

Amplificadores de Potencia

($P_o > 500\text{mW}$)

❖ Amplificadores lineales

- ✓ Clase A (360°)
- ✓ Clase B (180°)
- ✓ Clase AB ($<360^\circ$ y $>180^\circ$)

❖ Amplificadores clase C ($< 180^\circ$)

❖ Amplificadores por conmutación

- ✓ Clase D
- ✓ Clase E
- ✓ Clase F
- ✓ Clase S

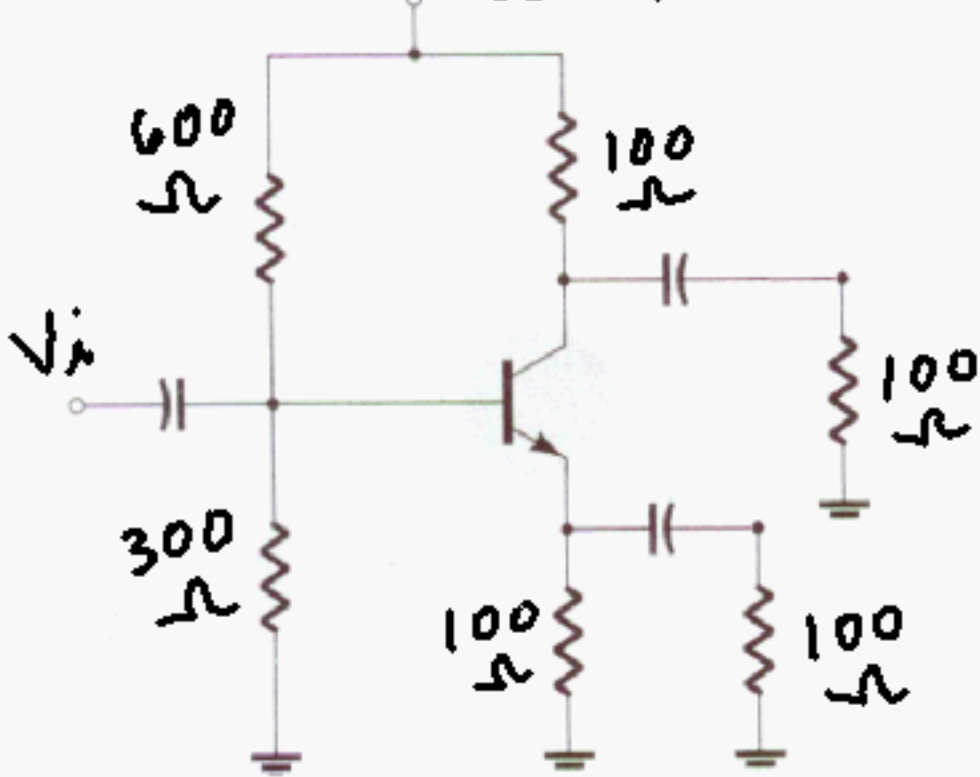
Amplificadores lineales

Amplificador Clase A

- ☐ **Conduce sobre los 360°**
- ☐ **Alta disipación de potencia**
- ☐ **Potencia de salida limitada**
- ☐ **Aplicación principal en etapas de baja potencia**
- ☐ **Eficiencia $< 50\%$**

Recta de carga de CA

$$V_{CC} = 15V$$



$$\beta R_E \geq 10 R_2 \checkmark$$

$$V_B = \frac{300}{900} (15V)$$

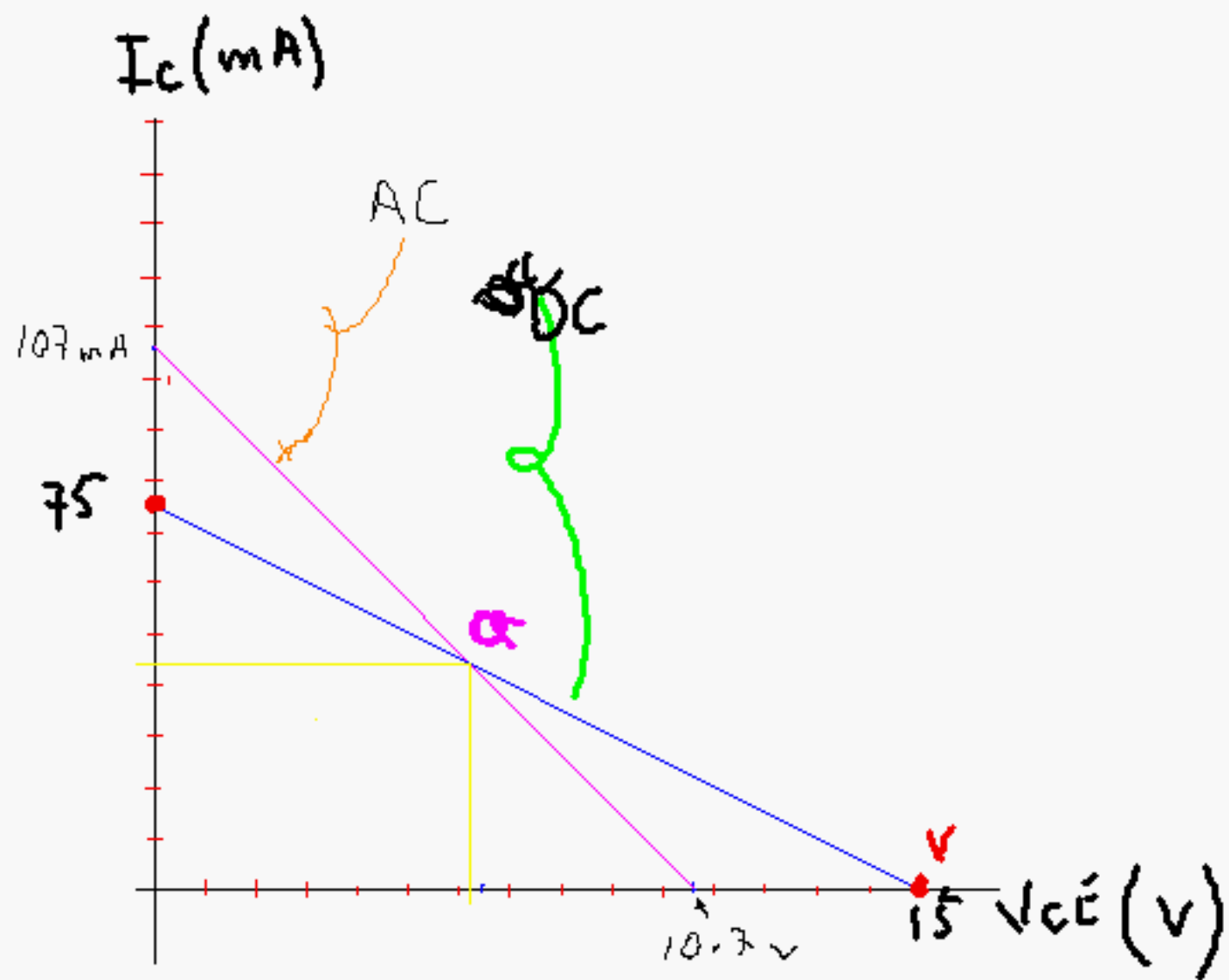
$$V_B = 5V$$

$$I_C \approx I_E = \frac{5V - 0.7}{100}$$

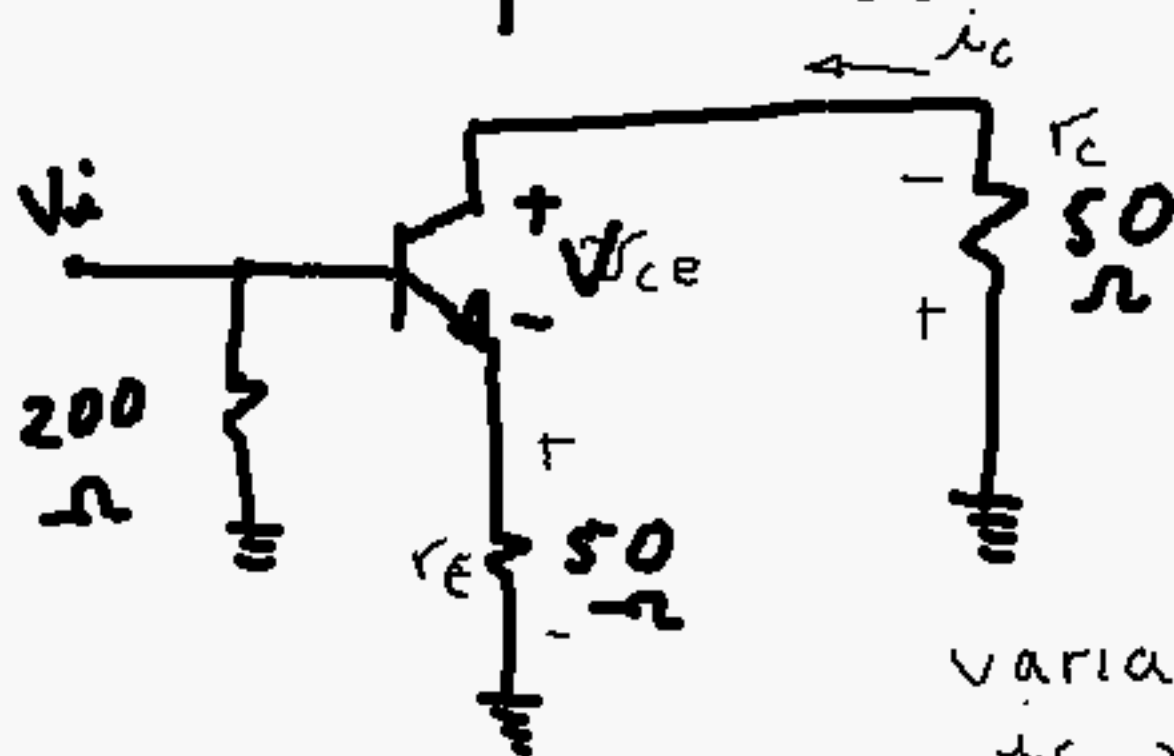
$$I_{CQ} = 43mA$$

$$V_{CEQ} = V_{CC} - I_{CQ} R_{L'} (200\Omega)$$

$$V_{CEQ} = 6.4V$$



Modelo equivalente



variaciones de
 i_c y V_{ce}

$$v_{ce} + i_c(r_e + r_c) = 0$$

$$i_c = - \frac{v_{ce}}{r_e + r_c}$$

$$i_c = I_C - I_{CQ}$$

$$v_{ce} = V_{CE} - V_{CEQ}$$

$$I_C - I_{CQ} = - \frac{V_{CE} - V_{CEQ}}{r_e + r_c}$$

despejando I_c

$$I_c = - \frac{V_{CE}}{r_E + r_c} + \frac{V_{CEQ}}{r_E + r_c} + I_{cQ}$$

para $I_c = 0$

$$\begin{aligned} V_{CE_{corte}} &= V_{CEQ} + I_{cQ}(r_E + r_c) \\ &= 6.4 + 43\text{mA}(100) \\ &= 10.7\text{V} \end{aligned}$$

Para $V_{CE} = 0$

$$I_{c_{sat}} = \frac{V_{CEQ}}{r_E + r_c} + I_{cQ} = \frac{6.4}{100} + 43\text{mA}$$

$$I_{c_{sat}} = 107\text{mA}$$

$$I_{sat} = 2 I_{CQ}$$

$$V_{CE\text{ corte}} = 2 V_{CEQ} \dots \textcircled{A}$$

considerando que

$$V_{CE\text{ corte}} = V_{CEQ} + I_{CQ}(r_E + r_C) \dots \textcircled{B}$$

Sustituyendo ~~A~~ en ~~A~~

$$2 V_{CEQ} = V_{CEQ} + I_{CQ}(r_E + r_C)$$

$$r_E + r_C = \frac{V_{CEQ}}{I_{CQ}}$$

Máxima potencia de salida (P_o)

$$P_{o(MAX)} = V_{rms} I_{rms} = \frac{V_{CEQ}}{\sqrt{2}} \frac{I_{CQ}}{\sqrt{2}}$$

$$P_{o(MAX)} = \frac{1}{2} V_{CEQ} I_{CQ}$$

Para el ejem.

$$P_o = 137.6 \text{ mW}$$

Disipación de potencia (P_D)

$$P_D = V_{CEQ} I_{CQ}$$

$$P_{oMAX} = \frac{1}{2} P_D$$

Para el ejemplo

$$P_D = 275 \text{ mW}$$

Eficiencia de salida (η)

Es la relación entre la potencia de salida de AB y la potencia de entrada de DC que se le proporciona al circuito colector-emisor.

