2 + \mathbf{Z}_{13}\mathbf{I}_3 + \dots + \mathbf{Z}_{1N}\mathbf{I}_N = \mathbf{V}_1$$

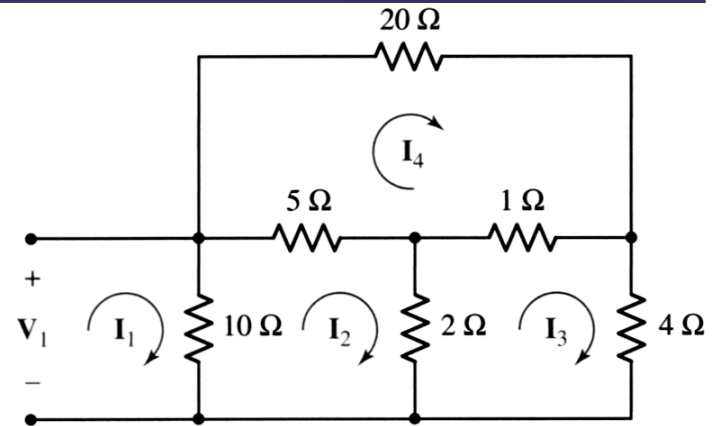
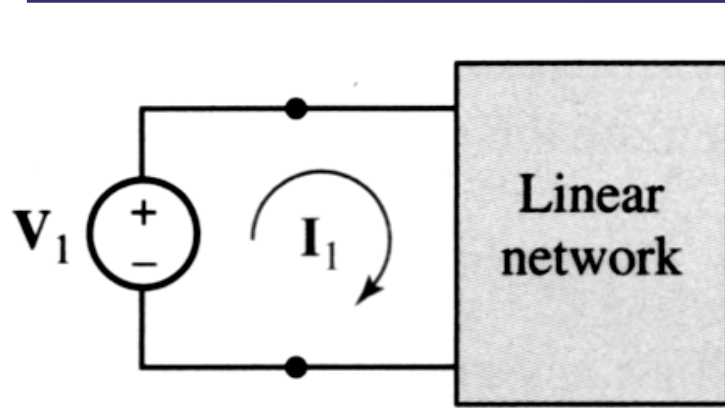
$$\mathbf{Z}_{21}\mathbf{I}_1 + \mathbf{Z}_{22}\mathbf{I}_2 + \mathbf{Z}_{23}\mathbf{I}_3 + \dots + \mathbf{Z}_{2N}\mathbf{I}_N = \mathbf{V}_2$$

$$\mathbf{Z}_{31}\mathbf{I}_1 + \mathbf{Z}_{32}\mathbf{I}_2 + \mathbf{Z}_{33}\mathbf{I}_3 + \dots + \mathbf{Z}_{3N}\mathbf{I}_N = \mathbf{V}_3$$

.....

$$\mathbf{Z}_{N1}\mathbf{I}_1 + \mathbf{Z}_{N2}\mathbf{I}_2 + \mathbf{Z}_{N3}\mathbf{I}_3 + \dots + \mathbf{Z}_{NN}\mathbf{I}_N = \mathbf{V}_N$$

A multiport Network:



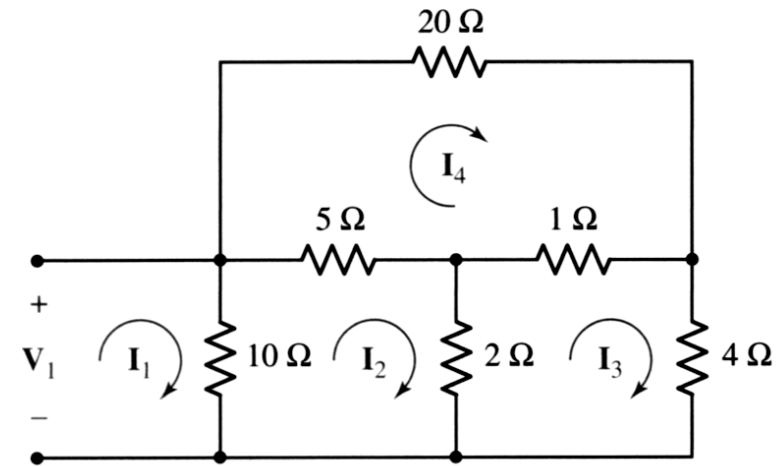
The circuit determinant:

$$\Delta_{\mathbf{Z}} = \begin{vmatrix} \mathbf{Z}_{11} & \mathbf{Z}_{12} & \mathbf{Z}_{13} & \dots & \mathbf{Z}_{1N} \\ \mathbf{Z}_{21} & \mathbf{Z}_{22} & \mathbf{Z}_{23} & \dots & \mathbf{Z}_{2N} \\ \mathbf{Z}_{31} & \mathbf{Z}_{32} & \mathbf{Z}_{33} & \dots & \mathbf{Z}_{3N} \\ \dots & \dots & \dots & \dots & \dots \\ \mathbf{Z}_{N1} & \mathbf{Z}_{N2} & \mathbf{Z}_{N3} & \dots & \mathbf{Z}_{NN} \end{vmatrix}$$

A multiport Network:

The Cramer's rule:

$$\mathbf{I}_1 = \frac{\begin{vmatrix} \mathbf{V}_1 & \mathbf{Z}_{12} & \mathbf{Z}_{13} & \dots & \mathbf{Z}_{1N} \\ 0 & \mathbf{Z}_{22} & \mathbf{Z}_{23} & \dots & \mathbf{Z}_{2N} \\ 0 & \mathbf{Z}_{32} & \mathbf{Z}_{33} & \dots & \mathbf{Z}_{3N} \\ \dots & \dots & \dots & \dots & \dots \\ 0 & \mathbf{Z}_{N2} & \mathbf{Z}_{N3} & \dots & \mathbf{Z}_{NN} \end{vmatrix}}{\begin{vmatrix} \mathbf{Z}_{11} & \mathbf{Z}_{12} & \mathbf{Z}_{13} & \dots & \mathbf{Z}_{1N} \\ \mathbf{Z}_{21} & \mathbf{Z}_{22} & \mathbf{Z}_{23} & \dots & \mathbf{Z}_{2N} \\ \mathbf{Z}_{31} & \mathbf{Z}_{32} & \mathbf{Z}_{33} & \dots & \mathbf{Z}_{3N} \\ \dots & \dots & \dots & \dots & \dots \\ \mathbf{Z}_{N1} & \mathbf{Z}_{N2} & \mathbf{Z}_{N3} & \dots & \mathbf{Z}_{NN} \end{vmatrix}}$$

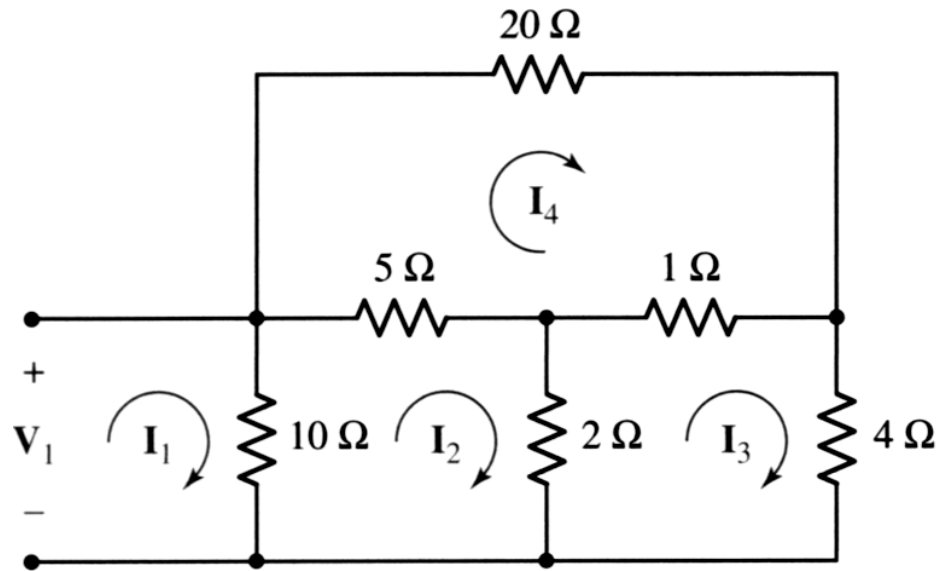
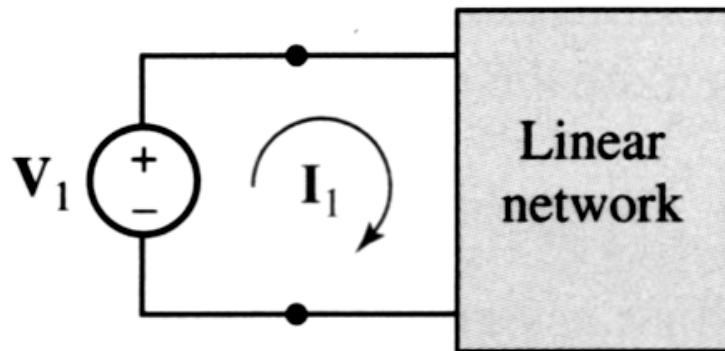


$$\mathbf{I}_1 = \frac{\mathbf{V}_1 \Delta_{11}}{\Delta_Z}$$

minor

$$\mathbf{Z}_{in} = \frac{\mathbf{V}_1}{\mathbf{I}_1} = \frac{\Delta_Z}{\Delta_{11}}$$

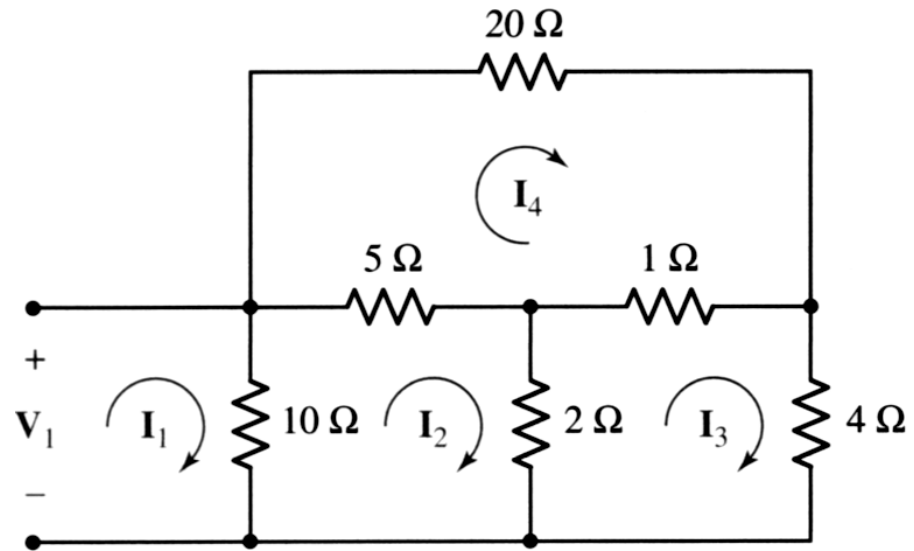
Example:



Calculate the input impedance:

Example:

By inspection:



$$V_1 = 10I_1 - 10I_2$$

$$0 = -10I_1 + 17I_2 - 2I_3 - 5I_4$$

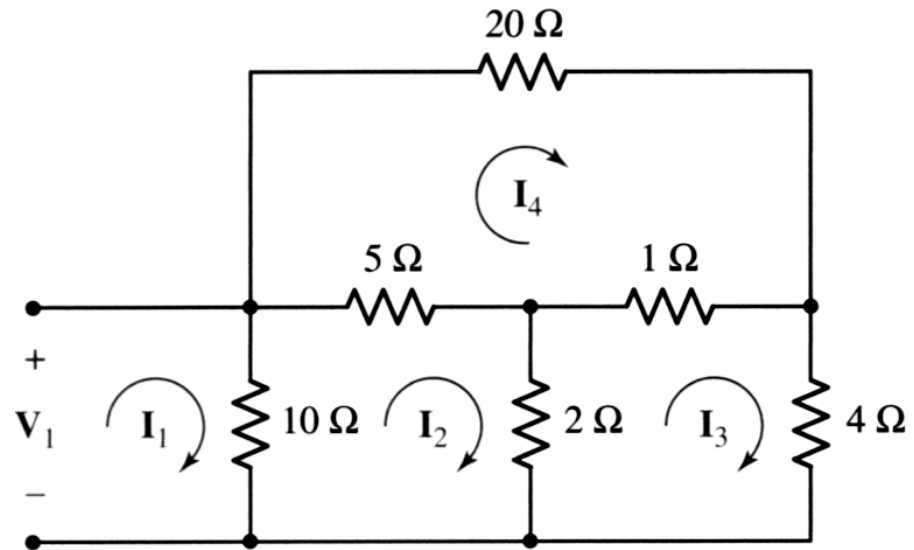
$$0 = -2I_2 + 7I_3 - I_4$$

$$0 = -5I_2 - I_3 + 26I_4$$

Example:

By inspection:

$$\begin{aligned} V_1 &= 10I_1 - 10I_2 \\ 0 &= -10I_1 + 17I_2 - 2I_3 - 5I_4 \\ 0 &= -2I_2 + 7I_3 - I_4 \\ 0 &= -5I_2 - I_3 + 26I_4 \end{aligned}$$

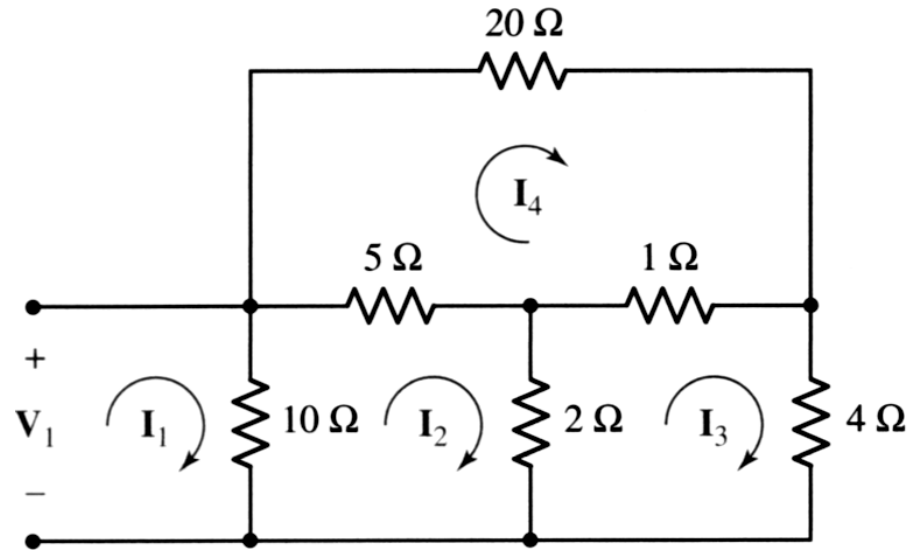


$$\Delta_Z = \begin{vmatrix} 10 & -10 & 0 & 0 \\ -10 & 17 & -2 & -5 \\ 0 & -2 & 7 & -1 \\ 0 & -5 & -1 & 26 \end{vmatrix} = 9680 \, \Omega^4$$

Example:

By inspection:

$$\begin{aligned} V_1 &= 10I_1 - 10I_2 \\ 0 &= -10I_1 + 17I_2 - 2I_3 - 5I_4 \\ 0 &= -2I_2 + 7I_3 - I_4 \\ 0 &= -5I_2 - I_3 + 26I_4 \end{aligned}$$

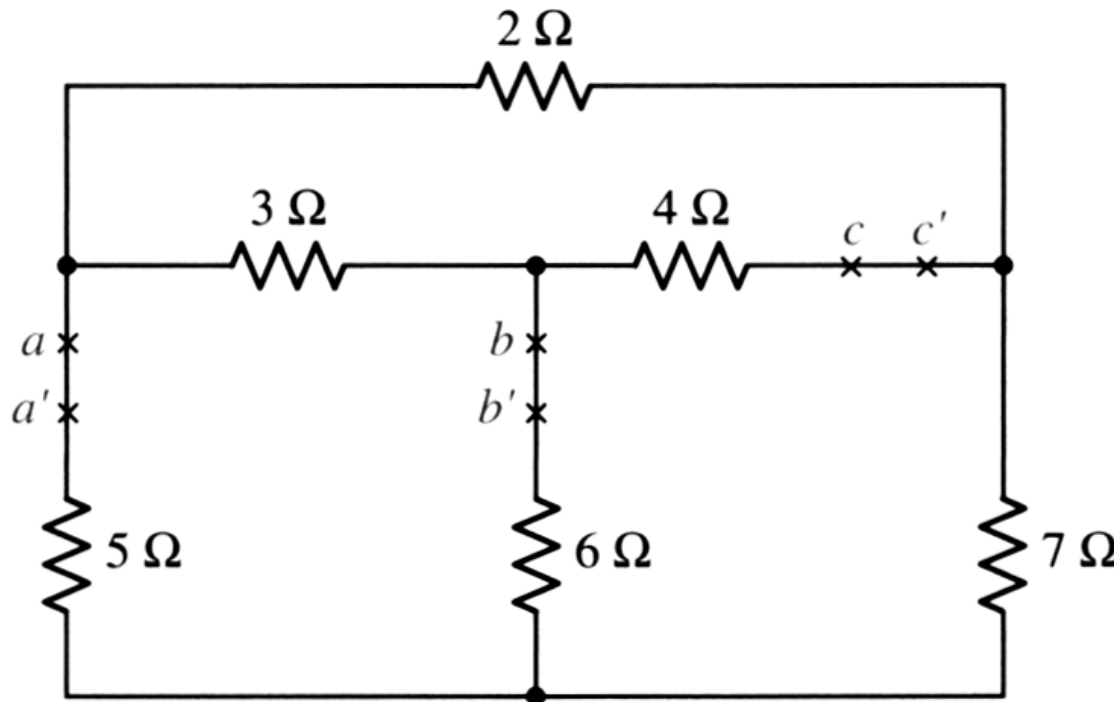


$$\Delta_{11} = \begin{vmatrix} 17 & -2 & -5 \\ -2 & 7 & -1 \\ -5 & -1 & 26 \end{vmatrix} = 2778$$

$$\mathbf{Z}_{in} = \frac{9680}{2778} = 3.485 \, \Omega$$

Practice: 17.1

Find the input impedance of the network shown in Figure below if it is formed into a one-port network by breaking it at terminals: (a) a and a' ; (b) b and b' ; (c) c and c' .



