

## Amplificadores de Potencia

( $P_o > 500\text{mW}$ )

- ❖ Amplificadores lineales

- ✓ Clase A (360°)
- ✓ Clase B (180°)
- ✓ Clase AB (<360° y >180°)

- ❖ Amplificadores clase C (< 180°)

- ❖ Amplificadores por commutación

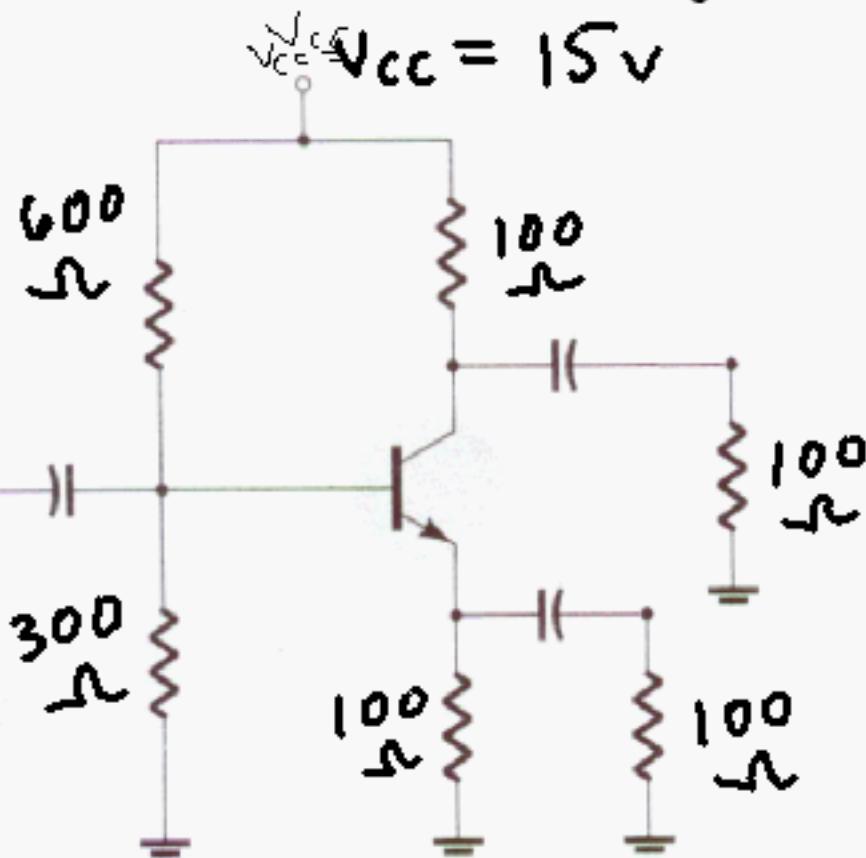
- ✓ Clase D
- ✓ Clase E
- ✓ Clase F
- ✓ Clase S

## Amplificadores lineales

### Amplificador Clase A

- Conduce sobre los 360°
- Alta disipación de potencia
- Potencia de salida limitada
- Aplicación principal en etapas de baja potencia
- Eficiencia < 50%

Recta de carga de CA



$$\beta R_E \geq 10 R_L \checkmark$$

$$V_B = \frac{30V}{900} (1.1) \quad \text{BRE} \geq 10 R_L$$

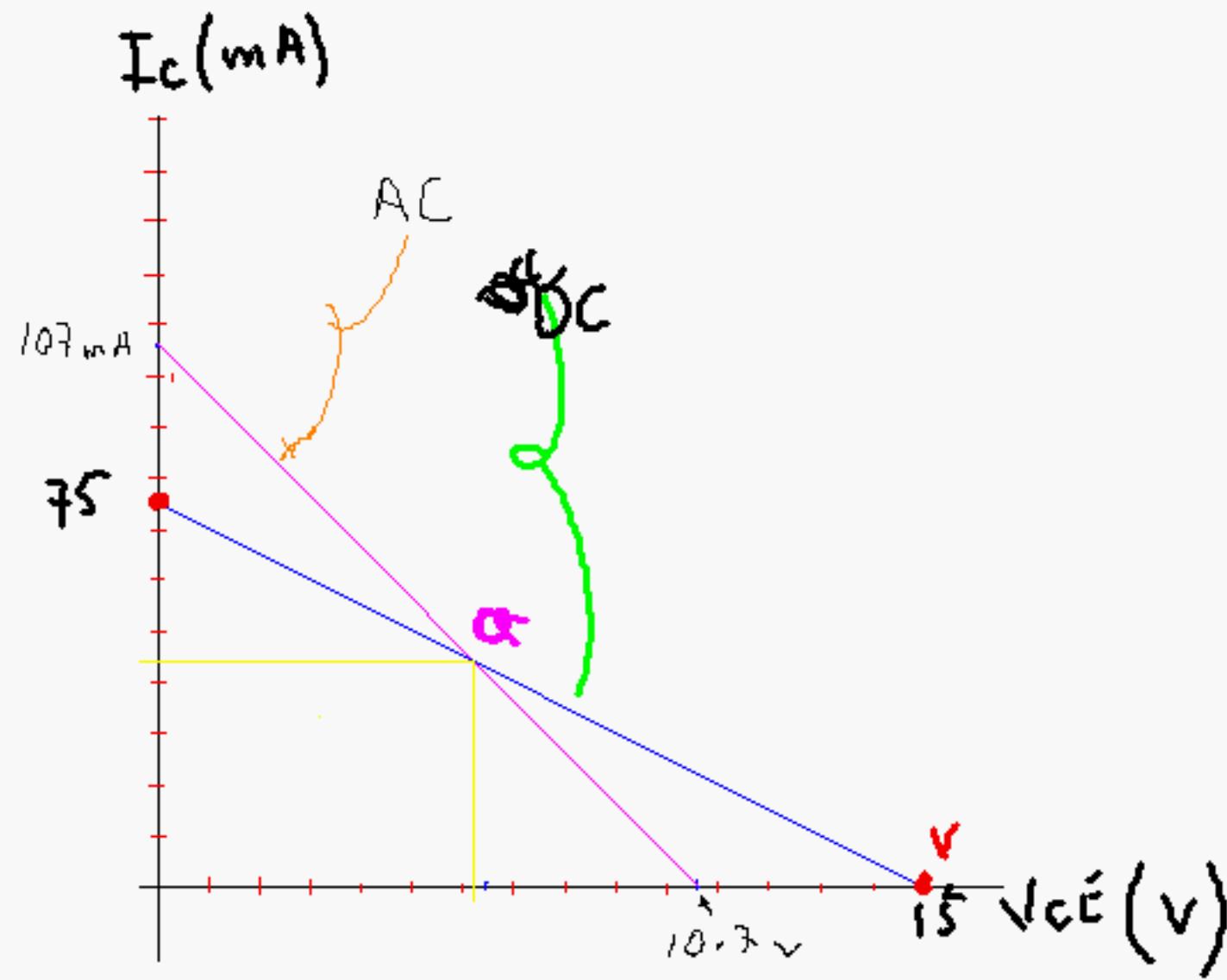
$$V_B = 5V$$

$$I_C \approx I_E = \frac{5V - 0.7}{100}$$

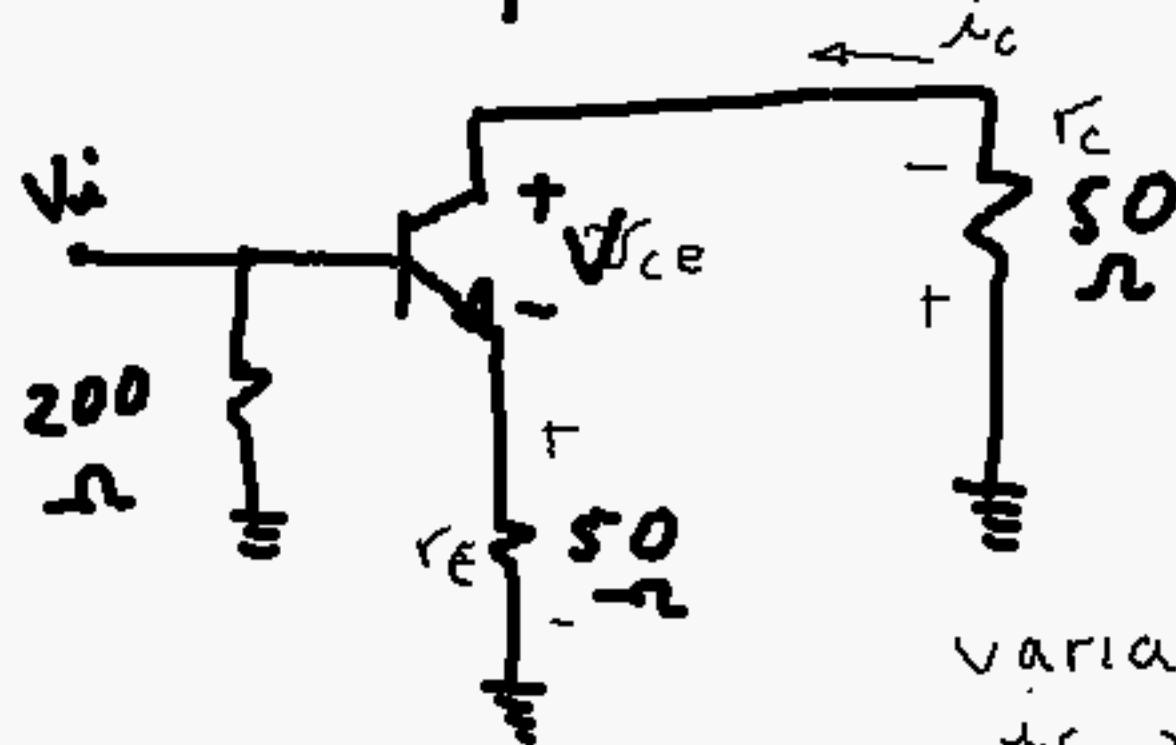
$$I_{CA} \approx 43mA$$

$$V_{CEA} \approx N_{CE} 43mA (200\Omega)$$

$$V_{CEA} \approx 6.4V$$



# Modelo equivalente



$$V_{CE} = i_C (r_E + r_C) = 0$$

$$i_C = - \frac{V_{CE}}{r_E + r_C}$$

variaciões de  
iC y VCE

$$i_C = I_C - I_{CQ}$$

$$V_{CE} = V_{CE} - V_{CEQ}$$

$$I_C - I_{CQ} = - \frac{V_{CE} - V_{CEQ}}{r_E + r_C}$$

despejando  $I_c$

$$I_c = -\frac{V_{CE}}{r_E + r_c} + \frac{V_{CEQ}}{r_E + r_c} + I_{CQ}$$

para  $I_c = 0$

$$\begin{aligned} V_{CE \text{ corte}} &= V_{CEQ} + I_{CQ}(r_E + r_c) \\ &= 6.4 + 43 \text{mA} (100) \\ &= 10.7 \text{v} \end{aligned}$$

Para  $V_{CE} = 0$

$$I_{C \text{ sat}} = \frac{V_{CEQ}}{r_E + r_c} + I_{CQ} = \frac{6.4}{100} + 43 \text{mA}$$

$$I_{C \text{ sat}} = 107 \text{mA}$$

$$I_{CSAT} = 2 I_{CQ}$$

$$V_{CEcorte} = 2 V_{CEQ} \dots A$$

considerando que

$$V_{CEcorte} = V_{CEQ} + I_{CQ}(r_E + r_C) \dots B$$

Sustituyendo B en B

$$2 V_{CEQ} = V_{CEQ} + I_{CQ}(r_E + r_C)$$

$$r_E + r_C = \frac{V_{CEQ}}{I_{CQ}}$$

Maxima potencia de salida ( $P_o$ )

$$P_o(\text{MAX}) = V_{\text{rms}} I_{\text{rms}} = \frac{V_{\text{CEQ}}}{\sqrt{2}} \frac{I_{\text{CQ}}}{\sqrt{2}}$$

$$P_o(\text{MAX}) = \frac{1}{2} V_{\text{CEQ}} I_{\text{CQ}}$$

Para el ejem.

$$P_o = 137.6 \text{ mW}$$

Dissipación de potencia ( $P_D$ )

$$P_D = V_{\text{CEQ}} I_{\text{CQ}}$$

Para el ejemplo

$$P_o(\text{MAX}) = \frac{1}{2} P_D$$

$$P_D = 275 \text{ mW}$$

## Eficiencia de salida ( $\eta$ )

Es la relación entre la potencia de salida de RF y la potencia de entrada de DC que se le proporciona al circuito colector-emisor.

