ME 332 Project 1 By Austin Vaden-Kiernan, Christian Bergdorf

1. Problem statement and objective:

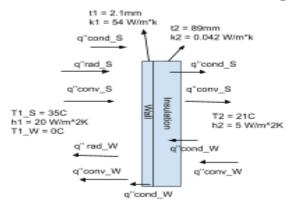
Our objective is to determine the heating and cooling requirements for a shipping container over the course of a year with both insulation and without insulation. In this analysis we must account for radiation, convection, conduction and applied flux. We then must do a cost analysis of our system to determine the annual energy cost. Finally we can determine the cost of insulation so that we can directly compare it to the daily energy cost without insulation through payback period.

Givens:

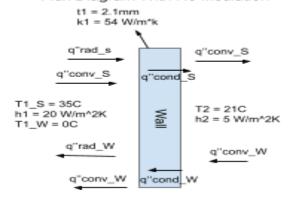
$$\begin{split} \varepsilon_{w} &= 0.925, \ \varepsilon_{R} = 0.22, \ k_{window} = 1.4W/mK, \ k_{in} = 0.042W/mK, \ k_{ER} = 14.9W/mK, \ k_{wall} = 54W/mK, \\ t_{ER} &= 0.002m, \ t_{wall} = 0.0021m, \ t_{= 0.089m}, \ t_{window} = 0.005m, \ t_{gap} = 0.025m, \ \sigma = 5.67 * 10^{-8}W/(m^{2}K^{4}) \\ T_{1,S} &= 35^{\circ}C, \ T_{1,W} = 0^{\circ}C, \ T_{2} = 21^{\circ}C, \ h_{1} = 20W/m^{2}K, \ h_{2} = 5W/m^{2}K, \ \eta_{1} = 50\%, \ \eta_{H} = 90\%, \\ L_{wall} &= 12.2m, \ W_{wall} = 2.4m, \ h_{wall} = 2.7m, \ W_{win} = 0.5m, \ h_{1} = 1.0m \end{split}$$

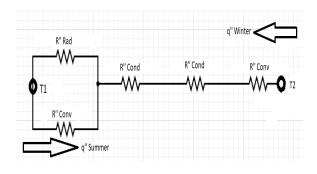
2. Diagrams:

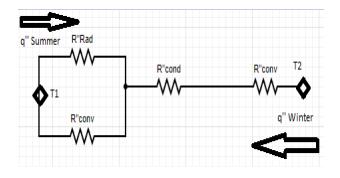
Summer and Winter Wall Heat Flux Diagram



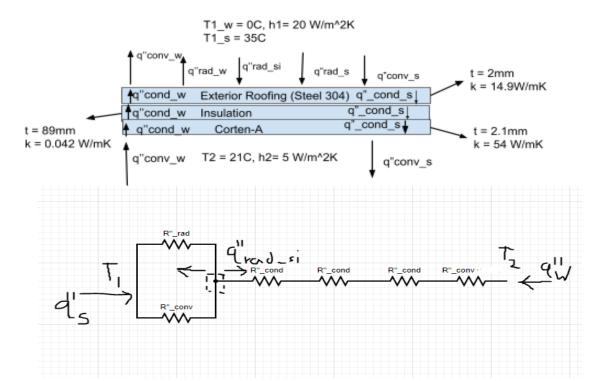
Summer and Winter Wall Heat Flux Diagram With No Insulation



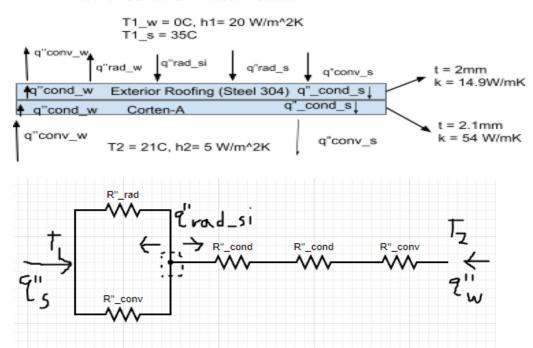


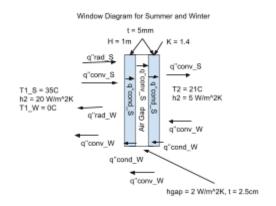


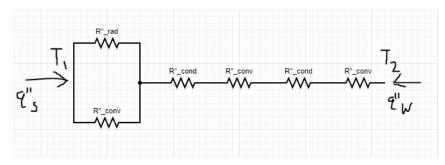
Roof of Container with Insulation



Roof of Container Without Insulation







3. Approach:

<u>Assumptions:</u> Steady-state, 1-D, neglect contact resistance between surfaces, all given properties at 300K, CORTEN-A treated as clean stainless steel (for emissivity on walls), roof has the same dimensions as floor (no roof overhang), no generation aside from applied flux.