Practice: 17.1

- Assign clockwise mesh currents \mathbf{I}_1 , \mathbf{I}_2 , \mathbf{I}_3 to the top, left-hand and right-hand meshes, respectively.

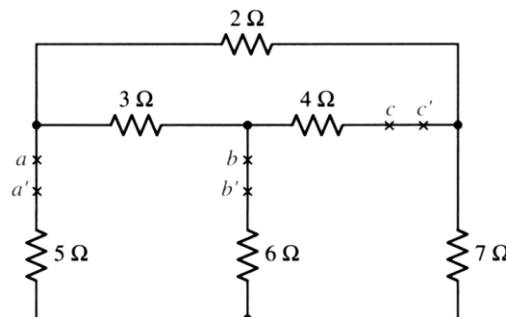
$$\begin{aligned} \mathbf{V}_{cc'} &= 9 \mathbf{I}_1 - 3 \mathbf{I}_2 - 4 \mathbf{I}_3 \\ \mathbf{V}_{aa'} - \mathbf{V}_{bb'} &= -3 \mathbf{I}_1 + 14 \mathbf{I}_2 - 6 \mathbf{I}_3 \\ \mathbf{V}_{bb'} - \mathbf{V}_{cc'} &= -4 \mathbf{I}_1 - 6 \mathbf{I}_2 + 17 \mathbf{I}_3 \end{aligned}$$

The circuit determinant is $\Delta_z = \begin{vmatrix} 9 & -3 & -4 \\ -3 & 14 & -6 \\ -4 & -6 & 17 \end{vmatrix} = 1297.$

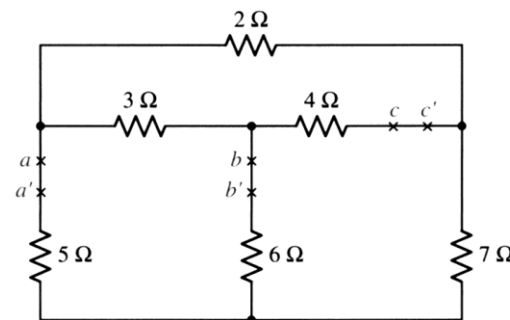
(a) $\mathbf{Z}_{aa'} = \mathbf{V}_{aa'} / \mathbf{I}_2$ with $\mathbf{V}_{bb'} = \mathbf{V}_{cc'} = 0.$

$$\mathbf{I}_2 = \frac{\begin{vmatrix} 9 & 0 & -4 \\ -3 & \mathbf{V}_{aa'} & -6 \\ -4 & 0 & 17 \end{vmatrix}}{\Delta_z} = \frac{\mathbf{V}_{aa'}}{\Delta_z} \begin{vmatrix} 9 & -4 \\ -4 & 17 \end{vmatrix} = \frac{137}{1297} \mathbf{V}_{aa'}$$

Thus, $\mathbf{Z}_{aa'} = 1297/137 = 9.467 \Omega.$



Practice: 17.1



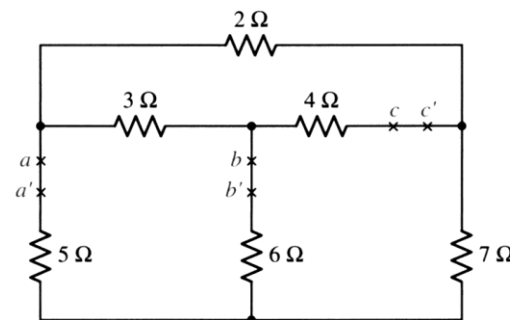
(b) $\mathbf{Z}_{bb'} = \frac{\mathbf{V}_{bb'}}{\mathbf{I}_3 - \mathbf{I}_2}$ with $\mathbf{V}_{aa'} = \mathbf{V}_{cc'} = 0$.

$$\Delta_z \cdot \mathbf{I}_3 = \begin{vmatrix} 9 & -3 & 0 \\ -3 & 14 & -\mathbf{V}_{bb'} \\ -4 & -6 & \mathbf{V}_{bb'} \end{vmatrix} = \mathbf{V}_{bb'} \begin{vmatrix} 9 & -3 \\ -4 & -6 \end{vmatrix} + \mathbf{V}_{bb'} \begin{vmatrix} 9 & -3 \\ -3 & 14 \end{vmatrix} = \mathbf{V}_{bb'} (-66 + 117) = 51\mathbf{V}_{bb'}$$

$$\Delta_z \cdot \mathbf{I}_2 = \begin{vmatrix} 9 & 0 & -4 \\ -3 & -\mathbf{V}_{bb'} & -6 \\ -4 & \mathbf{V}_{bb'} & 17 \end{vmatrix} = -\mathbf{V}_{bb'} \begin{vmatrix} 9 & -4 \\ -4 & 17 \end{vmatrix} - \mathbf{V}_{bb'} \begin{vmatrix} 9 & -4 \\ -3 & -6 \end{vmatrix} = -\mathbf{V}_{bb'} (137 - 66) = -71\mathbf{V}_{bb'}$$

so $\mathbf{Z}_{bb'} = \frac{\Delta_z}{51 + 71} = \frac{1297}{122} = \boxed{10.63 \Omega}$

Practice: 17.1



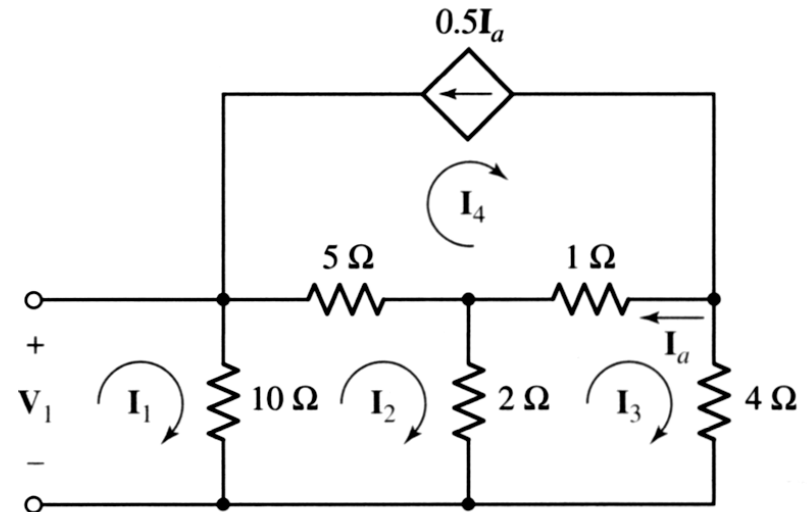
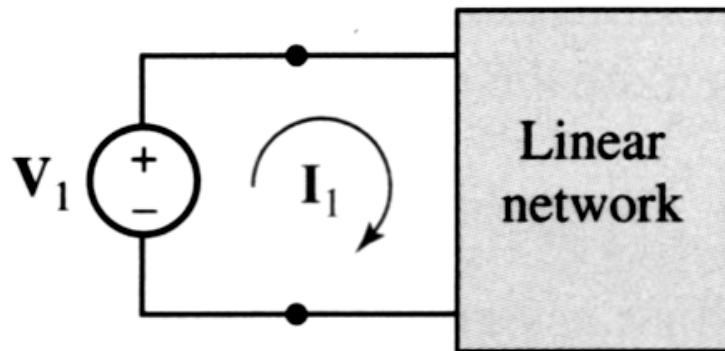
(c) $Z_{cc'} = \frac{V_{cc'}}{I_1 - I_3}$ with $V_{aa'} = V_{bb'} = 0$.

$$\Delta_z \cdot I_1 = \begin{vmatrix} V_{cc'} & -3 & -4 \\ 0 & 14 & -6 \\ -V_{cc'} & -6 & 17 \end{vmatrix} = V_{cc'} \begin{vmatrix} 14 & -6 \\ -6 & 17 \end{vmatrix} - V_{cc'} \begin{vmatrix} -3 & -4 \\ 14 & -6 \end{vmatrix} = V_{cc'}(202 - 74) = 128V_{cc'}$$

$$\Delta_z \cdot I_3 = \begin{vmatrix} 9 & -3 & V_{cc'} \\ -3 & 14 & 0 \\ -4 & -6 & -V_{cc'} \end{vmatrix} = V_{cc'} \begin{vmatrix} -3 & 14 \\ -4 & -6 \end{vmatrix} - V_{cc'} \begin{vmatrix} 9 & -3 \\ -3 & 14 \end{vmatrix} = V_{cc'}(74 - 117) = -43V_{cc'}$$

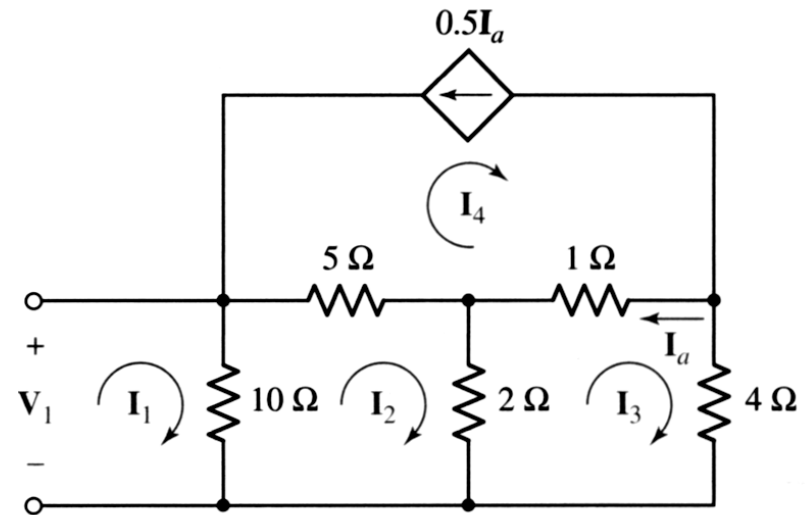
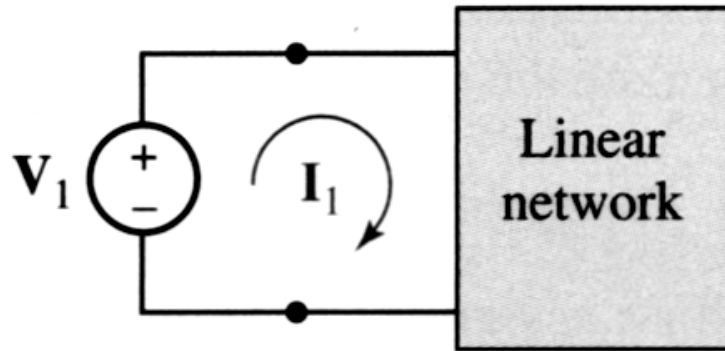
$$\text{so } Z_{cc'} = \frac{\Delta_z}{128 + 43} = \frac{1297}{171} = \boxed{7.585 \Omega}$$

Example:



Calculate the input impedance:

Example:



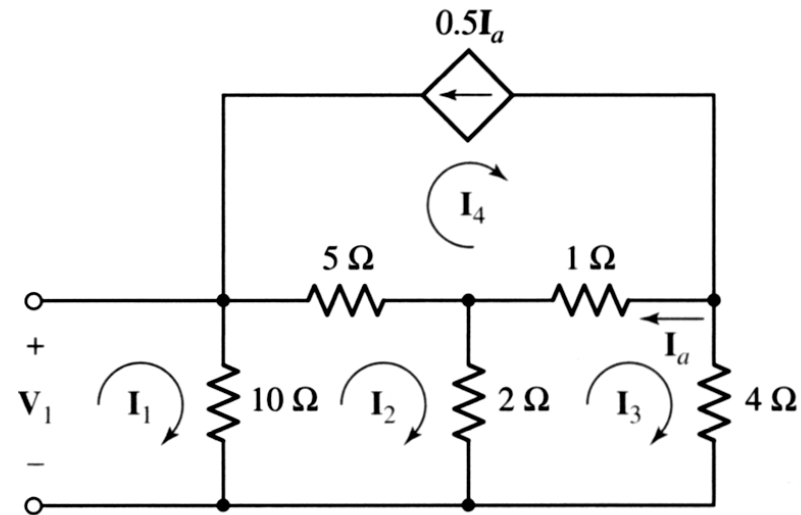
$$\begin{aligned} 10\mathbf{I}_1 - 10\mathbf{I}_2 &= \mathbf{V}_1 \\ -10\mathbf{I}_1 + 17\mathbf{I}_2 - 2\mathbf{I}_3 - 5\mathbf{I}_4 &= 0 \\ -2\mathbf{I}_2 + 7\mathbf{I}_3 - \mathbf{I}_4 &= 0 \end{aligned}$$

and $\mathbf{I}_4 = -0.5\mathbf{I}_a = -0.5(\mathbf{I}_4 - \mathbf{I}_3)$

or $-0.5\mathbf{I}_3 + 1.5\mathbf{I}_4 = 0$

Example:

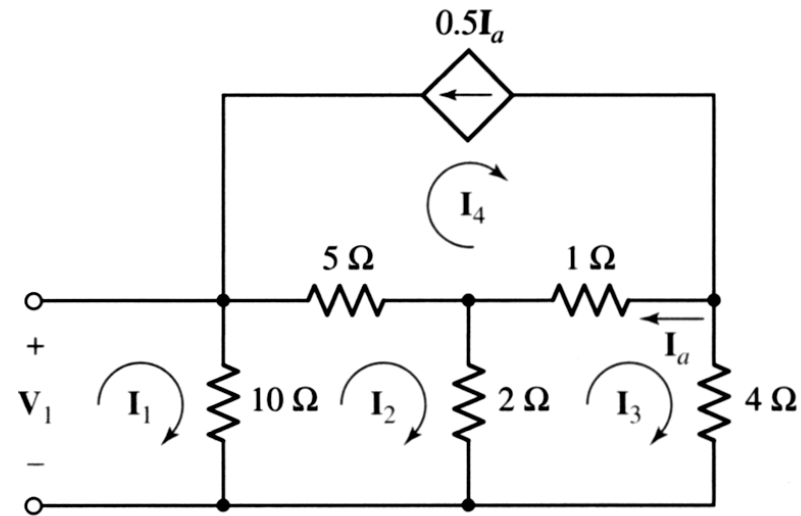
$$\begin{aligned}
 10\mathbf{I}_1 - 10\mathbf{I}_2 &= \mathbf{V}_1 \\
 -10\mathbf{I}_1 + 17\mathbf{I}_2 - 2\mathbf{I}_3 - 5\mathbf{I}_4 &= 0 \\
 -2\mathbf{I}_2 + 7\mathbf{I}_3 - \mathbf{I}_4 &= 0 \\
 -0.5\mathbf{I}_3 + 1.5\mathbf{I}_4 &= 0
 \end{aligned}$$



$$\Delta_{\mathbf{Z}} = \begin{vmatrix} 10 & -10 & 0 & 0 \\ -10 & 17 & -2 & -5 \\ 0 & -2 & 7 & -1 \\ 0 & 0 & -0.5 & 1.5 \end{vmatrix} = 590\ \Omega$$

Example:

$$\begin{aligned}
 10\mathbf{I}_1 - 10\mathbf{I}_2 &= \mathbf{V}_1 \\
 -10\mathbf{I}_1 + 17\mathbf{I}_2 - 2\mathbf{I}_3 - 5\mathbf{I}_4 &= 0 \\
 -2\mathbf{I}_2 + 7\mathbf{I}_3 - \mathbf{I}_4 &= 0 \\
 -0.5\mathbf{I}_3 + 1.5\mathbf{I}_4 &= 0
 \end{aligned}$$

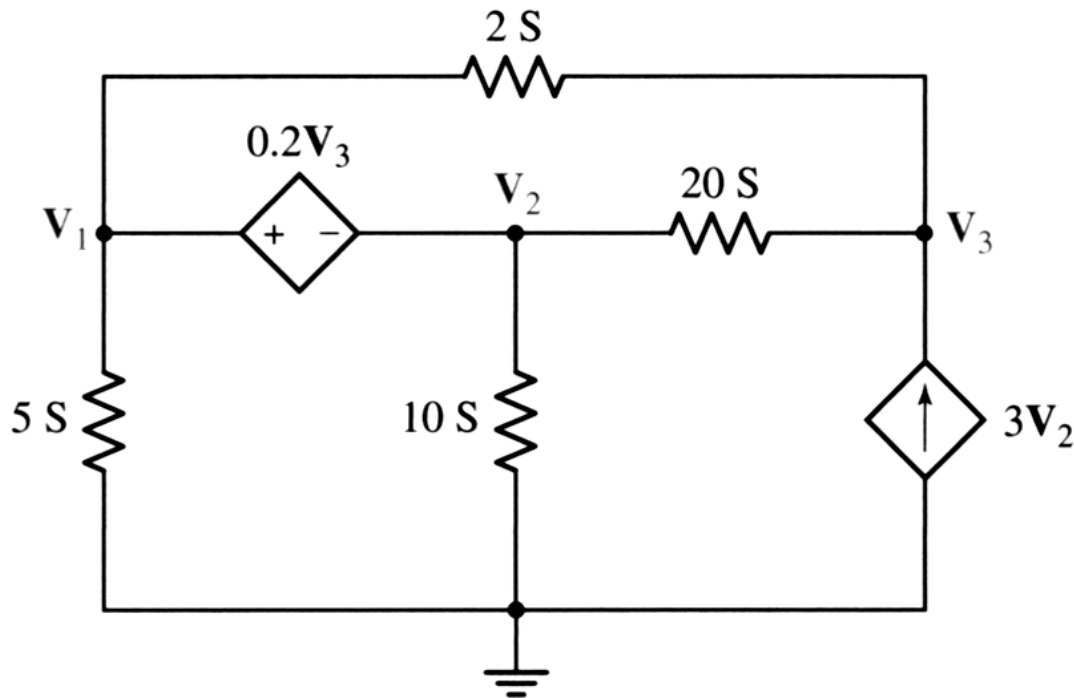


$$\Delta_{11} = \begin{vmatrix} 17 & -2 & -5 \\ -2 & 7 & -1 \\ 0 & -0.5 & 1.5 \end{vmatrix} = 159\ \Omega$$

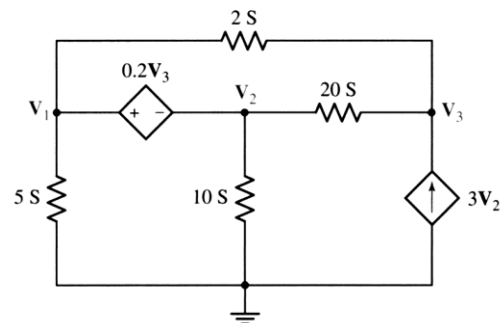
$$\mathbf{Z}_{in} = \frac{590}{159} = 3.711\ \Omega$$

Practice: 17.2

Write a set of nodal equations for the circuit of figure below, calculate Δ_Y , and then find the input admittance seen between: (a) node 1 and the reference node; (b) node 2 and the reference.