$$\eta = \frac{P_o}{P_{DC}} \times 100$$

donde:  $P_{DC} = V_{CC} I_{CQ}$

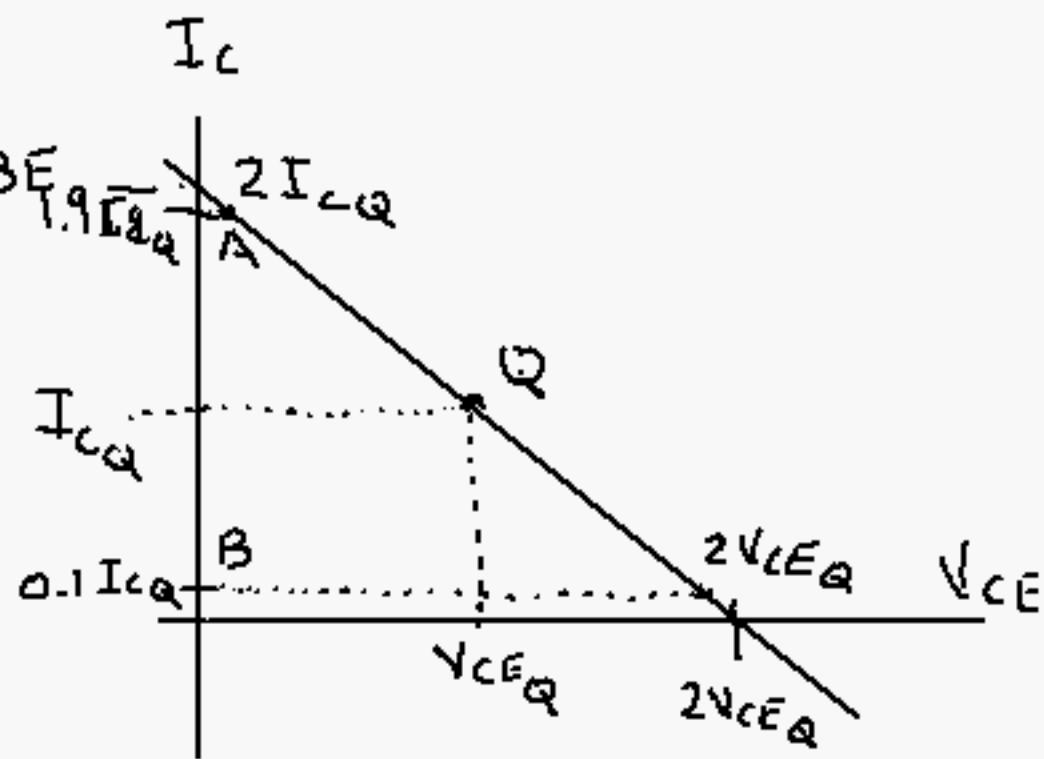
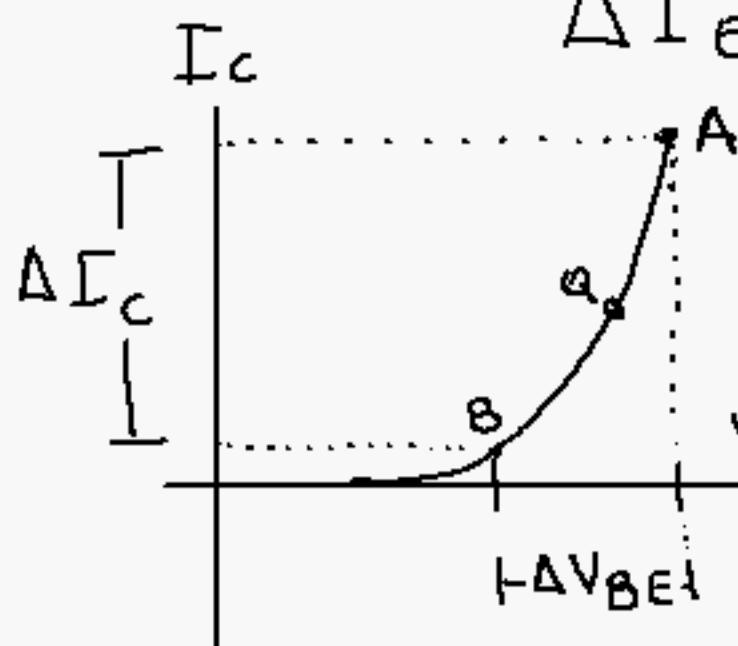
Para circuitos con doble fuente

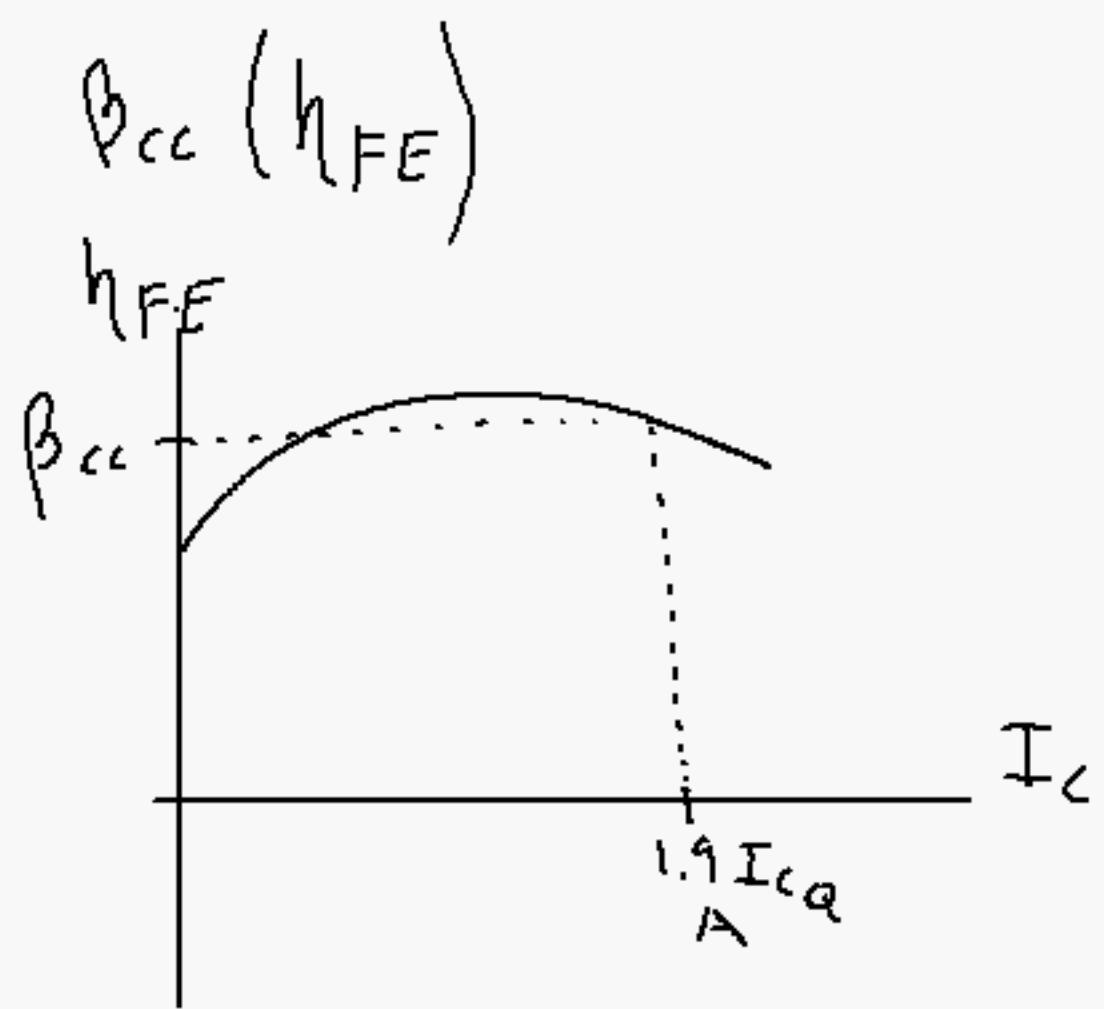
$$P_{DC} = (V_{CC} + V_{EE}) I_{CQ}$$

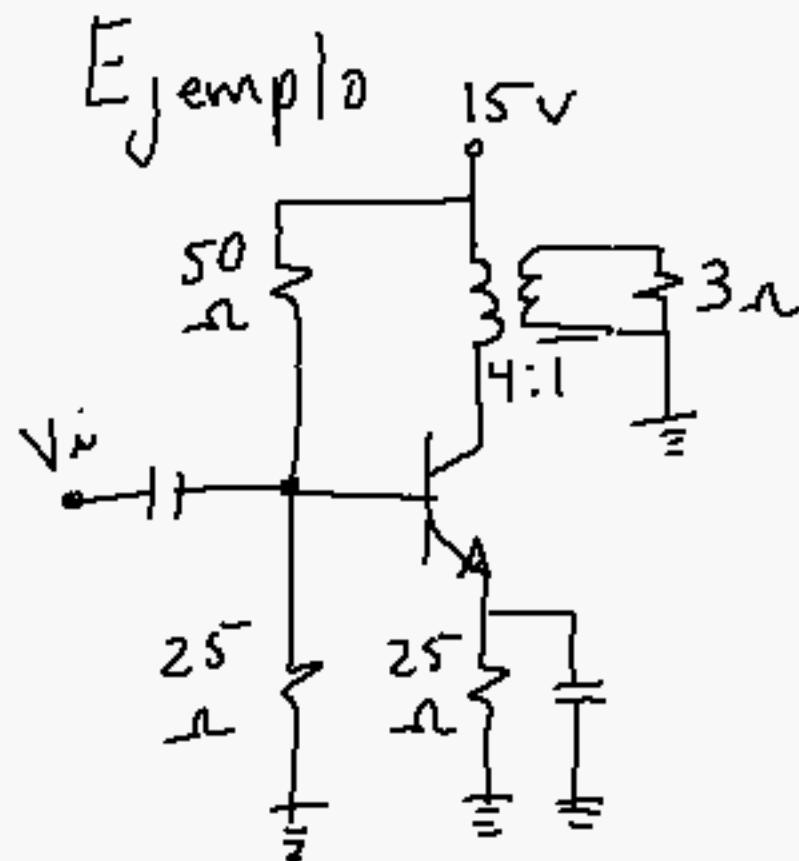
# Ganancia e impedancia

~~$$V_T = \frac{26mV}{T}$$~~

$$R_E \approx \frac{\Delta V_{BE}}{\Delta I_E} \approx \frac{\Delta V_{BE}}{\Delta I_C}$$







✓ Transformador ideal

- Recta de carga AC
- Potencia de AC en c primario de transf.
- Potencia de AC en  $R_L$
- $n$
- $P_D$

$$a) I_{c_{SAT}} = I_{cQ} + \frac{V_{CEQ}}{r_E + r_C}$$

$$V_{CE_{CORT}} = V_{CEQ} + I_{cQ}(r_E + r_C)$$

$$V_B = \frac{25}{75} (15) = 5V$$

$$I_E = \frac{5V - 0.7}{25} = 172mA$$

$$I_C \approx I_E = 172mA \neq I_{cQ}$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

$$V_{CE} = 15 - 172mA (25)$$

$$V_{CEQ} = 10.7V$$

$$I_{c, SAT} = 172 \text{ mA} + \frac{10.7}{48} = 394.9 \text{ mA}$$

$$n = \frac{N_p}{N_s} = 4$$

$$r_c = 48 \text{ n}$$

$$\frac{N_p}{N_s} = \frac{V_p}{V_s} = \frac{I_s}{I_p} = \frac{\frac{V_s}{R_s}}{\frac{V_p}{R_p}}$$

$$\frac{V_p}{V_s} = I_p R_p$$

$$\frac{V_p}{V_s} = \frac{I_s R_p}{I_p R_s}$$

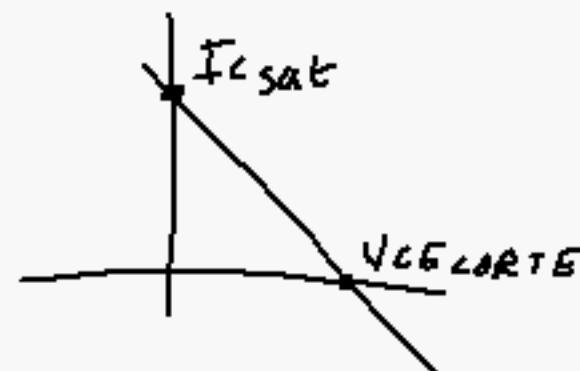
$$\frac{V_p}{V_s} = \frac{R_p}{R_s} \cdot \frac{I_s}{I_p}$$

$$\frac{V_p}{V_s} = \frac{R_p}{R_s} \cdot n$$

$$R_p = \left(\frac{V_p}{V_s}\right)^2 R_s = n^2 R_s$$

$$V_{CE\text{ CORTE}} = 10.7 \text{ V} + 172 \text{ mA} (48)$$

$$V_{CE\text{ CORTE}} = 18.97 \text{ V}$$



b) Potencia en primario <sup>AC</sup>

$$P_o = \frac{V_{CEA} I_{CA}}{2} = \frac{(10.7)(172 \text{ mA})}{2}$$

$$P_o = 0.92 \text{ W}$$

c) Potencia de AC en secundario

Para transformador ideal

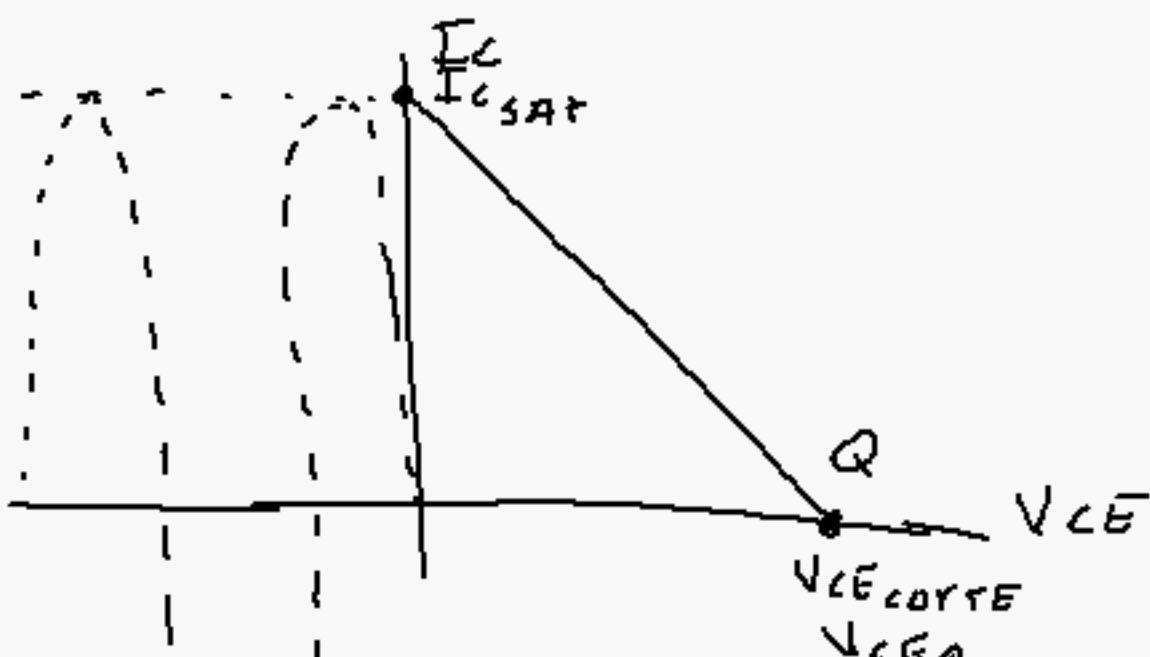
$$P_s = P_p = 0.92 \text{ W}$$

$$d) \eta = 35.65\%$$

$$e) P_D = 1.84 \text{ W}$$

Amplificadores clase B  
en oposición de fase

- $P_D$  es la quinta parte de la potencia de carga
- Consumo de corriente sin señal de aproximadamente 1% de  $I_{CSAT}$