4. Energy balance, energy cost equations, and other relevant analyses:

Evaluation of Walls and Flooring:

$$\begin{split} R_{rad,S}^* &= 1/h_{rad,S} \\ R_{rad,W}^* &= 1/h_{rad,W} \\ h_{rad,S} &= 4 * \sigma * \epsilon_R * T_{avg,S}^4 \\ h_{rad,W} &= 4 * \sigma * \epsilon_R * T_{avg,W}^4 \\ T_{avg,S} &= (T_{1,S} + T_2)/2 \\ T_{avg,W} &= (T_{1,W} + T_2)/2 \\ R_{convL}^* &= 1/h_1 \\ R_{convR}^* &= 1/h_2 \\ R_{condin}^* &= t_{in}/k_{in} \\ \Sigma R_{wall, insulation}^* &= 1/(1/R_{rad,S/W}^* + 1/R_{convL}^*) + R_{condw}^* + R_{convR}^* + R_{convR}^* \\ q_{wall, insulation, summer}^* &= (T_{1,S} - T_2)/\Sigma R_{wall, insulation}^* \\ 2R_{wall, in insulation}^* &= 1/(1/R_{rad,S/W}^* + 1/R_{convL}^*) + R_{cond}^* + R_{convR}^* \\ q_{wall, insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, insulation}^* \\ R_{wall, no insulation, summer}^* &= (T_{1,S} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, summer}^* &= (T_{1,S} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insulation}^* \\ q_{wall, no insulation, winter}^* &= (T_{1,W} - T_2)/\Sigma R_{wall, no insula$$

Evaluation of Windows:

$$\begin{split} R"_{conv \, gap} &= 1/h_{gap} \\ R"_{condwindow} &= t_{window}/k_{window} \\ R"_{radw,S/W} &= 1/h_{rad,S/W} \\ h_{rad,S} &= 4 * \sigma * \varepsilon_W * T_{avg,S}^{\quad 4} \\ h_{rad,W} &= 4 * \sigma * \varepsilon_W * T_{avg,W}^{\quad 4} \\ \Sigma R"_{window, \, no \, insulation} &= 1/(1/R"_{radw,S/W} + 1/R"_{convL}) + R"_{cond \, window} + R"_{conv \, gap} + R"_{cond \, window} + R"_{convR} \\ q"_{window, \, summer} &= (T_{1,S} - T_{2})/\Sigma R"_{window, \, no \, insulation} \\ q"_{window, \, winter} &= (T_{2} - T_{1,W})/\Sigma R"_{window, \, no \, insulation} \end{split}$$

Evaluation of Roof (Day):

$$\begin{split} R^{"}_{condER} &= t_{ER}/k_{ER} \\ q^{"}_{roof, in, day, S/W} &= q^{"}_{R, in, day, S/W} + q^{"}_{L, in, day, S/W} \\ q^{"}_{L, in, day, S/W} &= (T_{1, S/W} - T_{0, S/W})/(1/(1/R^{"}_{rad, S/W} + 1/R^{"}_{convL})) \\ q^{"}_{R, in, day, S/W} &= (T_{0, S/W} - T_{2})/(R^{"}_{condER} + R^{"}_{condin} + R^{"}_{condW} + R^{"}_{convR}) \\ q^{"}_{roof, non-in, day, S/W} &= q^{"}_{R, non-in, day, S/W} + q^{"}_{L, non-in, day, S/W} \\ q^{"}_{L, non-in, day, S/W} &= (T_{1, S/W} - T_{0, S/W})/(1/(1/R^{"}_{rad, S/W} + 1/R^{"}_{convL})) \\ q^{"}_{R, non-in, day, S/W} &= (T_{0, S/W} - T_{2})/(R^{"}_{condER} + R^{"}_{condW} + R^{"}_{convR}) \end{split}$$

