

DESIGN CRITERIA:

- A.** Code: CBC 2010, Wind: C, 85 mph, Category: D
- B.** Wood Species: Douglas Fir Larch with maximum 19% moisture content prior to Installation of Finish Material
- 4X Members: No.2 or Better
- 6X, 8X Beams and Headers: No.1 or Better
- 2X Joists and Rafters: No.2 or Better
- Plates and Blocking: Standard Grade or Better
- Studs: Stud Grade or Better
- Mud Sills: Pressure Treated Utility Grade or Better

PRIMARY ROOF LOADING

Pitch	4.0:12
K = Increase for pitch	1.05
Rafter(2x8 16" O/C) Joist(2x10 16" O/C) x K	6.10
Plywood(1/2") x K	1.63
	0.00
Shingle x K	3.16
Sprinkler	1.00
Misc.(Insul.,Elect.,ETC)	2.10
Snow Load	0.00
Live Load	20.00
Dead Load	14.00

SECONDARY ROOF LOADING

Pitch	4.0:12
K = Increase for pitch	1.05
Rafter(2x8 16" O/C) Joist(No Ceil'G Joists) x K	2.70
Plywood(1/2") x K	1.63
	0.00
Shingle x K	3.16
Sprinkler	1.00
Misc.(Insul.,Elect.,ETC)	1.50
Snow Load	0.00
Live Load	20.00
Dead Load	10.00