$$\eta = \frac{P_o}{P_{DC}} \times 100$$

donde: $P_{DC} = V_{CC} I_{CQ}$

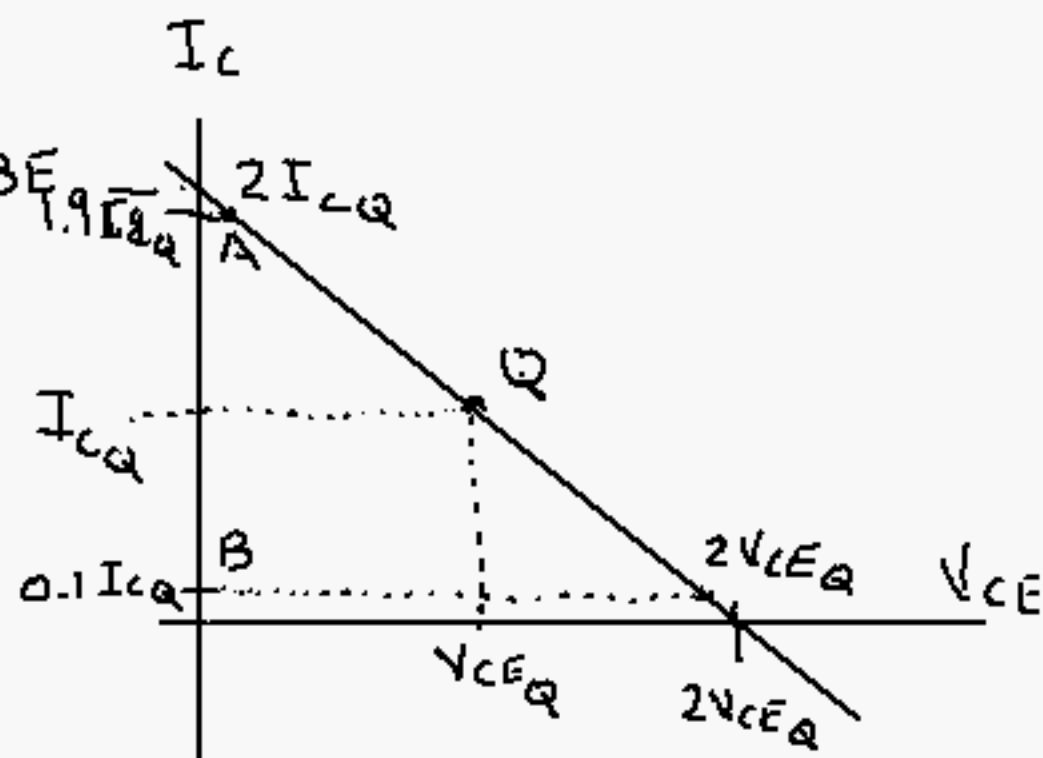
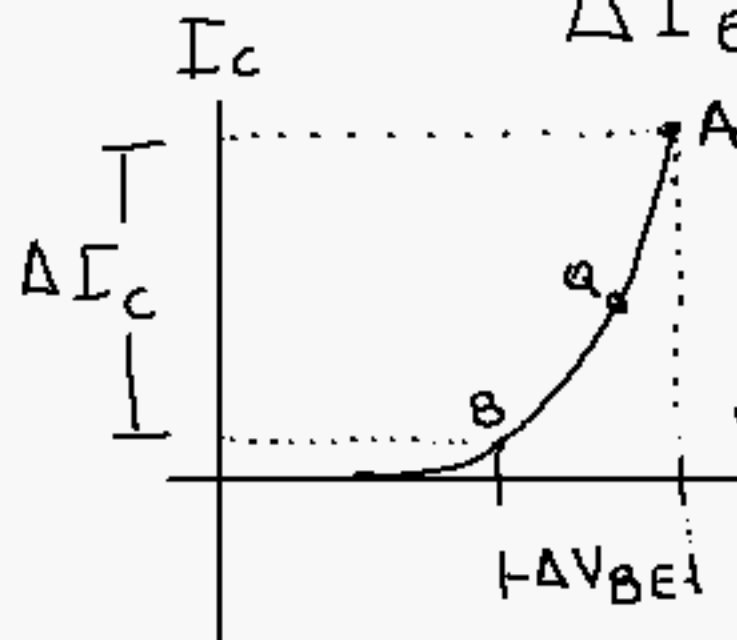
Para circuitos con doble fuente

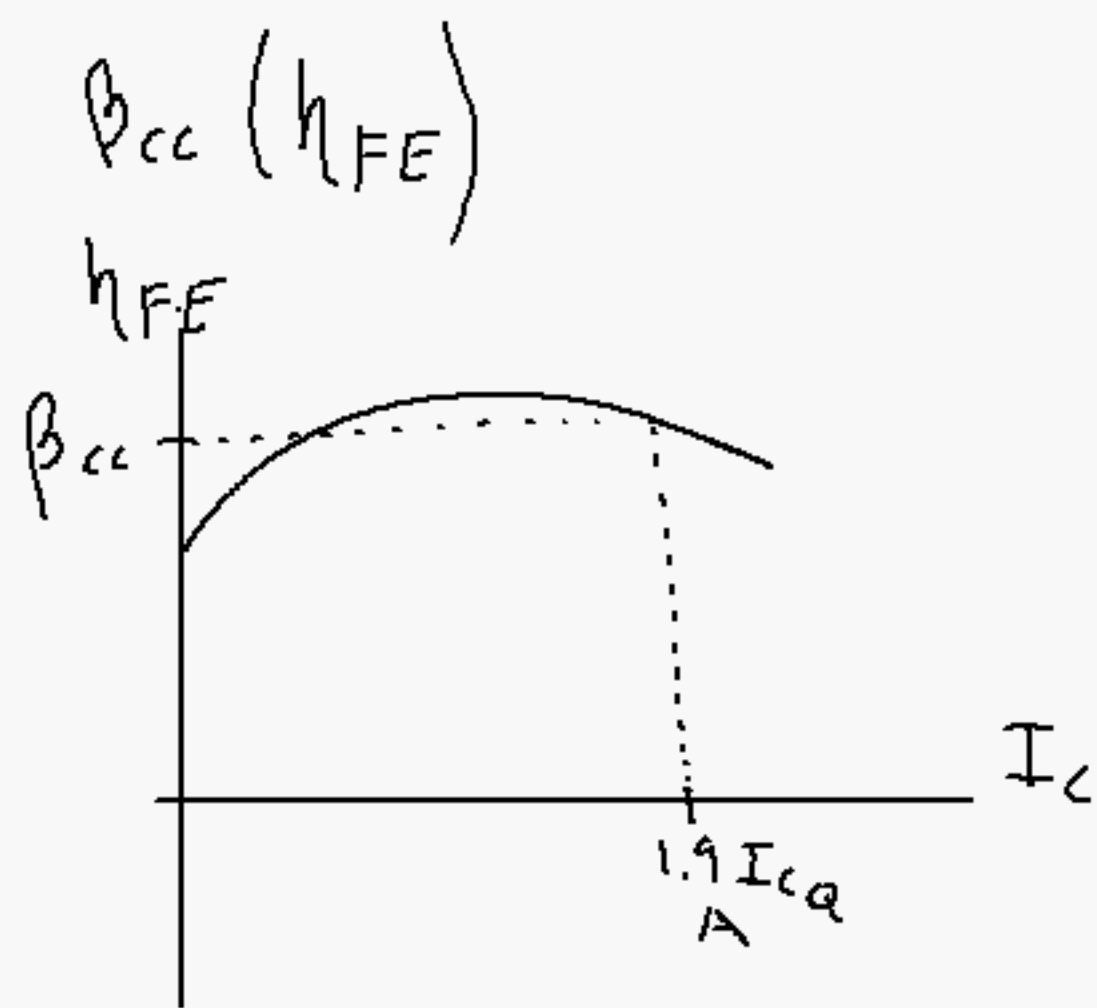
$$P_{DC} = (V_{CC} + V_{EE}) I_{CQ}$$

Ganancia e impedancia

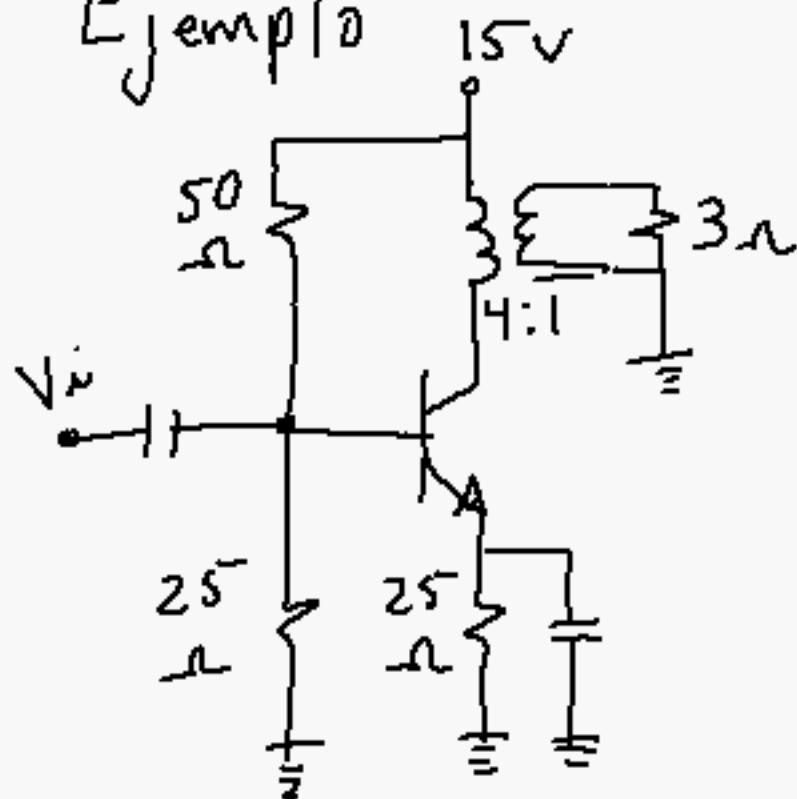
~~$$r_e = \frac{26\text{mV}}{I_E}$$~~

$$R_e r_e \frac{\Delta V_{BE}}{\Delta I_E} \cong \frac{\Delta V_{BE}}{\Delta I_C}$$





Ejemplo



✓ Transformador ideal

a) Recta de carga AC

b) Potencia de AC en

c primario de transf.

c) Potencia de AC en R_L

d) η e) P_D

$$a) I_{C_{SAT}} = I_{CQ} + \frac{V_{CEQ}}{r_E + r_L}$$

$$V_{CE_{CORTE}} = V_{CEQ} + I_{EQ}(r_E + r_L)$$

$$V_B = \frac{25}{75}(15) = 5V$$

$$I_E = \frac{5 - 0.7}{25} = 172 \text{ mA}$$

$$I_C \approx I_E = 172 \text{ mA} = I_{CQ}$$

$$V_{CE} = V_{CC} - I_C(R_C + R_E)$$

$$V_{CE} = 15 - 172 \text{ mA}(25)$$

$$V_{CEQ} = 10.7 \text{ V}$$

$$I_{L\text{ SAT}} = 172 \text{ mA} + \frac{10.7}{48} = 394.9 \text{ mA}$$

$$V_C = \frac{(4)^2}{(43)^2} (3)$$

$$n = \frac{N_P}{N_S} = \frac{4}{1}$$

$$V_C = 48 \text{ V}$$

$$\frac{N_P}{N_S} = \frac{V_P}{V_S} = \frac{I_S}{I_P} = \frac{\frac{V_S}{R_S}}{\frac{V_P}{R_P}}$$

$$\begin{aligned} V_P &= I_P R_P \\ \frac{V_P}{V_S} &= \frac{I_P R_P}{I_S R_S} \\ \frac{V_P}{V_S} &= \frac{I_S R_P}{V_P R_S} \end{aligned}$$

$$\Rightarrow \left(\frac{V_P}{V_S} \right)^2 = \frac{R_P}{R_S}$$

$$R_P = \left(\frac{V_P}{V_S} \right)^2 R_S = n^2 R_S$$

$$V_{CE\text{CORT}} = 10.7 \text{ V} + 172 \text{ mA} (40)$$

$$V_{CE\text{CORT}} = 18.97 \text{ V}$$



b) Potencia en primario ^{AC}

$$P_o = \frac{V_{CEQ} I_{CQ}}{2} = \frac{(10.7)(172 \text{ mA})}{2}$$

$$P_o = 0.92 \text{ W}$$

c) Potencia de AC en secundario

Para transformador ideal

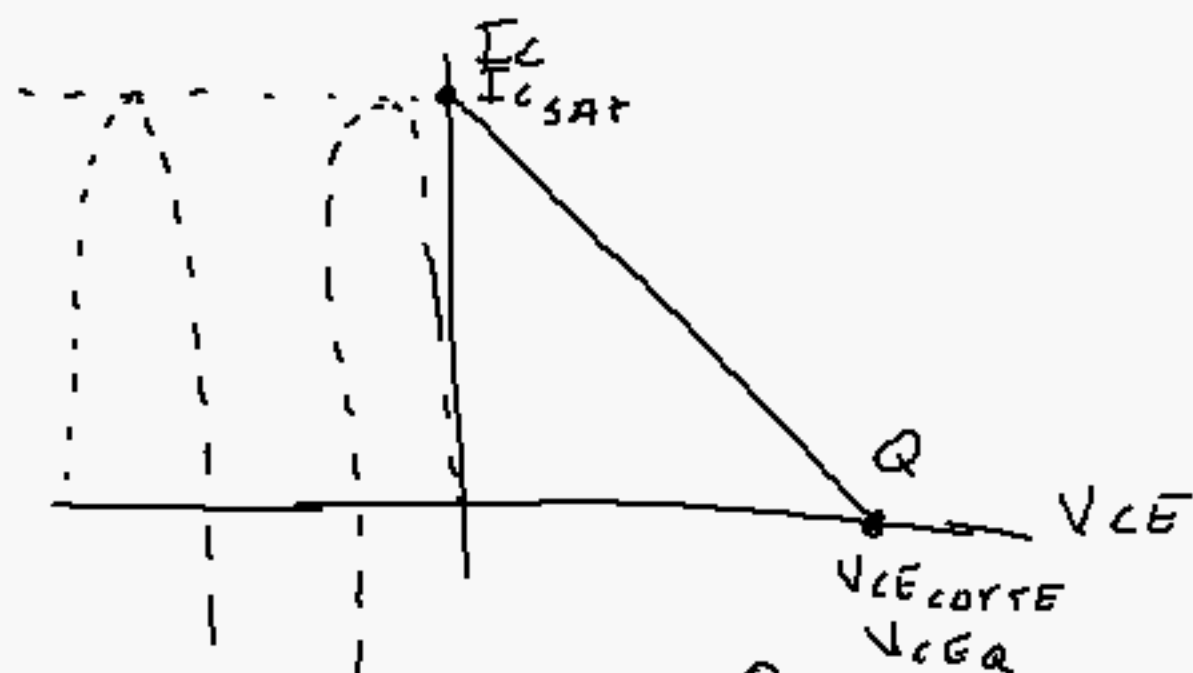
$$P_s = P_p = 0.92 \text{ W}$$

$$d) \eta = 35.65\%$$

$$e) P_D = 1.84 \text{ W}$$

Amplificadores clase B en oposición de fase

- P_D es la quinta parte de la potencia de carga
- Consumo de corriente sin señal de aproximadamente 1% de I_{csat}