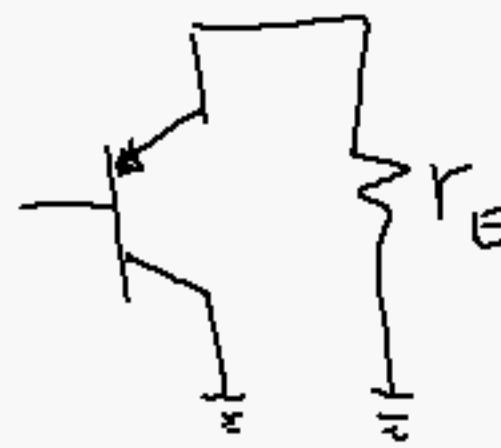
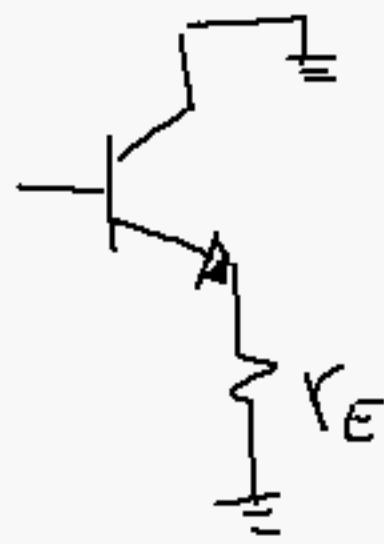
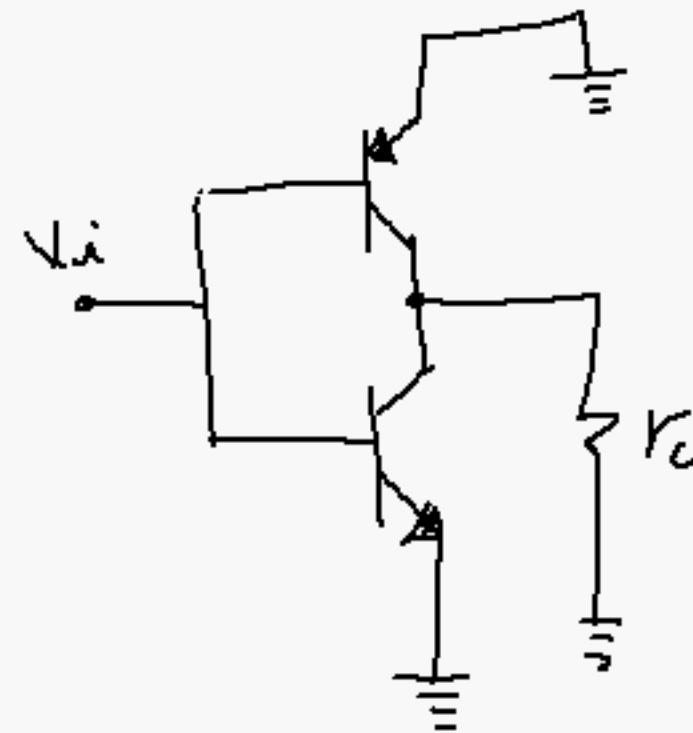
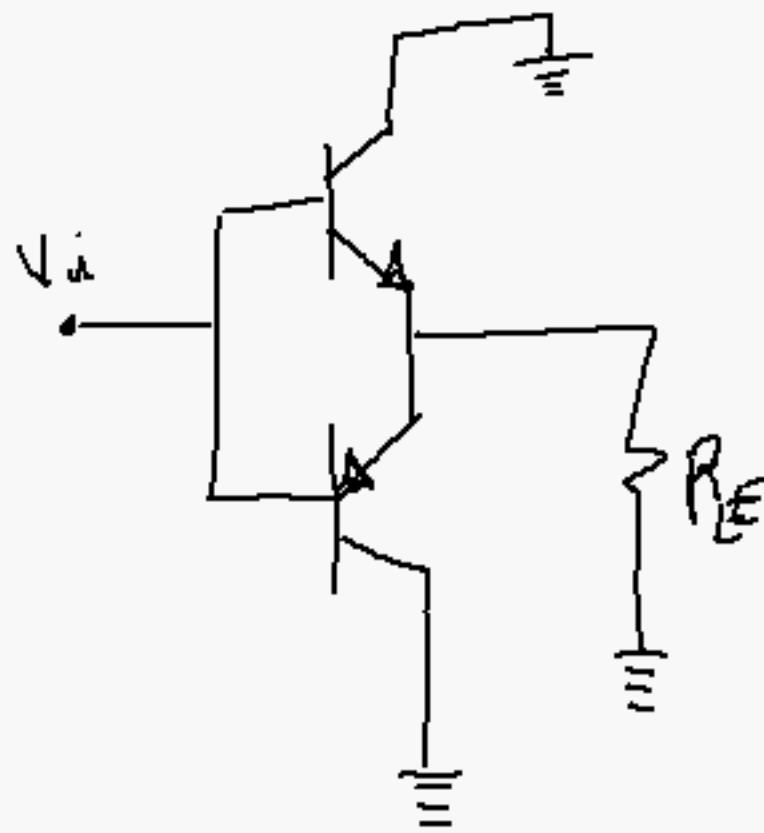
$$I_{CQ} = 0$$

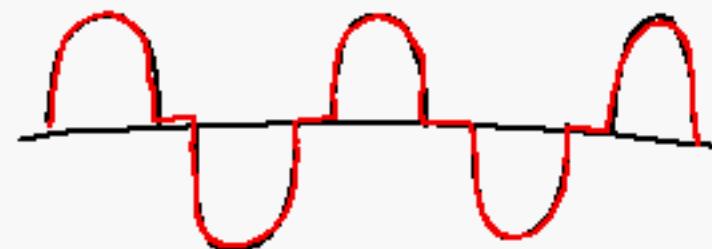
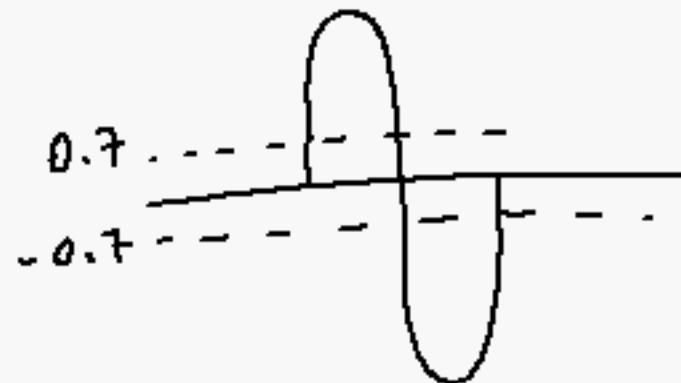
$$V_{CE, CORTE} = V_{CEQ} + I_{CQ}(r_E + r_C)$$

$$V_{CE, CORTE} = V_{CEQ}$$

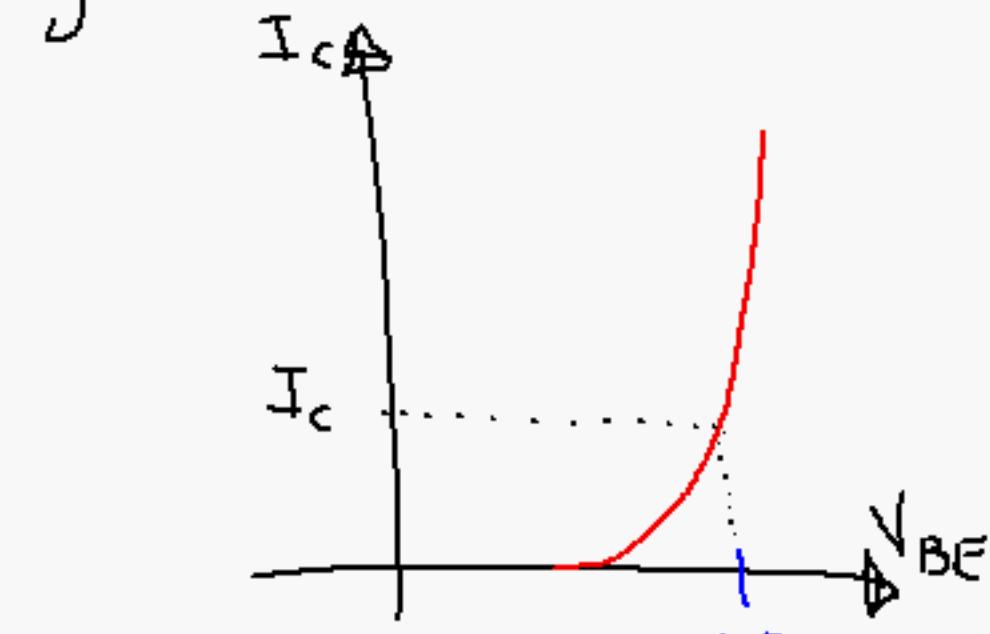
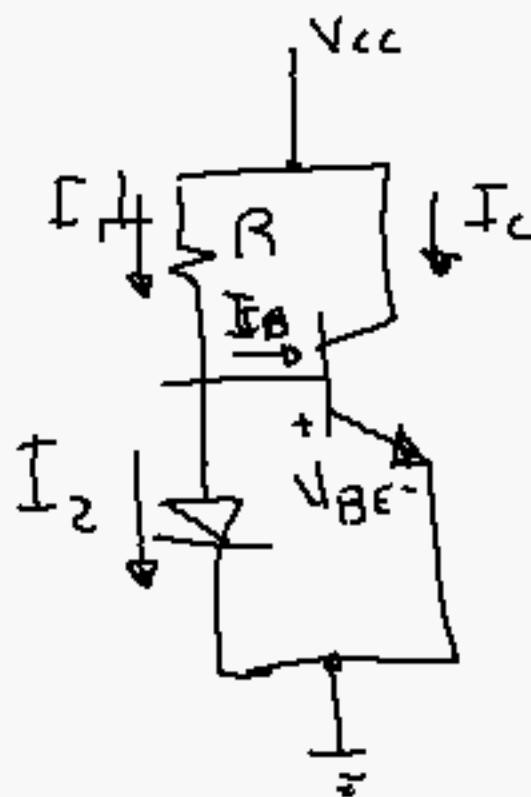
$$I_{C, sat} = I_{CQ} + \frac{V_{CEQ}}{R_E + r_C}$$

$$I_{C, sat} = \frac{V_{CEQ}}{R_E + r_C}$$





Circuito espejo de corriente

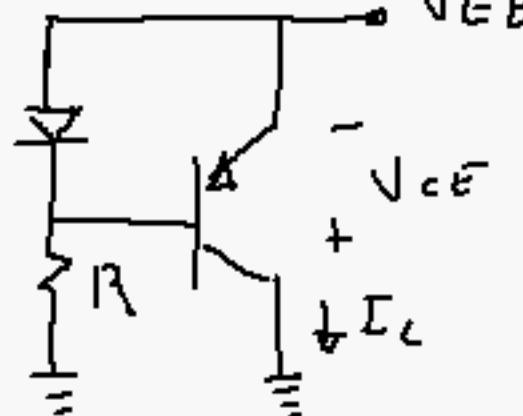


$$I_2 = I_c$$

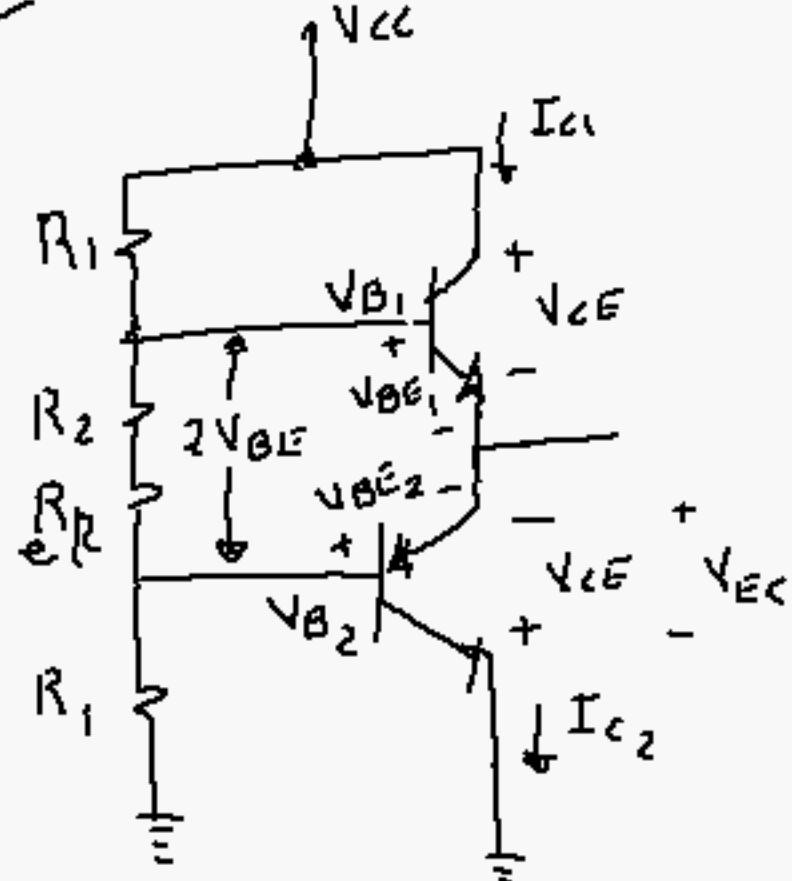
$$I_2 >> I_B$$

$$I_2 = I_2 + I_B \Rightarrow I_1 \approx I_2$$

PNP



Punto de operación para el amplificador clase B



$$V_{CE} \approx \frac{V_{CC}}{2} \approx \frac{1}{2} V_{CC}$$

$$V_{BE1} \approx 0.7 \text{ V}$$

$$V_{BE2} = -0.7 \text{ V}$$

$$V_{BE} = V_B - V_E$$

$$V_B = V_{BE1} + V_E$$

pero  $V_{E1} = V_{E2} = V_{EC2} = V_{CE1}$

$$V_{B1} = 0.7 + \frac{1}{2} V_{CC}$$

$$V_{B2} = V_{BE2} + V_{E2}$$

$$V_{B2} = -0.7 + \frac{1}{2} V_{CC}$$

$$V_{B_1} - V_{B_2} = 0.7 + \frac{1}{2}V_{CE} - \left( -0.7 + \frac{1}{2}V_{CE} \right)$$