Using these equations of q_R^* and q_L^* we can find $T_{O,S/W}$ which is the outside surface temperature of our wall. We then use those values to calculate the values for q_R^* and q_L^* which we use to calculate the other temperature values for the roof (equation shown under temperature evaluation). Evaluation of Roof (Night):

$$\begin{split} \Sigma R^{"}_{roof,\,in,\,night,\,S/W} &= 1/(1/R^{"}_{rad,S/W} + 1/R^{"}_{convL}) + R^{"}_{condER} + R^{"}_{condin} + R^{"}_{condw} + R^{"}_{convR} \\ q^{"}_{roof,\,in,\,night,\,S} &= (T_{1,S} - T_{2})/\Sigma R^{"}_{roof,\,in,\,night,\,S} \\ q^{"}_{roof,\,in,\,night,\,W} &= (T_{2} - T_{1,W})/\Sigma R^{"}_{roof,\,in,\,night,\,W} \\ \Sigma R^{"}_{roof,\,non-in,\,night,\,S/W} &= 1/(1/R^{"}_{rad,S/W} + 1/R^{"}_{convL}) + R^{"}_{condER} + R^{"}_{condw} + R^{"}_{convR} \\ q^{"}_{roof,\,non-in,\,night,\,S} &= (T_{1,S} - T_{2})/\Sigma R^{"}_{roof,\,non-in,\,night,\,S} \\ q^{"}_{roof,\,non-in,\,night,\,W} &= (T_{2} - T_{1,W})/\Sigma R^{"}_{roof,\,non-in,\,night,\,W} \end{split}$$

Equation for temperature evaluation:

$$q'' = (T_H - T_C)/\Sigma R''$$

We use this base equation to solve for all inner and outer wall temperatures, in summer T_H (hot temperature) comes from outside, in winter T_H comes from inside. $\Sigma R''$ only contains the resistance over the portion of the circuit we are looking at. For example:

$$q''_{Wall,S} = (Ti_{Wall,S} - T_2)/R''_{convR} \Rightarrow Ti_{Wall,S} = (q''_{Wall,S} * R''_{convR}) + T_2$$

Totals:

$$q'_{Window, W/S, in/non-in} = 4 * (q''_{window, in/non-in, S/W} * (W_{win} * h_{win}))$$

Multiply by 4 because there are 4 windows

$$q_{wall, W/S, in/non-in} = 2 * (q''_{wall, in/non-in, S/W} * (L_{wall} * h_{wall} - W_{win} * h_{win})) + 2 * (q''_{wall, in/non-in, S/W} * (W_{wall} * h_{wall} - W_{win} * h_{win})) + q''_{wall, in/non-in, S/W} (L_{wall} * W_{wall})$$

Two walls have different lengths, subtract window area from wall area, add floor at the end

because
$$q''_{wall} = q''_{floor}$$

$$q_{Roof(Day), W/S, in} = q''_{roof, day, in, S/W} (L_{wall} * W_{wall})$$

$$\textbf{Daytime total:} \ q_{\textit{day,S/W,in/non-in}} \ = \ q_{\textit{Window,W/S,in/non-in}} \ + \ q_{\textit{Wall,W/S,in/non-in}} \ + \ q_{\textit{Roof(Day),W/S,in/non-in}} \ + \ q_{$$

$$q_{Roof(night), W/S, in} = q''_{roof, night, in, S/W} (L_{wall} * W_{wall})$$

$$\textbf{Nighttime total:} \ \ q_{night,S/W,\,in/non-in} \ \ = q_{\textit{Window},\,W/S,in/non-in} \ + \ q_{\textit{Wall},\,W/S,in/non-in} \ + \ q_{\textit{Roof}(Night),\,W/S,in/non-in}$$

Daily total heat transfer:
$$DTHT_{in/no\ in} = 28800s * q_{S/W,in/no\ in} + 57600s * q_{S/W,\ in/no\ in}$$

Multiplying by 28800 seconds because the day lasts 28800 seconds and the night lasts 57600 seconds.

Single day cooling energy:
$$SDCE_{in/no\,in}=((8hr*q_{S/W,in/no\,in})/\eta_C)/1000$$

Multiplying by 8 hr because the day lasts 8 hrs.

Single night cooling energy:
$$SNCE_{in/no in} = ((16hr * qnight_{S/W,in/no in})/\eta_C)/1000$$

Multiplying by 16 hr because the night lasts 16 hrs.