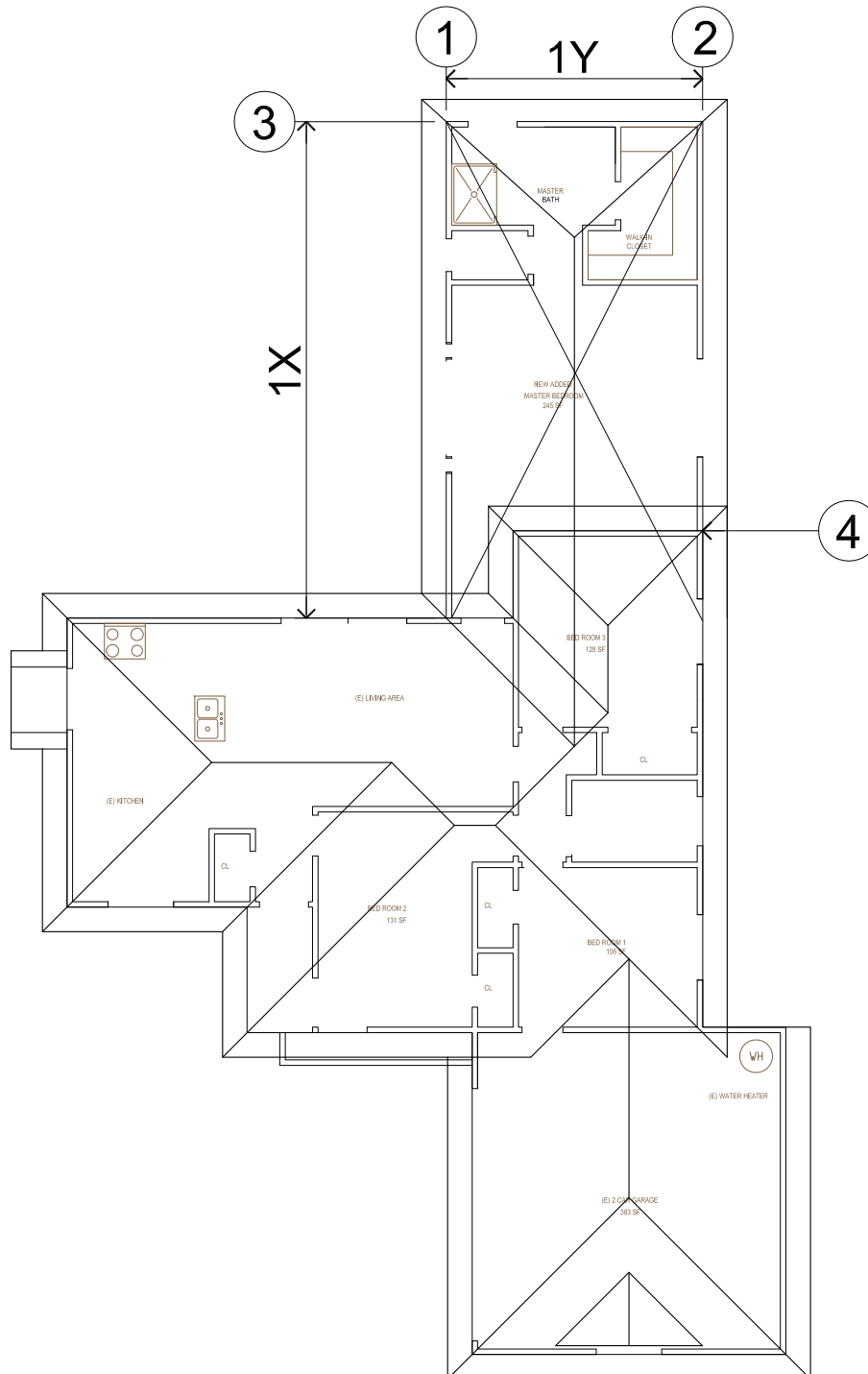
LATERAL SECTION

SHEET: L1

JOB NO.: 66925

DATE: 08/08/2012

CLIENT: REMODELING/ADDITION



PROPOSAL FLOOR PLAN
SHEAR WALL LAYOUT

LATERAL ANALYSIS
CBC 2010
POURING NON MONO

SHEET : L - 1
JOB NO. : 66925
CLIENT : Remodel
PLAN NO. : 1
DATE : 5/14/2012(Ver400)

Y DIRECTION SECTION 1Y

BLDG DIMENSION (FT): BASE HT=0.5, SLOPE ROOF HT=14.0, GABLE MEAN ROOF HT=12.5, L=30.5, B=16.0
FLOOR HT (FT): 1-FLR=9.0

WIND PARAMETERS: **WIND SPEED=85 MPH. WIND EXPOSURE=C**

COEFFICIENTS: $K_d=0.85$, $K_{zt}=1.00$, $G=0.85$, $GC_{Di}=\pm 0.18$, $\omega=1.00$

INTERPOLATION: L/B \Rightarrow YES, h/L \Rightarrow YES, $\theta \Rightarrow$ YES, $q_h=13.35$

WIND HEIGHT (FT): 15 UPLIFT (AVE.)

WALL PRESSURE ωP (PSF): 12.69 8.86

OVERHANGS: 19.00/1.50

GABLE: 16.00(WW)/15.50, 16.00(LW)/15.50

WIND LOAD ROOF (PLF): $+Y/+GC_{Di}=78.24(R)$ $+Y/-GC_{Di}=78.24(R)$ $-Y/+GC_{Di}=78.24(R)$ $-Y/-GC_{Di}=78.24(R)$ MAX TOTAL=78.24

$R_v=6.5$, SITE CLASS: D, $S_{DS}=2F_aS_d/3=2 \times 1.00 \times 1.50/3=1.000$, $S_{D1}=2F_vS_1/3=2 \times 1.50 \times 0.60/3=0.600$, $S_{DC}=D$, $k=1.0000$

$V=S_{DS}IW/1.4R_v=(1.000)(1.00)W/(1.4 \times 6.5)=$

ROOF: DL ROOF = $14.0 \times 32.0 =$ 0.1099W 448.00 PLF

DL EXT WALL = $15.0[1.0(9.00-4.50)] =$ 67.50 PLF

DL INT WALL = $10.0[2.5(9.00-4.50)] =$ 112.50 PLF

SHEAR = $0.1099(448.00+67.50+112.50) = 0.1099(628.00) =$ 69.01 PLF (89.71 PLF)

TOTAL SEISMIC LOAD = 69.01 = 69.01 PLF (89.71 PLF)

ROOF: 78.24 PLF WIND GOVERN

ROOF DIAPHRAGM $V =$ 89.71 PLF (DIAPH.ONLY)

MAX SHEAR = $89.71 \times 16.00 / (2 \times 30.50) =$ 23.53 PLF

USE: 15/32" CDX RATED UNBLKED 32/16 W/8d COMMON NAILS AT 6", 6", 12" O.C.