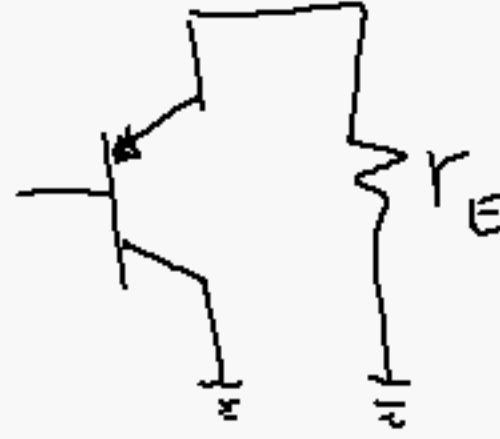
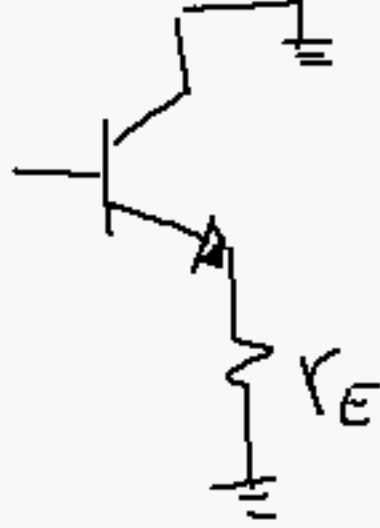
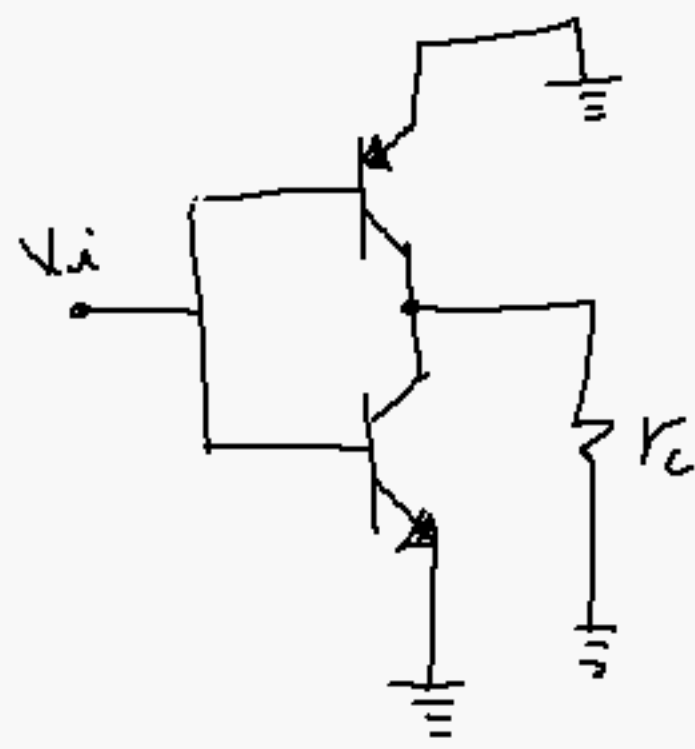
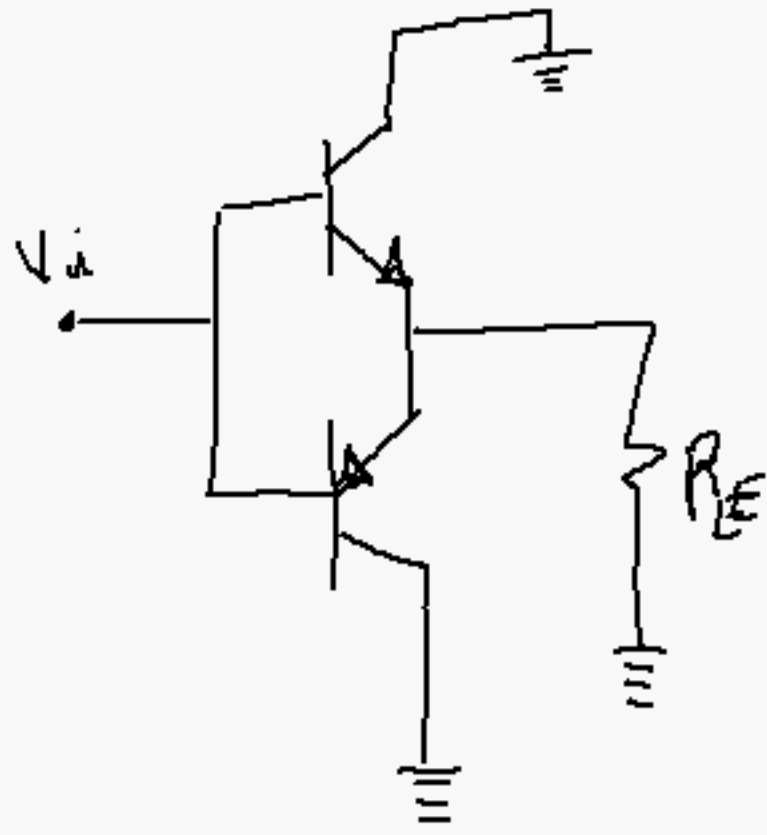
$$I_{CQ} = 0$$

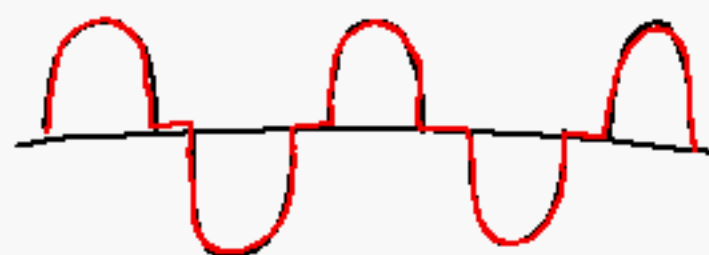
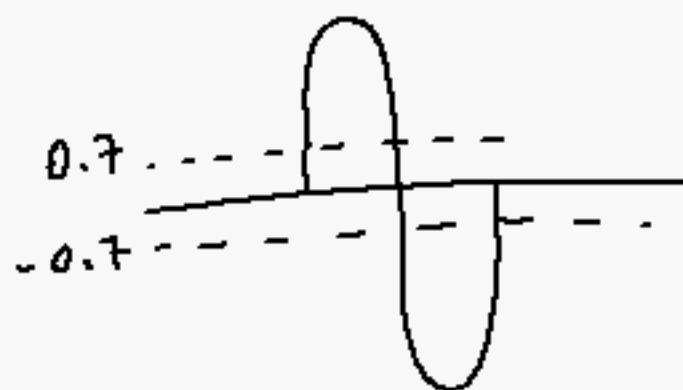
$$V_{CE_CORTE} = V_{CEQ} + I_{CQ}(r_E + r_C)$$

$$V_{CE_CORTE} = V_{CEQ}$$

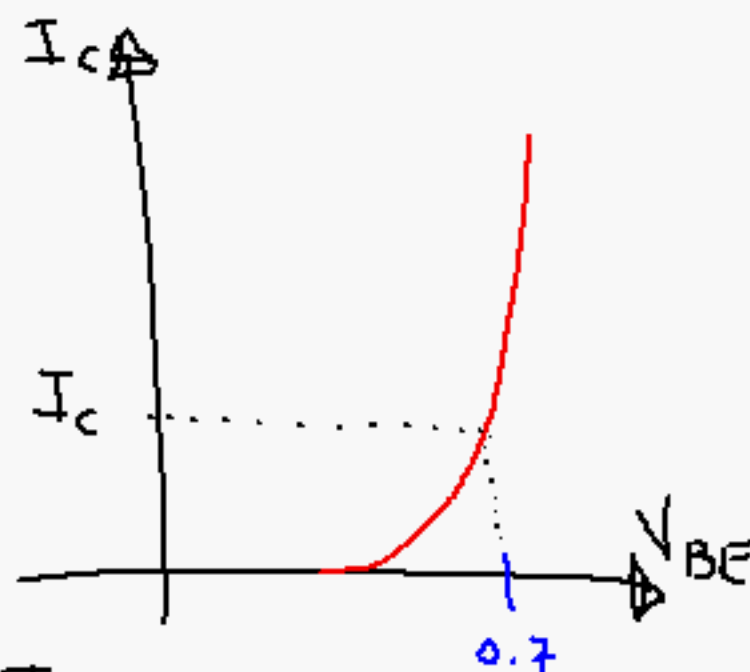
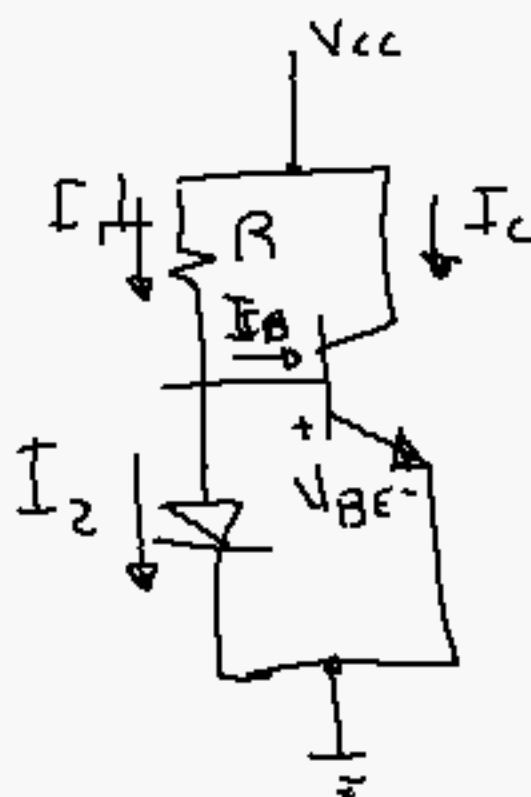
$$I_{C_sat} = I_{CQ} + \frac{V_{CEQ}}{r_E + r_C}$$

$$I_{C_sat} = \frac{V_{CEQ}}{r_E + r_C}$$





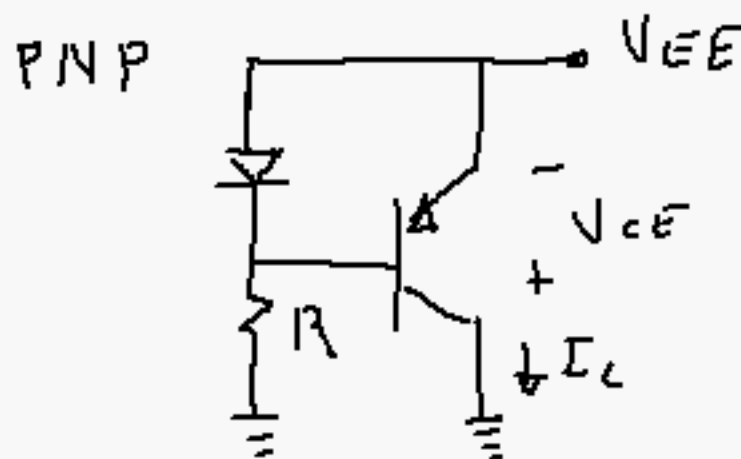
Circuito espejo de corriente



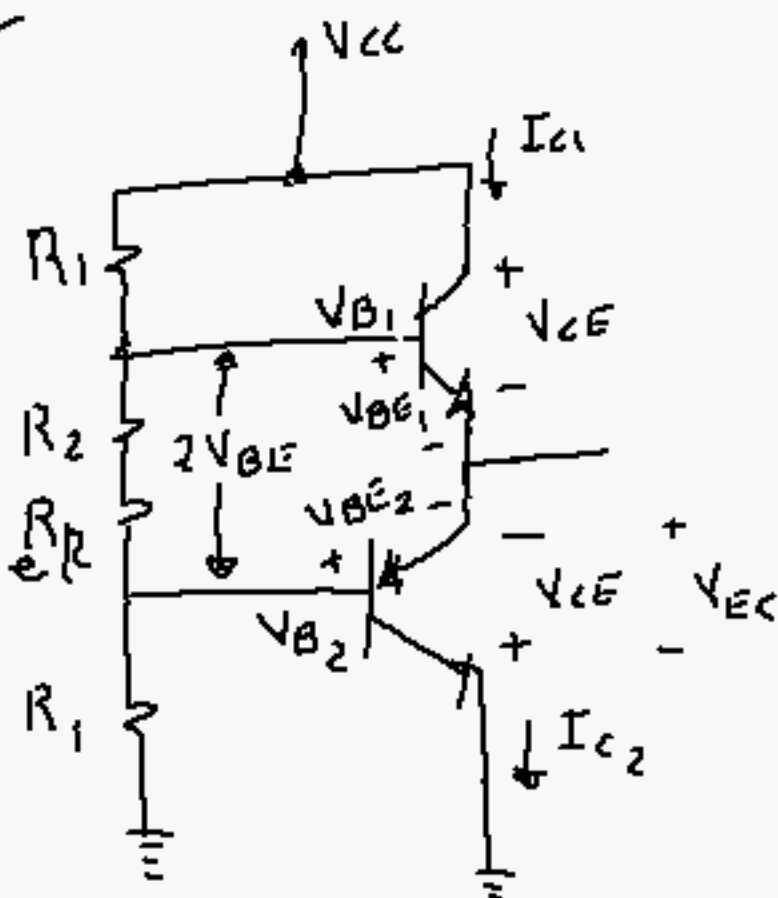
$$I_2 = I_C$$

$$I_2 \gg I_B$$

$$I_2 = I_2 + I_B \Rightarrow I_1 \approx I_2$$



Punto de operación para el amplificador clase B



$$V_{CE} = \frac{1}{2} V_{CC} = \frac{1}{2} V_{CC}$$

$$V_{BE1} = V_{BE2} = 0.7 \text{ V}$$

$$V_{BE2} = -0.7 \text{ V}$$

$$V_{BE} = V_B - V_E$$

$$V_{B1} = V_{BE1} + V_{E1}$$

pero $V_{E1} = V_{E2} = V_{EC2} = V_{CE1}$

$$V_{B1} = 0.7 + \frac{1}{2} V_{CC}$$

$$V_{B2} = V_{BE2} + V_{E2}$$

$$V_{B2} = -0.7 + \frac{1}{2} V_{CC}$$

$$V_{B_1} - V_{B_2} = 0.7 + \frac{1}{2}V_{CC} - \left(-0.7 + \frac{1}{2}V_{CC}\right)$$