Practice: 17.2



At the 1,2 supernode: $0 = 5V_1 + 10V_2 + 2(V_1 - V_3) + 20(V_2 - V_3)$ [1]

At node 3: $3V_2 = 20(V_3 - V_2) + 2(V_3 - V_1)$ [2]

And: $V_1 - V_2 = 0.2V_3$ [3]

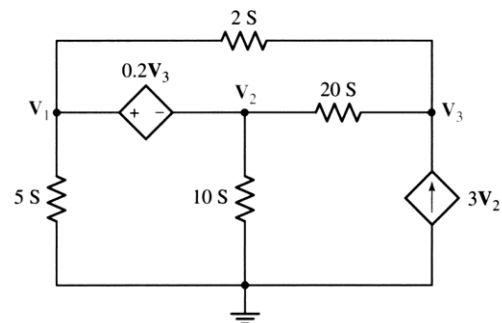
Simplifying, $7V_1 + 30V_2 - 22V_3 = 0$ [1]

$-2V_1 - 23V_2 + 22V_3 = 0$ [2]

$V_1 - V_2 - 0.2V_3 = 0$ [3]

$$\Delta_Y = \begin{vmatrix} 7 & 30 & -22 \\ -2 & -23 & 22 \\ 1 & -1 & -0.2 \end{vmatrix} = 284.2$$

Practice: 17.2



- (a) If we inject a current \mathbf{I} into node 1 by connecting a current source in parallel with the 5-S conductance, we obtain:

$$\mathbf{V}_1 = \frac{\begin{vmatrix} \mathbf{I} & 30 & -22 \\ 0 & -23 & 22 \\ 0 & -1 & -0.2 \end{vmatrix}}{\Delta_Y} = \frac{\mathbf{I} \begin{vmatrix} -23 & 22 \\ -1 & -0.2 \end{vmatrix}}{\Delta_Y} = \mathbf{I} \frac{26.6}{284.2}$$

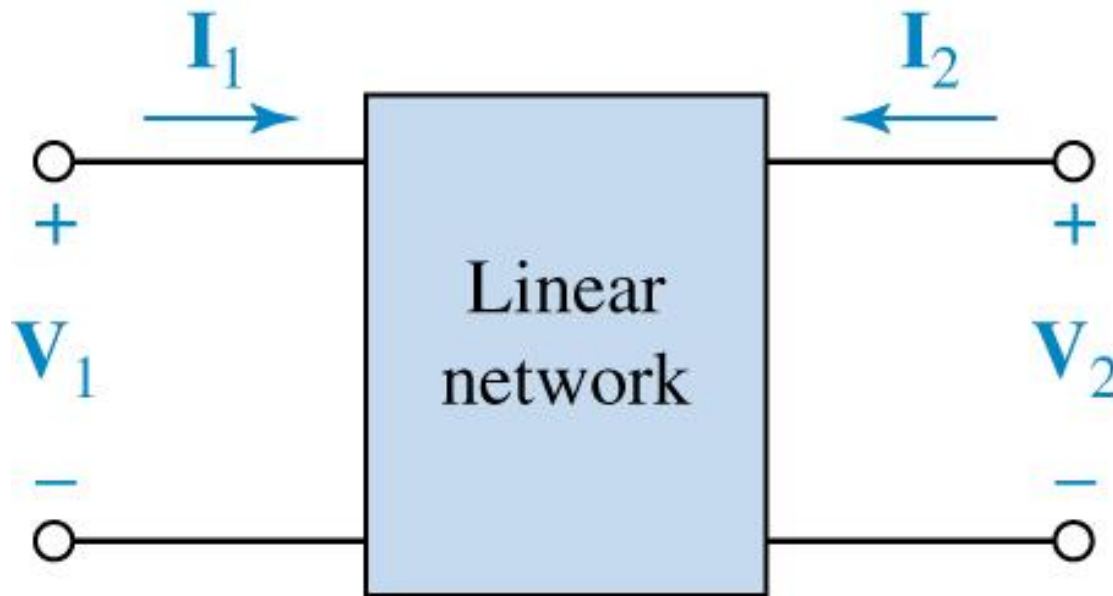
Thus, the input admittance is $\mathbf{I}/\mathbf{V}_1 = 284.2/26.6 = 10.68 \text{ S}$.

- (b) We now connect the current source between node 2 and ground.

$$\mathbf{V}_2 = \frac{\begin{vmatrix} 7 & \mathbf{I} & -22 \\ -2 & 0 & 22 \\ 1 & 0 & -0.2 \end{vmatrix}}{\Delta_Y} = \frac{-\mathbf{I} \begin{vmatrix} -2 & 22 \\ 1 & -0.2 \end{vmatrix}}{\Delta_Y} = -\mathbf{I} \frac{(-21.6)}{284.2}$$

Thus, the input admittance is $\mathbf{I}/\mathbf{V}_2 = 284.2/21.6 = 13.16 \text{ S}$.

Admittance Parameters:



A general two-port with terminal voltages and currents specified.

The two-port is composed of:

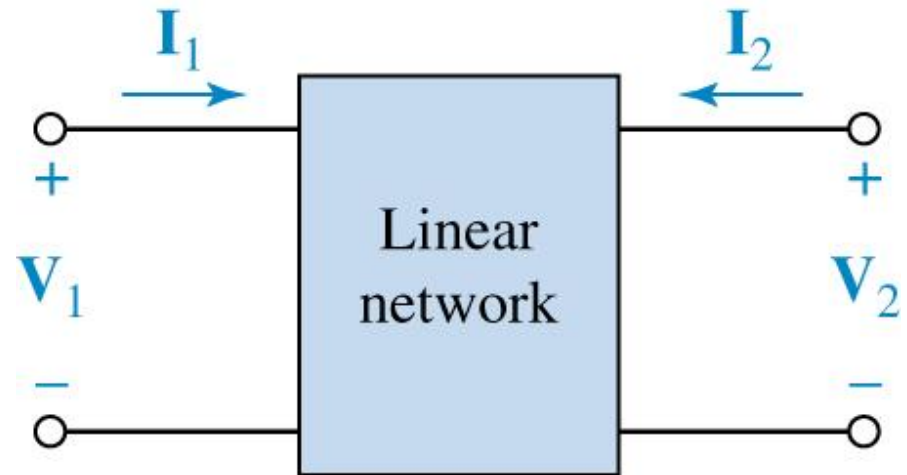
- **linear elements**, no energy stored within the circuits
- possibly including **dependent sources**,
- but **not** containing **any independent sources**.
- **all external connections must be made to either the input port or the output port.**

Admittance Parameters:

We may begin with the set of equations:

$$\mathbf{I}_1 = \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2$$



The matrix equation:

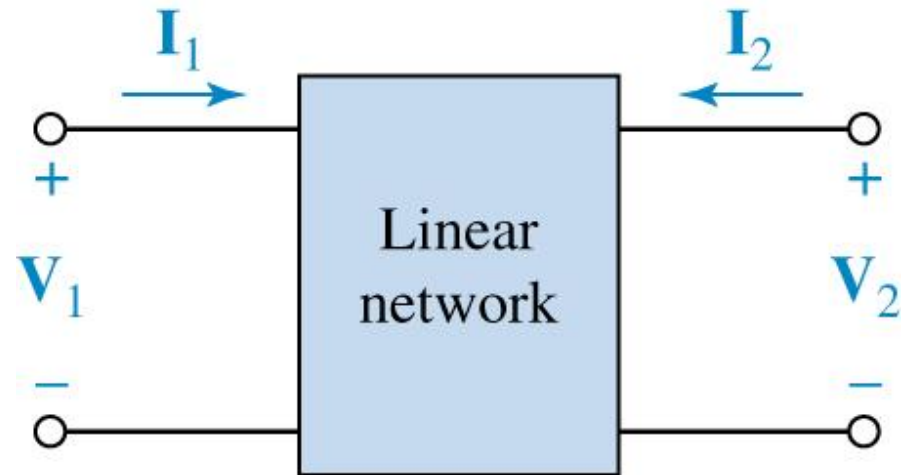
$$\begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} \mathbf{y}_{11} & \mathbf{y}_{12} \\ \mathbf{y}_{21} & \mathbf{y}_{22} \end{bmatrix} \begin{bmatrix} \mathbf{V}_1 \\ \mathbf{V}_2 \end{bmatrix}$$

Admittance Parameters:

We may begin with the set of equations:

$$\mathbf{I}_1 = \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2$$



The short-circuit admittance parameters

The short-circuit input admittance:

$$\mathbf{y}_{11} = \left. \frac{\mathbf{I}_1}{\mathbf{V}_1} \right|_{\mathbf{V}_2=0}$$

The short-circuit output admittance:

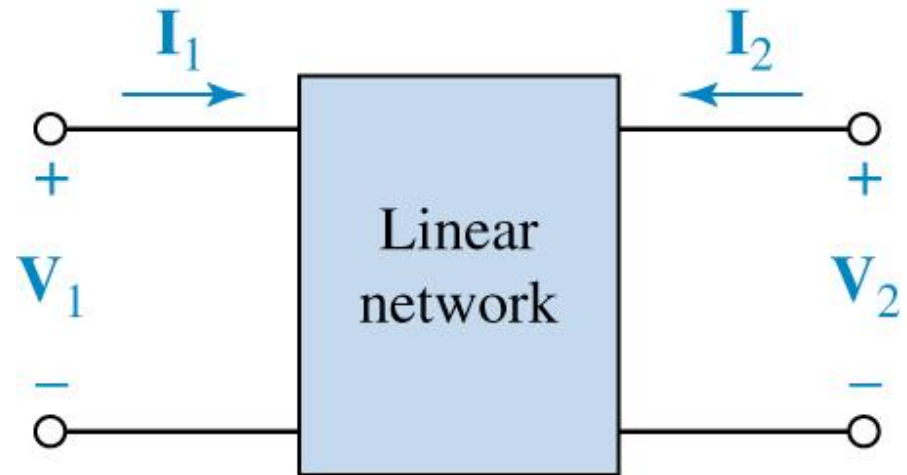
$$\mathbf{y}_{22} = \left. \frac{\mathbf{I}_2}{\mathbf{V}_2} \right|_{\mathbf{V}_1=0}$$

Admittance Parameters:

We may begin with the set of equations:

$$\mathbf{I}_1 = \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2$$



The short-circuit admittance parameters

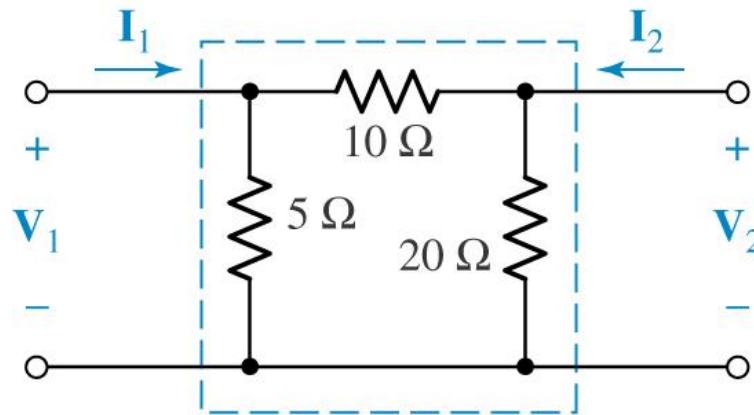
The short-circuit transfer admittance:

$$\mathbf{y}_{12} = \left. \frac{\mathbf{I}_1}{\mathbf{V}_2} \right|_{\mathbf{V}_1=0}$$

$$\mathbf{y}_{21} = \left. \frac{\mathbf{I}_2}{\mathbf{V}_1} \right|_{\mathbf{V}_2=0}$$

Example:

Find the short-circuit admittance parameters:



$$y_{11} = \left. \frac{I_1}{V_1} \right|_{V_2=0}$$

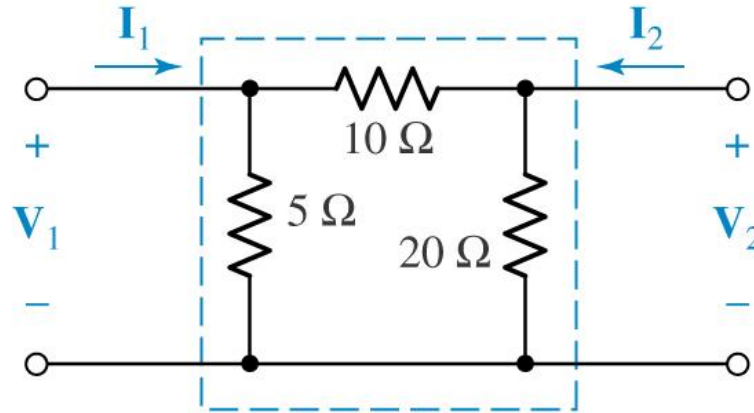
$$y_{12} = \left. \frac{I_1}{V_2} \right|_{V_1=0}$$

$$y_{22} = \left. \frac{I_2}{V_2} \right|_{V_1=0}$$

$$y_{21} = \left. \frac{I_2}{V_1} \right|_{V_2=0}$$

Example:

Find the short-circuit admittance parameters:

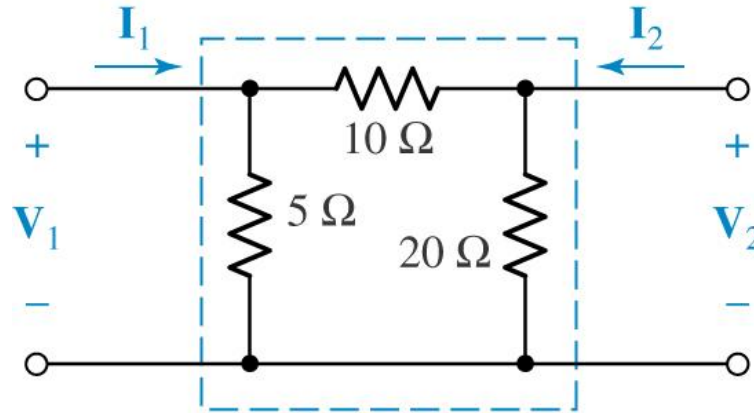


$$\mathbf{y}_{11} = \left. \frac{\mathbf{I}_1}{\mathbf{V}_1} \right|_{\mathbf{V}_2=0} = \frac{15}{5 \cdot 10} = 0.3 \quad \text{S.}$$

$$\mathbf{y}_{22} = \left. \frac{\mathbf{I}_2}{\mathbf{V}_2} \right|_{\mathbf{V}_1=0} = \frac{30}{10 \cdot 20} = 0.15 \quad \text{S.}$$

Example:

Find the short-circuit admittance parameters:

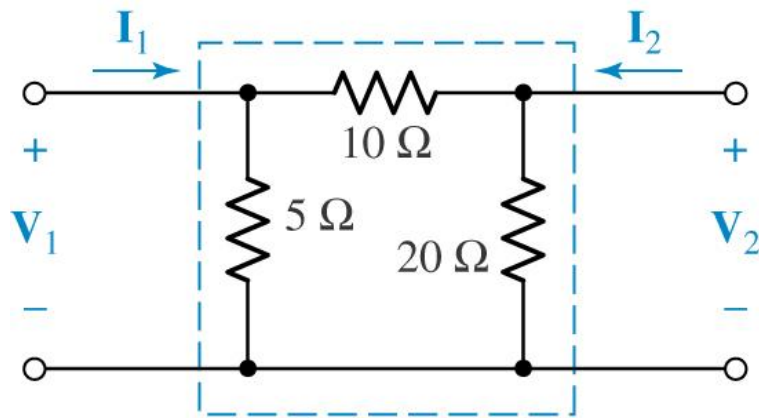


$$\text{When } \mathbf{V}_1 = 0, \mathbf{I}_1 = \frac{-\mathbf{V}_2}{10} \quad \therefore \mathbf{y}_{12} = \left. \frac{-\mathbf{V}_2/10}{\mathbf{V}_2} \right|_{\mathbf{V}_1=0} = -0.1 \text{ S.}$$

$$\text{When } \mathbf{V}_2 = 0, \mathbf{I}_2 = \frac{-\mathbf{V}_1}{10} \quad \therefore \mathbf{y}_{21} = \left. \frac{-\mathbf{V}_1/10}{\mathbf{V}_1} \right|_{\mathbf{V}_2=0} = -0.1 \text{ S.}$$

Example:

Find the short-circuit admittance parameters:



$$\mathbf{I}_1 = \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2$$

Write the expressions:

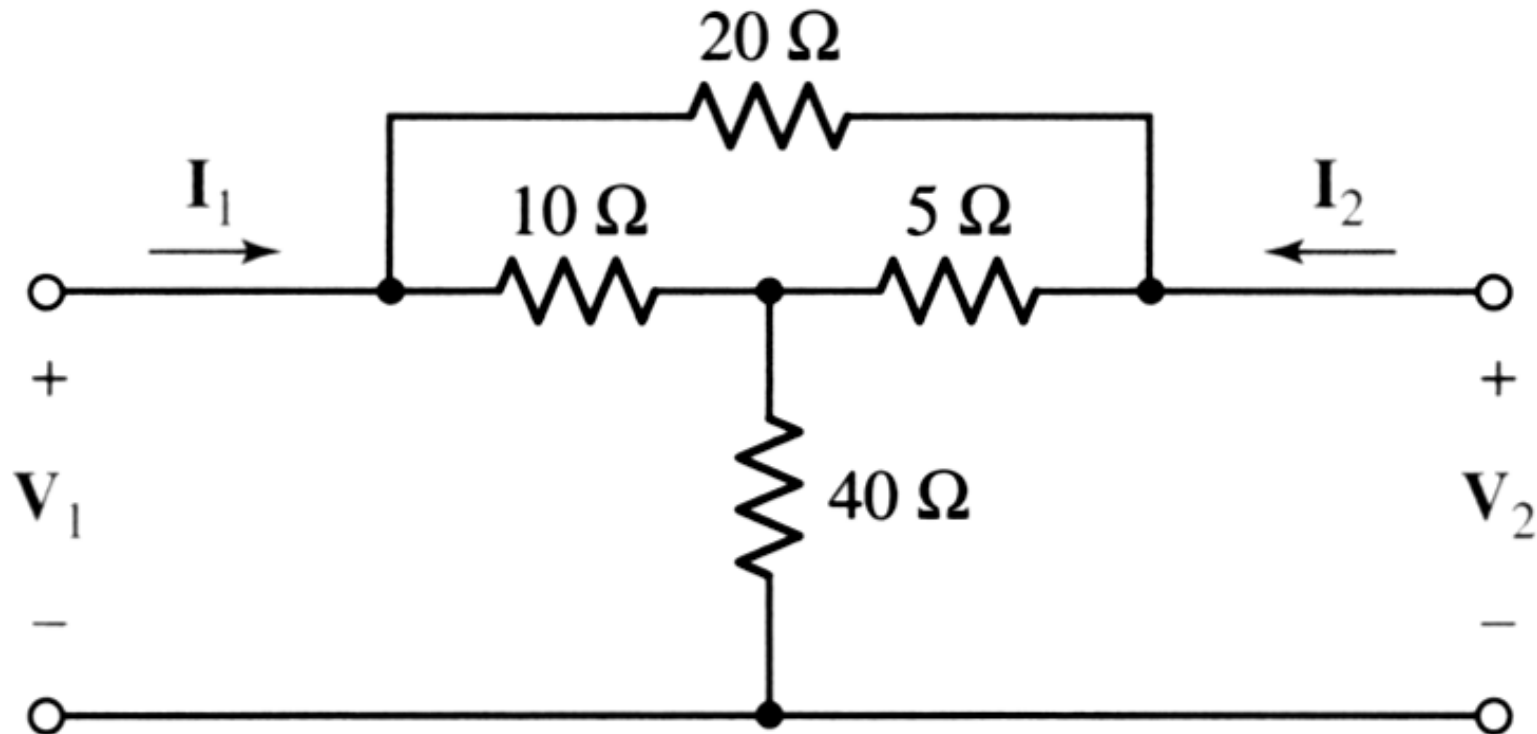
$$\mathbf{I}_1 = \frac{\mathbf{V}_1}{5} + \frac{\mathbf{V}_1 - \mathbf{V}_2}{10} = 0.3\mathbf{V}_1 - 0.1\mathbf{V}_2$$

$$\mathbf{I}_2 = \frac{\mathbf{V}_2 - \mathbf{V}_1}{10} + \frac{\mathbf{V}_2}{20} = -0.1\mathbf{V}_1 + 0.15\mathbf{V}_2$$

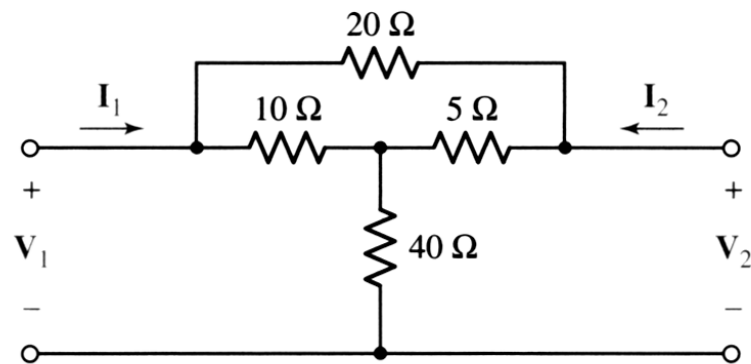
$$\Rightarrow \mathbf{y} = \begin{bmatrix} 0.3 & -0.1 \\ -0.1 & 0.15 \end{bmatrix}$$

Practice: 17.3

By applying the appropriate 1-V sources and short circuits to the circuit shown in figure below, find (a) y_{11} ; (b) y_{21} ; (c) y_{22} ; (d) y_{12}



Practice: 17.3



(a) $y_{11} = \left. \frac{I_1}{V_1} \right|_{V_2=0}$ so short right terminals and apply $V_1 = 1$ V.

$$5 \Omega \parallel 40 \Omega = 4.444 \Omega; \quad 20 \Omega \parallel (10 + 4.444) = 8.387 \Omega.$$

Thus, $y_{11} = 1/8.387 = \boxed{119.2 \text{ mS}}.$

(b) $y_{21} = \left. \frac{I_2}{V_1} \right|_{V_2=0}$ so short right terminals and apply $V_1 = 1$ V.

Define a clockwise current I_3 in the top mesh.

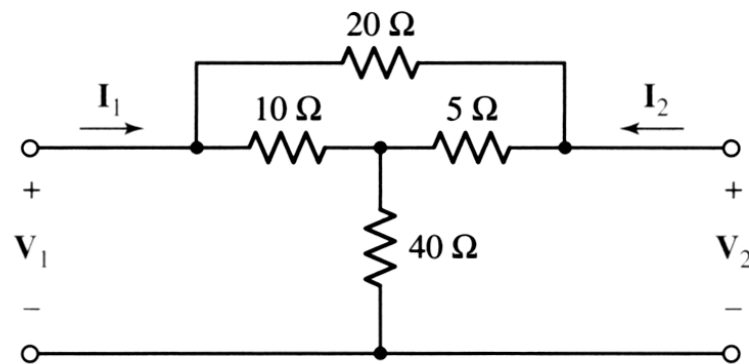
Mesh 1: $-1 + 50 I_1 - 10 I_3 + 40 I_2 = 0$

Mesh 2: $-40 I_1 - 5 I_3 - 45 I_2 = 0$

Top mesh: $-10 I_1 + 35 I_3 + 5 I_2 = 0$

Solving, $I_2 = \boxed{-111.5 \text{ mS}}.$

Practice: 17.3



(c) $y_{22} = \left. \frac{I_2}{V_2} \right|_{V_1=0}$ so short left terminals and apply $V_2 = 1$ V.

$$10 \, \Omega \parallel 40 \, \Omega = 8 \, \Omega; \quad 20 \, \Omega \parallel (8 + 5) = 7.879 \, \Omega.$$

Thus, $y_{22} = 1/7.879 = \boxed{126.9 \text{ mS.}}$

(d) $y_{12} = \left. \frac{I_1}{V_2} \right|_{V_1=0}$ so short left terminals and apply $V_2 = 1$ V.

Mesh 1: $50 I_1 - 10 I_3 + 40 I_2 = 0$

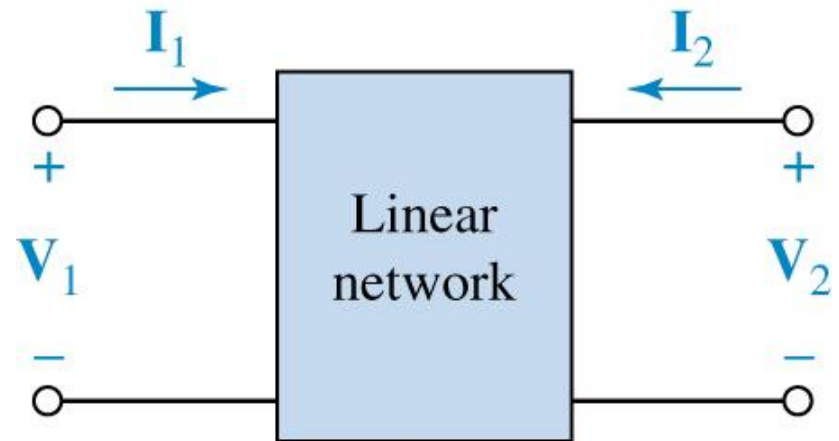
Mesh 2: $-40 I_1 - 5 I_3 - 45 I_2 = -1$

Top mesh: $-10 I_1 + 35 I_3 + 5 I_2 = 0$

Solving, $I_1 = \boxed{-111.5 \text{ mS.}}$

The Terminal Equations:

There are six different ways in which to combine the four variables:



$$\mathbf{V}_1 = \mathbf{z}_{11}\mathbf{I}_1 + \mathbf{z}_{12}\mathbf{I}_2$$

$$\mathbf{V}_2 = \mathbf{z}_{21}\mathbf{I}_1 + \mathbf{z}_{22}\mathbf{I}_2$$

$$\mathbf{V}_1 = \mathbf{a}_{11}\mathbf{V}_2 - \mathbf{a}_{12}\mathbf{I}_2$$

$$\mathbf{I}_1 = \mathbf{a}_{21}\mathbf{V}_2 - \mathbf{a}_{22}\mathbf{I}_2$$

$$\mathbf{V}_1 = \mathbf{h}_{11}\mathbf{I}_1 + \mathbf{h}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{h}_{21}\mathbf{I}_1 + \mathbf{h}_{22}\mathbf{V}_2$$

$$\mathbf{I}_1 = \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2$$

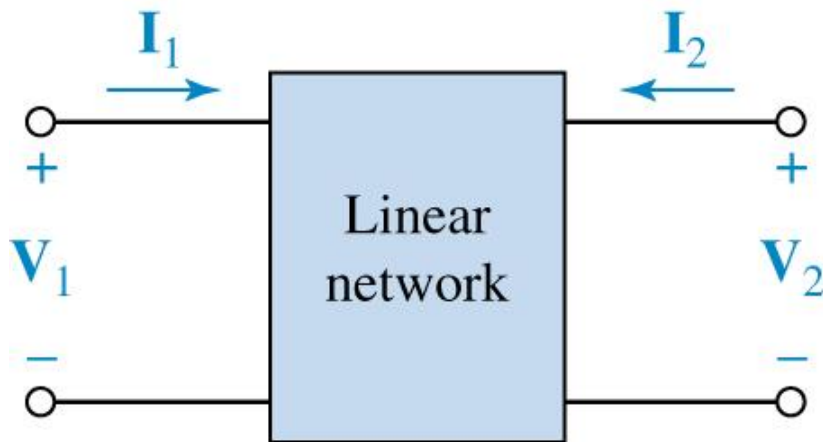
$$\mathbf{V}_2 = \mathbf{b}_{11}\mathbf{V}_1 - \mathbf{b}_{12}\mathbf{I}_1$$

$$\mathbf{I}_2 = \mathbf{b}_{21}\mathbf{V}_1 - \mathbf{b}_{22}\mathbf{I}_1$$

$$\mathbf{I}_1 = \mathbf{g}_{11}\mathbf{V}_1 + \mathbf{g}_{12}\mathbf{I}_2$$

$$\mathbf{V}_2 = \mathbf{g}_{21}\mathbf{V}_1 + \mathbf{g}_{22}\mathbf{I}_2$$

Admittance parameters:



$$\mathbf{I}_1 = \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2$$

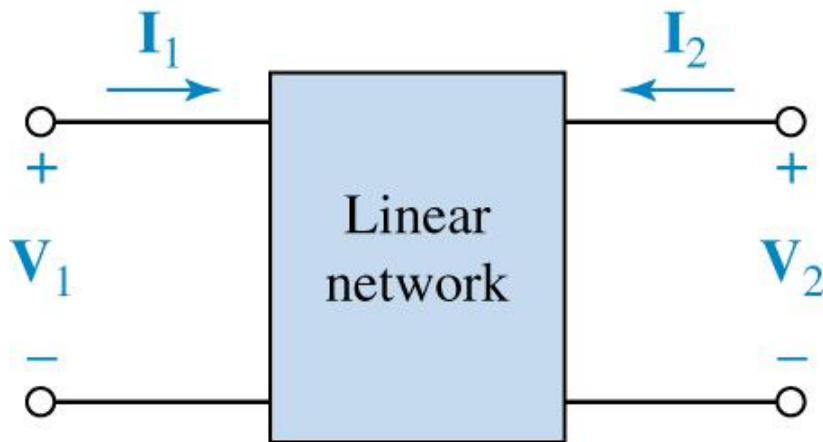
$$\mathbf{y}_{11} = \left. \frac{\mathbf{I}_1}{\mathbf{V}_1} \right|_{\mathbf{V}_2=0}$$

$$\mathbf{y}_{12} = \left. \frac{\mathbf{I}_1}{\mathbf{V}_2} \right|_{\mathbf{V}_1=0}$$

$$\mathbf{y}_{22} = \left. \frac{\mathbf{I}_2}{\mathbf{V}_2} \right|_{\mathbf{V}_1=0}$$

$$\mathbf{y}_{21} = \left. \frac{\mathbf{I}_2}{\mathbf{V}_1} \right|_{\mathbf{V}_2=0}$$

impedance parameters:



$$\mathbf{V}_1 = \mathbf{z}_{11}\mathbf{I}_1 + \mathbf{z}_{12}\mathbf{I}_2$$

$$\mathbf{V}_2 = \mathbf{z}_{21}\mathbf{I}_1 + \mathbf{z}_{22}\mathbf{I}_2$$

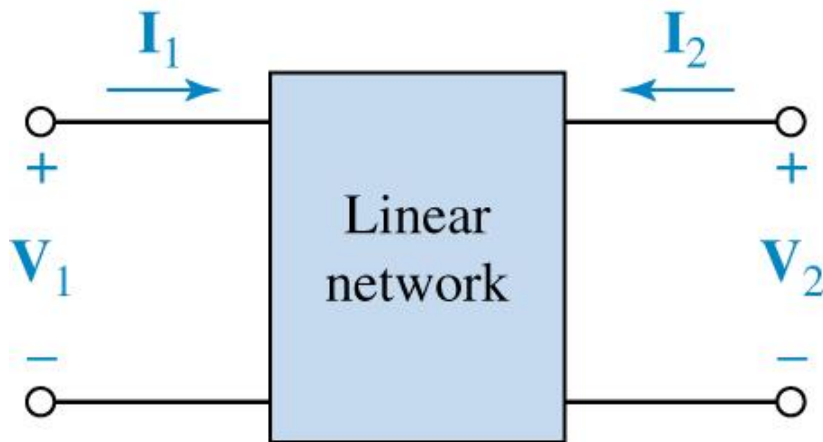
$$\mathbf{z}_{11} = \left. \frac{\mathbf{V}_1}{\mathbf{I}_1} \right|_{\mathbf{I}_2=0}$$

$$\mathbf{z}_{22} = \left. \frac{\mathbf{V}_2}{\mathbf{I}_2} \right|_{\mathbf{I}_1=0}$$

$$\mathbf{z}_{12} = \left. \frac{\mathbf{V}_1}{\mathbf{I}_2} \right|_{\mathbf{I}_1=0}$$

$$\mathbf{z}_{21} = \left. \frac{\mathbf{V}_2}{\mathbf{I}_1} \right|_{\mathbf{I}_2=0}$$

transmission parameters:



$$\mathbf{V}_1 = \mathbf{a}_{11}\mathbf{V}_2 - \mathbf{a}_{12}\mathbf{I}_2$$

$$\mathbf{I}_1 = \mathbf{a}_{21}\mathbf{V}_2 - \mathbf{a}_{22}\mathbf{I}_2$$

$$\mathbf{a}_{11} = \left. \frac{\mathbf{V}_1}{\mathbf{V}_2} \right|_{\mathbf{I}_2=0}$$

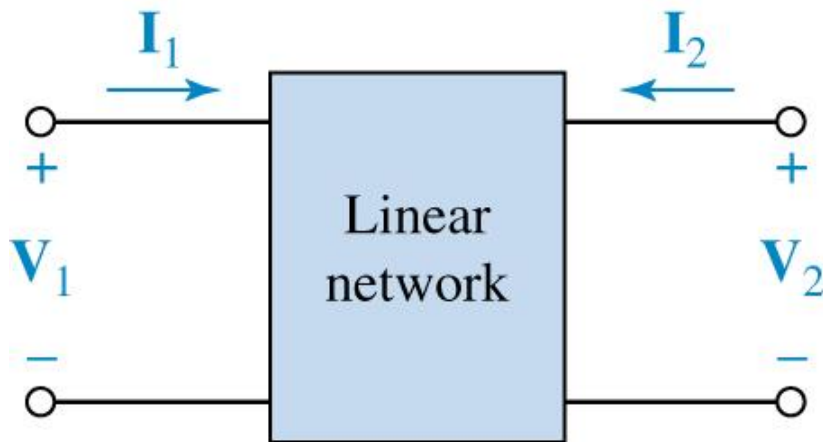
$$\mathbf{a}_{12} = \left. \frac{-\mathbf{V}_1}{\mathbf{I}_2} \right|_{\mathbf{V}_2=0} \quad \Omega$$

$$\mathbf{a}_{22} = \left. \frac{-\mathbf{I}_1}{\mathbf{I}_2} \right|_{\mathbf{V}_2=0}$$

$$\mathbf{a}_{21} = \left. \frac{\mathbf{I}_1}{\mathbf{V}_2} \right|_{\mathbf{I}_2=0} \quad \text{S.}$$