CHORD FORCE = $89.71 \times 16.00 \times 16.00 / (8 \times 30.50) =$ 94.13 LBS

SPLICE W/ MINI (5) 16d SINKER NAILS EACH SIDE OF SPLICE @ 8 IN. O.C. (STANDARD CONSTRUCTION)

LATERAL ANALYSIS
CBC 2010
POURING NON MONO

SHEET : L - 2
JOB NO. : 66925
CLIENT : Remodel
PLAN NO. : I
DATE : 5/14/2012(Ver400)

X DIRECTION SECTION IX

BLDG DIMENSION (FT): BASE HT=0.5, SLOPE ROOF HT=14.0, GABLE MEAN ROOF HT=12.5, L=16.0, B=30.5
FLOOR HT (FT): 1-FLR=9.0

WIND PARAMETERS: **WIND SPEED=85 MPH. WIND EXPOSURE=C**

COEFFICIENTS: $K_d=0.85$, $K_{zt}=1.00$, $G=0.85$, $GC_{di}=\pm 0.18$, $\omega=1.00$

INTERPOLATION: L/B \Rightarrow YES, h/L \Rightarrow YES, $\theta \Rightarrow$ YES, $q_h=13.35$

WIND HEIGHT (FT): 15 UPLIFT (AVE.)

WALL PRESSURE ωP (PSF): 14.75 8.95

ROOF: 30.50(WW)/8.00/18.43°, 30.50(LW)/8.00/18.43°; OVERHANGS: 32.00/3.00

WIND LOAD ROOF (PLF): MINIMUM LOAD=(10*5.00*1.00)+66.36=116.36

MAX TOTAL=116.36

$R_x=6.5$. SITE CLASS: D. $S_{DS}=2F_aS_s/3=2 \times 1.00 \times 1.50/3=1.000$, $S_{D1}=2F_vS_1/3=2 \times 1.50 \times 0.60/3=0.600$, $S_{DC}=D$, $k=1.0000$

$V=S_{DS}IW/1.4R_x=(1.000)(1.00)W/(1.4*6.5)=$

0.1099W

ROOF: DL ROOF = 14.0x19.0 =

266.00 PLF

DL EXT WALL = 15.0f2.0(9.00-4.50)l =

135.00 PLF

DL INT WALL = 10.0f1.5(9.00-4.50)l =

67.50 PLF

SHEAR = 0.1099(266.00+135.00+67.50) = 0.1099(468.50) =

51.48 PLF

TOTAL SEISMIC LOAD = 51.48 =

51.48 PLF (66.93 PLF)

ROOF: 116.36 PLF WIND GOVERN

(DIAPH.ONLY)

ROOF DIAPHRAGM V =

116.36 PLF

MAX SHEAR = 116.36 x 25.00 / (2 x 16.00) =

90.91 PLF

USE: 15/32" CDX RATED UNBLKED 32/16 W/8d COMMON NAILS AT 6", 6", 12" O.C.

CHORD FORCE = 116.36 x 25.00 x 25.00 / (8 x 16.00) =

568.17 LBS

SPLICE W/ MINI (5)16d SINKER NAILS EACH SIDE OF SPLICE @ 8 IN. O.C. (STANDARD CONSTRUCTION)

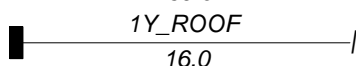
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SHEARWALS DESIGN

2010-CBC

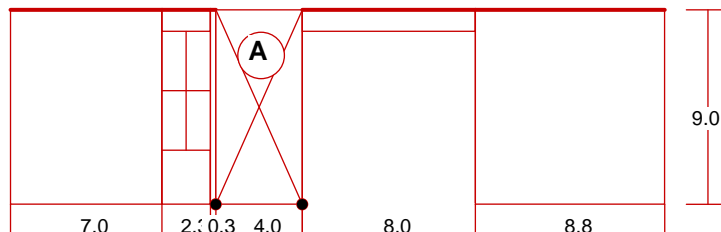
Wind: 626 Seismic: 552

wind 78.2
seismic 69.0

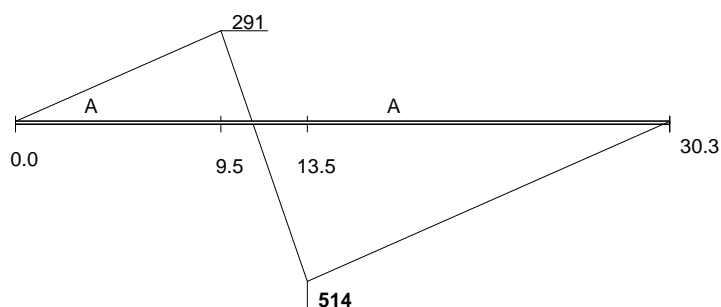


1 @Left of Elevation 1ST Floor 2-Pour Exterior Wall(Y Dir.)