$$V_{B_1} - V_{B_2} = 2(0.7) = 2|V_{BE}|$$

$$V_{R_1} = I_{R_1}R_1 = V_{CC} - V_{B_1} = V_{CC} - 0.7 - \frac{1}{2}V_{CC}$$

$$V_{R_1} = \frac{1}{2}V_{CC} - 0.7 = V_{B_2}$$

$$I_{R_1} = \frac{\frac{1}{2}V_{CC} - 0.7}{R_1} = \frac{V_{CC} - 2(0.7)}{2R_1}$$

$$I_{R_1} = \frac{V_{CC} - 2V_{BE}}{2R_1}$$

$$I_{R_1} = I_{C_r}$$

$$2V_{BE} = 2R_2 I_{C_r}$$

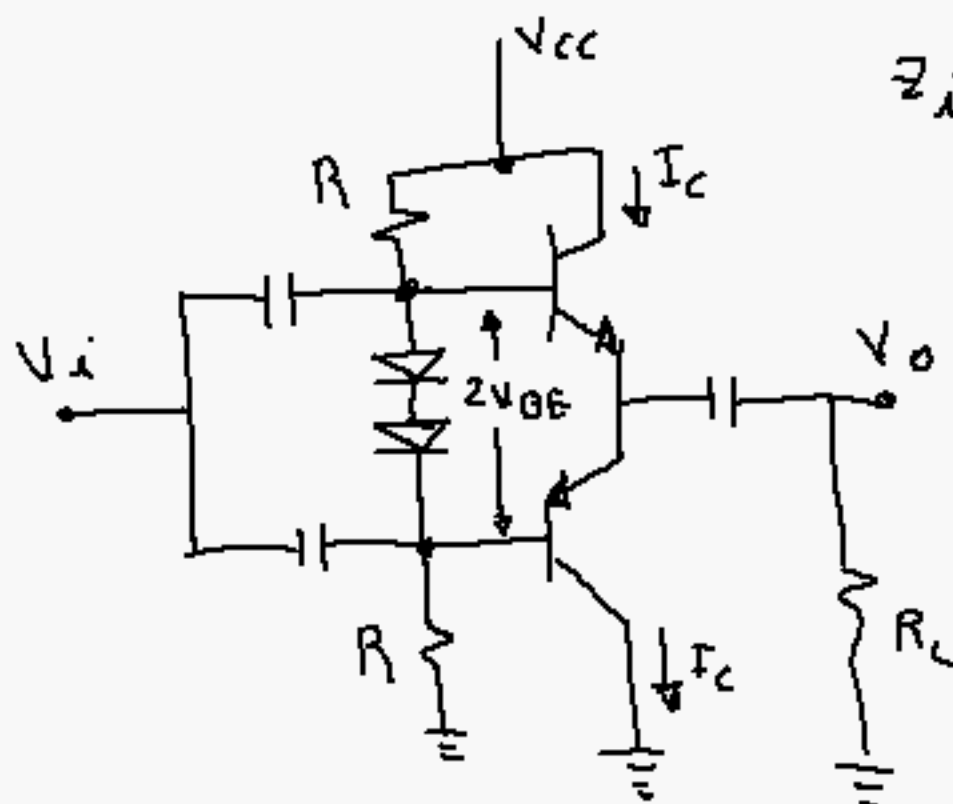
$$R_2 = \frac{V_{BE}}{I_{C_r}}$$

$$I_{Cr} = (1\% - 5\%) I_{Csat}$$

$$I_{Csat} = \frac{V_{CEQ}}{r_E + r_C}$$

$$r_E = R_L$$

Polarización por diodos



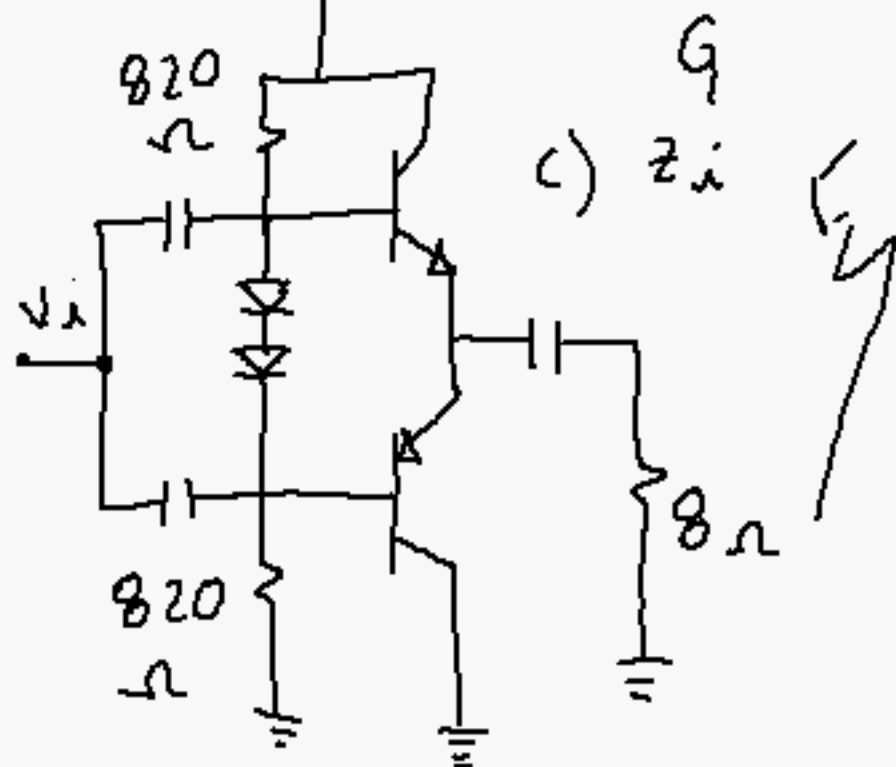
$$Z_i = R \parallel R \parallel (h_{FE}(r_E + R_e))$$

$$A_v = \frac{r_E}{r_E + R_e} = \frac{R_L}{R_L + R_e}$$

Ganancia en potencia

$$G = h_{FE} \left(\frac{R_L}{R_L + R_e} \right)$$

Ejemplo: a) I_{C_r}
 20V b) A_v



$$h_{FE} = 60$$

$$R_e = 0.5 \Omega$$

$$a) I_R = I_{C_r} = \frac{V_{CC} - 2V_{BE}}{2R}$$

$$I_{C_r} = 11.3 \text{ mA} \approx \frac{1}{10} I_{C_{sat}}$$

$$I_{C_{sat}} = \frac{V_{CC} R_e}{r_E + R_c} = \frac{10}{8}$$

$$I_{C_{sat}} = 1.25 \text{ A}$$

$$b) A_v = \frac{R_L}{R_L + R_e} = 0.94$$

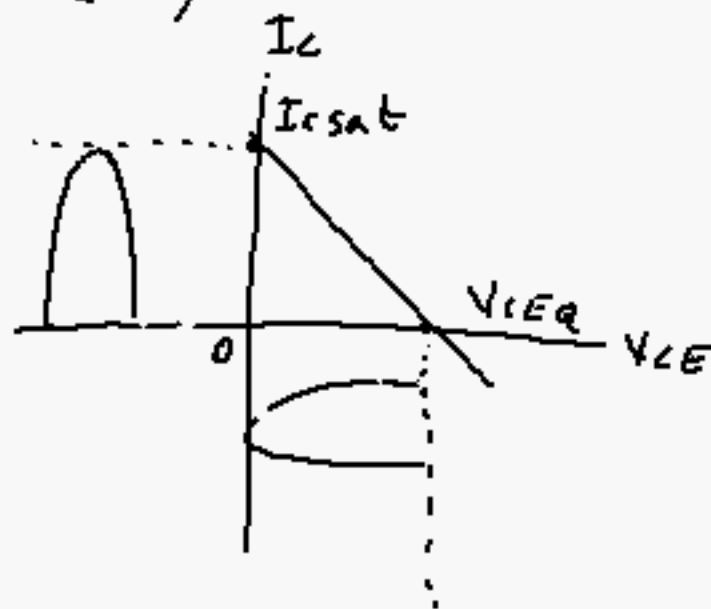
$$G = h_{FE} A_v = 56.4$$

$$c) z_i = \frac{1}{2} R \parallel h_{FE} (r_E + R_e)$$

$$z_i = 227.21 \Omega$$

Potencia de salida (P_o)

$$P_{o\text{ MAX}} = \frac{V_{CEQ} I_{C\text{ sat}}}{2}$$

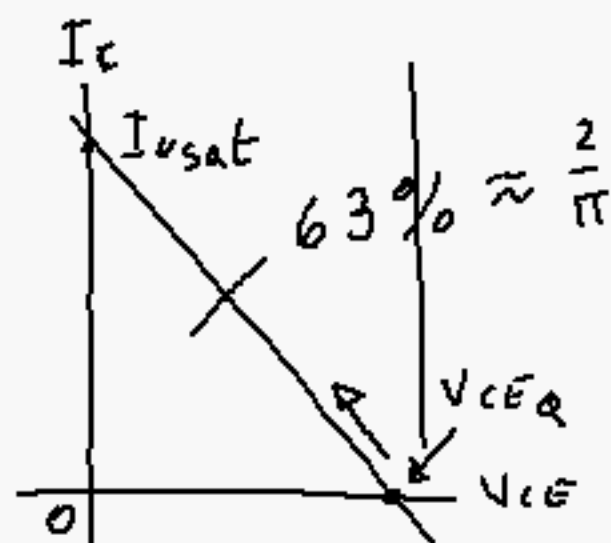


Eficiencia (η)

$$\eta = \frac{P_o}{P_{DC}} \times 100 \quad P_{DC} = V_{CC} \frac{I_{C\text{ sat}}}{\pi} \quad \text{pero } V_{CEQ} = \frac{1}{2} V_{CC}$$

$$\eta = \frac{\frac{V_{CEQ} I_{C\text{ sat}}}{2}}{\frac{V_{CC} I_{C\text{ sat}}}{\pi}} = \frac{\frac{V_{CC} I_{C\text{ sat}}}{4}}{\frac{V_{CC} I_{C\text{ sat}}}{\pi}} = \frac{\pi}{4} = 0.785 \Rightarrow 78.5\%$$

Potencia disipada (P_D)



$$P_{D_{MAX}} = \frac{\left(\frac{2}{\pi} \frac{V_{CEQ}}{\sqrt{2}}\right) \left(\frac{2}{\pi} \frac{I_{C_{sat}}}{\sqrt{2}}\right)}{2}$$