Total daily cooling energy:
$$TDCE_{in/noin} = ((8hr * q_{S/W,in/noin})/\eta_c)/1000 +$$

$$((16hr * qnight_{S/W, in/noin})/\eta_C)/1000$$

Single day heating energy:
$$SDHE_{in/no\ in} = ((8hr\ ^*\ DTHT_{in/no\ in})/\eta_{H})/1000$$

Single night heating energy:
$$SNHE_{in/no\ in} = ((16hr * DTHT_{in/no\ in})/\eta_H)/1000$$

Total daily heating energy:
$$TDHE_{in/no\ in} = (SDHE_{in/\ no\ in} + SNHE_{in/\ no\ in})$$

Total annual energy:
$$TAE_{in/no in} = 180 days * TDCE_{in/no in} + 180 days * SNHE_{in/no in}$$

$$\textbf{Total annual energy cost:} \ \textit{TAEC}_{in,no\ in} = \$0.\ 13\ *\ 180 days\ *\ \textit{TDCE}_{in/no\ in} +\ \$0.\ 03\ *\ 180 days\ *\ \textit{SNHE}_{in/no\ in}$$

Cost to insulate trailer:
$$CTIT = \$5.00((L_{wall} * h_{wall} - W_{win} * h_{win}) * t_{wall} + (L_{wall} * h_{wall} - W_{win} * h_{win})$$

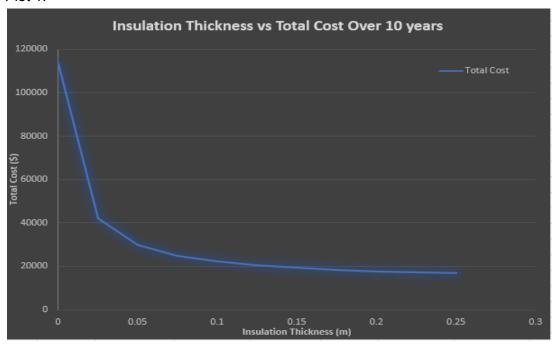
*
$$t_{wall}$$
 + 2 * $(L_{wall}$ * W_{wall} * t_{wall}))

Payback period:
$$PP = (CTIT/(TAEC_{non-in} - TAEC_{in})) * 360 days$$

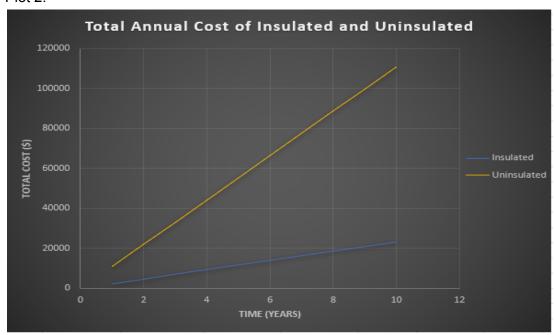
This payback period will show us how many days it will take to be in profit from buying insulation rather than having no insulation.

5. Results:

Plot 1:



Plot 2:



6. Conclusions:

a.

The total cost for insulation is extremely low, because of this it is completely undebatable that buying the insulation is the best option. Because of the high cost of energy when there is no insulation, the payback period is less than one day when you buy insulation. In plot 1 the optimal thickness for energy-saving features such as insulation was determined by iteration and can be asymptotically found based on the developed plot to be around 0.2m and 0.25m. This range of thickness is optimal because it requires less annual energy which reduces the total cost. In plot 2 the total annual cost of insulated and uninsulated is represented over a 10 year period. This shows the the immense cost of uninsulated vs the relatively lower cost associated with insulation for the container.

b.

To reduce the energy usage more insulative materials could be used in the container, this would increase the resistance through the walls/floor/roof. This would decrease the amount of heat that is able to transfer through the walls, requiring less heating and cooling from inside the container. They also could keep the inside temperature of the container at a slightly higher temperature in Summer (21<Ti<35), this way there would be less energy required to keep the container at said temperature. You can also apply this in winter, you would need to keep the temperature inside the container at a lower temperature though (0<Ti<21). One way to improve the efficiency of the window would be to simply increase the thickness.

C.

If the price of energy increases then our total cost will also increase. If the system was moved to a more temperate area where the outside temperature is lower in summer and higher in winter then the total energy cost would decrease. If the system were moved to a more extreme environment where temperature is higher in summer and lower in winter, the total energy cost would increase because it would take more energy to keep the inside temperature of the container at 21 degrees Celsius.

d. Extended learning:

Assuming we cover the roof in solar panels ($A=30m^2$) the initial cost will be \$4008.33 and they produce 7800kWh/yr. This means they produce 21.67kWh/day which we factor into our cost analysis.