Wind 626(Uplift on Roof=8.9 PSF)
Seismic 928=(552+ 161)*1.30



● Strap(E)



Drag Force Analysis

A: Simpson ST22 (1192 LB) ALT (10) # 16d sinker per top plate splice
Total Wall Length = 30.25(FT) Total Panel Length = 4.00(FT) P.T./User Desian
Shear Diaphragm = $928 / 30.25 = 31(\text{PLF})$ $P = 1.30$
Use (3 A35) or (2 LS50) Along Line of Shear Panel or for Framing Clips Spacing See S.W. Schedule
Design Wall Shear(S) = $928 / 4.00 = 232(\text{PLF})$ (Flexible ,SW $V_{allow}(\text{Seismic})$ Ajusted for H/W Ratio) Max. Drag = 514(LB)

Use TYPE 2

Max. Panel Deflection: $\Delta M = (4.0/1.0) \times \Delta s \times 1.4 = 1.671" \leq 0.02 \times 108.0 = 2.160"$

Dead Loads:

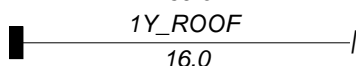
Wall 135.0= 15 * 9.0'
Roof_P 56.0 = 14 * 8.0/2 FROM 0.0' TO 30.0'

OVERTURN ANALYSIS		UPLIFT(T)	DOWN(C)	
Panel	(A)	Left Side : T= 2077(LB)	C= 2289(LB)	HDU2/4x4
		Right Side : T= 2077(LB)	C= 2289(LB)	HDU2/4x4

Use HDU2/4x4 on both ends
w/(2)5/8" x 12" Anchor Bolt (@ 48" O.C. Max.)

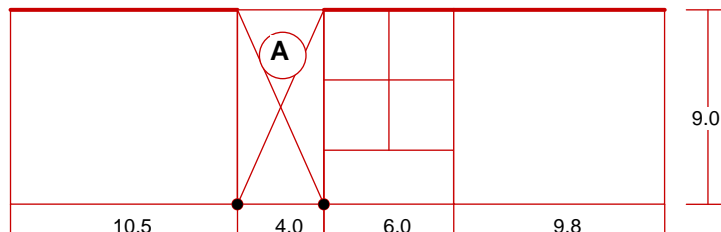
Wind: 626 Seismic: 552

wind 78.2
seismic 69.0

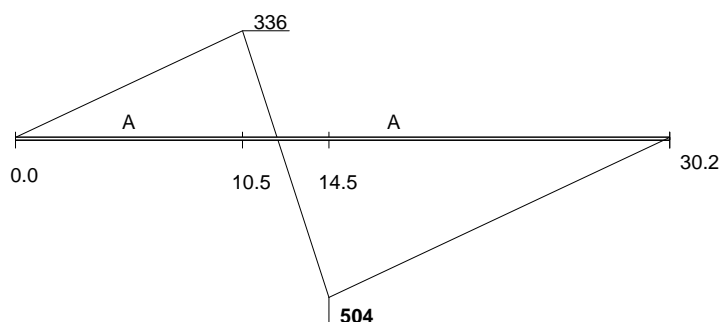


2 @Right of Elevation 1ST Floor 2-Pour Exterior Wall(Y Dir.)