$$V_{B_1} - V_{B_2} = 2(0.7) = 2|V_{BE}|$$

$$V_{R_1} \approx I_R R_1 = V_{CE} - V_{B_1} = V_{CE} - 0.7 - \frac{1}{2}V_{CE}$$

$$V_{R_1} \approx \frac{1}{2}V_{CE} - 0.7 = V_{B_2}$$

$$I_{R_1} = \frac{\frac{1}{2}V_{CE} - 0.7}{R_1} = \frac{V_{CE} - 2(0.7)}{2R_1}$$

$$I_{R_1} = \frac{V_{CE} - 2V_{BE}}{2R_1}$$

$$I_{R_1} = I_{C_r}$$

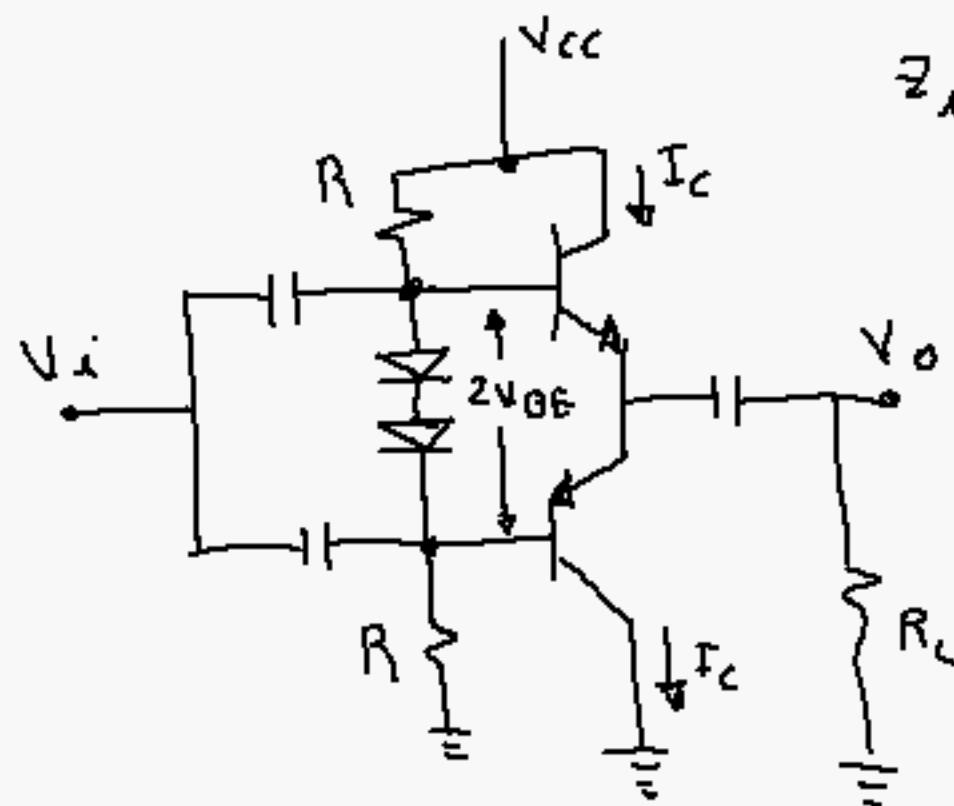
$$2V_{BE} = 2R_2 I_{C_r}$$

$$R_2 = \frac{V_{BE}}{I_{C_r}}$$

$$I_{c,r} = (1\% - 5\%) I_{c,sat}$$

$$I_{c,sat} = \frac{V_{CEQ}}{r_E + r_C} \quad r_E = R_L$$

Polarización por diodos



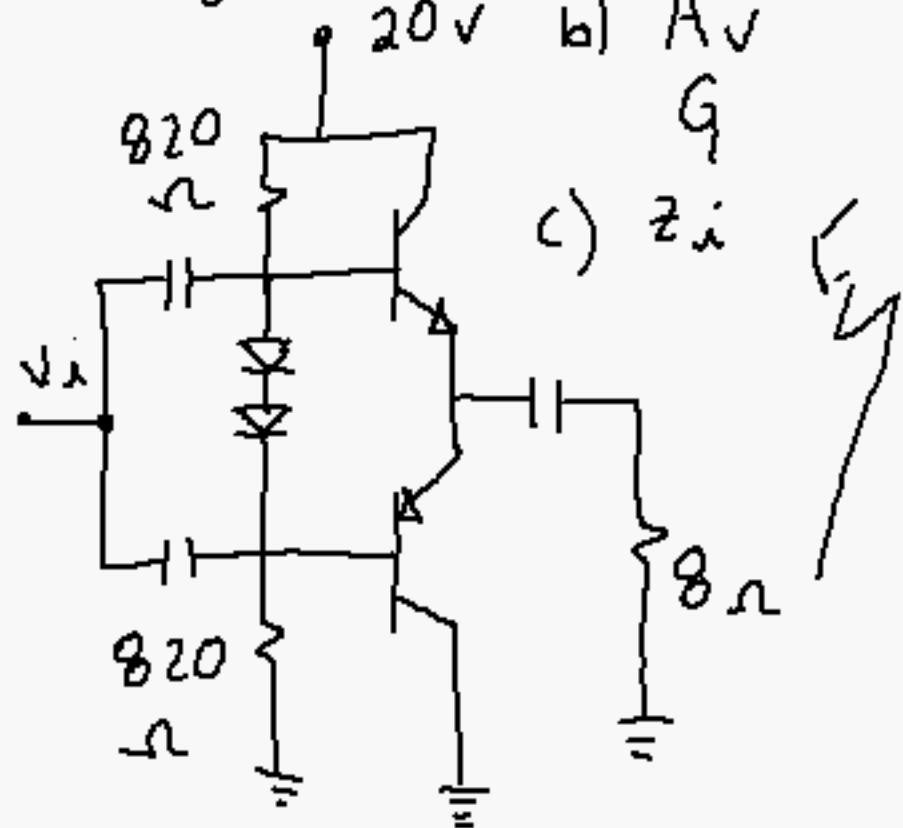
$$Z_i = R \parallel R_f \parallel (h_{FE}(r_E + R_e))$$

$$A_v = \frac{r_E}{r_E + R_e} = \frac{R_L}{R_L + R_e}$$

Ganancia en potencia

$$G = h_{FE} \left( \frac{R_L}{R_L + R_e} \right)$$

Ejemplo: a)  $I_{C_r}$



c)  $z_i$

$$h_{FE} = 60$$

$$R_E = 0.5 \Omega$$

$$a) I_R = I_{C_r} = \frac{V_{CC} - 2V_{BE}}{2R}$$

$$I_{C_r} = 11.3 \text{ mA}$$

≈ 1% of  $I_{C_{sat}}$

$$I_{C_{sat}} = \frac{V_{CEQ}}{r_E + R_C} = \frac{10}{8}$$

$$I_{C_{sat}} = 1.25 \text{ A}$$

$$b) A_V = \frac{R_L}{R_L + R_E} = 0.94$$

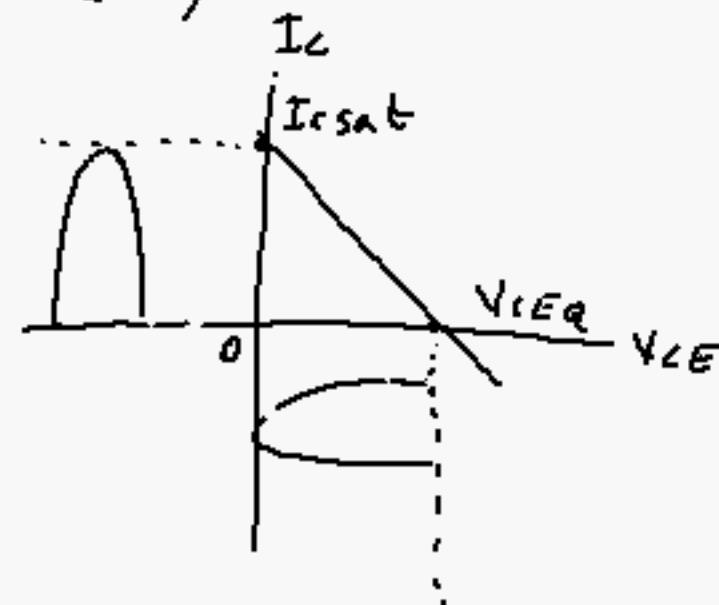
$$G = h_{FE} (A_V = 56.4)$$

$$c) z_i = \frac{1}{2} R \parallel h_{FE} (r_E + R_E)$$

$$z_i = 227.21 \Omega$$

# Potencia de salida ( $P_o$ )

$$P_o \text{ MAX} = \frac{V_{CEQ} I_{C\text{sat}}}{2}$$



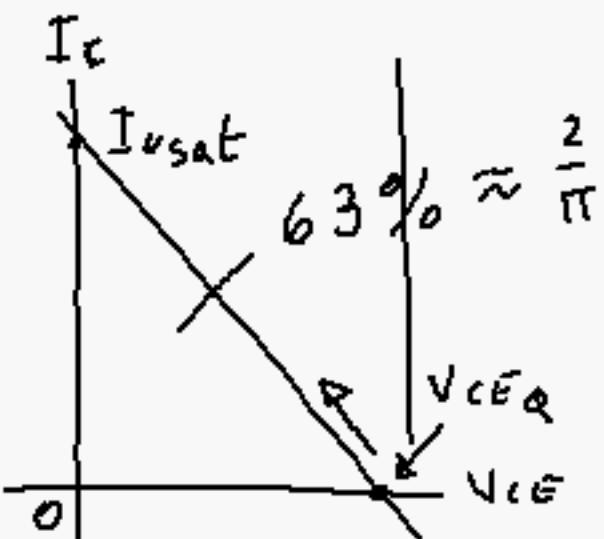
# Eficiencia ( $\eta$ )

$$\eta = \frac{P_o}{P_{DC}} \times 100 \quad P_{DC} = V_{CC} \frac{I_{C\text{sat}}}{\frac{\pi}{4}} \quad \text{pero } V_{CEQ} = \frac{1}{2} V_{CC}$$

$$\eta = \frac{V_{CEQ} I_{C\text{sat}}}{2} \quad \text{pero } V_{CEQ} = \frac{1}{2} V_{CC}$$

$$\eta = \frac{V_{CC} I_{C\text{sat}}}{\frac{\pi}{4} \frac{V_{CC} I_{C\text{sat}}}{\pi}} = \frac{\pi}{4} = 0.785 \Rightarrow 78.5\%$$