$$P_{D_{MAX}} = \frac{V_{CEQ} I_{C_{sat}}}{\pi^2}$$

$$P_{D_{MAX}} \approx \frac{V_{CEQ} I_{C_{sat}}}{10}$$

Si $P_o = \frac{V_{CEQ} I_{C_{sat}}}{2}$

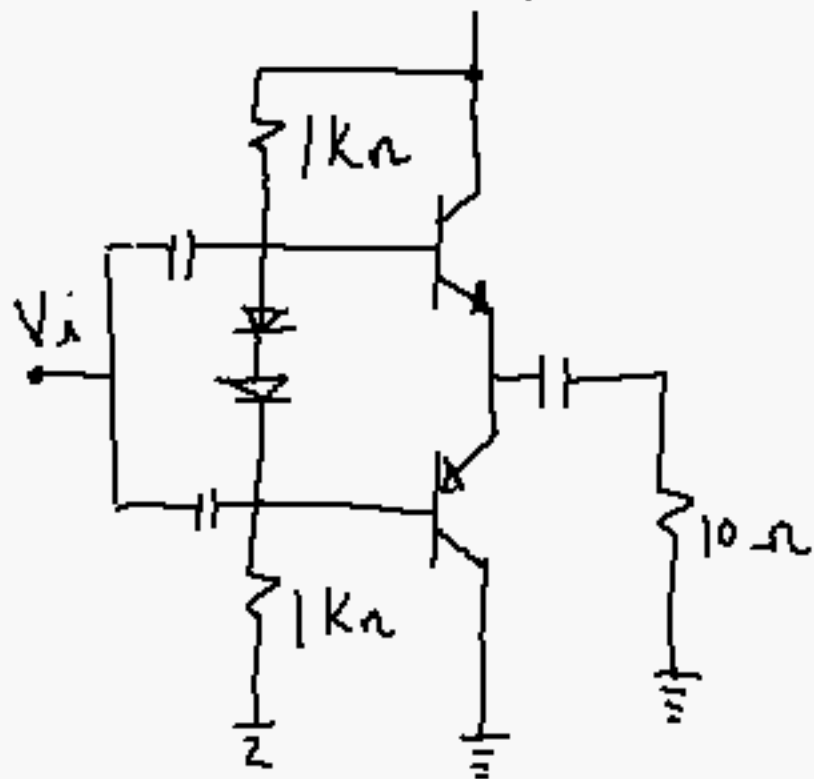
\Rightarrow

$$P_D = \frac{P_o}{5}$$

entonces

$$P_{D_{MAX}} = \frac{P_o}{5}$$

Ejemplo
40V



Obtener $P_{o\max}$, $P_{D\max}$
 $P_{o\max}$
 $P_{D\max}$
 η

$$P_{o\max} = \frac{V_{CEQ} I_{C\text{sat}}}{2}$$

$$V_{CEQ} = \frac{1}{2} V_{CC} = \frac{40}{2} = 20$$

$$I_{C\text{sat}} = \frac{V_{CEQ}}{r_E}$$

$$P_{o\max} = \frac{V_{CEQ}^2}{2 r_E} = \frac{(20)^2}{2(10)}$$

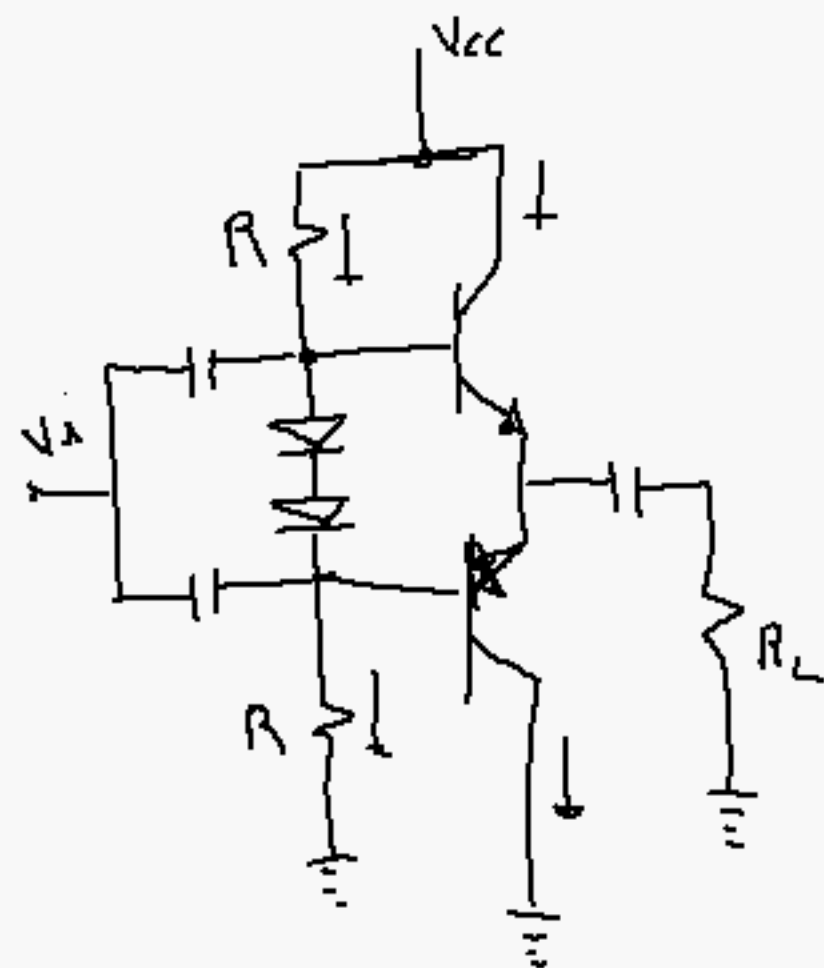
$$P_{o\max} = 20 \text{ W}$$

$$P_{D\max} = \frac{20}{5} = 4 \text{ W}$$

$$\eta = 78.5\%$$

Ejemplo

Diseñar un amplificador clase B en oposición de fase de 25 W de salida para una carga de 8 Ω .



$$P_o = \frac{V_{CEQ} I_{Csat}}{2}$$

$$I_{Csat} = \frac{V_{CEQ}}{R_L} = \frac{V_{CEQ}}{8} = 2.5 \text{ A}$$

$$P_o = \frac{V_{CEQ}^2}{2 R_L} \quad \text{pero } V_{CEQ} = \frac{1}{2} V_{CC}$$

$$P_o = \frac{V_{CC}^2}{8 R_L} \Rightarrow \boxed{V_{CC} = 40 \text{ V}}$$

$$I_{Csat} = \frac{V_{CEQ}}{R_L} = \frac{20}{8} = 2.5 \text{ A}$$

$$I_{C_r} = (2.5\%) I_{Csat} = 62.5 \text{ mA}$$

$$I_{C_r} = \frac{V_{CC} - 2V_{BE}}{2R}$$

$$R = 308.8 \Omega$$

$$P_{D_{max}} = \frac{25}{5} = 5 \text{ W}$$

$$h_{FE} = 70$$

$$A_v = \frac{I_o}{I_i} \cong h_{FE} = 70$$

$$I_i = \frac{2.5}{70} = 35.7 \text{ mA}$$

Ejemplo: Obtener

- P_O y P_D
- I_{CQ} en la etapa de salida
- A_v total considerando $\beta_{CC} = 100$ para todos los transistores y una $R_e = 1\Omega$
- Estimar la amplitud máxima de salida y amplitud máxima de entrada de la señal de AC.

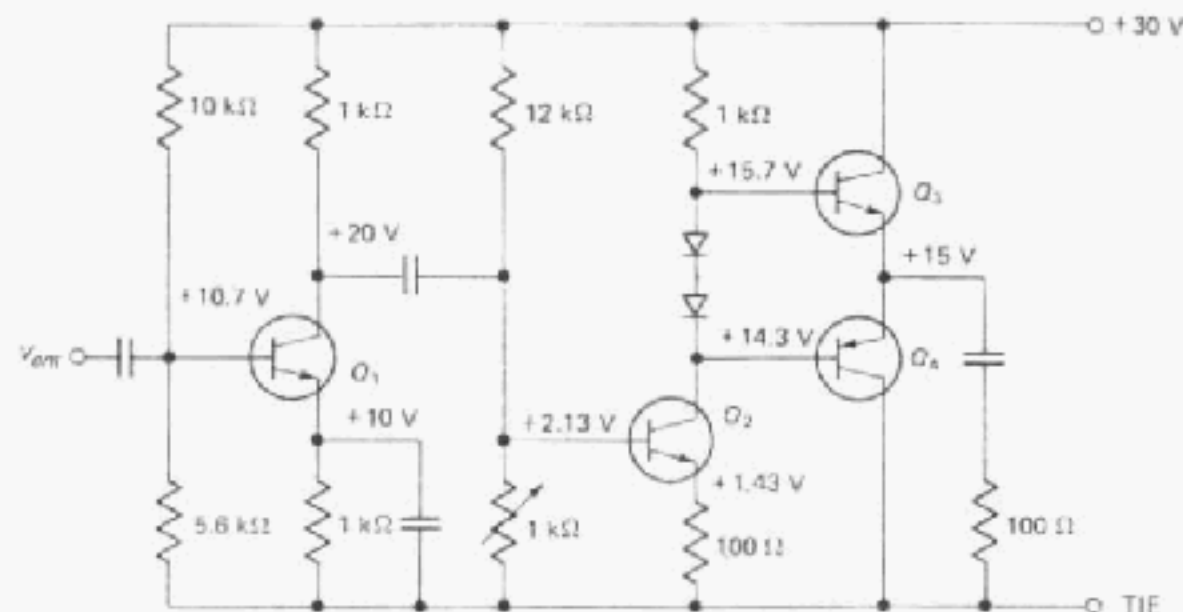


Figura 11-16. Ejemplo de un amplificador completo.

Solución

Datos: $h_{FE} = 100$, $R_E = 1 \Omega$

a) P_o , P_D

$$P_o = \frac{V_{CEQ} I_{C \text{ sat}}}{2} = \frac{V_{CEQ}^2}{2 R_E} = \text{pero } V_{CEQ} = \frac{1}{2} V_{CC}$$

$$P_o = 1.125 \text{ W}$$

$$P_D = \frac{1.125}{.5} = 225 \text{ mW}$$

b) $I_{C_r} = \frac{1.43}{100} = 14.3 \text{ mA}$

c) $A_v = \frac{1 \text{ k}\Omega \parallel 12 \text{ k}\Omega \parallel 1 \text{ k}\Omega \parallel 100(100) +}{2.6}$

$$A_v = 136$$

$$I_{R_A} = \frac{10}{1000} = 10 \text{ mA}$$

$$r_e = \frac{26 \text{ mV}}{10 \text{ mA}} = 2.6 \Omega$$

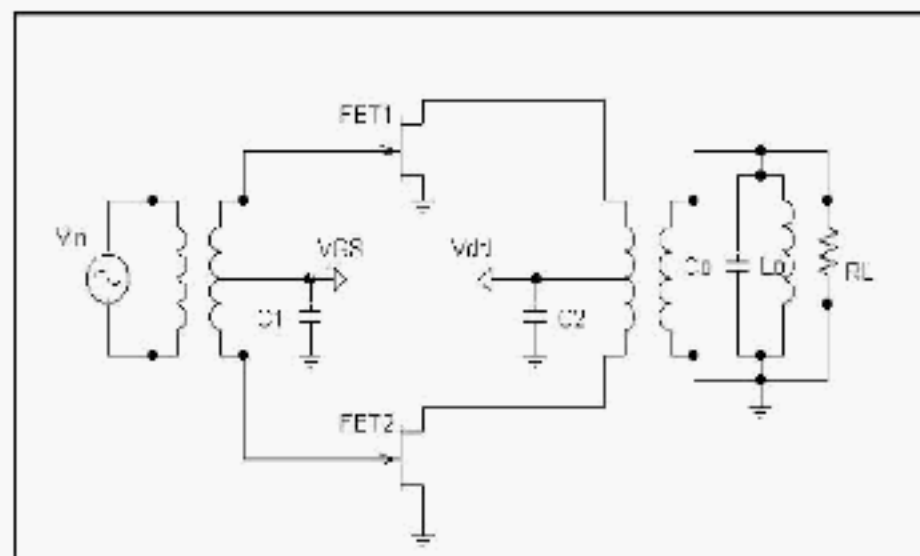
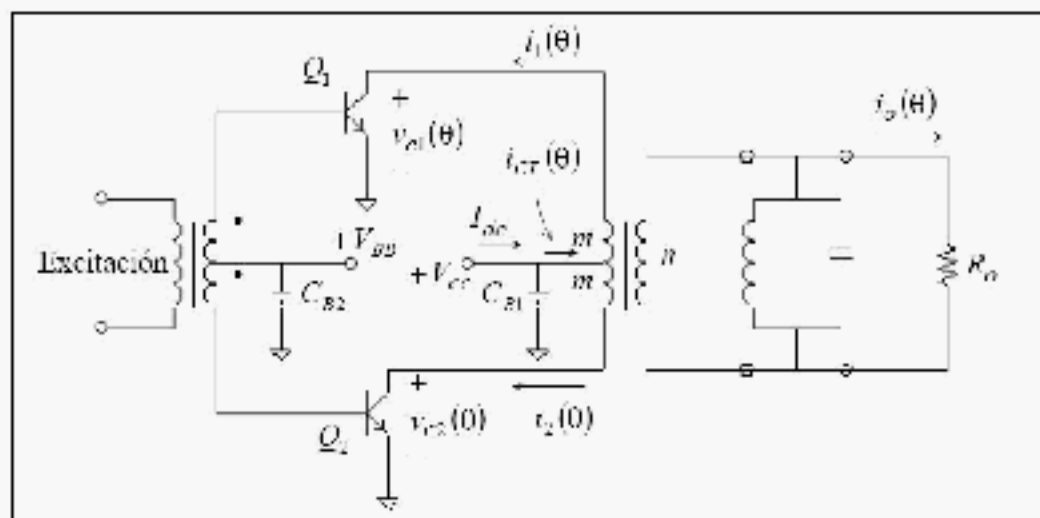
$$A_2 = \frac{r_c}{r_E} = \frac{1k\Omega \parallel 100(1+100)}{1+100} = 9$$

$$A_3 = \frac{R_L}{R_L + R_E} = \frac{100}{100+1} = 0.99$$

$$A_v = A_1 A_2 A_3 = 1568$$

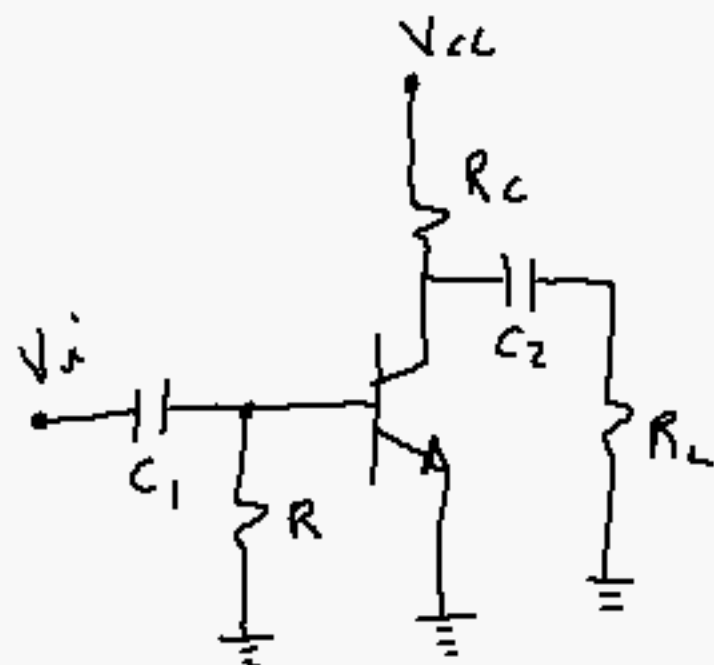
d) $V_{CEQ} = \frac{1}{2} V_{CC} = 15V$ (Salida máx)