Wind 626(Uplift on Roof=8.9 PSF)
Seismic 968=(552+ 192)*1.30



● Strap(E)



Drag Force Analysis

A: Simpson ST22 (1192 LB)

ALT (10) # 16d sinker per top plate splice

Total Wall Length = 30.25(FT) Total Panel Length = 4.00(FT) P.T./User Desian

Shear Diaphragm = $968 / 30.25 = 32(\text{PLF})$

$P = 1.30$

Use (3 A35) or (2 LS50) Along Line of Shear Panel or for Framing Clips Spacing See S.W. Schedule

Design Wall Shear(S) = $968 / 4.00 = 242(\text{PLF})$ (Flexible ,SW $V_{allow}(\text{Seismic})$ Ajusted for H/W Ratio) Max. Drag = 504(LB)

Use TYPE 2

Max. Panel Deflection: $\Delta M = (4.0/1.0) \times \Delta s \times 1.4 = 1.775" \leq 0.02 \times 108.0 = 2.160"$

Dead Loads:

Wall 135.0= $15 \times 9.0'$

Roof_P 0.0 = $14 \times 0.0/2$ FROM 0.0' TO 65.0'

OVERTURN ANALYSIS

UPLIFT(T) DOWN(C)

Panel (A) Left Side : T= 2225(LB) C= 2348(LB)

HDU2/4x4

Right Side : T= 2225(LB) C= 2348(LB)

HDU2/4x4

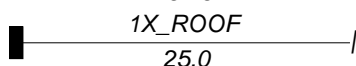
Use HDU2/4x4 on both ends

w/(2)5/8" x 12" Anchor Bolt (@ 48" O.C. Max.)

Wind: 1455 Seismic: 644

wind 116.4

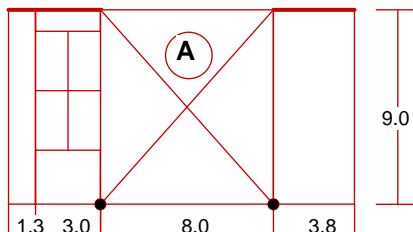
seismic 51.5



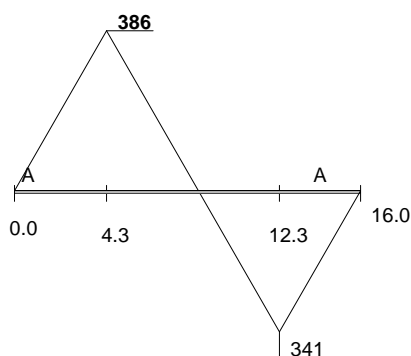
3 @Rear of Master Bath 1ST Floor 2-Pour Exterior Wall(X Dir.)

Wind 1455(Uplift on Roof=8.9 PSF)

Seismic 973=(644+ 105)*1.30



● Strap(E)



Drag Force Analysis

A: Simpson ST22 (1192 LB)

ALT (10) # 16d sinker per top plate splice

Total Wall Length = 16.00(FT) Total Panel Length = 8.00(FT) P.T./User Desian

Shear Diaphragm = 1455/ 16.00 = 91(PLF)

$\rho = 1.30$

Use (4 A35) or (3 LS50) Along Line of Shear Panel or for Framing Clips Spacing See S.W. Schedule

Design Wall Shear(W) = 1455/ 8.00= 182(PLF)(Flexible) Max. Drag = 386(LB)

Use TYPE 1

Max. Panel Deflection: $\Delta M = (4.0/1.0) \times \Delta s \times 1.4 = 0.588" \leq 0.02 \times 108.0 = 2.160"$

Dead Loads:

Wall 135.0= 15 * 9.0'

Roof_P 70.0 = 14 * 10.0/2 FROM 0.0' TO 16.0'

OVERTURN ANALYSIS UPLIFT(T) DOWN(C)

Panel (A) Left Side : T= 1458(LB) C= 1930(LB)

HDU2/4x4

Right Side : T= 1391(LB) C= 1930(LB)

HDU2/4x4

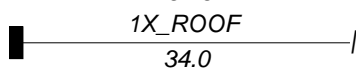
Use HDU2/4x4 on both ends

w/(2)5/8" x 12" Anchor Bolt (@ 72" O.C. Max.)

Wind: 1978 Seismic: 875

wind 116.4

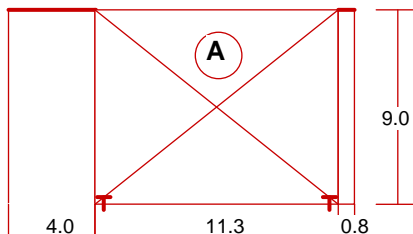
seismic 51.5



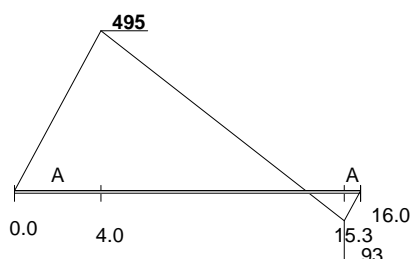
4 @Front of Dining Room 1ST Floor 2-Pour Exterior Wall(X Dir.)