Potencia disipada ( $P_D$ )



$$P_{D_{MAX}} = \frac{\left(\frac{2}{\pi} \frac{V_{CEQ}}{\sqrt{2}}\right) \left(\frac{2}{\pi} \frac{I_{CSAT}}{\sqrt{2}}\right)}{2}$$

$$P_{D_{MAX}} = \frac{V_{CEQ} I_{CSAT}}{\pi^2}$$

$$P_{D_{MAX}} \approx \frac{V_{CEQ} I_{CSAT}}{10}$$

$$P_D = \frac{P_0}{10}$$

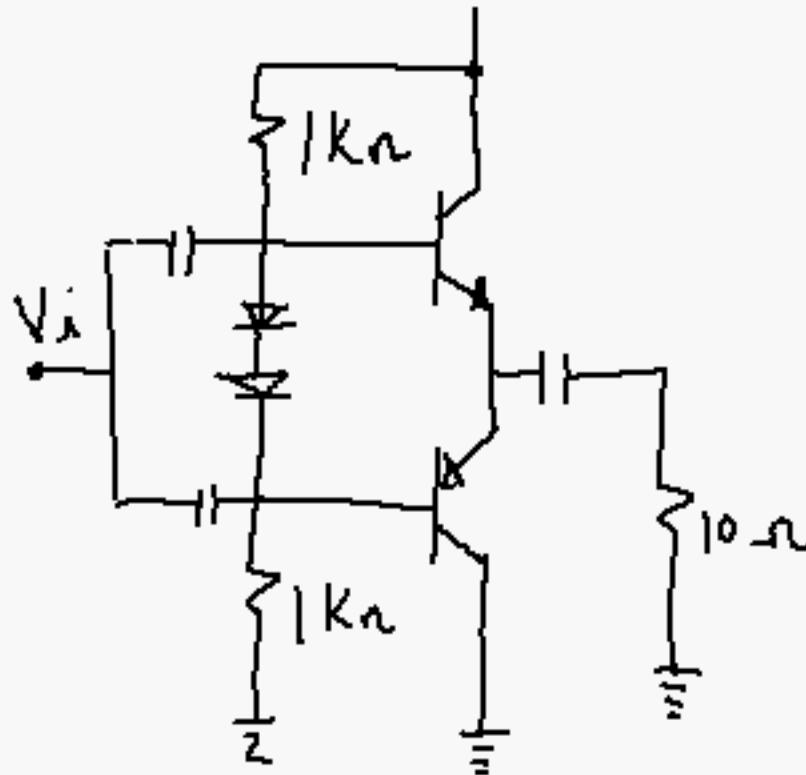
$$\text{Si } P_0 = \frac{V_{CEQ} I_{CSAT}}{2} \Rightarrow$$

entonces

$$P_{D_{MAX}} = \frac{P_0}{5}$$

Ejemplo

40V



$$P_{o\max} = \frac{V_{CEQ} I_{CSAT}}{2}$$

$$V_{CEQ} = \frac{1}{2} V_{CC} = \frac{40}{2} = 20$$

$$I_{CSAT} = \frac{V_{CEQ}}{r_E}$$

$$P_{o\max} = \frac{V_{CEQ}^2}{2 r_E} = \frac{(20)^2}{2(10)}$$

$$P_{o\max} = 20 \text{ W}$$

$$P_{D\max} = \frac{20}{5} = 4 \text{ W}$$

Obtener  $P_{o\max}$ ,  $P_{D\max}$

$P_{o\max}$

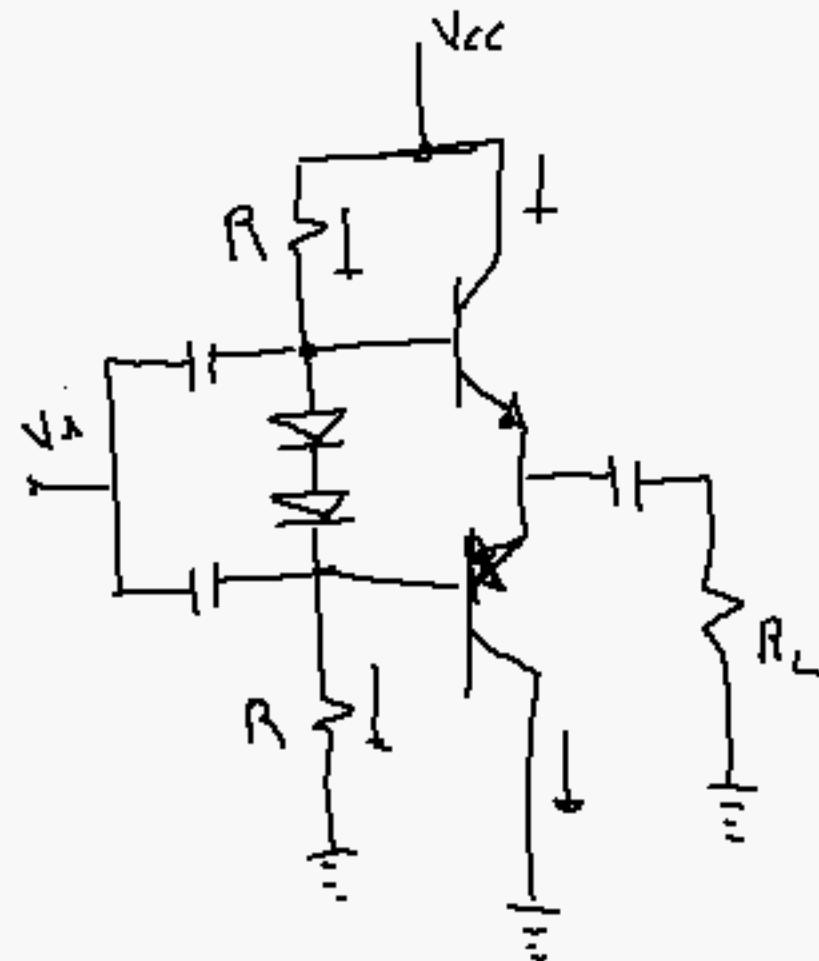
$P_{D\max}$

$\eta$

$$\eta = 78.5\%$$

## Ejemplo

Diseñar un amplificador clase B en oposición de fase de 25 W de salida para una carga de 8 Ω.



$$P_o = \frac{V_{CEQ} I_{CSAT}}{2}$$

$$I_{CSAT} = \frac{V_{CEQ}}{r_E} = \frac{V_{CEQ}}{R_L} = 2.5 \text{ A}$$

$$P_o = \frac{V_{CEQ}^2}{2 R_L} \quad \text{pero } V_{CEQ} = \frac{1}{2} V_{CC}$$

$$P_o = \frac{V_{CC}^2}{8 R_L} \Rightarrow V_{CC} = 40 \text{ V}$$

$$I_{CSAT} = \frac{V_{CEQ}}{R_L} = \frac{20}{8} = 2.5 \text{ A}$$

$$I_{CR} = (2.5\%) I_{CSAT} = 62.5 \text{ mA}$$

$$I_{C_r} = \frac{V_{CC} - 2V_{BE}}{2R}$$

$$R = 308.8 \Omega$$

$$P_{D_{max}} = \frac{25}{5} = 5 \text{ W} \quad h_{FE} = 70$$

$$A_x = \frac{I_o}{I_i} \cong h_{FE} = 70$$

$$I_i = \frac{2.5}{70} = 35.7 \text{ mA}$$

Ejemplo: Obtener

- $P_o$  y  $P_D$
- $I_{CQ}$  en la etapa de salida
- $A_v$  total considerando  $\beta_{CC} = 100$  para todos los transistores y una  $R_E = 1\Omega$ ,
- Estimar la amplitud máxima de salida y amplitud máxima de entrada de la señal de AC.

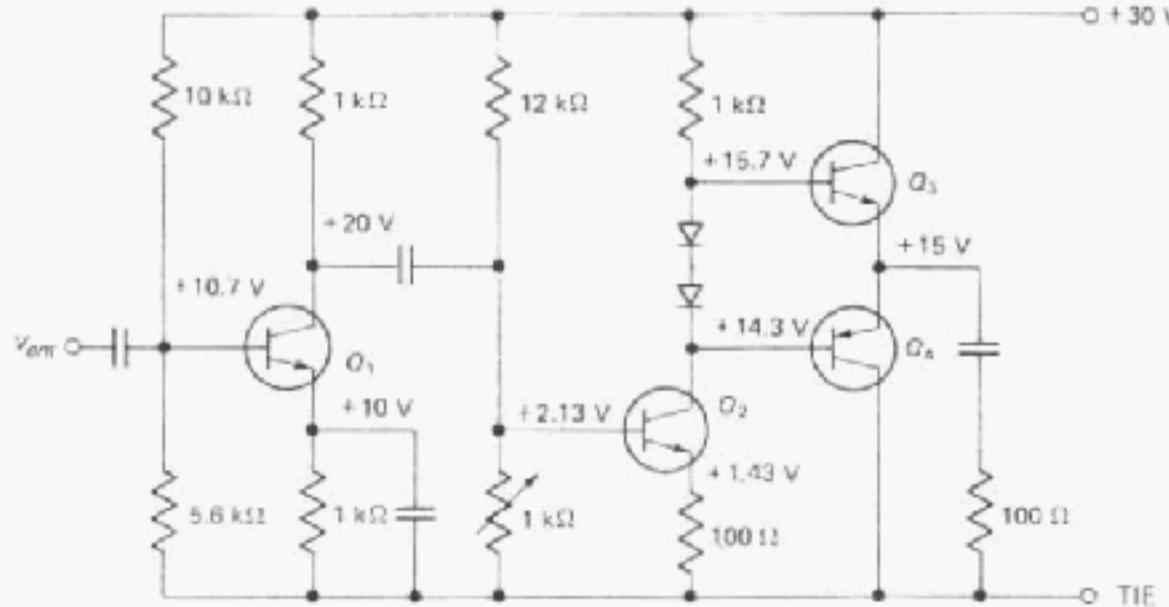


Figura 11-16. Ejemplo de un amplificador completo.

Solución

Datos:  $h_{FE} = 100$ ,  $Re = 1 k\Omega$

a)  $P_o, P_D$

$$P_o = \frac{V_{CEQ} I_{C, \text{sat}}}{2} = \frac{V_{CEQ}^2}{2 R_E} = \text{pero } V_{CEQ} = \frac{1}{2} V_{CC}$$

$$P_o = 1.125 \text{ W}$$

$$P_D = \frac{1.125}{.5} = 2.25 \text{ mW}$$

b)  $I_{C_r} = \frac{1.43}{100} = 14.3 \text{ mA}$

c)  $A_v = \frac{1k\Omega \parallel 12k\Omega \parallel 1k\Omega \parallel 100(100)}{2.6} = 176$   $I_{RA} \frac{10}{1000} = 10 \text{ mA}$

$$A_v = 176$$

$$r_e = \frac{26 \text{ mV}}{10 \text{ mA}} = 2.6 \text{ }\Omega$$

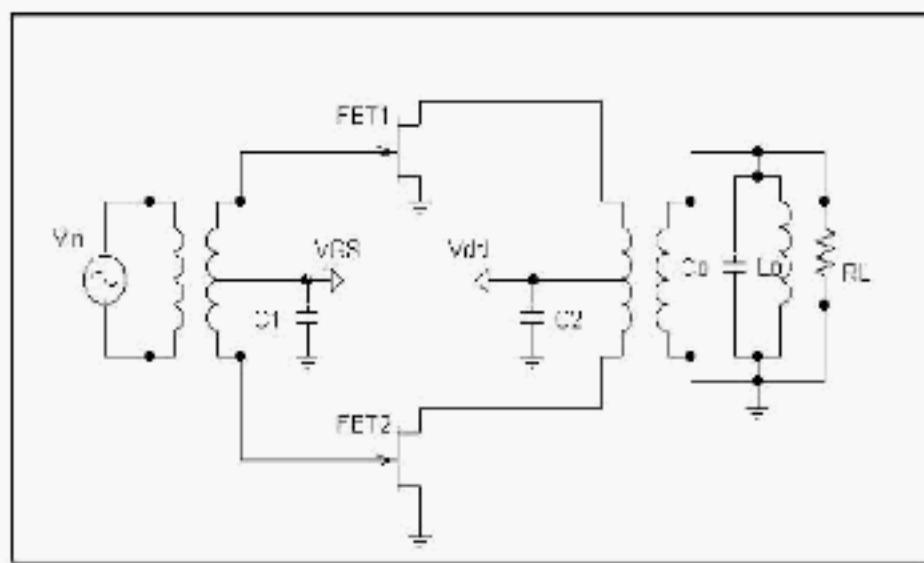
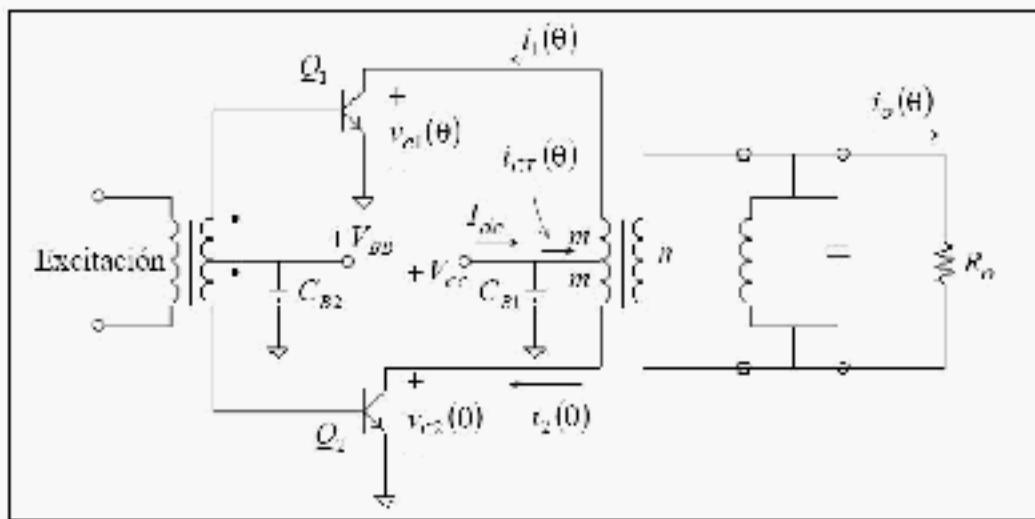
$$A_2 = \frac{r_e}{r_L} = \frac{1k\Omega / 100(1+100)}{1+100} = 9$$