Note: Hayt's use "t" instead of "a"

transmission parameters:



$$\mathbf{V}_2 = \mathbf{b}_{11}\mathbf{V}_1 - \mathbf{b}_{12}\mathbf{I}_1$$

$$\mathbf{I}_2 = \mathbf{b}_{21}\mathbf{V}_1 - \mathbf{b}_{22}\mathbf{I}_1$$

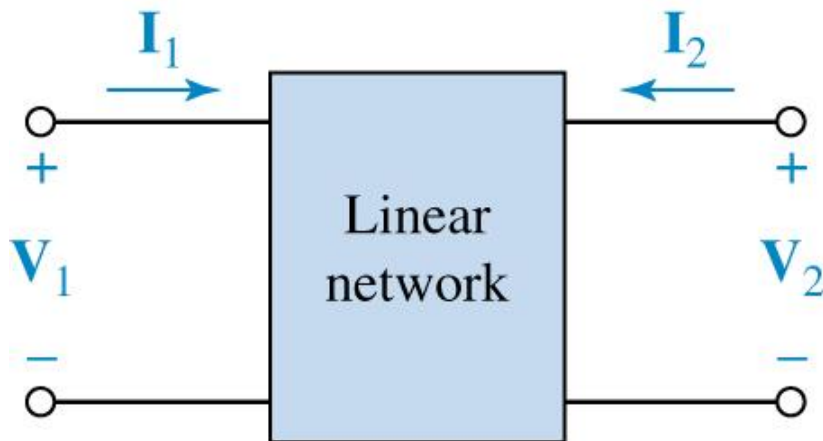
$$\mathbf{b}_{11} = \left. \frac{\mathbf{V}_2}{\mathbf{V}_1} \right|_{\mathbf{I}_1=0}$$

$$\mathbf{b}_{22} = \left. \frac{-\mathbf{I}_2}{\mathbf{I}_1} \right|_{\mathbf{V}_1=0}$$

$$\mathbf{b}_{12} = \left. \frac{-\mathbf{V}_2}{\mathbf{I}_1} \right|_{\mathbf{V}_1=0} \quad \Omega$$

$$\mathbf{b}_{21} = \left. \frac{\mathbf{I}_2}{\mathbf{V}_1} \right|_{\mathbf{I}_1=0} \quad \text{S.}$$

hybrid parameters:



$$\mathbf{V}_1 = \mathbf{h}_{11}\mathbf{I}_1 + \mathbf{h}_{12}\mathbf{V}_2$$

$$\mathbf{I}_2 = \mathbf{h}_{21}\mathbf{I}_1 + \mathbf{h}_{22}\mathbf{V}_2$$

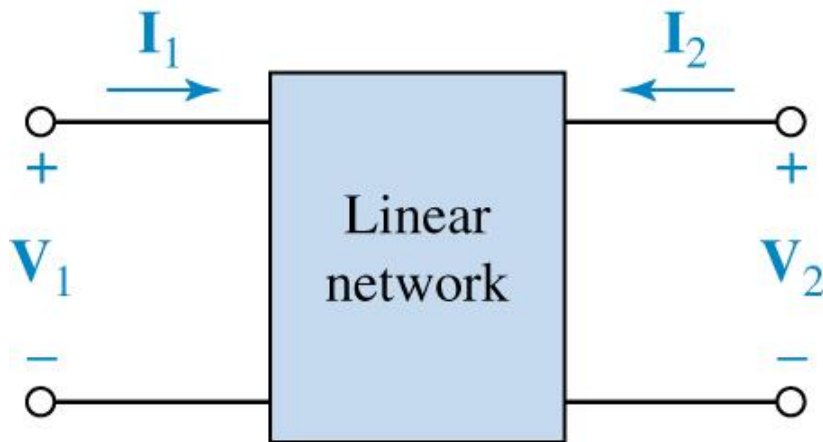
$$\mathbf{h}_{11} = \left. \frac{\mathbf{V}_1}{\mathbf{I}_1} \right|_{\mathbf{V}_2=0} \quad \Omega$$

$$\mathbf{h}_{22} = \left. \frac{\mathbf{I}_2}{\mathbf{V}_2} \right|_{\mathbf{I}_1=0} \quad \text{S.}$$

$$\mathbf{h}_{12} = \left. \frac{\mathbf{V}_1}{\mathbf{V}_2} \right|_{\mathbf{I}_1=0}$$

$$\mathbf{h}_{21} = \left. \frac{\mathbf{I}_2}{\mathbf{I}_1} \right|_{\mathbf{V}_2=0}$$

hybrid parameters:



$$\mathbf{I}_1 = \mathbf{g}_{11}\mathbf{V}_1 + \mathbf{g}_{12}\mathbf{I}_2$$

$$\mathbf{V}_2 = \mathbf{g}_{21}\mathbf{V}_1 + \mathbf{g}_{22}\mathbf{I}_2$$

$$\mathbf{g}_{11} = \left. \frac{\mathbf{I}_1}{\mathbf{V}_1} \right|_{\mathbf{I}_2=0} \quad \text{S.}$$

$$\mathbf{g}_{22} = \left. \frac{\mathbf{V}_2}{\mathbf{I}_2} \right|_{\mathbf{V}_1=0} \quad \Omega$$

$$\mathbf{g}_{12} = \left. \frac{\mathbf{I}_1}{\mathbf{I}_2} \right|_{\mathbf{V}_1=0}$$

$$\mathbf{g}_{21} = \left. \frac{\mathbf{V}_2}{\mathbf{V}_1} \right|_{\mathbf{I}_2=0}$$

Relationships Among ...:

To find the **z-parameters** as function of **y-parameters**,

$$\mathbf{I}_1 = \mathbf{y}_{11}\mathbf{V}_1 + \mathbf{y}_{12}\mathbf{V}_2$$

$$\mathbf{V}_1 = \mathbf{z}_{11}\mathbf{I}_1 + \mathbf{z}_{12}\mathbf{I}_2$$

$$\mathbf{I}_2 = \mathbf{y}_{21}\mathbf{V}_1 + \mathbf{y}_{22}\mathbf{V}_2$$

$$\mathbf{V}_2 = \mathbf{z}_{21}\mathbf{I}_1 + \mathbf{z}_{22}\mathbf{I}_2$$

$$\begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix} = \begin{bmatrix} \mathbf{y}_{11} & \mathbf{y}_{12} \\ \mathbf{y}_{21} & \mathbf{y}_{22} \end{bmatrix} \begin{bmatrix} \mathbf{V}_1 \\ \mathbf{V}_2 \end{bmatrix}$$

$$\begin{bmatrix} \mathbf{V}_1 \\ \mathbf{V}_2 \end{bmatrix} = \begin{bmatrix} \mathbf{y}_{11} & \mathbf{y}_{12} \\ \mathbf{y}_{21} & \mathbf{y}_{22} \end{bmatrix}^{-1} \begin{bmatrix} \mathbf{I}_1 \\ \mathbf{I}_2 \end{bmatrix}$$

$$\mathbf{V}_1 = \frac{\begin{vmatrix} \mathbf{I}_1 & \mathbf{y}_{12} \\ \mathbf{I}_2 & \mathbf{y}_{22} \end{vmatrix}}{\begin{vmatrix} \mathbf{y}_{11} & \mathbf{y}_{12} \\ \mathbf{y}_{21} & \mathbf{y}_{22} \end{vmatrix}} = \frac{\mathbf{y}_{22}}{\Delta \mathbf{y}} \mathbf{I}_1 - \frac{\mathbf{y}_{12}}{\Delta \mathbf{y}} \mathbf{I}_2$$

$$\mathbf{V}_2 = \frac{\begin{vmatrix} \mathbf{I}_1 & \mathbf{y}_{12} \\ \mathbf{I}_2 & \mathbf{y}_{22} \end{vmatrix}}{\Delta \mathbf{y}} = \frac{\mathbf{y}_{22}}{\Delta \mathbf{y}} \mathbf{I}_1 - \frac{\mathbf{y}_{12}}{\Delta \mathbf{y}} \mathbf{I}_2$$

Transformation between ...:

Table 17.1 | Transformations between **y**, **z**, **h**, and **t** parameters

	y		z		h		t	
y	y_{11}	y_{12}	$\frac{z_{22}}{\Delta_z}$	$-\frac{z_{12}}{\Delta_z}$	$\frac{1}{h_{11}}$	$-\frac{h_{12}}{h_{11}}$	$\frac{t_{22}}{t_{12}}$	$-\frac{\Delta_t}{t_{12}}$
	y_{21}	y_{22}	$-\frac{z_{21}}{\Delta_z}$	$\frac{z_{11}}{\Delta_z}$	$\frac{h_{21}}{h_{11}}$	$\frac{\Delta_h}{h_{11}}$	$-\frac{1}{t_{12}}$	$\frac{t_{11}}{t_{12}}$
z	$\frac{y_{22}}{\Delta_y}$	$-\frac{y_{12}}{\Delta_y}$	z_{11}	z_{12}	$\frac{\Delta_h}{h_{22}}$	$\frac{h_{12}}{h_{22}}$	$\frac{t_{11}}{t_{21}}$	$\frac{\Delta_t}{t_{21}}$
	$-\frac{y_{21}}{\Delta_y}$	$\frac{y_{11}}{\Delta_y}$	z_{21}	z_{22}	$-\frac{h_{21}}{h_{22}}$	$\frac{1}{h_{22}}$	$\frac{1}{t_{21}}$	$\frac{t_{22}}{t_{21}}$
h	$\frac{1}{y_{11}}$	$-\frac{y_{12}}{y_{11}}$	$\frac{\Delta_z}{z_{22}}$	$\frac{z_{12}}{z_{22}}$	h_{11}	h_{12}	$\frac{t_{12}}{t_{22}}$	$\frac{\Delta_t}{t_{22}}$
	$\frac{y_{21}}{y_{11}}$	$\frac{\Delta_y}{y_{11}}$	$-\frac{z_{21}}{z_{22}}$	$\frac{1}{z_{22}}$	h_{21}	h_{22}	$-\frac{1}{t_{22}}$	$\frac{t_{21}}{t_{22}}$
t	$-\frac{y_{22}}{y_{21}}$	$-\frac{1}{y_{21}}$	$\frac{z_{11}}{z_{21}}$	$\frac{\Delta_z}{z_{21}}$	$-\frac{\Delta_h}{h_{21}}$	$-\frac{h_{11}}{h_{21}}$	t_{11}	t_{12}
	$-\frac{\Delta_y}{y_{21}}$	$-\frac{y_{11}}{y_{21}}$	$\frac{1}{z_{21}}$	$\frac{z_{22}}{z_{21}}$	$-\frac{h_{22}}{h_{21}}$	$-\frac{1}{h_{21}}$	t_{21}	t_{22}

For all parameter sets: $\Delta_p = p_{11}p_{22} - p_{12}p_{21}$.

Reciprocal Two-Port Circuits:

The following relationship exist,

$$\mathbf{z}_{12} = \mathbf{z}_{21},$$

$$\mathbf{y}_{12} = \mathbf{y}_{21},$$

$$\mathbf{a}_{11}\mathbf{a}_{22} - \mathbf{a}_{12}\mathbf{a}_{21} = \Delta\mathbf{a} = 1,$$

$$\mathbf{b}_{11}\mathbf{b}_{22} - \mathbf{b}_{12}\mathbf{b}_{21} = \Delta\mathbf{b} = 1,$$

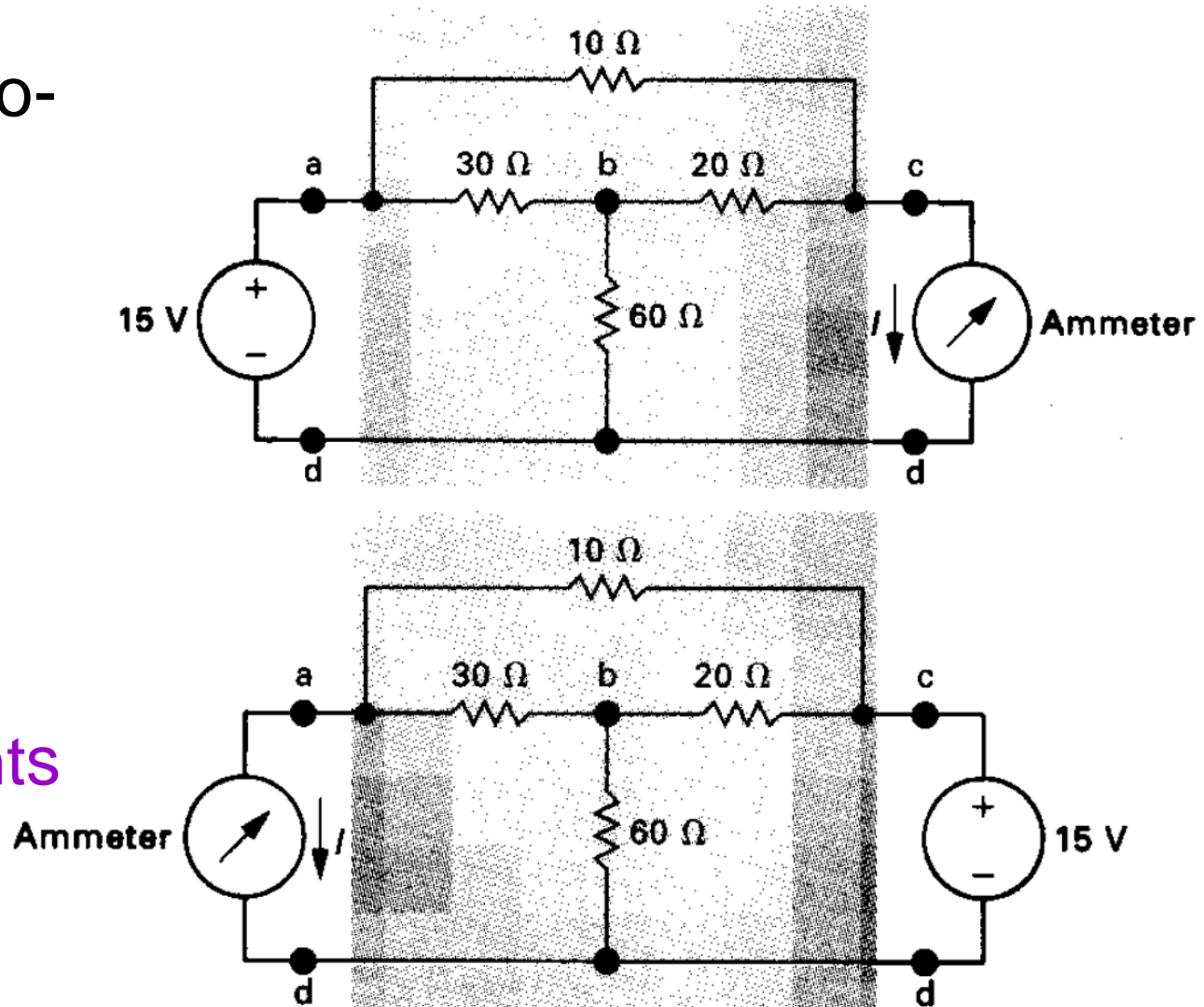
$$\mathbf{h}_{12} = -\mathbf{h}_{21},$$

$$\mathbf{g}_{12} = -\mathbf{g}_{21}$$

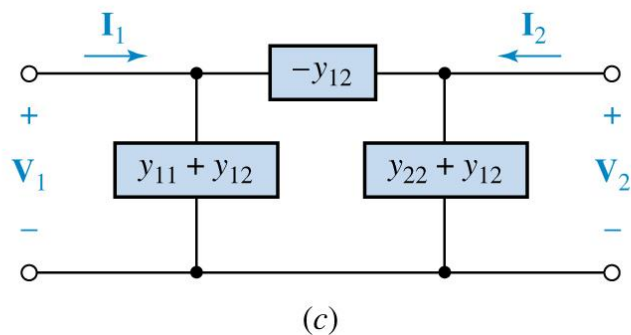
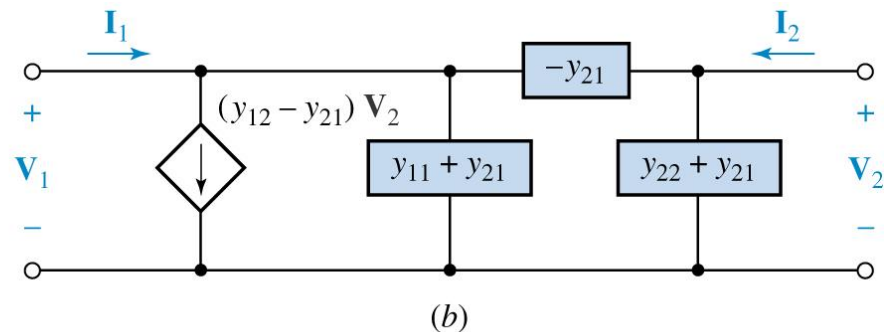
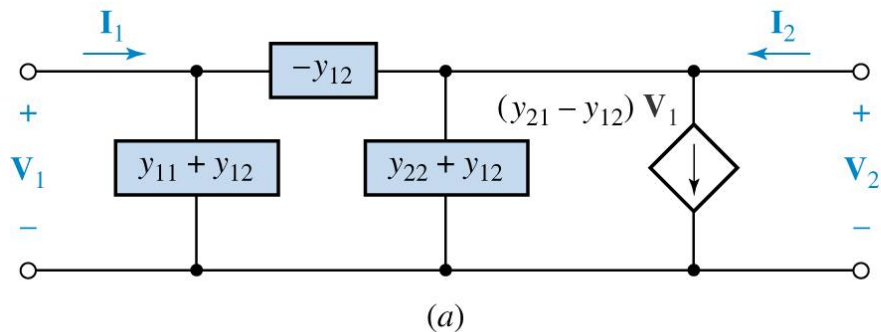
Reciprocal Two-Port Circuits:

A reciprocal two-port circuit:

A reciprocal two-port circuit **is symmetric** if its ports can be **interchanged** without disturbing the values of the terminal currents and voltages.