Wind 1978(Uplift on Roof=8.9 PSF)

Seismic 1253=(875+ 89)*1.30



● Strap(E) T HD



Drag Force Analysis

A: Simpson ST22 (1192 LB)

ALT (10) # 16d sinker per top plate splice

Total Wall Length = 16.00(FT) Total Panel Length = 11.25(FT) P.T./User Desian

Shear Diaphragm = 1978/ 16.00 = 124(PLF)

$\rho = 1.30$

Use (5 A35) or (4 LS50) Along Line of Shear Panel or for Framing Clips Spacing See S.W. Schedule

Design Wall Shear(W) = 1978/11.25= 176(PLF)(Flexible) Max. Drag = 495(LB)

Use TYPE 1

Max. Panel Deflection: $\Delta M = (4.0/1.0) \times \Delta s \times 1.4 = 0.426" \leq 0.02 \times 108.0 = 2.160"$

Dead Loads:

Wall 135.0= 15 * 9.0'

Roof_P 70.0 = 14 *10.0/2 FROM 0.0' TO 0.0'

OVERTURN ANALYSIS

UPLIFT(T) DOWN(C)

Panel (A) Left Side : T= 1169(LB) C= 1625(LB)

Right Side : T= 1169(LB) C= 1625(LB)

HDU2/4x4(I) w/DBL BLK'G ***

HDU2/4x4(I) w/DBL BLK'G ***

Use HDU2/4x4(I) on both ends

w/(2)5/8" x 12" Anchor Bolt (@ 72" O.C. Max.)

(I) Holddown inside of panel

*** User preferred

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BEAMS DESIGN

2010-CBC

Beam ID: 1 Hip Bm Over the Master Bath

Loads (Downward +)

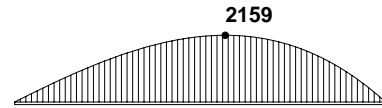
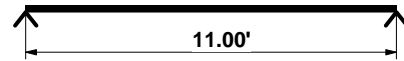
Beam Weight 20.0 PLF @ 0.0' to 11.0'
Secondary Roof 0 PLF= 0.0'x(10+20)/2 @ 0.00' to 240 PLF=16.0'x(10+20)/2 @11.00'

Reactions(DL+LL/Max. Load Combination)

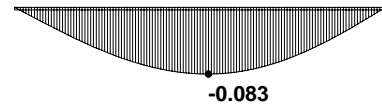
Down 550/550 990/990
Up 0/0 0/0

Use DFL NO2 2-2 x 10(Fb= 900 Fv=180)

Critical Shear =-905 LB @10.67' $1.5 \times \text{Shear} / (F_v \times A) = 0.217$
 $F_v = 225$ A= 27.75
Critical Moment =2159 LBxFT @ 6.25' Ratio=0.489
 $F_b = 1238$ S= 42.78
Critical Deflection = -0.083 INCH @ 5.75'



Moment Diagram:DL + RF_L



Deflection Diagram:LL

Beam ID: 2 Clg Bm Over the Master Bath

Loads (Downward +)

Beam Weight 30.0 PLF from 0.0' to 15.3'
Point Load(P1) From right of BM 1 @ 7.50
Point Load(P2) From left of BM 1 @ 7.50

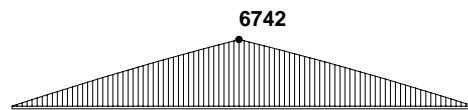
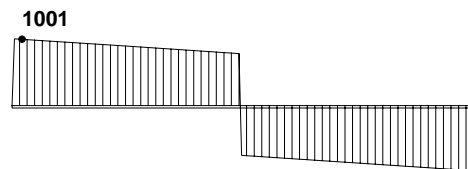
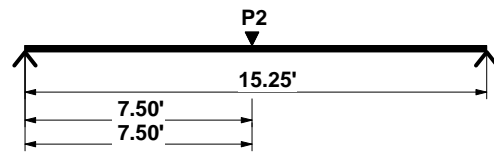
▼ :Point Load Location