$$A_3 = \frac{R_L}{R_L + R_e} = \frac{100}{100 + 1} = 0.99$$

$$A_v = A_1 A_2 A_3 = 1563$$

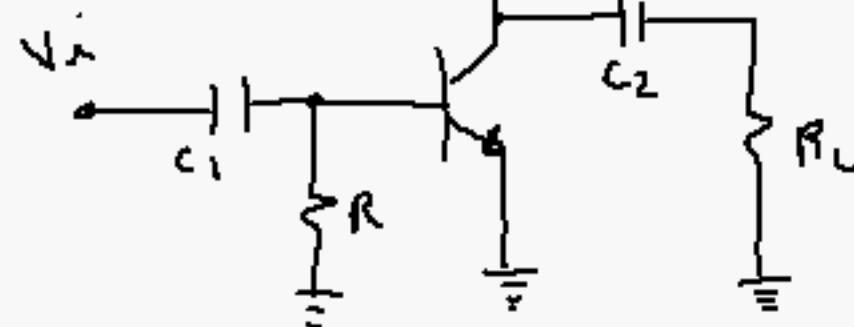
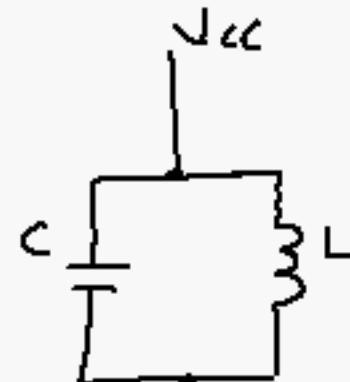
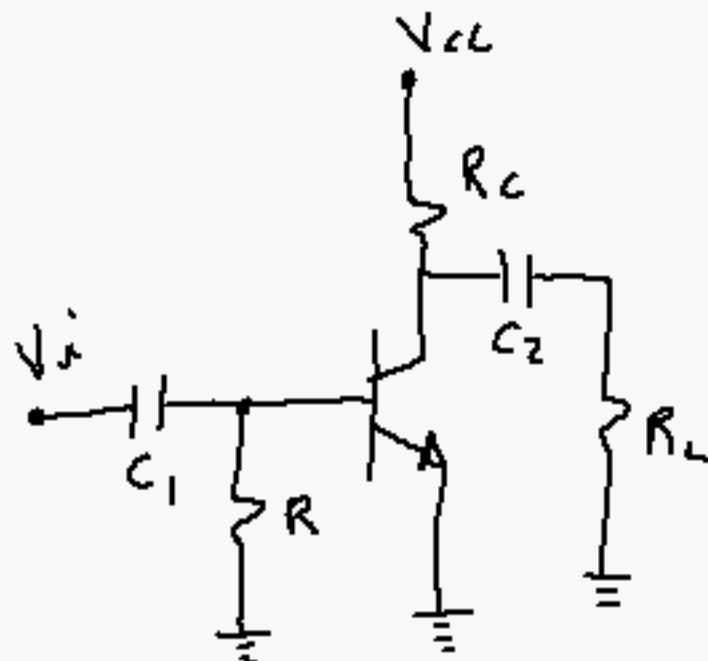
d)  $V_{CEQ} = \frac{1}{2} V_{CC} = 15V$  (Solido máx)

$$V_o = V_A A_v \Rightarrow V_o = \frac{V_o}{A_v} = 9.57mV$$

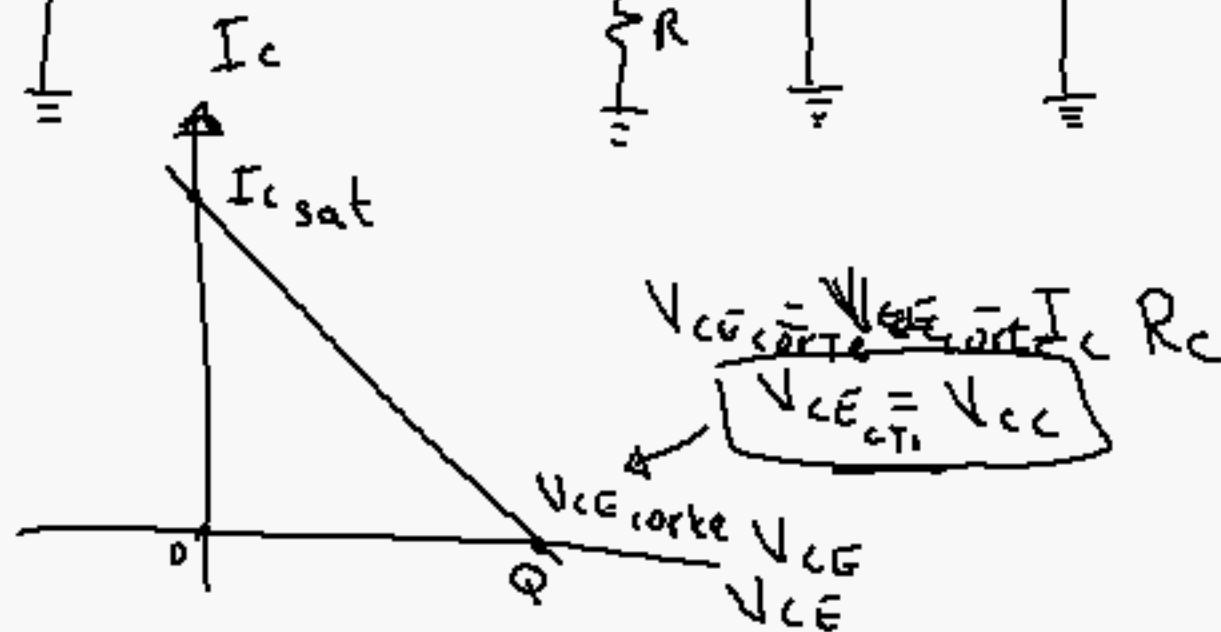


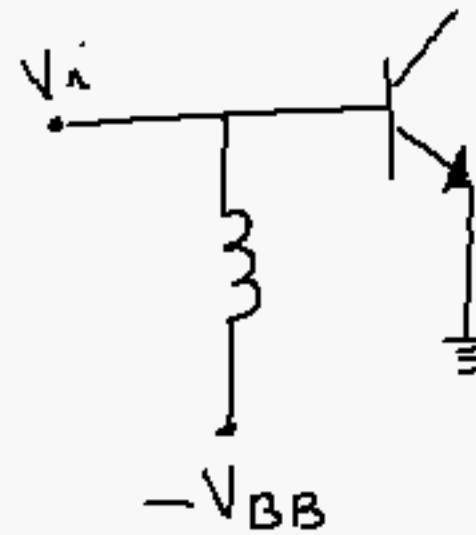
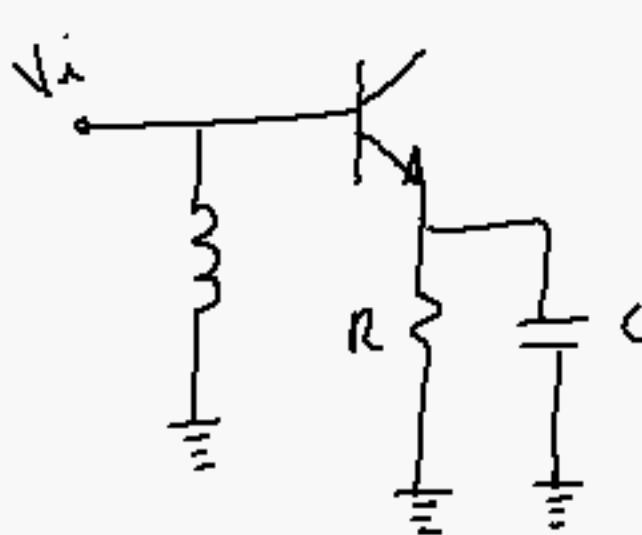
# Amplificadores clase C

- La corriente del colector circula menos de  $180^\circ$  de la señal de AC

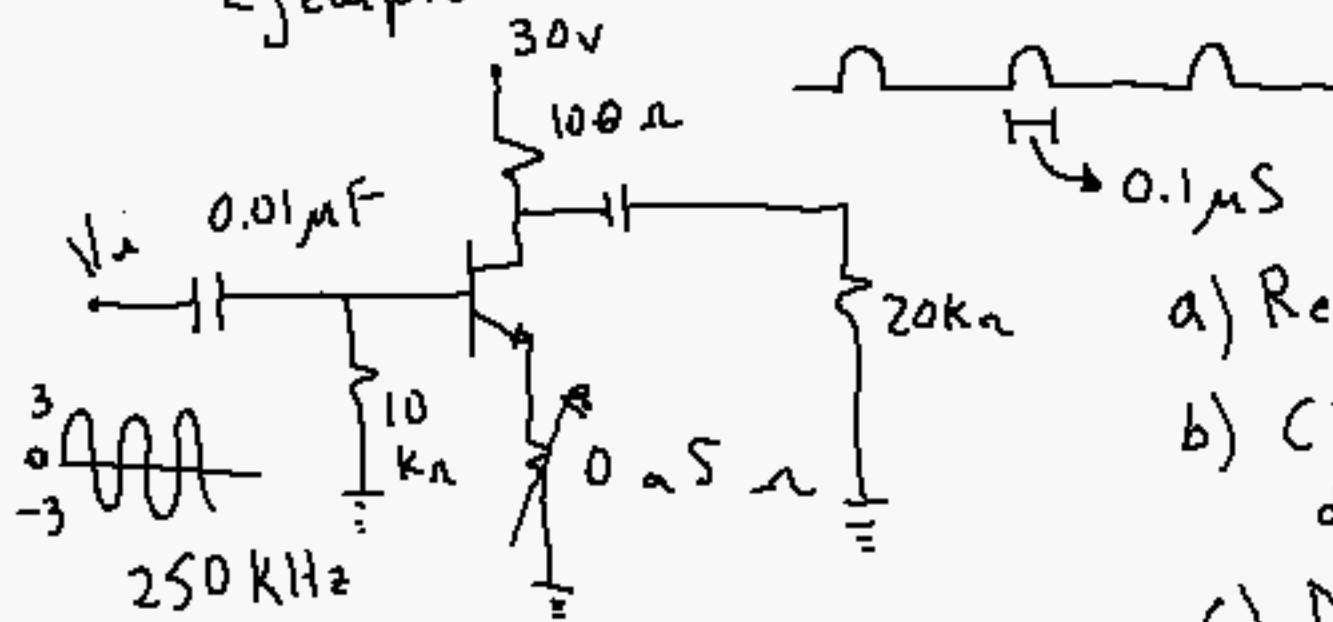


$$I_{c, \text{sat}} = \frac{V_{CEQ}}{R_C}$$



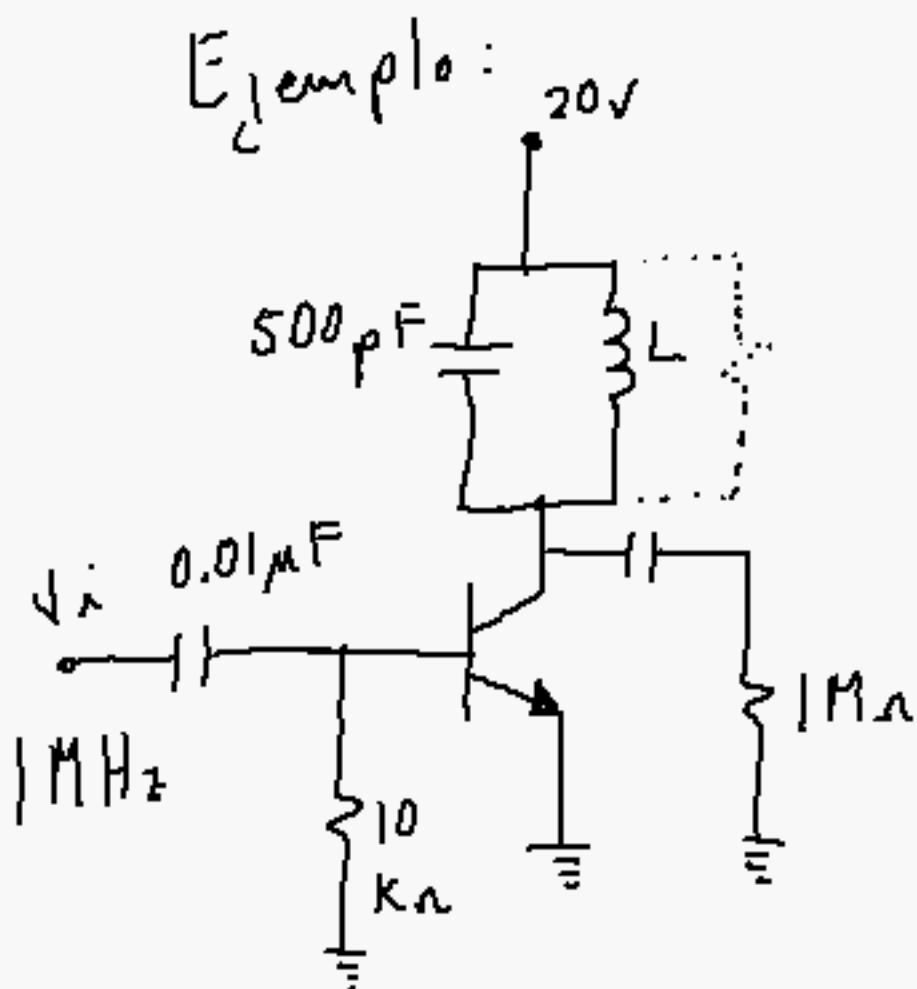


Ejemplo:



- a) Recta de carga
- b) CT de la forma de onda de salida.
- c) Dibujar forma de onda de la base del tr.

Ejemplo:



a) Obtener el valor de L para 1 MHz

b) Si el inductor tiene una resistencia serie de 10Ω a 1 MHz, obtener la Q del circuito.