Annual Energy Cost (insulated):

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(\$0.13 * 180 days * (TDCE - 21.67)) + (\$0.03 * 180 days * (TDHE - 21.67)) \Rightarrow \$1700.32
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There is also a one time \$4008.33 installation fee.

Payback Period:

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4008.33/(2324.42\$/yr - 1700.32\$/yr) = 6.42 years
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\$4008.33 is the initial investment for solar panels, and \$2324.42-\$1700.32 is how much money you save annually with solar panels vs without solar panels. According to our equation, it will take 6.42 years to break even, after that you are saving money with the panels.

7. Appendix:

4	Α	В	С	D	Е	F	G	Н	1	J	K	L	M	N	0
1				h values			k values								
2		Temps		h1	20		k1	54		etac	0.5		q" S	550	
	T1_W	. 0	0	h2	5		k2	0.042		etah	0.9		q"_W	175	
4	T1_S	35	35	hgap	2		k3	14.9					_	ep_W	0.925
5	T2_in	21	21	hrad_S	1.3627442					CEC	0.13				
6	T_avg_S	28	301.15	hrad_W	1.1387125					CGH	0.03				
7	T_avg2_W	10.5	283.65	W_hrad_S	5.73										
8				W_hrad_W	4.79										
9															
10															
11															
12				Wall		Total The	rmal Resistance	25		Window			Wall		
13				Summer	Winter					Summer	Winter		q_s	q_w	
14		Insulated		2.3659	2.3664					0.746008	0.747485335	Insulated	5.917417435	8.874265306	
15		Non Insul	ated	0.25	0.2473455							Non Insulate	56.71475233	84.9014978	
16				Wall (Insulate	ed)		Wall (Non-Ins	ulated)		Window					
17				Summer	Winter		Summer	Winter		Summer	Winter				
18			R"rad	0.73	0.88	R"rad	0.7338	0.878184779	R"rad	0.174529	0.208865569				
19			R"conv	0.05	0.05	R"conv	0.05	0.05	R"conv	0.05	_			Roof Insulation (DAY	')
20			R"cond	3.88889E-05	3.889E-05	R"cond	3.88889E-05	3.88889E-05	R"cond	0.003571	0.003571429			q_s	q_w
21			R"cond	2.119047619	2.1190476	R"conv	0.2	0.2	R"conv	0.5	0.5			112.7874912	29.98214964
22 23			R"conv	0.2	0.2				R"cond	0.003571	0.003571429				
23									R"conv	0.2	0.2				
24															
25 26															
27			Roof Non-Ins	ulated (NIGHT)		Roof Insulated				Roof Insulate			Roof Non-Insulated	` '
28			Summer	Winter				Winter			Summer	Winter		Summer	Winter
29		R"rad		0.878184779		R"rad	0.733813448			R"rad		0.878184779			0.878184779
30		R"conv	0.05	0.05		R"conv	0.05	0.05		R"conv	0.05		R"conv	0.05	0.05
31		R"cond		0.000134228		R"cond	0.000134228			R"cond		0.000134228	R"cond	0.000134228	0.000134228
32		R"cond		3.88889E-05		R"cond	2.119047619			R"cond		2.119047619			
33		R"conv	0.2	0.2		R"cond		3.88889E-05		R"cond		3.88889E-05			3.88889E-05
34						R"conv	0.2	0.2		R"conv	0.2	0.2	R"conv	0.2	0.2