Reactions(DL+LL/Max. Load Combination)

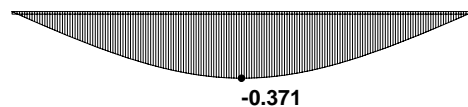
Down 1011/1011 986/986
Up 0/0 0/0

Use DFL NO2 4-2 x 10(Fb=900 Fv=180)

Critical Shear =1001 LB @ 0.33' $1.5 \times \text{Shear} / (F_v \times A) = 0.235$
 $F_v = 213$ A= 52.25
Critical Moment =6742 LBxFT @ 7.50' Ratio=0.779
 $F_b = 1688$ S= 82.73
Critical Deflection =-0.371 Inch @ 7.58' L/240=0.762



Moment Diagram:DL + RF_L



Deflection Diagram:DL+LL

Beam ID: 3(Drop) Header @ Left of the Master Bedroom

Loads (Downward +)

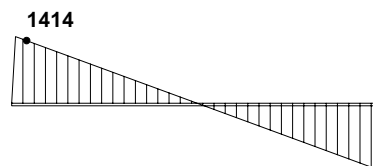
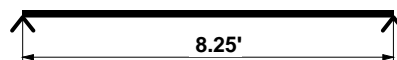
Beam Weight 20.0 PLF @ 0.0' to 8.3'
Primary Roof 323 PLF=19.0'x(14+20)/2 @ 0.00' to 8.25'
Exterior Wall 30 PLF= 2.0'x15.0 @ 0.00' to 8.25'

Reactions(DL+LL/Max. Load Combination)

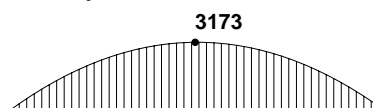
Down 1539/1539 1539/1539
Up 0/0 0/0

Use DFL NO2 4 x 10(Fb= 900 Fv=180)

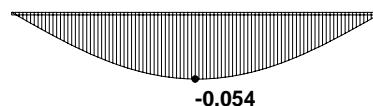
Critical Shear =1414 LB @ 0.33' 1.5xShear/(FvxA)=0.291
Fv=225 A= 32.38
Critical Moment =3173 LBxFT @ 4.17' Ratio=0.573
Fb= 1331 S= 49.91
Critical Deflection = -0.054 INCH @ 4.17'



Shear Diagram:DL + RF_L



Moment Diagram:DL + RF_L



Deflection Diagram:LL

Beam ID: 4(Drop) Header @ Left of the Master Bedroom

Loads (Downward +)

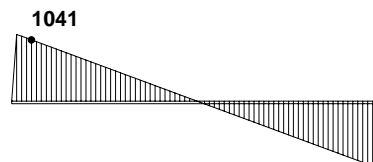
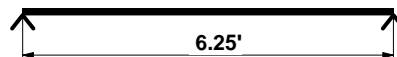
Beam Weight 20.0 PLF from 0.0' to 6.3'
Primary Roof 323 PLF=19.0'x(14+20)/2 @ 0.00' to 6.25'
Exterior Wall 30 PLF= 2.0'x15.0 @ 0.00' to 6.25'

Reactions(DL+LL/Max. Load Combination)

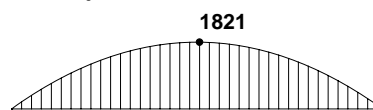
Down 1166/1166 1166/1166
Up 0/0 0/0

Use DFL NO2 4 x 8(Fb= 900 Fv=180)

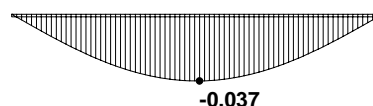
Critical Shear =1041 LB @ 0.33' 1.5xShear/(FvxA)=0.274
Fv=225 A= 25.38
Critical Moment =1821 LBxFT @ 3.17' Ratio=0.491
Fb= 1451 S= 30.66
Critical Deflection = -0.037 INCH @ 3.17'



Shear Diagram:DL + RF_L



Moment Diagram:DL + RF_L



Deflection Diagram:LL