Solución

$$a) L = \frac{1}{4\pi^2 f^2 C}$$

$$L = 50.66 \mu\text{H}$$

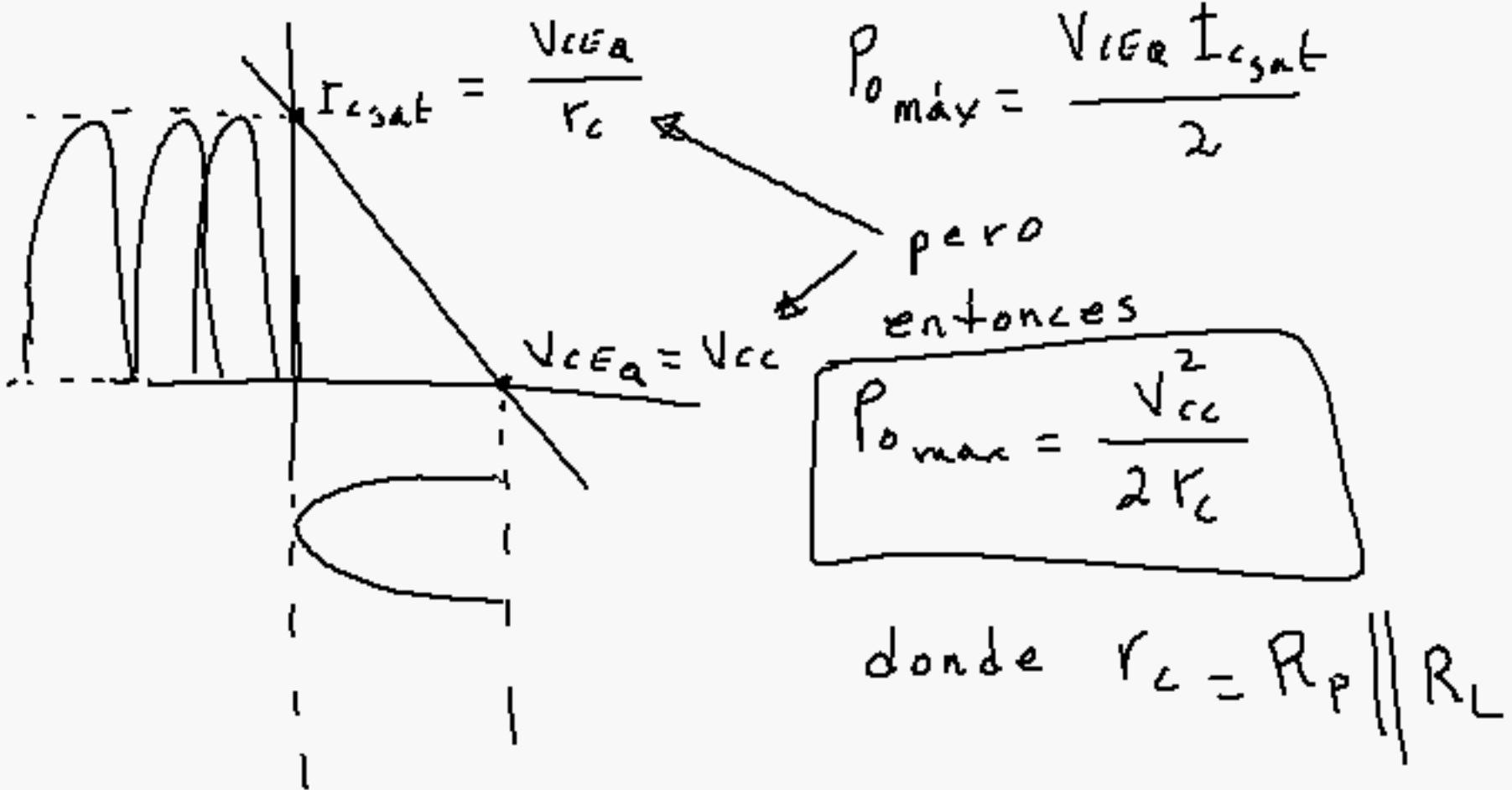
$$b) Q_L = \frac{\omega L}{R_s}$$

$$Q_L e = \frac{R_p}{\omega L} \omega L \Rightarrow R_p = Q \omega L$$

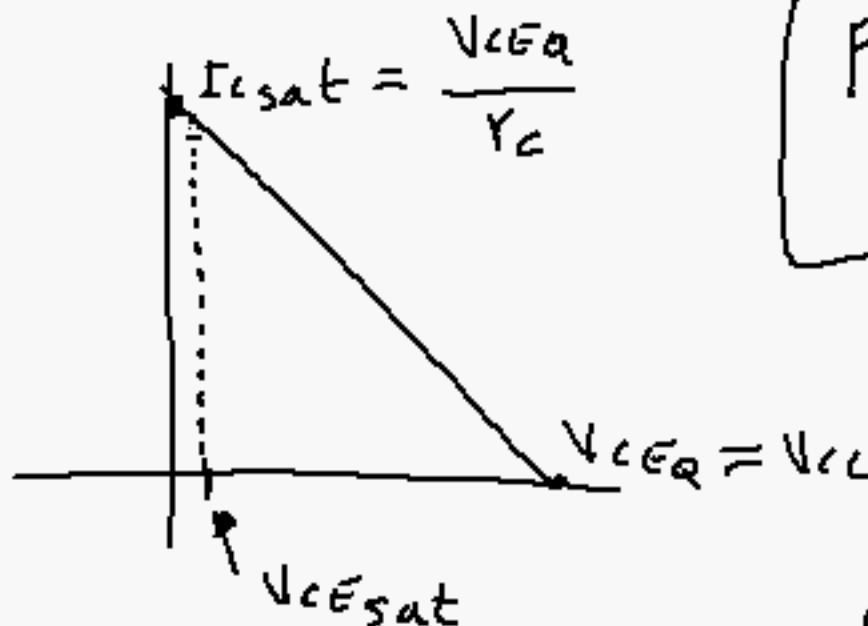
$$Q = \frac{R_{sh}}{\omega L}$$

$$R_{sh} = R_p \parallel R_L$$

## Potencia de salida



## Potencia disipada



$$P_D \approx \frac{V_{CEQ} V_{CC}}{2 R_C}$$

Potencia disipada mínima

Peor caso, potencia de disipación máxima (50% de la recta de carga)

$$P_D = \frac{I_{c\text{sat}} V_{CC}}{2\sqrt{2}} = \frac{I_{c\text{sat}} V_{CC}}{8}$$

$$P_D = \frac{V_{CC}^2}{8 R_C}$$

$$\frac{P_D}{P_{o\max}} = \frac{\frac{V_{CEsat} V_{CC}}{2r_c}}{\frac{V_{CC}^2}{2r_c}} = \frac{V_{CEsat}}{V_{CC}}$$

por lo que:

$$P_D = \frac{V_{CEsat}}{V_{CC}} P_{o\max}$$

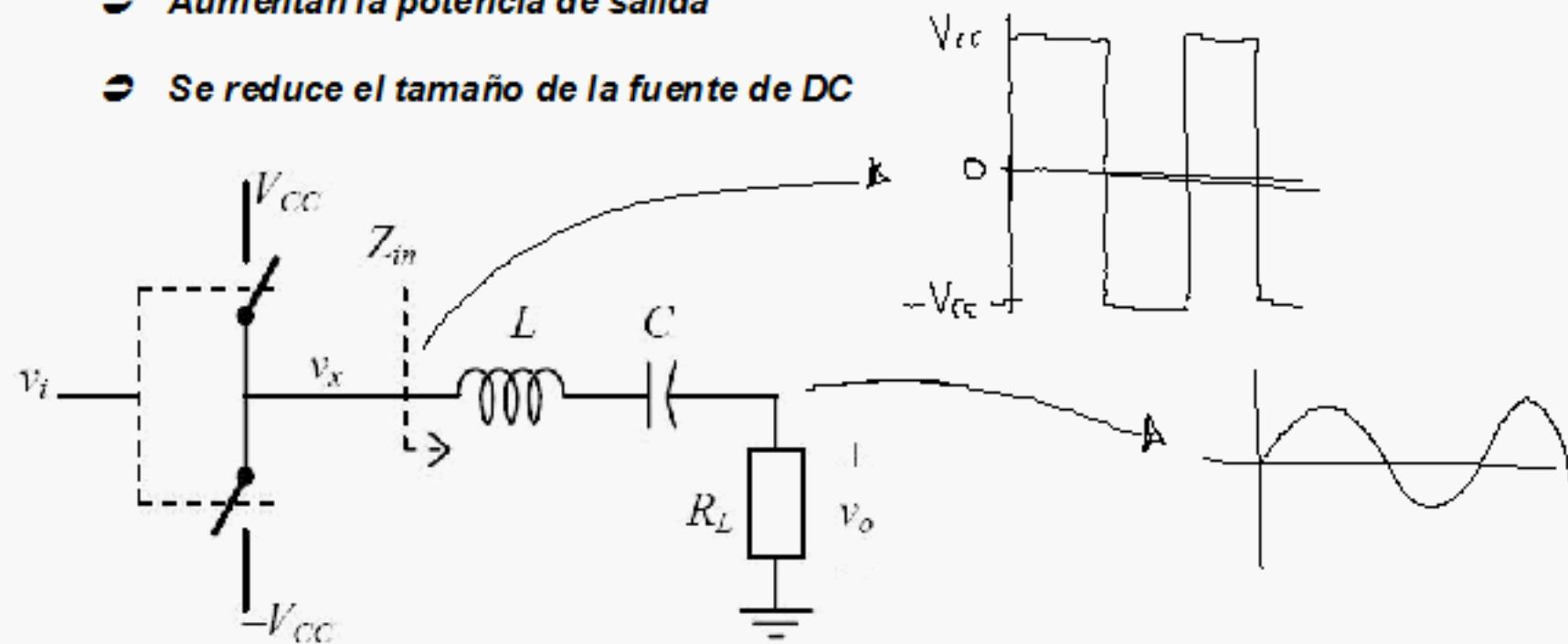
Eficiencia

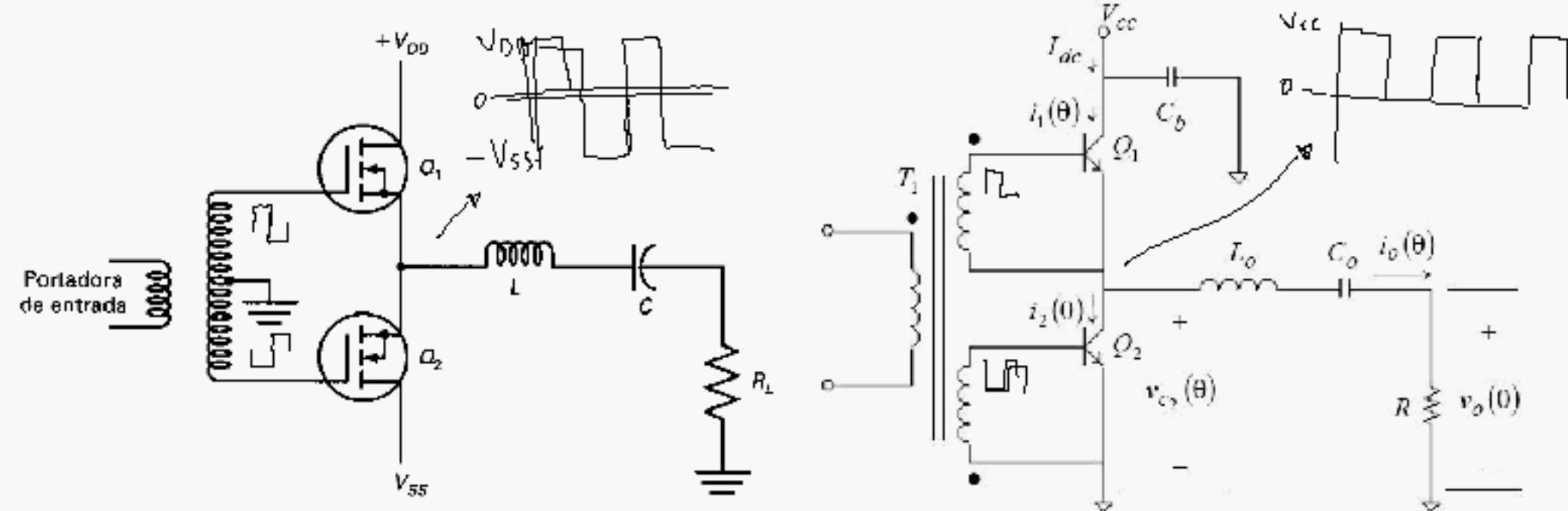
$$P_{DC} = P_{o\max} + P_D$$

entonces  $\eta = \frac{P_{o\max}}{P_{DC}} = \frac{P_{o\max}}{P_{o\max} + (P_D)} = \frac{V_{CC}}{V_{CC} + V_{CEsat}}$

## Amplificador clase D

- **Amplificadores por commutación**
- **Los dispositivos activos se utilizan como interruptores en lugar de fuente de corriente**
- **Mejoran la eficiencia**
- **Aumentan la potencia de salida**
- **Se reduce el tamaño de la fuente de DC**





$$V_{C2} = \frac{1}{2} V_{CC} + \frac{1}{2} V_{CC} S(\theta)$$

$$\text{donde } s(\theta) = \left( \frac{4}{\pi} \left( \sin \theta \right) + \frac{1}{3} \sin 3\theta + \frac{1}{5} \sin 5\theta + \dots \right)$$

$$V_o(\theta) = \frac{1}{2} V_{cc} \frac{4}{\pi} \sin \theta = \frac{2 V_{cc}}{\pi} \sin \theta$$

$$i_o(t) = \frac{2V_{cc}}{\pi R_L} \sin \theta$$

Potencia de salida

$$P_o = \frac{V_o}{\sqrt{2}} \frac{i_o}{\sqrt{2}} = \frac{1}{2} \frac{V_o^2}{R_L}$$

$$P_o = \frac{1}{2} \frac{\left(\frac{2V_{cc}}{\pi}\right)^2}{R_L} = \frac{2V_{cc}^2}{R_L \pi^2}$$

Las corrientes en los colectores son medias sinusoides con valor pico de  $\frac{2V_{cc}}{\pi R_L}$

La corriente de entrada es el promedio de  $\frac{2V_{cc}}{\pi R_L}$ , es decir

$$I_{DC} = \frac{\frac{2V_{cc}}{\pi R_L}}{\pi} = \frac{2V_{cc}}{\pi^2 R_L}$$

entonces:

$$P_{DC} = V_{cc} I_{DC} = \frac{2V_{cc}^2}{\pi^2 R_L}$$

por tanto

$$\eta = \frac{P_o}{P_{DC}} = 100\%$$

Ejemplo:

Determinar  $V_{CC}$  e  $I_{DC}$  para un amplificador de potencia clase D de voltaje complementario para que proporcione 25W a una carga de  $50\Omega$

Solución

$$\text{Si: } P_o = \frac{2V_{CC}^2}{\pi^2 R} \Rightarrow V_{CC} = \sqrt{\frac{\pi^2 P_o R}{2}} = 78,53\text{V}$$

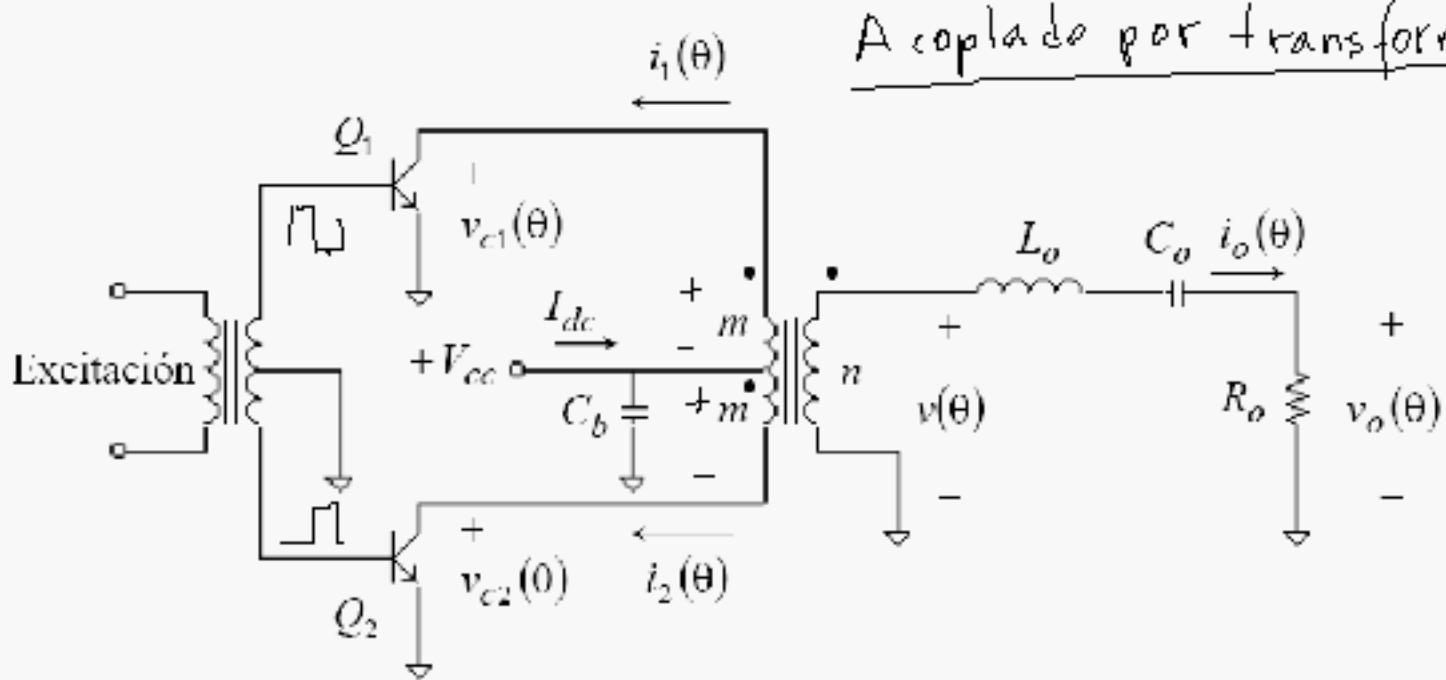


$BV_{CBO}$

$$I_{DC} = \frac{2V_{CC}}{\pi^2 R} \approx 0.318\text{mA}$$

Voltaje de ruptura

## A copiado por transformados



Cuando  $Q_2$  se satura  $\Rightarrow \frac{n}{m} V_{cc}$

Cuando  $Q_1$  se satura  $\Rightarrow -\frac{n}{m} V_{cc}$

$$V(\theta) = \frac{n}{m} V_{cc} \quad S(\theta) = \left( \frac{n}{m} V_{cc} \frac{4}{\pi} \left( \sin \theta + \frac{1}{3} \sin 3\theta + \dots \right) \right)$$

$$V_o(\theta) = V_{cc} \frac{n}{m} \frac{4}{\pi} \sin \theta \quad \text{pero } i_o(\theta) = \frac{V_o(\theta)}{R_o}$$

Potencia de salida es:

$$P_o = \frac{V_o}{\sqrt{2}} \frac{i_o}{\sqrt{2}} = \frac{1}{2} \frac{V_o^2}{R_o} = \frac{8}{R_o} \left( \frac{V_{cc}}{\pi} \frac{n}{m} \right)^2$$

$$\text{Si } I_c = i_o \frac{n}{m} \quad \text{e}$$

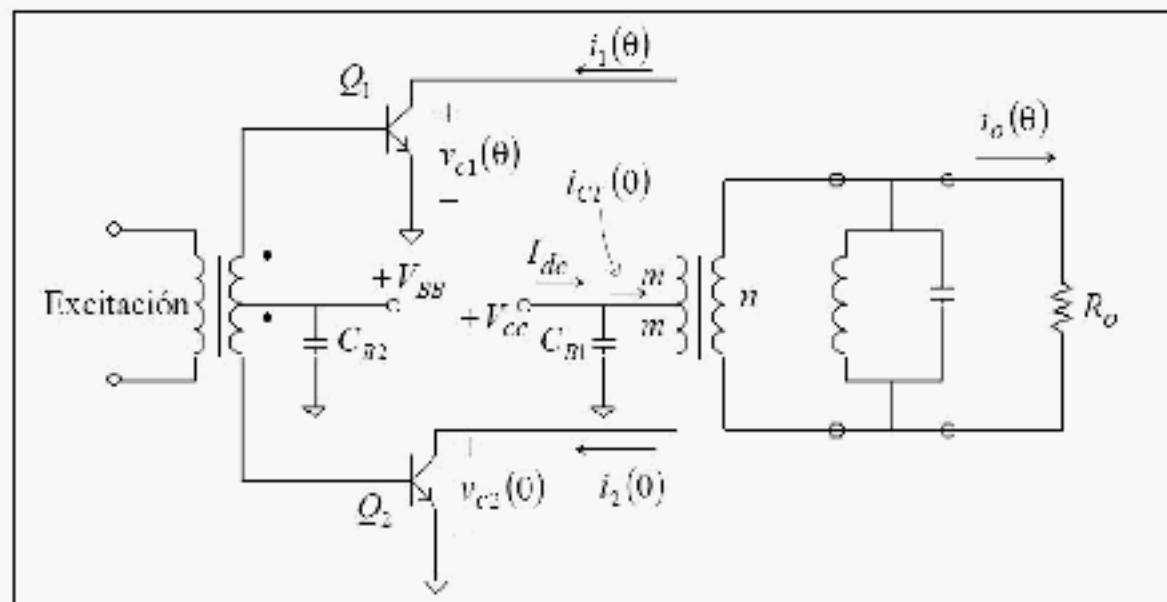
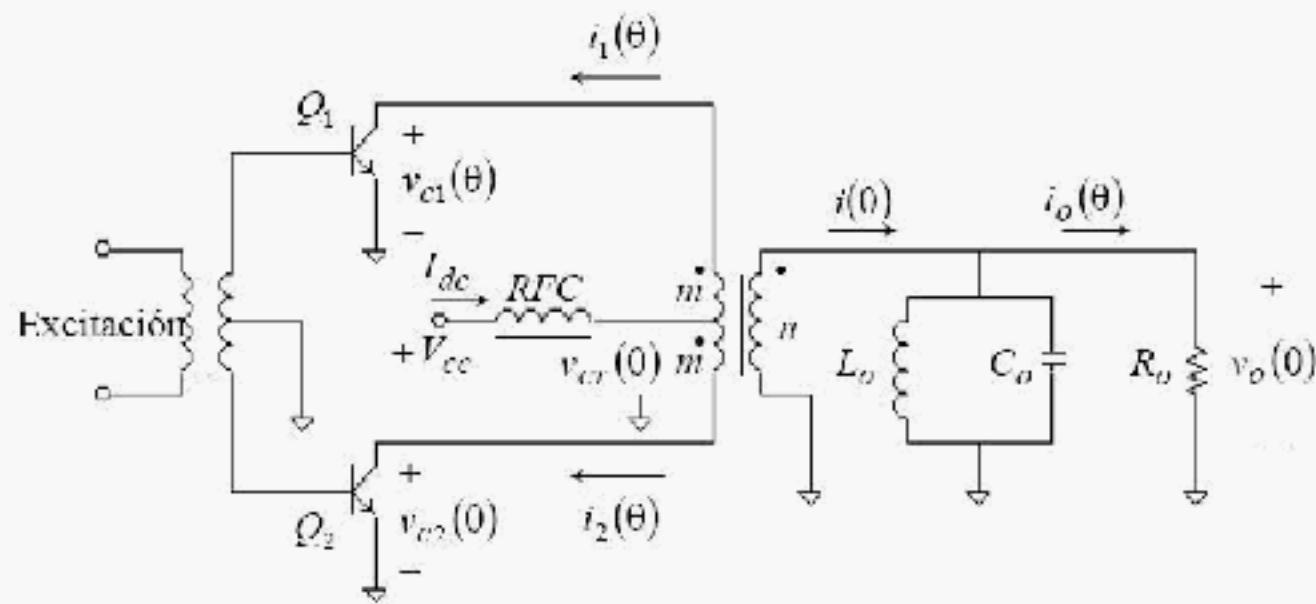
$$I_{DC} = \frac{2 I_c}{\pi}$$

entonces:

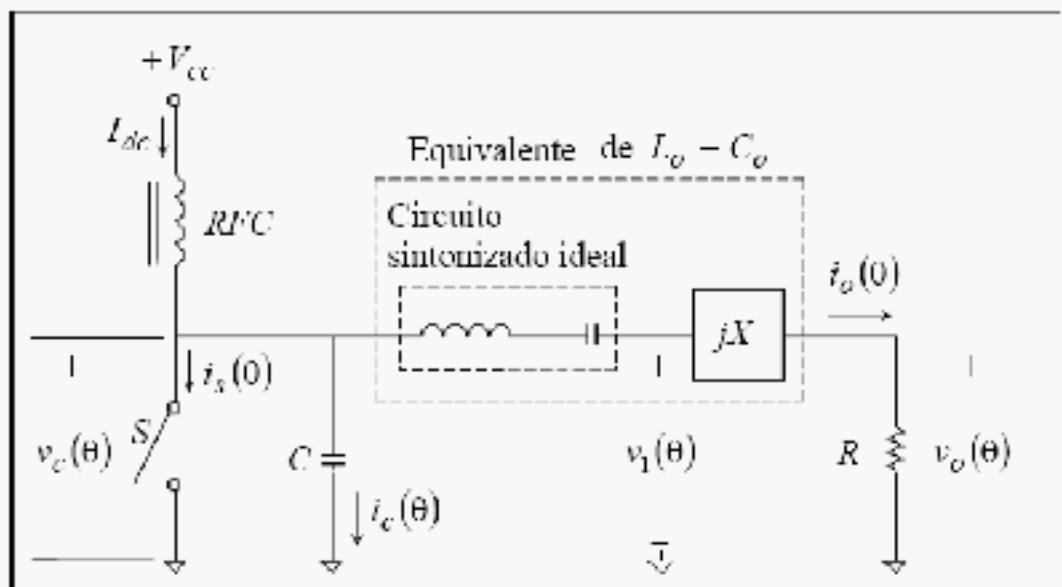
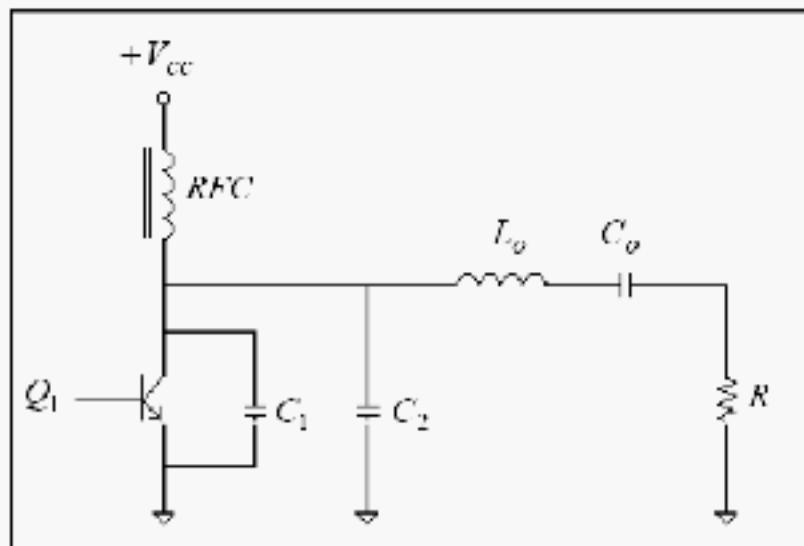
$$I_{DC} = \frac{8 V_{cc}}{R_o \pi^2} \frac{n^2}{m^2}$$

$$P_{DC} = V_{cc} I_{DC} = \frac{8}{R_o} \left( \frac{V_{cc}}{\pi} \frac{n}{m} \right)^2$$

$$\eta = \frac{P_o}{P_{DC}} \approx 100\%$$



## Amplificadores clase E



C: Capacitor en derivación

$\left\{ \begin{array}{l} \text{C1: Capacitor inherente al transistor} \\ \text{C2: Capacitor externo} \end{array} \right.$