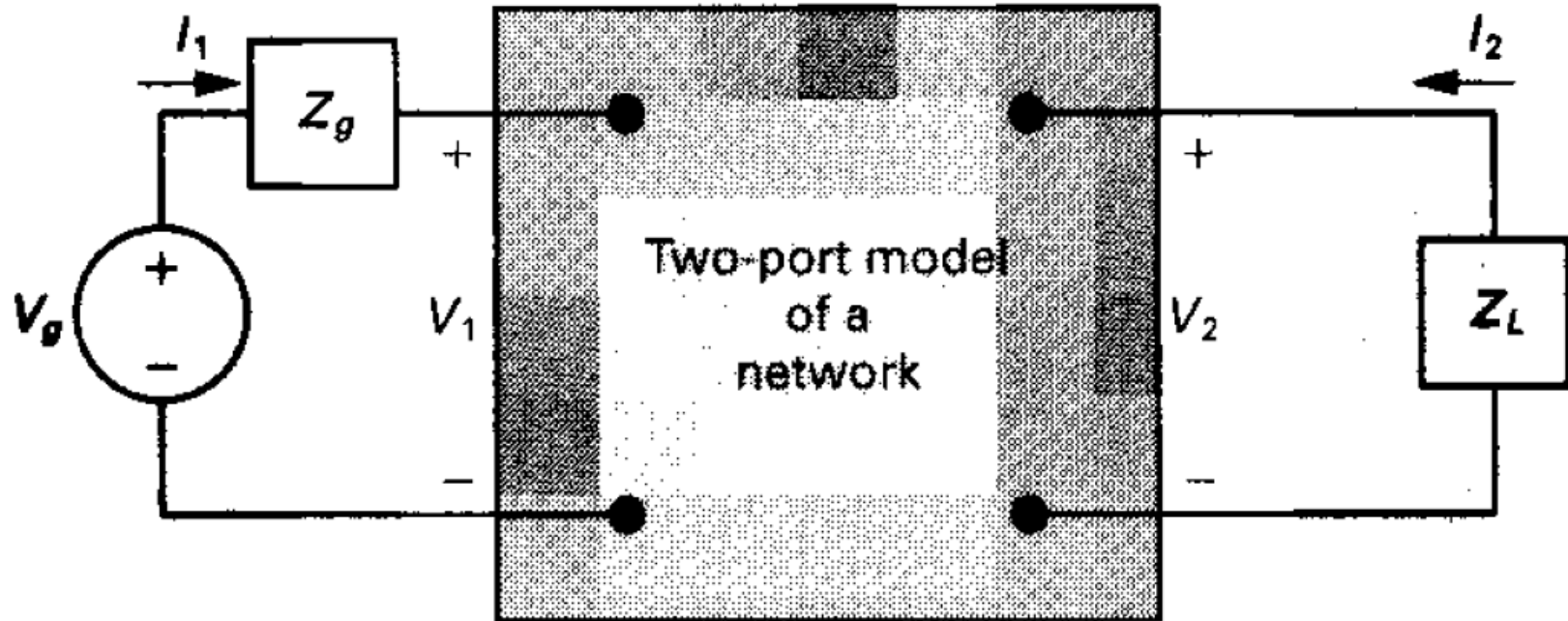


Some Equivalent Networks:



(a, b) Two-ports which are equivalent to any general linear two-port. The dependent source in part a depends on \mathbf{V}_1 , and that in part b depends on \mathbf{V}_2 . (c) An equivalent for a bilateral network.

Analysis of the Terminated ...:



Six characteristics of the terminated two-port circuits define its terminal behavior:

Analysis of the Terminated ...:

Six characteristics of the terminated two-port circuits define its terminal behavior:

1. The input impedance

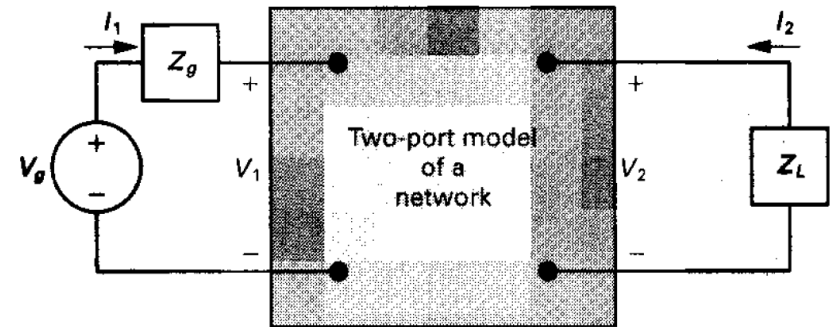
2. the output current

3. the Thevenin voltage and impedance

4. The current gain

5. The voltage gain $\frac{V_2}{V_1}$

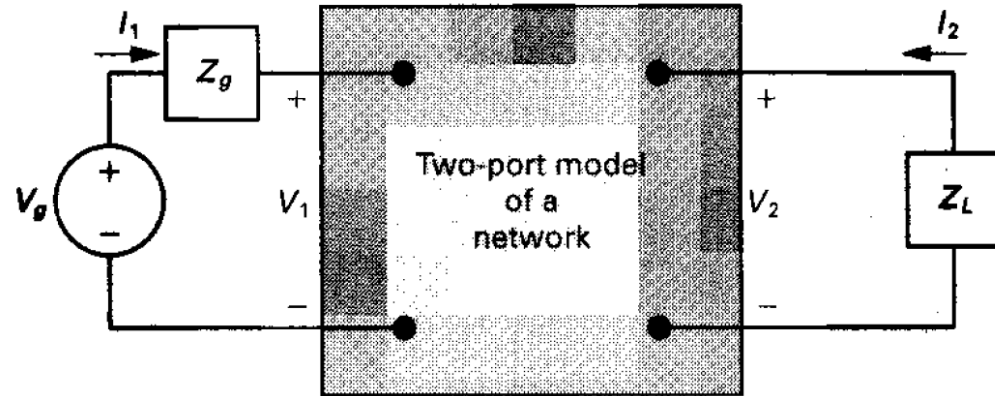
6. The voltage gain $\frac{V_2}{V_g}$



Analysis of the Terminated ...:

Six characteristics in terms of the z-parameters:

The input impedance:
(the impedance seen looking into port 1)



$$V_1 = z_{11}I_1 + z_{12}I_2 \quad \dots *$$

$$V_2 = z_{21}I_1 + z_{22}I_2 \quad \dots **$$

$$V_1 = V_g - I_1 Z_g \quad \dots ***$$

$$V_2 = -I_2 Z_L \quad \dots ****$$

$$Z_{in} = \frac{V_1}{I_1}$$

$$V_2 = -I_2 Z_L = z_{21}I_1 + z_{22}I_2$$

$$\Rightarrow I_2 = \frac{-z_{21}I_1}{Z_L + z_{22}}$$

$$\text{sub } I_2 \text{ in } *$$

Analysis of the Terminated ...:

z PARAMETERS

$$Z_{\text{in}} = z_{11} - \frac{z_{12}z_{21}}{z_{22} + Z_L}$$

$$I_2 = \frac{-z_{21}V_g}{(z_{11} + Z_g)(z_{22} + Z_L) - z_{12}z_{21}}$$

$$V_{\text{Th}} = \frac{z_{21}}{z_{11} + Z_g} V_g$$

$$Z_{\text{Th}} = z_{22} - \frac{z_{12}z_{21}}{z_{11} + Z_g}$$

$$\frac{I_2}{I_1} = \frac{-z_{21}}{z_{22} + Z_L}$$

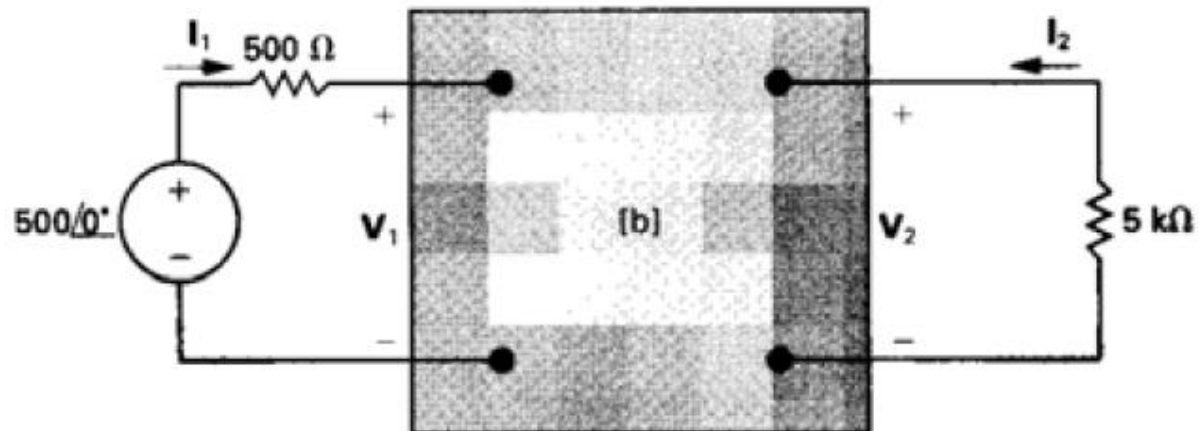
$$\frac{V_2}{V_1} = \frac{z_{21}Z_L}{z_{11}Z_L + \Delta z}$$

$$\frac{V_2}{V_g} = \frac{z_{21}Z_L}{(z_{11} + Z_g)(z_{22} + Z_L) - z_{12}z_{21}}$$

Example:

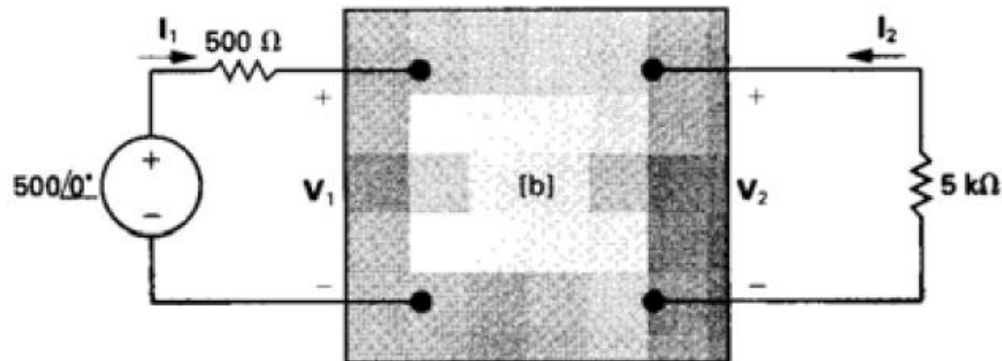
The two-port circuit shown in Fig. is described in terms of its b parameters, the values of which are

$$b_{11} = -20, \quad b_{12} = -3000 \, \Omega, \quad b_{21} = -2 \, \text{mS}, \quad \text{and} \quad b_{22} = -0.2.$$



- Find the phasor voltage V_2 .
- Find the average power delivered to the $5 \, \text{k}\Omega$ load.
- Find the average power delivered to the input port.
- Find the load impedance for maximum average power transfer.
- Find the maximum average power delivered to the load in (d).

Example:



- Find the phasor voltage V_2 .
- Find the average power delivered to the $5\text{ k}\Omega$ load.
- Find the average power delivered to the input port.
- Find the load impedance for maximum average power transfer.
- Find the maximum average power delivered to the load in (d).

b PARAMETERS

$$Z_{in} = \frac{b_{22}Z_L + b_{12}}{b_{21}Z_L + b_{11}}$$

$$I_2 = \frac{-V_g \Delta b}{b_{11}Z_g + b_{21}Z_g Z_L + b_{22}Z_L + b_{12}}$$

$$V_{Th} = \frac{V_g \Delta b}{b_{22} + b_{21}Z_g}$$

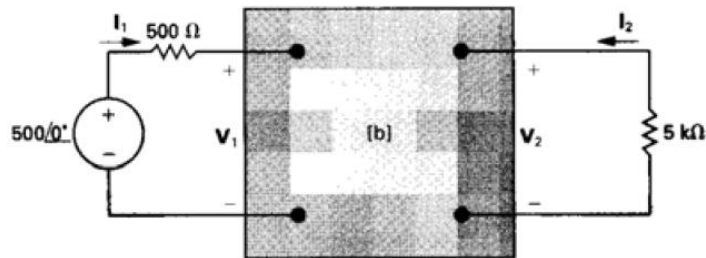
$$Z_{Th} = \frac{b_{11}Z_g + b_{12}}{b_{21}Z_g + b_{22}}$$

$$\frac{I_2}{I_1} = \frac{-\Delta b}{b_{11} + b_{21}Z_L}$$

$$\frac{V_2}{V_1} = \frac{\Delta b Z_L}{b_{12} + b_{22}Z_L}$$

$$\frac{V_2}{V_g} = \frac{\Delta b Z_L}{b_{12} + b_{11}Z_g + b_{22}Z_L + b_{21}Z_g Z_L}$$

Example:



$$\begin{aligned}\frac{V_2}{V_g} &= \frac{\Delta b Z_L}{b_{12} + b_{11}Z_g + b_{22}Z_L + b_{21}Z_g Z_L} \\ &= \frac{(-2)(5000)}{-3000 + (-20)500 + (-0.2)5000 + [-2 \times 10^{-3}(500)(5000)]} \\ &= \frac{10}{19}\end{aligned}$$

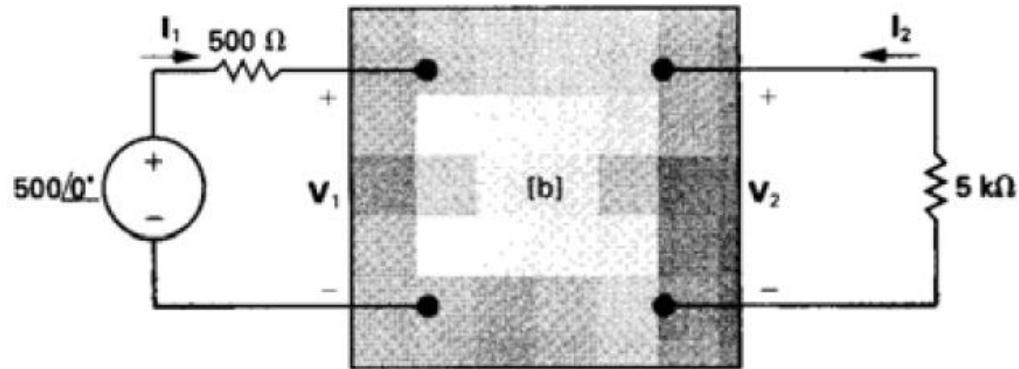
Then,

$$V_2 = \left(\frac{10}{19}\right) 500 = 263.16\angle 0^\circ \text{ V.}$$

b) The average power delivered to the $5000\ \Omega$ load is

$$P_2 = \frac{263.16^2}{2(5000)} = 6.93 \text{ W.}$$

Example:



$$\begin{aligned}
 Z_{in} &= \frac{b_{22}Z_L + b_{12}}{b_{21}Z_L + b_{11}} \\
 &= \frac{(-0.2)(5000) - 3000}{-2 \times 10^{-3}(5000) - 20} \\
 &= \frac{400}{3} = 133.33 \, \Omega.
 \end{aligned}$$

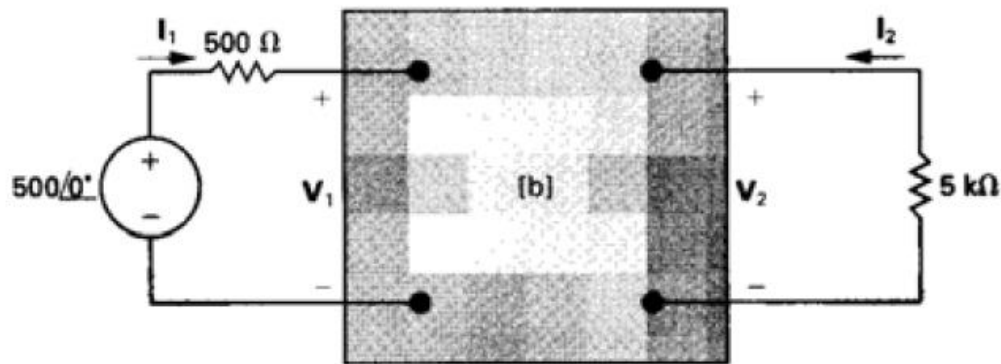
Now I_1 follows directly:

$$I_1 = \frac{500}{500 + 133.33} = 789.47 \, \text{mA}.$$

The average power delivered to the input port is

$$P_1 = \frac{0.78947^2}{2}(133.33) = 41.55 \, \text{W}.$$

Example:

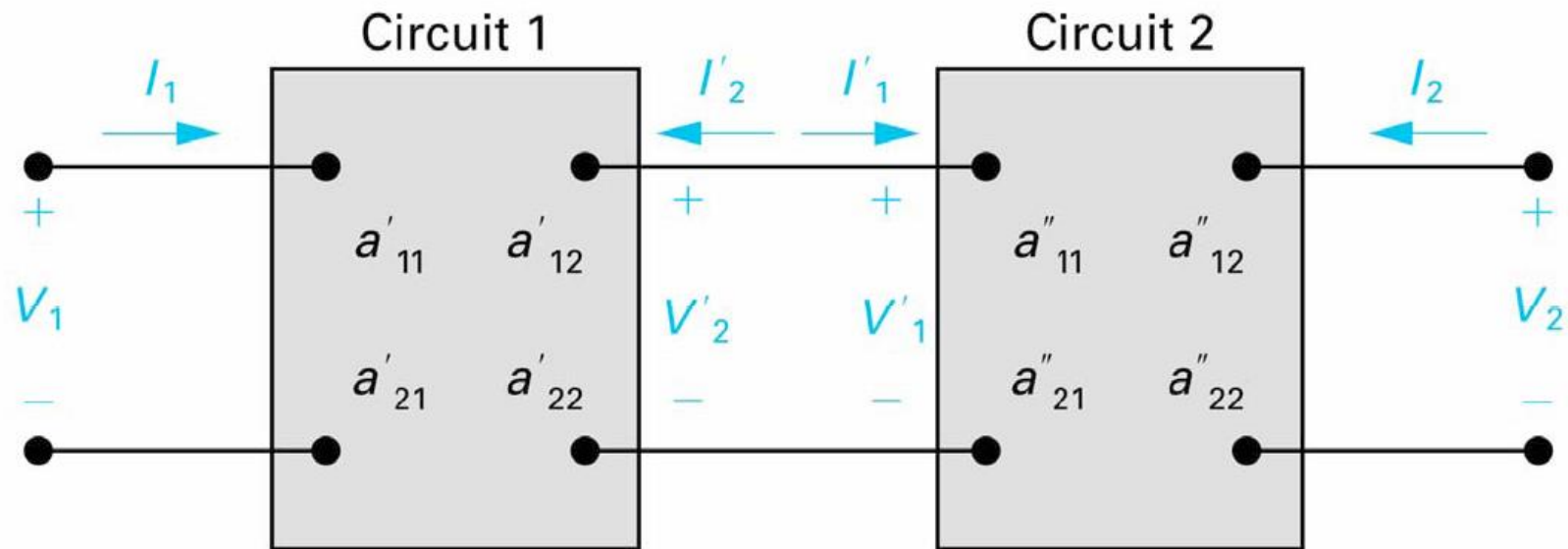


b) The average power delivered to the $5000\ \Omega$ load is

$$P_2 = \frac{263.16^2}{2(5000)} = 6.93\text{ W.}$$

Interconnected Two-port Circuits: Page 55

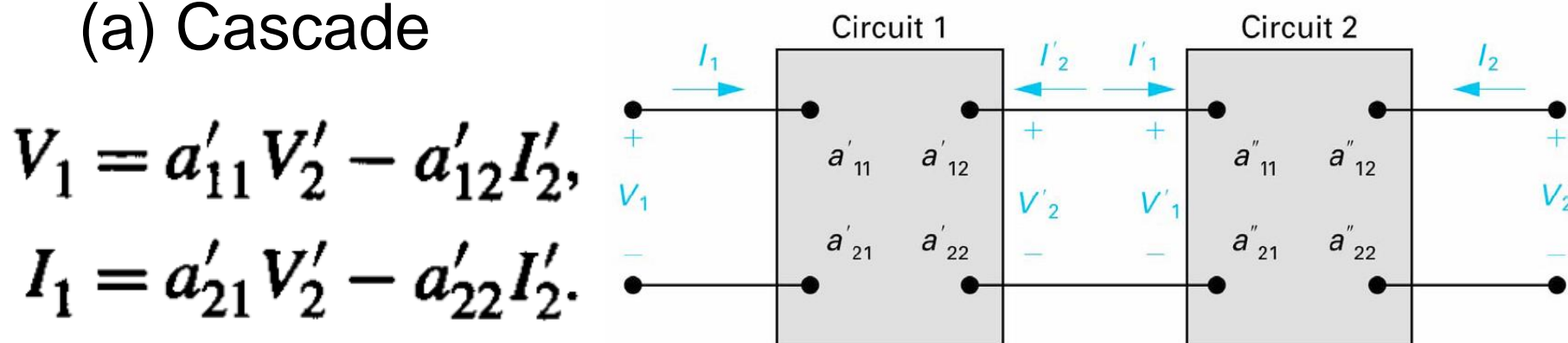
The five basic interconnections of two-port circuit:
(a) Cascade



$$V_1 = a'_{11} V'_2 - a'_{12} I'_2,$$

$$I_1 = a'_{21} V'_2 - a'_{22} I'_2.$$

(a) Cascade



$$V_1 = a'_{11} V'_2 - a'_{12} I'_2,$$

$$I_1 = a'_{21} V'_2 - a'_{22} I'_2.$$

$$V_1 = a'_{11} V'_1 + a'_{12} I'_1,$$

$$I_1 = a'_{21} V'_1 + a'_{22} I'_1.$$

$$V'_1 = a''_{11} V_2 - a''_{12} I_2,$$

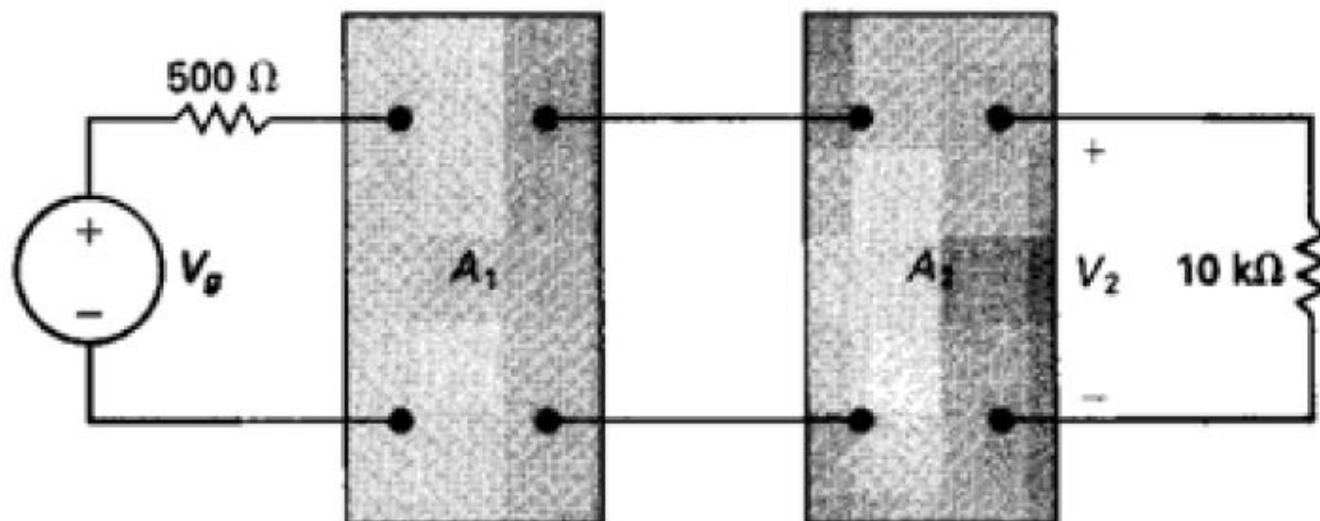
$$I'_1 = a''_{21} V_2 - a''_{22} I_2.$$

$$V_1 = (a'_{11} a''_{11} + a'_{12} a''_{21}) V_2 - (a'_{11} a''_{12} + a'_{12} a''_{22}) I_2,$$

$$I_1 = (a'_{21} a''_{11} + a'_{22} a''_{21}) V_2 - (a'_{21} a''_{12} + a'_{22} a''_{22}) I_2.$$

Example:

Two identical amplifiers are connected in cascade, as shown in Fig. 18.11. Each amplifier is described in terms of its h parameters. The values are $h_{11} = 1000 \Omega$, $h_{12} = 0.0015$, $h_{21} = 100$, and $h_{22} = 100 \mu\text{S}$. Find the voltage gain V_2/V_g .



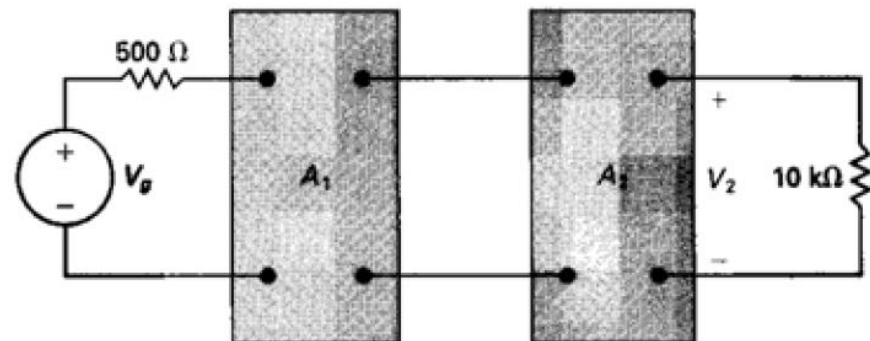
Example:

$$a'_{11} = \frac{-\Delta h}{h_{21}} = \frac{+0.05}{100} = 5 \times 10^{-4},$$

$$a'_{12} = \frac{-h_{11}}{h_{21}} = \frac{-1000}{100} = -10 \, \Omega,$$

$$a'_{21} = \frac{-h_{22}}{h_{21}} = \frac{-100 \times 10^{-6}}{100} = -10^{-6} \, \text{S},$$

$$a'_{22} = \frac{-1}{h_{21}} = \frac{-1}{100} = -10^{-2}.$$



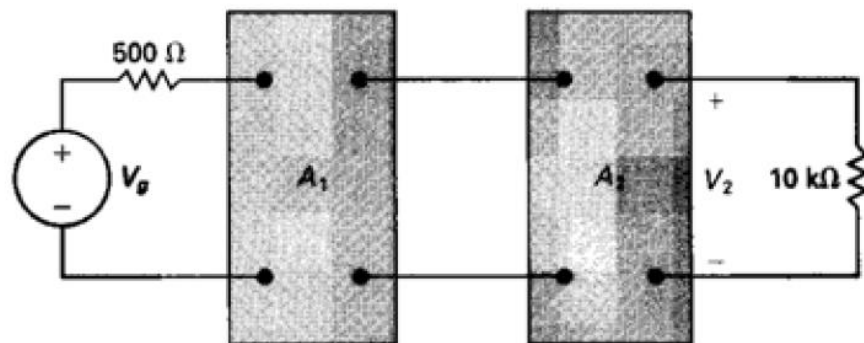
$$\begin{aligned} a_{11} &= a'_{11}a'_{11} + a'_{12}a'_{21} \\ &= 25 \times 10^{-8} + (-10)(-10^{-6}) = 10.25 \times 10^{-6}, \end{aligned}$$

$$\begin{aligned} a_{12} &= a'_{11}a'_{12} + a'_{12}a'_{22} \\ &= (5 \times 10^{-4})(-10) + (-10)(-10^{-2}) = 0.095 \, \Omega, \end{aligned}$$

$$\begin{aligned} a_{21} &= a'_{21}a'_{11} + a'_{22}a'_{21} \\ &= (-10^{-6})(5 \times 10^{-4}) + (-0.01)(-10^{-6}) \\ &= 0.0095 \times 10^{-6} \, \text{S}, \end{aligned}$$

$$\begin{aligned} a_{22} &= a'_{21}a'_{12} + a'_{22}a'_{22} \\ &= (-10^{-6})(-10) + (-10^{-2})^2 = 1.1 \times 10^{-4}. \end{aligned}$$

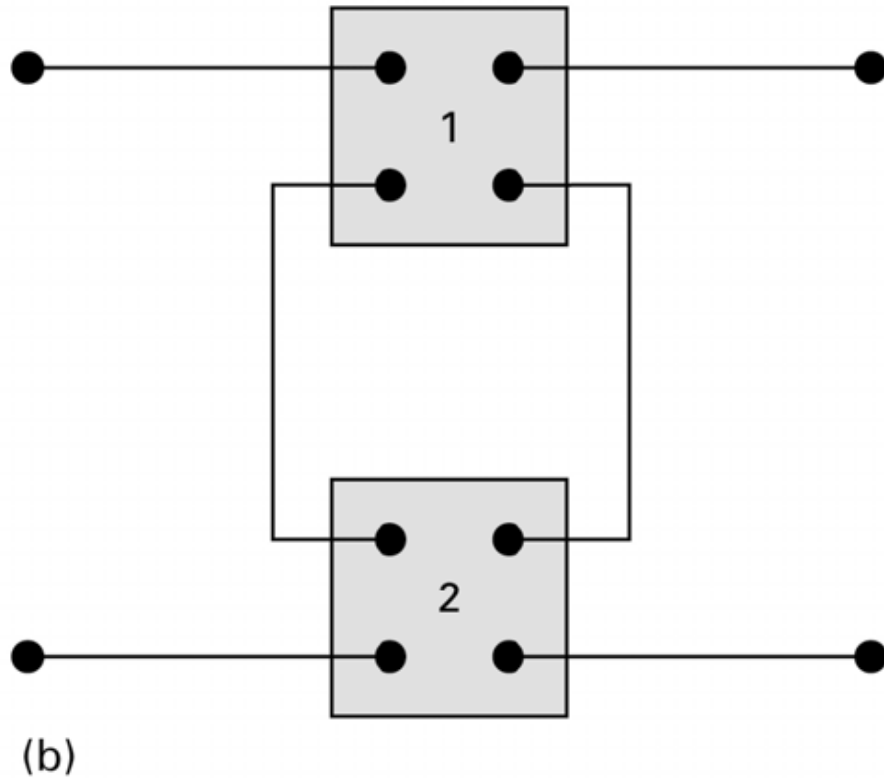
Example:



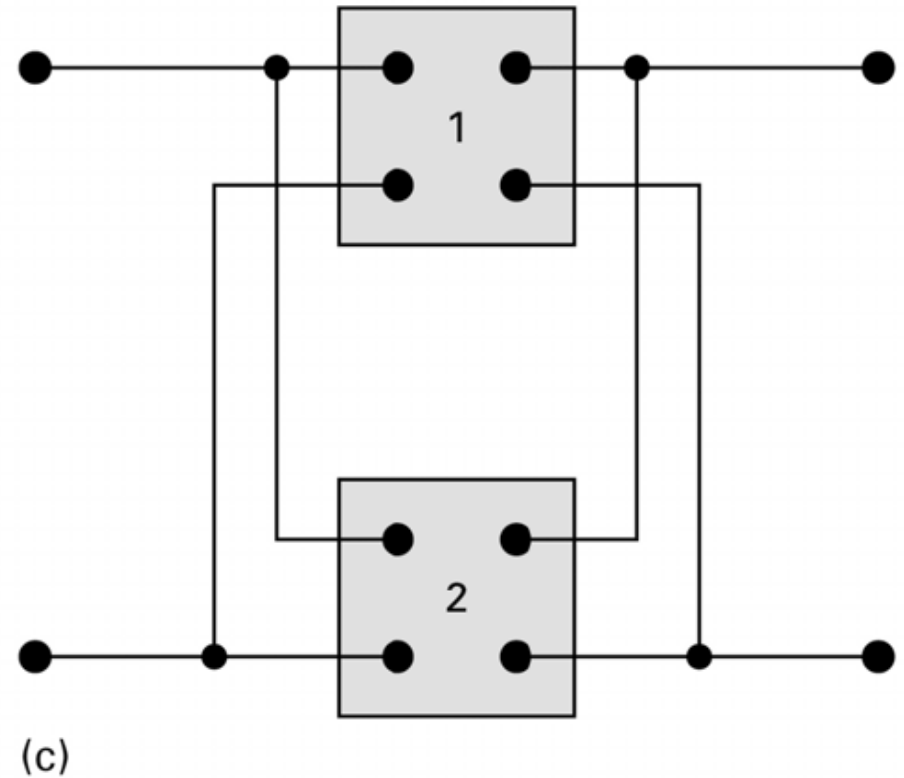
$$\begin{aligned}
 \frac{V_2}{V_g} &= \frac{Z_L}{(a_{11} + a_{21}Z_g)Z_L + a_{12} + a_{22}Z_g} \\
 &= \frac{10^4}{[10.25 \times 10^{-6} + 0.0095 \times 10^{-6}(500)]10^4 + 0.095 + 1.1 \times 10^{-4}(500)} \\
 &= \frac{10^4}{0.15 + 0.095 + 0.055} = \frac{10^5}{3} = 33,333.33.
 \end{aligned}$$

Interconnected Two-port Circuits: Page 60

(b) Series

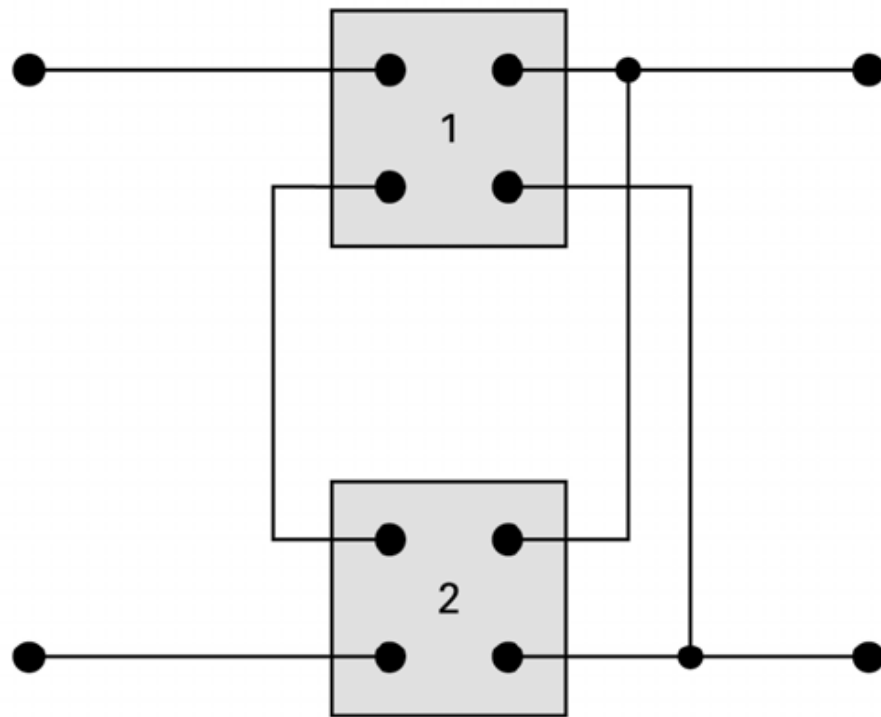


(c) Parallel



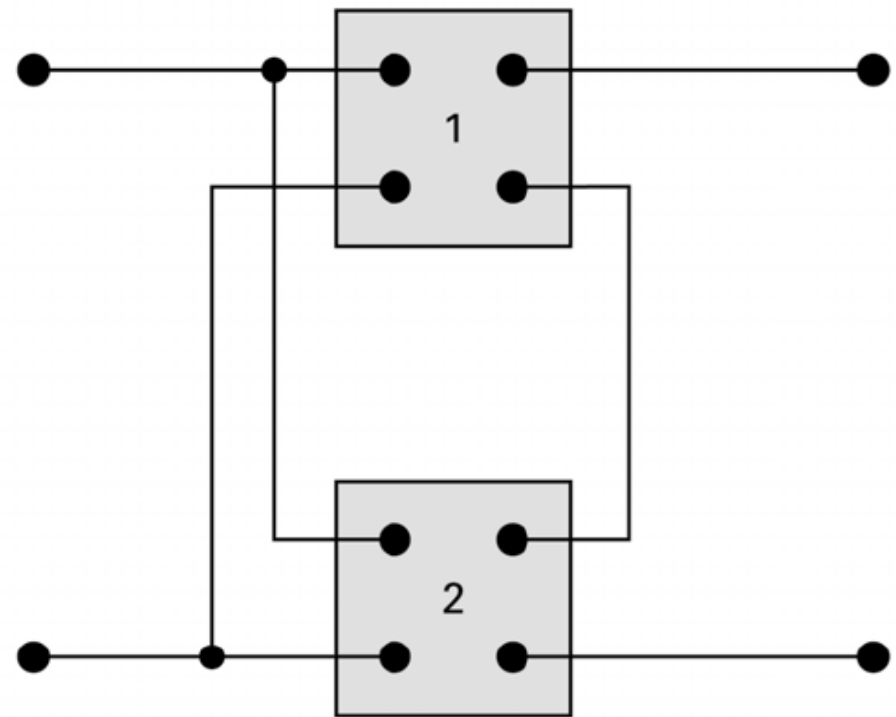
Interconnected Two-port Circuits: Page 61