Р	Q	R	S	T	U	V	W	Х	Υ	Z	AA	AB	AC	AD	A
sigma	5.67E-08														
ep_R	0.22					All Tempe									
T_s (Insulate						Insulated									
T_s (Non - In					To Wall_S		32.34516								
T_w (Insulate					To Wall_w										
T_w (Non - Ir	-4.11				Ti Wall_s	22.18348	32.34295								A
					Ti Wall_w	19.22515	4.0197				Insulated	Non-Insulat	ted		
			D	YAC	To roof_s	29.9	31.90282		Night	To roof_s	34.7230186	32.346599			
			0	PAY	To roof_w	1.39	4.11		Night	To roof_w	0.41978725	4.0142203			
			0	PAY	Ti roof_s	21.7675	31.8606		Night	Ti roof_s	22.1834163	32.336786			
	Window		D	PAY	Ti roof_w	20.88013	16.89355		Night	Ti roof_w	19.2252476	4.0289102			
	q_s	q_w			To Win_S	N/A	34.27063								
Non-Insulate	18.76654426	28.09419666			To Win_W	N/A	1.13339								
Insulated	N/A	N/A			Ti Win_S	N/A	24.75331								
					Ti Win_W	N/A	15.38116								
	Roof Non- Ins	ulation (DAY)	R	Roof Insul	lation (NIGH	IT)		Roof Non	-Insulation	(NIGHT)					A
		q_w ` ´			q_w `	•		q s	q_w	` '					
		107.4123361		_	8.873762			56.68393	84.85545						
			Т	Total Ther	mal Resista	nce (Roof o	day and nic	zht)							
	Roof Insulation (DAY)			Total Thermal Resistance (Roof Roof Non- Insulation (DAY)		Roof Insulation (NIGHT)			Roof Non-Insulation (NIGHT)		GHT)				
	Summer	Winter	S	Summer	Winter		Summer	Winter			Summer	Winter			
	2.366031202	2.366527307		0.246984	0.2474797		2.366031	2.366527	,		0.24698358	0.2474797			
	2.300031202	2.30052/30/		U.240984	0.24/4/9/		2.300031	2.300527			0.24698358	0.247	4/9/	(4/9/	(4/9/

	Cumanaa							
	Summer							
	Insulated	Non-Insulate	d					
Day Total q	3967.907168	9583.381235						
Night total q	838.7415798	7715.808064						
DTHT	162587241.4	720431924			Summer		Winter	
SDCE	63.48651468	153.3340998			Insulated		Insulated	
SNCE	26.83973055	246.905858		q" Left	108.95	q" Left	29.38281	
TDCE	90.32624524	400.2399578		q" Right	3.837496	q" Right	0.599339	
					Non-Insul	ated	Non-Insula	ated
	Winter			q" Left	66.16417	q" Left	86.88011	
	Insulated	Non-Insulated	d	q" Right	54.303	q" Right	20.53223	
Day Total q	1875.802769	12210.96854						
Night total q	1257.749178	11550.50288						
DTHT	126469472.4	1016984860		Lwall	12.2		A Wall 1	32.44
SDHE	16.67380239	108.5419426		H wall	2.7		A Wall 2	5.98
SNHE	22.35998539	205.3422735		W wall	2.4		A Floor	29.28
TDHE	39.03378778	313.884216		W windov	0.5		A Window	0.5
				H window	1		A Roof	29.28

	Annual					Insulation	
	Insulated	Non-Insulated	1		CIII	60.253	
TAE	23284.81	128601.4826			PP	2.480721257	
TAEC	2324.417	11068.27685					
	12.91343						
			TOTALS for q'				
Windows			Walls			Roof (DAY)	
Insulated	Non-Insul	ated	Insulated	Non-Insulat	ed	Insulated	Non-Insulated
37.533089	37.53309	Summer	627.9563382	6018.56952	Summer	3302.417741	3547.810324
56.188393	56.18839	Winter	941.7370343	9009.74695	Winter	877.8773415	3145.0332
						Roof (NIGHT)	
						Insulated	Non-Insulated
					Summer	173.2521531	1659.705458
					Winter	259.8237503	2484.567543
	TAEC Windows Insulated 37.533089	TAE 23284.81 TAEC 2324.417 12.91343 Windows Insulated Non-Insul 37.533089 37.53309	Insulated Non-Insulated TAE 23284.81 128601.4826 TAEC 2324.417 11068.27685 12.91343 Windows Insulated Non-Insulated 37.533089 37.53309 Summer	Insulated Non-Insulated TAE 23284.81 128601.4826 TAEC 2324.417 11068.27685 12.91343 TOTALS for q' Windows Walls Insulated Non-Insulated Insulated 37.533089 37.53309 Summer 627.9563382	Insulated Non-Insulated TAE 23284.81 128601.4826 TAEC 2324.417 11068.27685 12.91343 TOTALS for q' Windows Walls Insulated Non-Insulated Insulated Non-Insulated 37.533089 37.53309 Summer 627.9563382 6018.56952	Insulated Non-Insulated	Insulated Non-Insulated