$$V_o = V_i A_v \Rightarrow V_i = \frac{V_o}{A_v} = 9.57mV$$

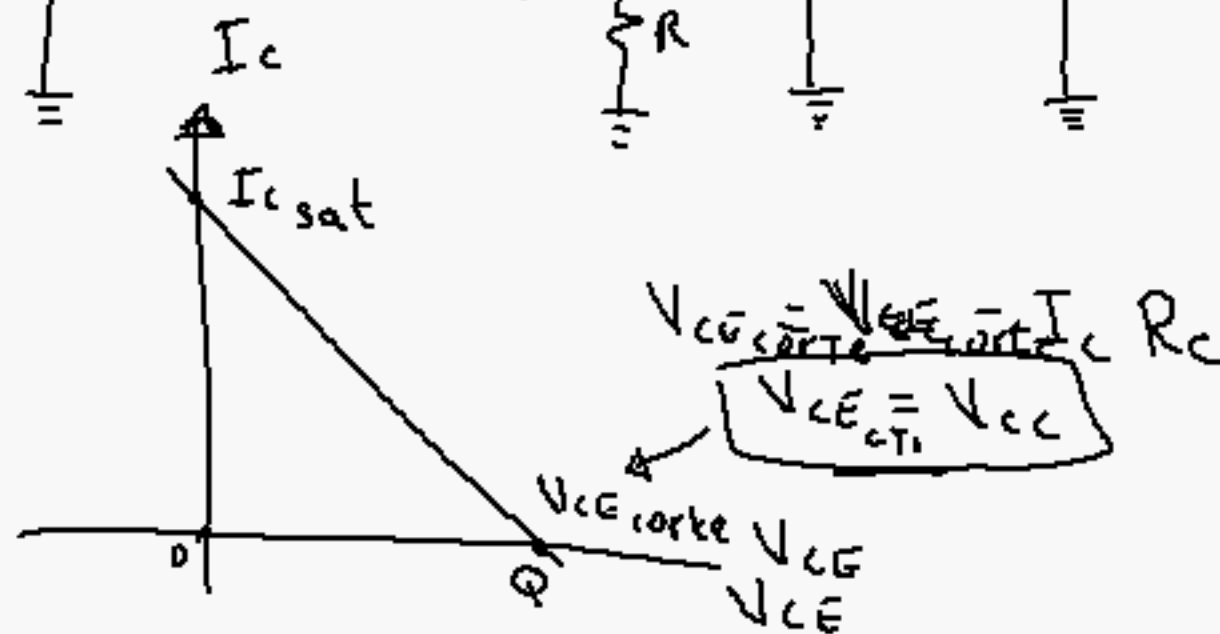
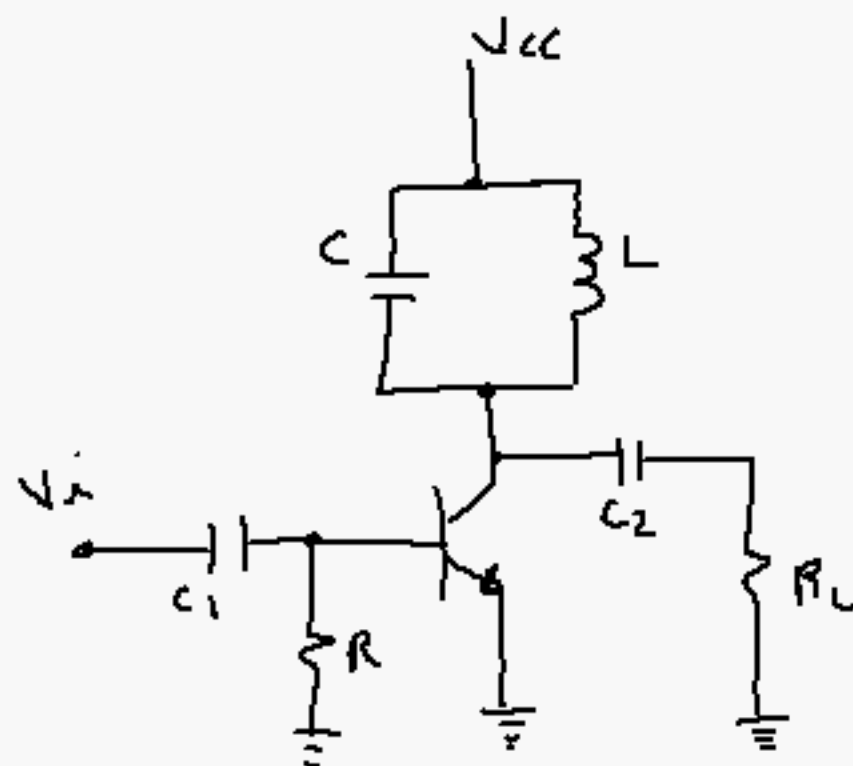


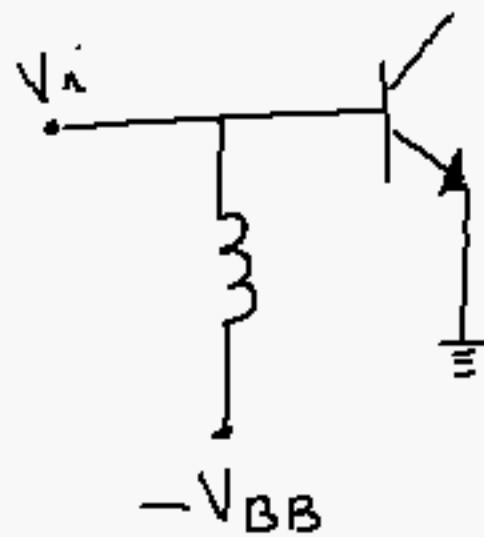
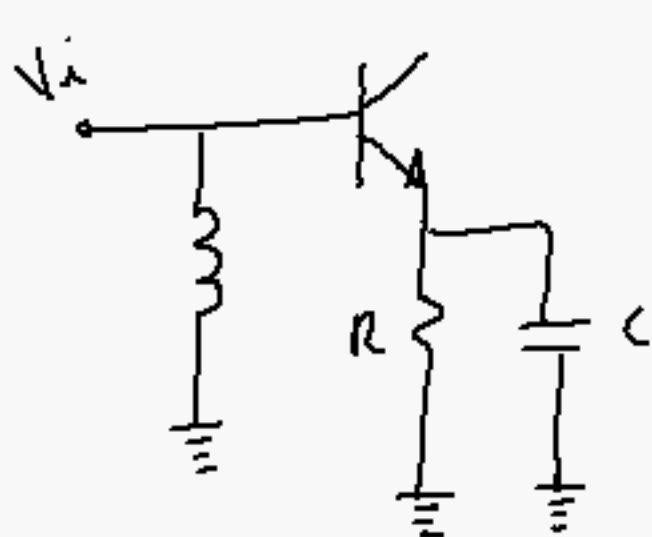
Amplificadores clase C

- la corriente del colector circula menos de 180° de la señal de AC

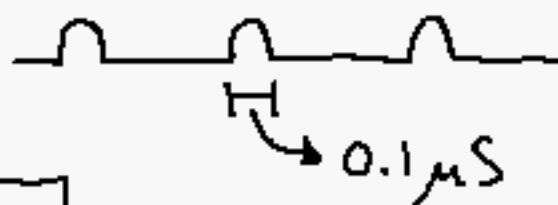
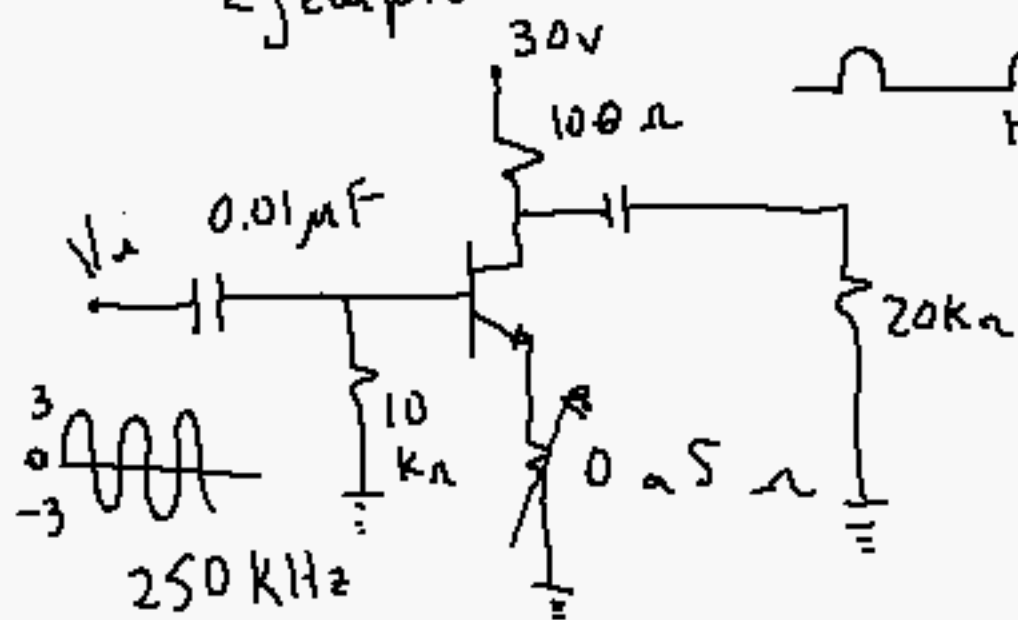


$$I_{c\text{sat}} = \frac{V_{CC} \beta_Q}{r_C}$$



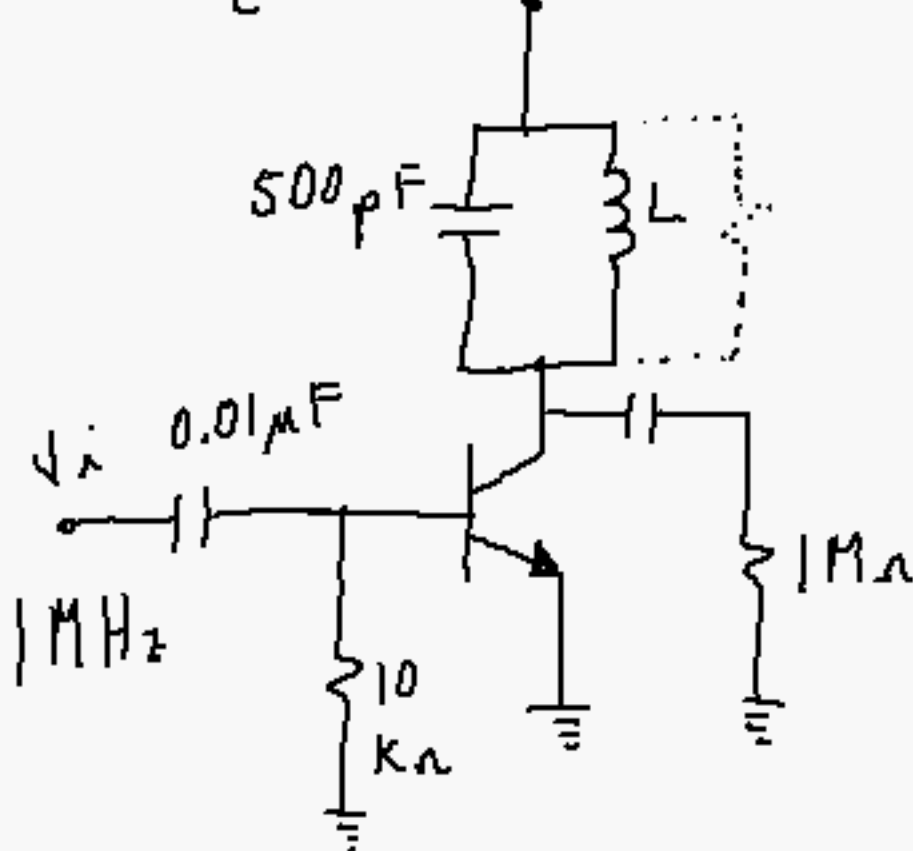


Ejemplo:



- Recta de carga
- CT de la forma de onda de salida.
- Dibujar forma de onda de la base del tr.

Ejemplo: 20V



a) Obtener el valor de L para 1 MHz

b) Si el inductor tiene una resistencia serie de 10Ω a 1 MHz, obtener la Q del circuito.