(d) Series- Parallel



(d)

(e) Parallel- Series



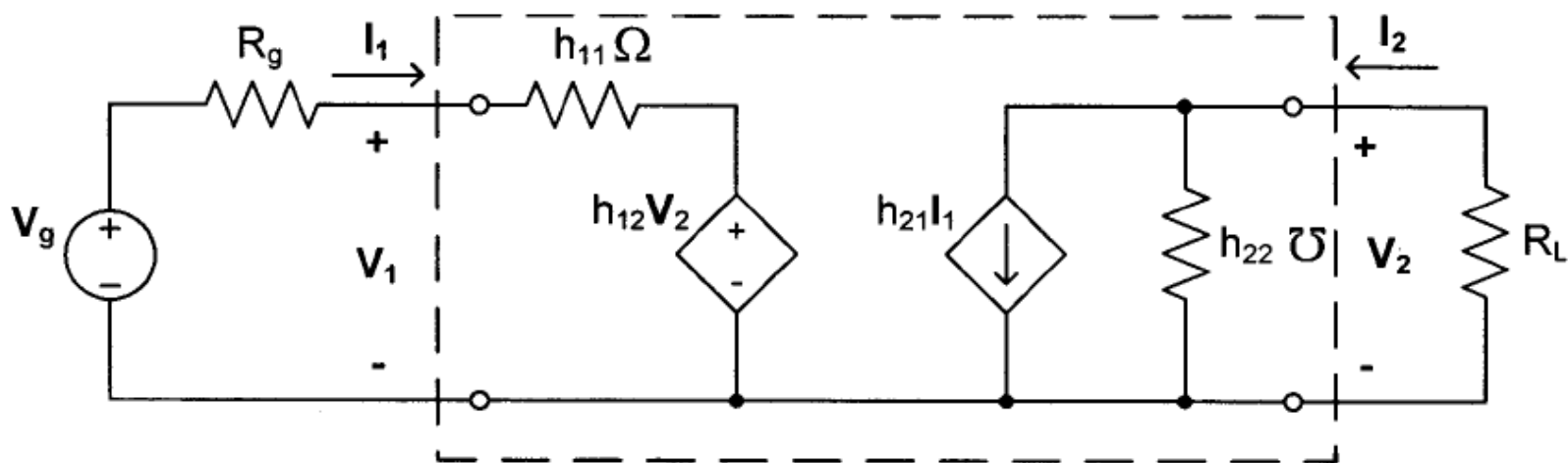
(e)

Example: Final 2/47

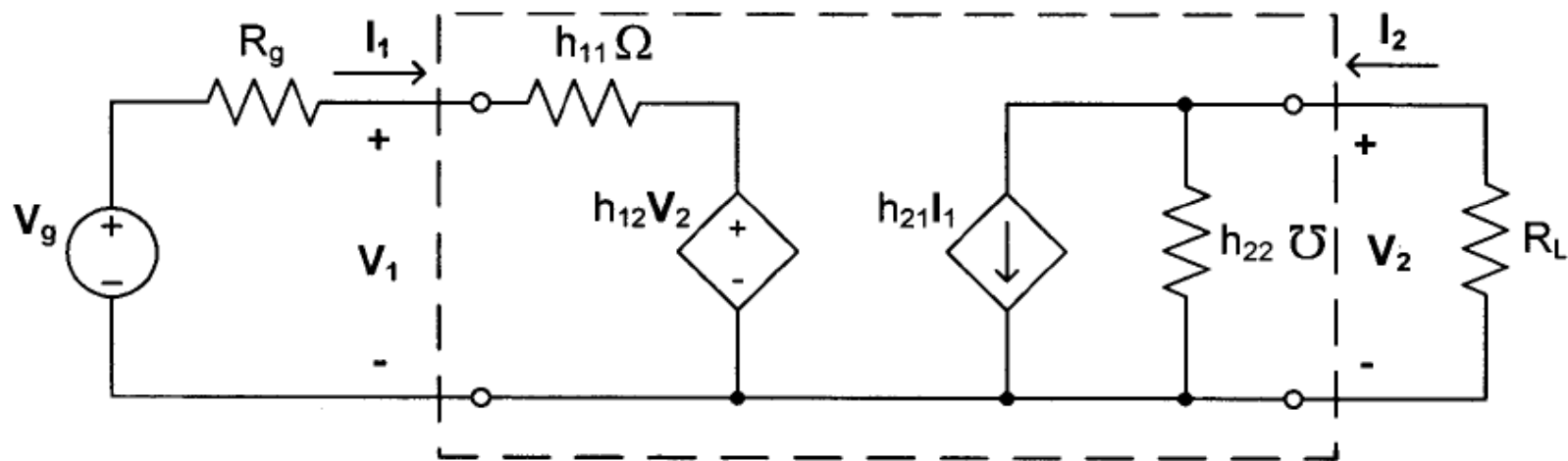
5.] จากระบบ (an equivalent circuit satisfied by the h-parameter equations) ตามรูป จงหา (20 คะแนน)

5.1.) The current gain, $A_i = \frac{I_2}{I_1}$

5.2.) The voltage gain, $A_v = \frac{V_2}{V_g}$



Example: Final 2/47



from $V_1 = h_{11} I_1 + h_{12} V_2 \dots (1)$

$$I_2 = h_{21} I_1 + h_{22} V_2 \dots (2)$$

$$V_2 = -R_L I_2 \dots (3)$$

$$V_1 = V_g - I_1 R_g \dots (4)$$

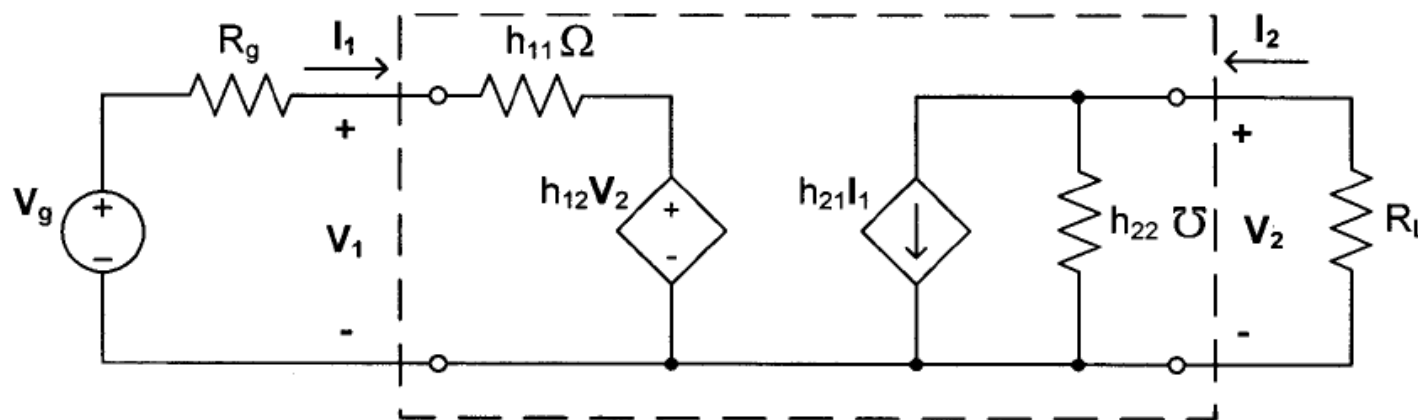
[5.1] into V_2 in (3) into (2);

$$I_2 = h_{21} I_1 + h_{22} (-R_L I_2)$$

$$(1 + h_{22} R_L) I_2 = h_{21} I_1$$

$$\therefore A_i = \frac{I_2}{I_1} = \frac{h_{21}}{1 + h_{22} R_L} \dots \underline{\underline{\text{Ans}}}$$

Example: Final 2/47



[5.2] من معادلتين (1) و (4) ;

$$V_g - I_1 R_g = h_{11} I_1 + h_{12} V_2$$

$$V_g = (h_{11} + R_g) I_1 + h_{12} V_2 \dots (5)$$

من معادلتين (2) و (3) ;

$$I_2 = -\frac{V_2}{R_L} = h_{21} I_1 + h_{22} V_2$$

$$\therefore I_1 = \left[\frac{-1}{h_{21} R_L} - \frac{h_{22}}{h_{21}} \right] V_2 \dots (6)$$

من معادلتين (5) و (6) نحل معادلتين (5) ;

$$V_g = (h_{11} + R_g) \left[\frac{-1}{h_{21} R_L} - \frac{h_{22}}{h_{21}} \right] V_2 + h_{12} V_2$$

$$\therefore \frac{V_g}{V_2} = \frac{-h_{11} - R_g - h_{11} h_{22} R_L - R_g h_{22} R_L + h_{22} h_{21} R_L}{h_{21} R_L}$$

$$\therefore \frac{V_2}{V_g} = \frac{h_{21} R_L}{-h_{11} - R_g - h_{11} h_{22} R_L - R_g h_{22} R_L + h_{22} h_{21} R_L}$$

Example: Final 2/46

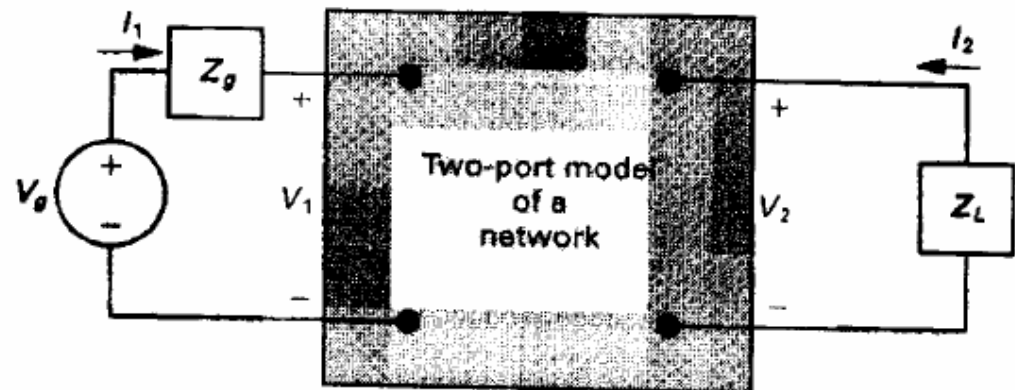
5.] จากวงจร the two-port network ตามรูป จงแสดงให้เห็นว่า $V_{Th} = \frac{-y_{21}V_g}{y_{22} + \Delta y Z_g}$ และ

$$Z_{Th} = \frac{1 + y_{11}Z_g}{y_{22} + \Delta y Z_g} \quad (20 \text{ คะแนน})$$

Note: $I_1 = y_{11}V_1 + y_{12}V_2$,

$$I_2 = y_{21}V_1 + y_{22}V_2 \text{ และ}$$

$$\Delta y = y_{11}y_{22} - y_{12}y_{21}$$

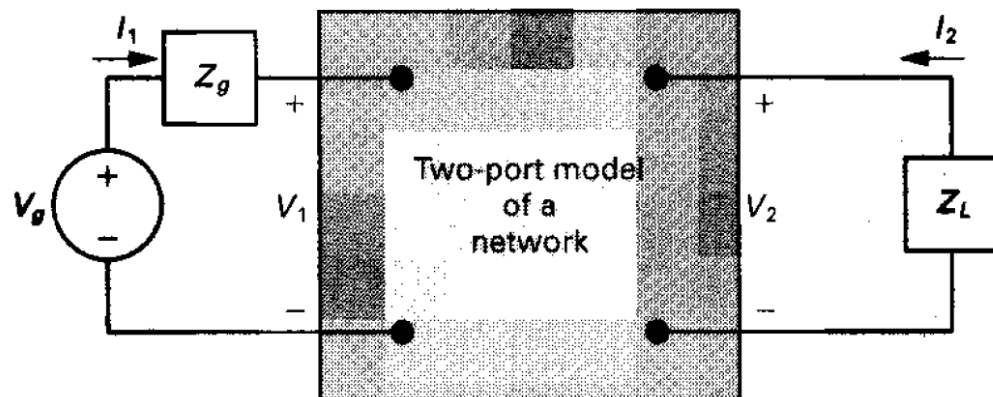


Example: Final 2/46

from (1) $I_1 = y_{11} V_1 + y_{12} V_2 \quad \dots [1]$

$I_2 = y_{21} V_1 + y_{22} V_2 \quad \dots [2]$

$V_1 = V_s - I_1 z_g \quad \dots [3]$



[1] ; $0 = y_{11} V_1 + y_{12} V_2 - I_1$

[2] ; $0 = y_{21} V_1 + y_{22} V_2 \quad ; I_2 = 0$

[3] ; $V_s = V_1 + I_1 z_g$

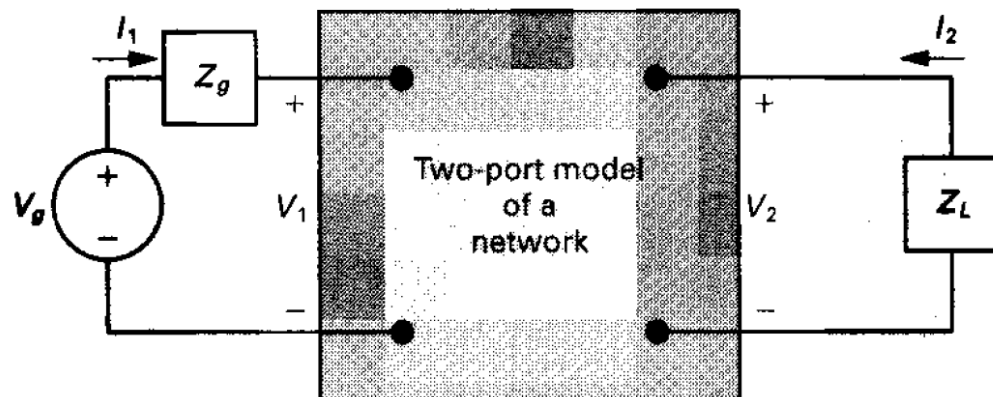
$$\begin{bmatrix} 0 \\ 0 \\ V_s \end{bmatrix} = \begin{bmatrix} y_{11} & y_{12} & -1 \\ y_{21} & y_{22} & 0 \\ 1 & 0 & z_g \end{bmatrix} \begin{bmatrix} V_1 \\ V_2 \\ I_1 \end{bmatrix}$$

Example: Final 2/46

$$\therefore V_2 = \frac{\begin{vmatrix} y_{11} & 0 & -1 \\ y_{21} & 0 & 0 \\ 1 & V_g & z_g \end{vmatrix}}{\begin{vmatrix} y_{11} & y_{12} & -1 \\ y_{21} & y_{22} & 0 \\ 1 & 0 & z_g \end{vmatrix}}$$

$$= \frac{-y_{21} V_g}{+y_{22} + z_g (y_{11} y_{22} - y_{12} y_{21})}$$

$$= \frac{-y_{21} V_g}{y_{22} + \Delta y z_g} \quad \text{Q.E.D.}$$



$$\text{Find } z_{in} = \left. \frac{V_1}{I_1} \right|_{V_2=0}$$

from [3]; $V_1 = -I_1 z_g \quad \dots [4]$

substituting \$V_2\$ from [2]; $I_1 = y_{11} (-I_1 z_g) + y_{12} V_2$

$$(1 + y_{11} z_g) I_1 = y_{12} V_2$$

$$I_1 = \left(\frac{y_{12}}{1 + y_{11} z_g} \right) V_2$$

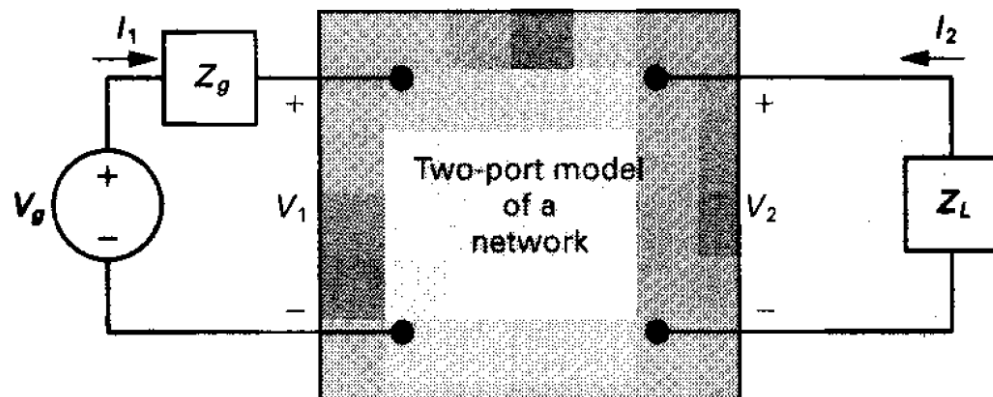
Example: Final 2/46

$$\text{when } V_1 = -I_1 Z_g \text{ as in (2);}$$

$$I_2 = y_{21} (-I_1 Z_g) + y_{22} V_2$$

$$= y_{21} \left(\frac{-y_{12}}{1+y_{11}Z_g} \right) Z_g + y_{22} V_2$$

$$= \left[\frac{-y_{12}y_{21}Z_g}{1+y_{11}Z_g} + y_{22} \right] V_2$$



$$\therefore \frac{V_L}{I_2} = \frac{1+y_{11}Z_g}{-y_{12}y_{21}Z_g + y_{22}(1+y_{11}Z_g)}$$

$$= \frac{1+y_{11}Z_g}{y_{22} + y_{11}y_{22}Z_g - y_{12}y_{21}Z_g}$$

$$= \frac{1+y_{11}Z_g}{y_{22} + \Delta y Z_g} \quad \text{Q.E.D.}$$

Reference:

•W.H. Hayt, Jr., J.E. Kemmerly, S.M. Durbin, Engineering Circuit Analysis, Sixth Edition.
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•James W. Nilsson, Susan A. Riedel, “Electric Circuits” Sixth edition, Addison Wesley, 2001