Solución

$$a) L = \frac{1}{4 \pi^2 f^2 C}$$

$$L = 50.66 \mu H$$

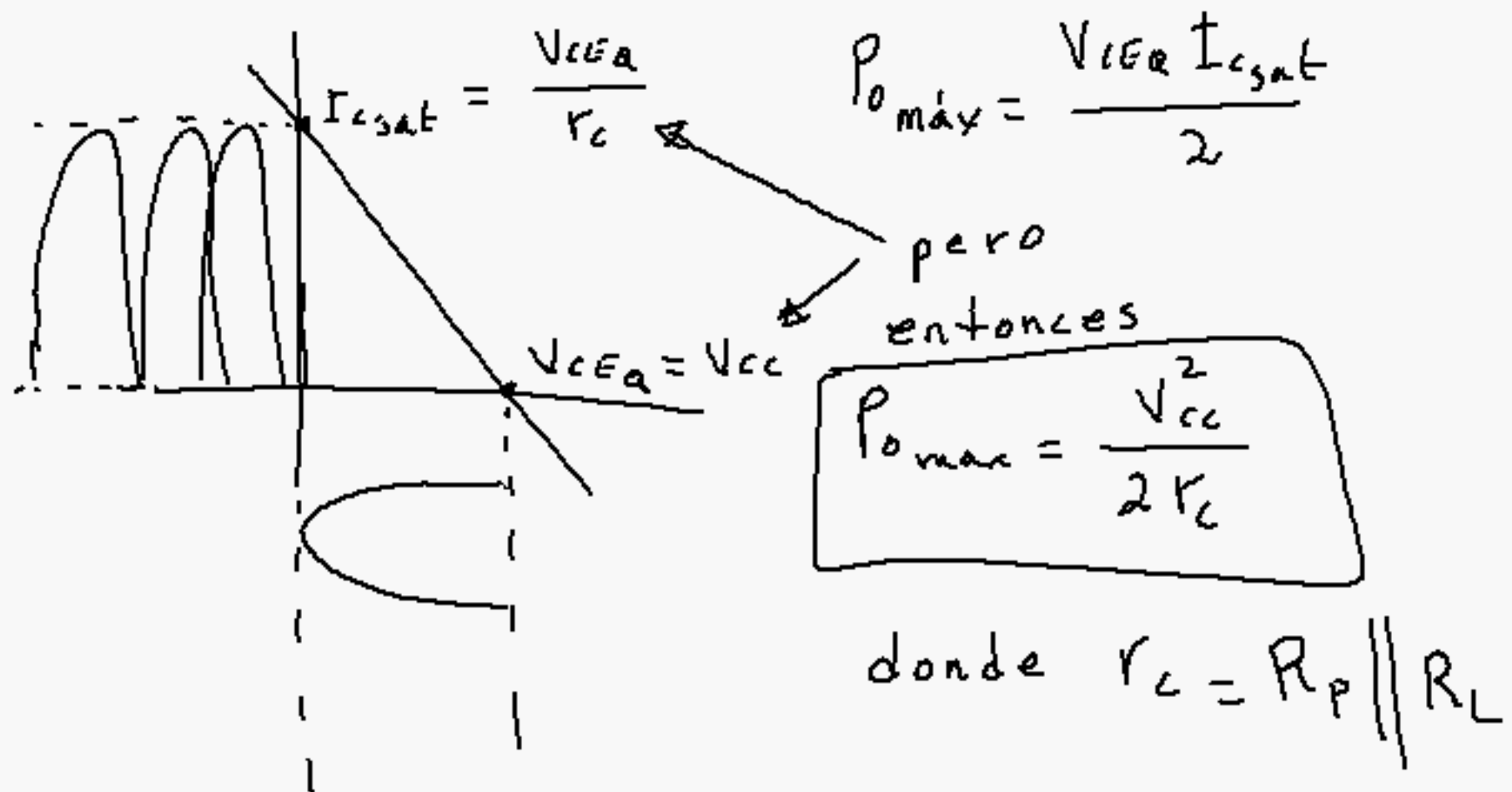
$$b) Q_L = \frac{\omega L}{R_S}$$

$$Q_L = \frac{R_P}{\omega L} \Rightarrow R_P = Q \omega L$$

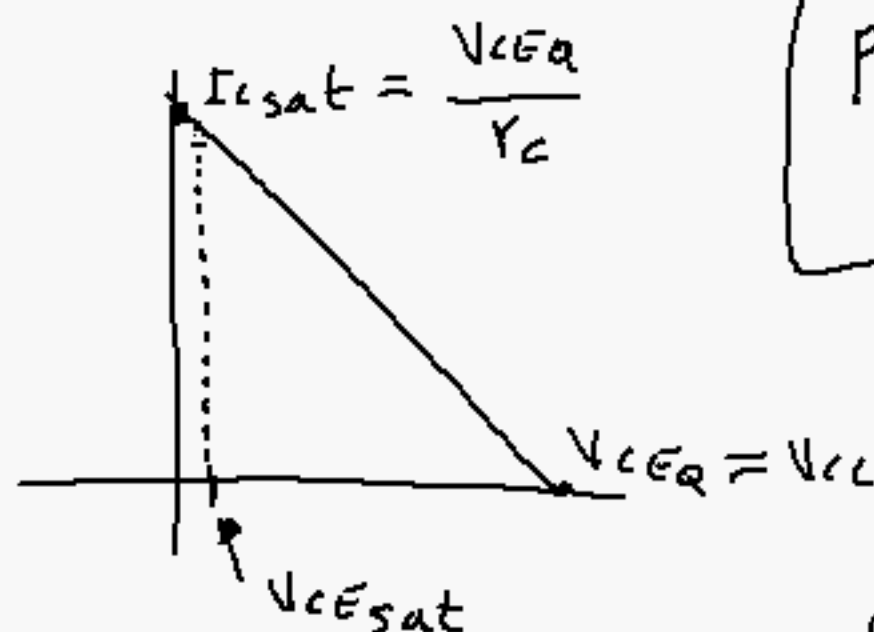
$$Q = \frac{R_{sh}}{\omega L}$$

$$R_{sh} = R_P || R_L$$

Potencia de salida



Potencia disipada



$$P_D \approx \frac{V_{CEsat} V_{CC}}{2 r_c}$$

Potencia disipada mínima

Peor caso, potencia de disipación máxima (50% de la recta de carga)

$$P_D = \frac{I_{sat} V_{CC}}{2\sqrt{2} \cdot 2\sqrt{2}} = \frac{I_{sat} V_{CC}}{8}$$

$$P_D = \frac{V_{CC}^2}{8 r_c}$$

$$\frac{P_D}{P_{O_{max}}} = \frac{\frac{V_{CEsat} V_{CC}}{2R_C}}{\frac{V_{CC}^2}{2R_C}} = \frac{V_{CEsat}}{V_{CC}}$$

por lo que:

$$P_D = \frac{V_{CEsat}}{V_{CC}} P_{O_{max}}$$

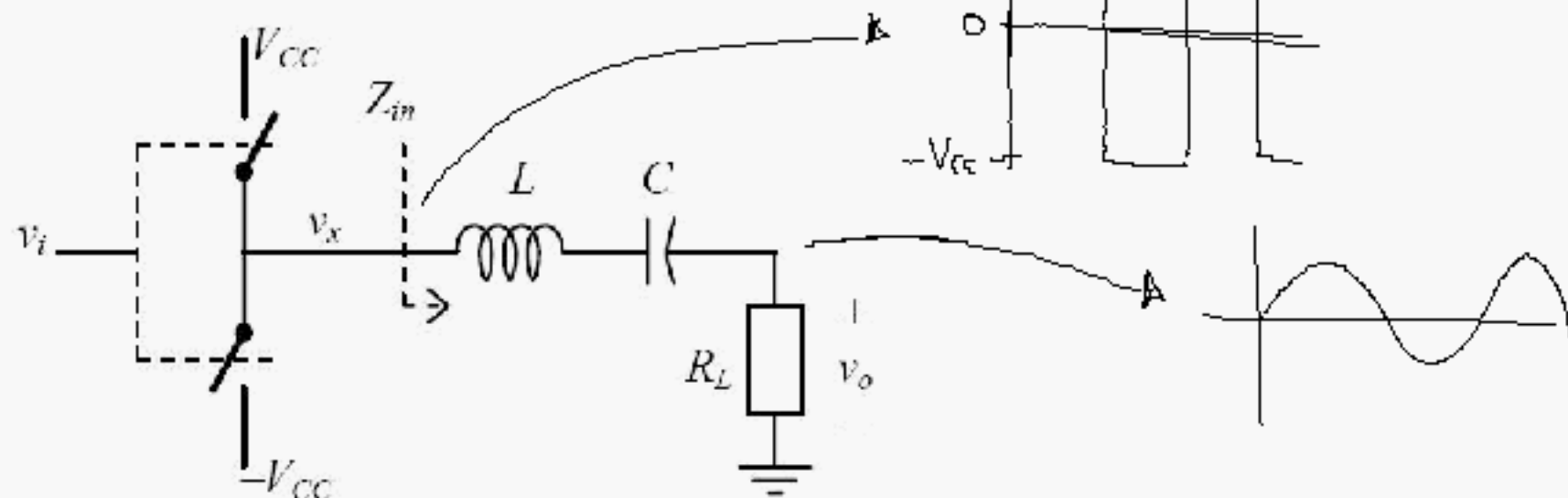
Eficiencia

$$P_{DC} = P_{O_{max}} + P_D$$

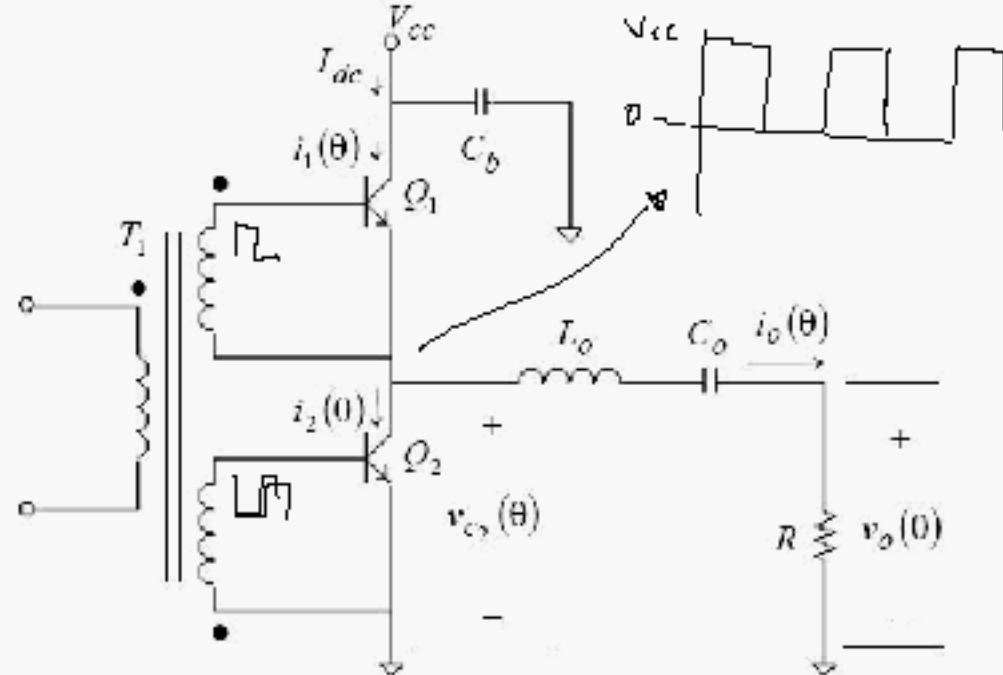
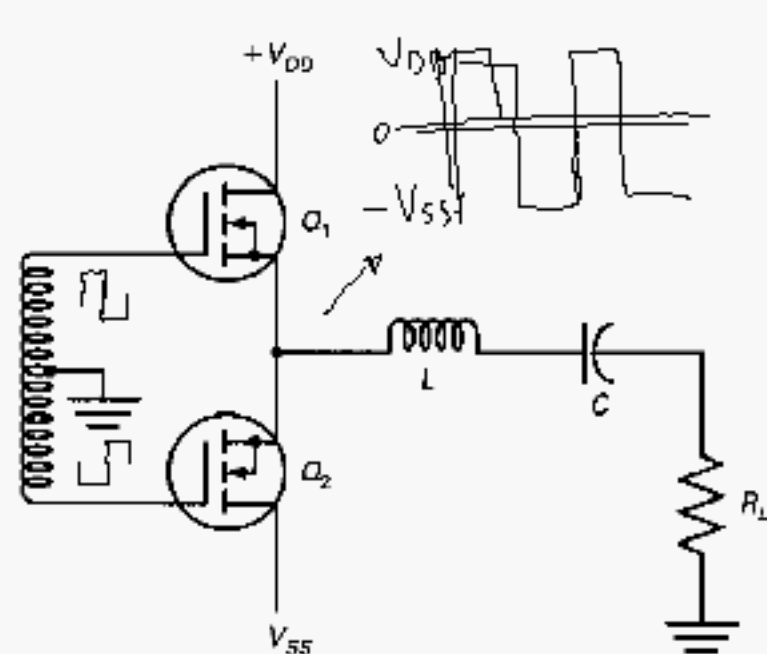
entonces $\eta = \frac{P_{O_{max}}}{P_{DC}} = \frac{P_{O_{max}}}{P_{O_{max}} + P_D} = \frac{V_{CC}}{V_{CC} + V_{CEsat}}$

Amplificador clase D

- **Amplificadores por conmutación**
- **Los dispositivos activos se utilizan como interruptores en lugar de fuente de corriente**
- **Mejoran la eficiencia**
- **Aumentan la potencia de salida**
- **Se reduce el tamaño de la fuente de DC**



Portadora de entrada



$$V_{c2} = \frac{1}{2} V_{cc} + \frac{1}{2} V_{cc} S(\theta)$$

$$\text{donde } S(\theta) = \left(\frac{4}{\pi} \left(\sin \theta + \frac{1}{3} \sin 3\theta + \frac{1}{5} \sin 5\theta + \dots \right) \right)$$

$$V_o(\theta) = \frac{1}{2} V_{cc} \frac{4}{\pi} \sin \theta \approx \frac{2 V_{cc}}{\pi} \sin \theta$$

$$i_o(\theta) = \frac{2V_{cc}}{\pi R_L} \sin \theta$$

Potencia de salida

$$P_o = \frac{V_o}{\sqrt{2}} \frac{i_o}{\sqrt{2}} = \frac{1}{2} \frac{V_o^2}{R_L}$$

$$P_o = \frac{1}{2} \left(\frac{2V_{cc}}{\pi} \right)^2 \frac{1}{R_L} = \frac{2V_{cc}^2}{R_L \pi^2}$$

Las corrientes en los colectores son medias senoides con valor pico de $\frac{2V_{cc}}{\pi R_L}$

La corriente de entrada es el promedio de $\frac{2V_{cc}}{\pi R_L}$, es decir

$$I_{DC} = \frac{\frac{2V_{cc}}{\pi R_L}}{\pi} = \frac{2V_{cc}}{\pi^2 R_L}$$

entonces:

$$P_{DC} = V_{cc} I_{DC} = \frac{2V_{cc}^2}{\pi^2 R_L}$$

por tanto

$$\eta = \frac{P_o}{P_{DC}} = 100\%$$

Ejemplo:

Determinar V_{CC} e I_{DC} para un amplificador de potencia clase D de voltaje complementario para que proporcione 25 W a una carga de 50Ω

Solución

$$\text{Si } P_o = \frac{2V_{CC}^2}{\pi^2 R} \Rightarrow V_{CC} = \sqrt{\frac{\pi^2 P_o R}{2}} = 78.53 \text{ V}$$

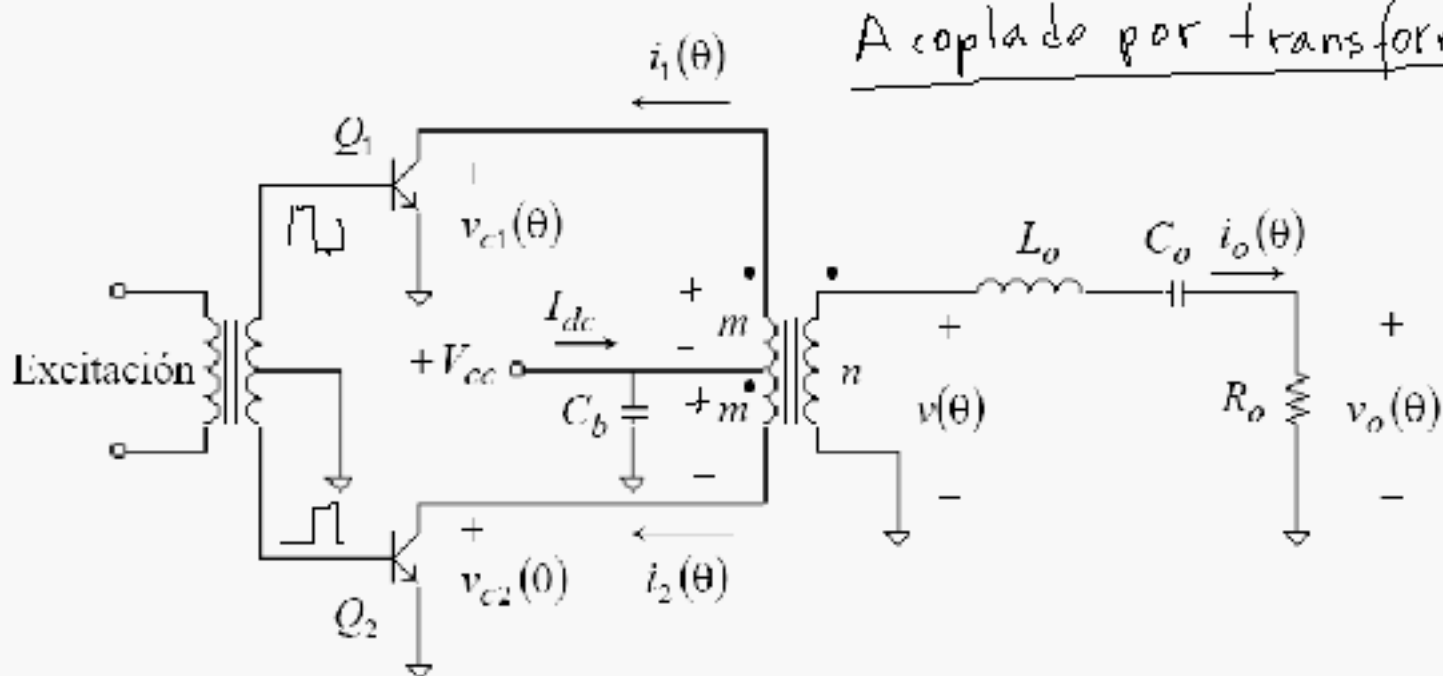


BV_{CBO}

Voltaje de ruptura

$$I_{DC} = \frac{2V_{CC}}{\pi^2 R} \approx 0.318 \text{ A}$$

A coplado por transformador



Cuando Q_2 se satura $\Rightarrow \frac{n}{m} V_{cc}$

Cuando Q_1 se satura $\Rightarrow -\frac{n}{m} V_{cc}$

$$V(\theta) = \frac{n}{m} V_{cc} S(\theta) = \left(\frac{n}{m} V_{cc} \frac{4}{\pi} \left(\sin \theta + \frac{1}{3} \sin 3\theta + \dots \right) \right)$$

$$V_o(\theta) = V_{cc} \frac{n}{m} \frac{4}{\pi} \sin \theta \quad \text{pero } i_o(\theta) = \frac{V_o(\theta)}{R_o}$$

Potencia de salida es:

$$P_o = \frac{V_o}{\sqrt{2}} \frac{i_o}{\sqrt{2}} = \frac{1}{2} \frac{V_o^2}{R_o} = \frac{8}{R_o} \left(\frac{V_{cc}}{\pi} \frac{n}{m} \right)^2$$

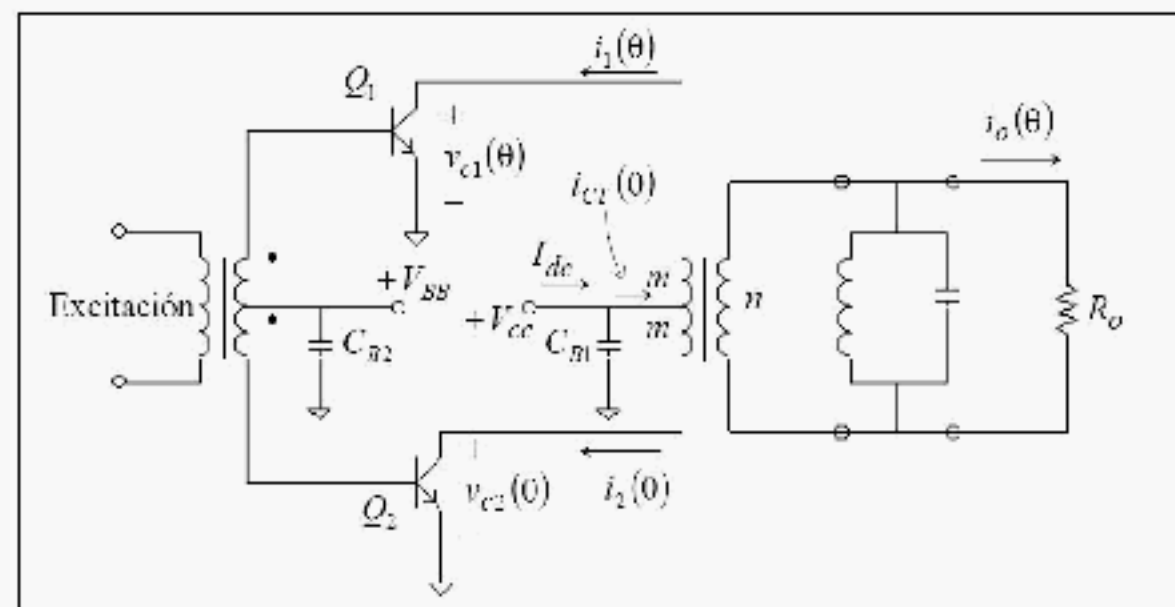
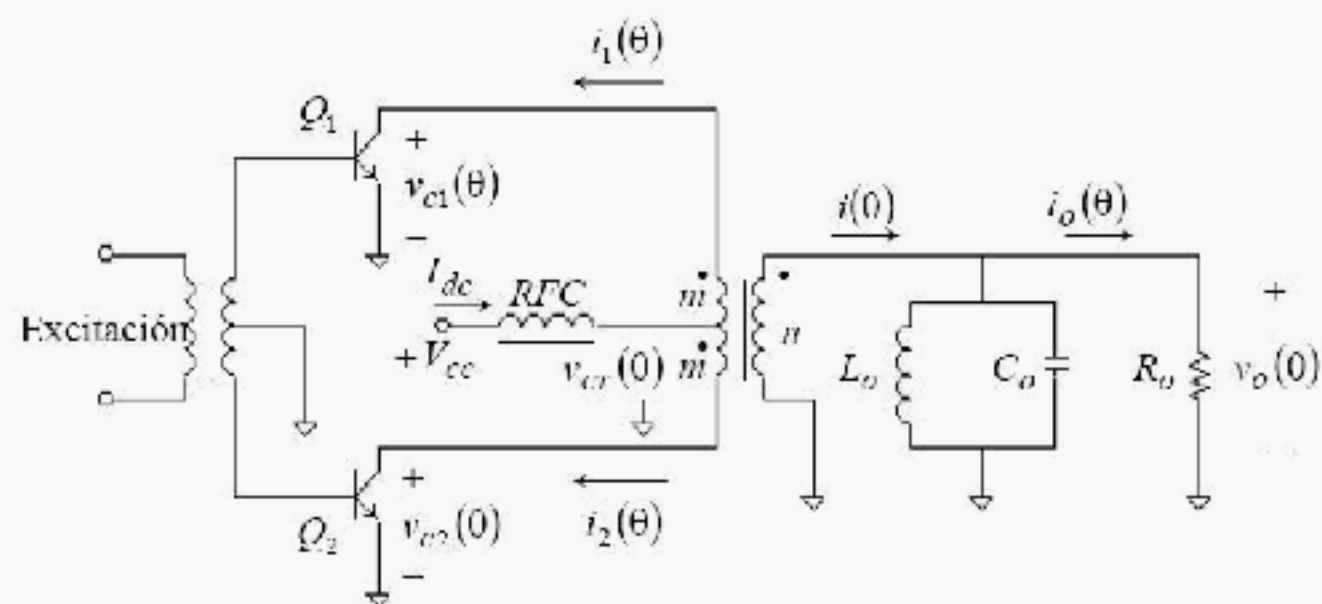
Si $I_c = i_o \frac{n}{m}$ e $I_{DC} = \frac{2 I_c}{\pi}$

entonces.

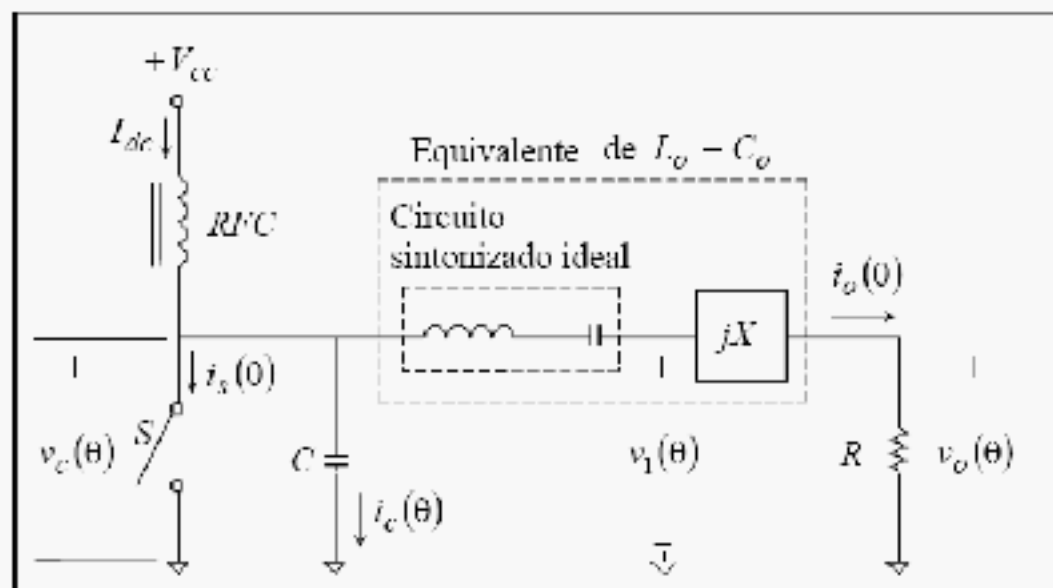
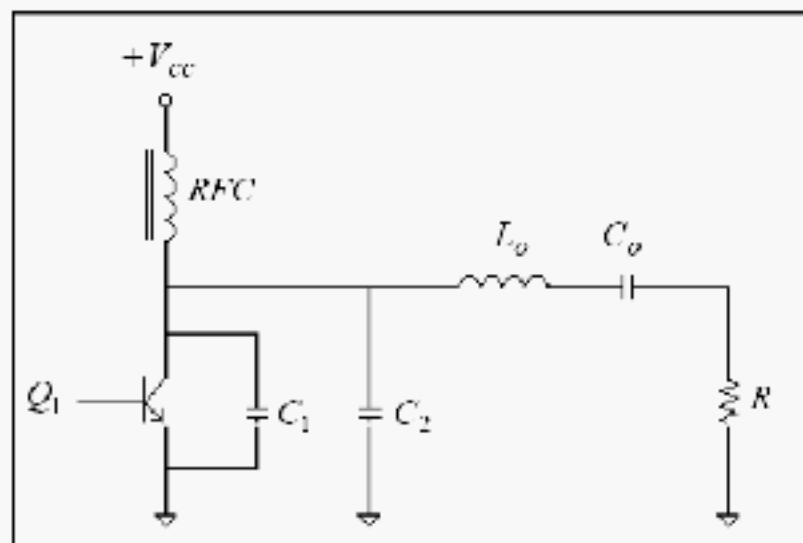
$$I_{DC} = \frac{8 V_{cc}}{R_o \pi^2} \frac{n^2}{m^2}$$

$$P_{DC} = V_{cc} I_{DC} = \frac{8}{R_o} \left(\frac{V_{cc}}{\pi} \frac{n}{m} \right)^2$$

$$\eta = \frac{P_o}{P_{DC}} \approx 100\%$$



Amplificadores clase E



C: Capacitor en derivación

- C1: Capacitor inherente al transistor
- C2: Capacitor externo