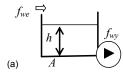
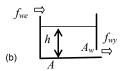
Otwarte układy hydrauliczne





1) Zawartość magazynu

$$V(t) = Ah(t)$$

2) Zmiana zawartości magazynu

$$\frac{dV(t)}{dt} = A\frac{dh(t)}{dt} = A\dot{h}(t)$$

3) Bilans strumieni wpływających i wypływających [m3/s]

$$A\dot{h}(t) = f_{we}(t) - f_{wy}(t)$$

(a) $f_{wy}(t)$

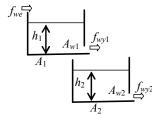
(b)
$$f_{wy}(t) = A_w \sqrt{2gh(t)} \approx ah(t)$$

(a) $A\dot{h}(t) = f_{we}(t) - f_{wv}(t)$

- (b₁) $A\dot{h}(t) = f_{we}(t) A_w \sqrt{2gh(t)}$
- $(b_2) \quad A\dot{h}(t) = f_{we}(t) ah(t)$
- 4) Zmienne wejściowe i wyjściowe, kompletność modelu

1

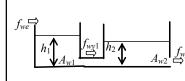
Otwarte układy hydrauliczne



 $\begin{cases} A_{1}\dot{h}_{1}(t) = f_{we}(t) - f_{wy1}(t) \\ A_{2}\dot{h}_{2}(t) = f_{wy1}(t) - f_{wy2}(t) \\ f_{wy1}(t) = A_{w1}\sqrt{2gh_{1}(t)} \approx a_{1}h_{1}(t) \\ f_{wy2}(t) = A_{w2}\sqrt{2gh_{2}(t)} \approx a_{2}h_{2}(t) \end{cases}$

$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - A_{w1} \sqrt{2gh_1(t)} \\ A_2 \dot{h}_2(t) = A_{w1} \sqrt{2gh_1(t)} - A_{w2} \sqrt{2gh_2(t)} \end{cases}$$

$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - a_1 h_1(t) \\ A_2 \dot{h}_2(t) = a_1 h_1(t) - a_2 h_2(t) \end{cases}$$



$$\begin{split} \begin{cases} A_1 \dot{h}_1(t) &= f_{we}(t) - f_{wy1}(t) \\ A_2 \dot{h}_2(t) &= f_{wy1}(t) - f_{wy2}(t) \\ f_{wy1}(t) &= A_{w1} \sqrt{2g(h_1(t) - h_2(t))} \approx a_1 \big(h_1(t) - h_2(t) \big) \end{cases} \end{split}$$

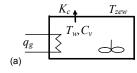
$$f_{wy1}(t) = A_{w1}\sqrt{2g(h_1(t) - h_2(t))} \approx a_1(h_1(t) - h_2(t))$$
$$f_{wy2}(t) = A_{w2}\sqrt{2gh_2(t)} \approx a_2h_2(t)$$

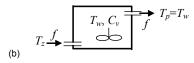
$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - A_{w1} \sqrt{2g(h_1(t) - h_2(t))} \\ A_2 \dot{h}_2(t) = A_{w1} \sqrt{2g(h_1(t) - h_2(t))} - A_{w2} \sqrt{2gh_2(t)} \end{cases}$$

$$\begin{cases} A_1 \dot{h}_1(t) = f_{we}(t) - a_1 \big(h_1(t) - h_2(t) \big) \\ A_2 \dot{h}_2(t) = a_1 \big(h_1(t) - h_2(t) \big) - a_2 h_2(t) \end{cases}$$

2

Obiekty cieplne





Założenie o doskonałym mieszaniu

- 1) Zawartość magazynu $Q(t) = c_p \rho V T(t) = C_V T(t)$
- 2) Zmiana zawartości magazynu $\frac{dQ(t)}{dt} = C_V \, \frac{dT_w(t)}{dt} = C_V \, \dot{T}_w(t)$
- 3) Bilans strumieni wpływających i wypływających [W] $C_{v}\dot{T}_{w}(t)=q_{we}(t)-q_{wv}(t)$

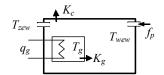
$$C_{v}\dot{T}_{w}(t) = q_{g}(t) - K_{c}(T_{w}(t) - T_{zew}(t))$$

$$C_{v}\dot{T}_{w}(t) = c_{p}\rho f(t)T_{z}(t) - c_{p}\rho f(t)T_{w}(t)$$

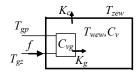
4) Zmienne wejściowe i wyjściowe, kompletność modelu

3

Obiekty cieplne



$$\begin{cases} C_{\scriptscriptstyle \mathcal{W}} \dot{T}_{\scriptscriptstyle \mathcal{W}ew}(t) = K_g \left(T_g(t) - T_{\scriptscriptstyle \mathcal{W}ew}(t) \right) - K_c \left(T_{\scriptscriptstyle \mathcal{W}ew}(t) - T_{\scriptscriptstyle \mathcal{Z}ew}(t) \right) - c_{pp} \rho_p f_p(t) \left(T_{\scriptscriptstyle \mathcal{W}ew}(t) - T_{\scriptscriptstyle \mathcal{Z}ew}(t) \right) \\ C_{\scriptscriptstyle \mathcal{V}g} \dot{T}_g(t) = q_g(t) - K_g \left(T_g(t) - T_{\scriptscriptstyle \mathcal{W}ew}(t) \right) \end{cases}$$



$$\begin{cases} C_{vg}\dot{T}_{gp}(t) = c_{pw}\rho_{pw}f(t)T_{gz}(t) - c_{pw}\rho_{pw}f(t)T_{gp}(t) - K_g\left(T_{gp}(t) - T_{wew}(t)\right) \\ C_{vw}\dot{T}_{wew}(t) = K_g\left(T_{gp}(t) - T_{wew}(t)\right) - K_c\left(T_{wew}(t) - T_{zew}(t)\right) \end{cases}$$

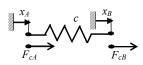
$$\begin{cases} C_{vg} \dot{T}_{gp}(t) = c_{pw} \rho_{pw} f(t) \Big(T_{gz}(t) - T_{gp}(t) \Big) - K_g \Big(T_{gp}(t) - T_{wew}(t) \Big) \\ C_{vw} \dot{T}_{wew}(t) = K_g \Big(T_{gp}(t) - T_{wew}(t) \Big) - K_c \Big(T_{wew}(t) - T_{zew}(t) \Big) \end{cases}$$

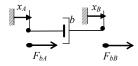
4

Proste układy mechaniczne

Założenie – jeden kierunek działania sił

1) Opis działania układu za pomocą idealnych elementów







$$\begin{split} F_{cA}(t) &= c \big(x_A(t) - x_B(t) \big) \\ F_{bA}(t) &= b \big(\dot{x}_A(t) - \dot{x}_B(t) \big) \\ F_{cB}(t) &= c \big(x_B(t) - x_A(t) \big) \\ \end{split}$$

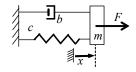
$$F_{bA}(t) = b(\dot{x}_A(t) - \dot{x}_B(t))$$

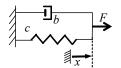
$$F_m(t) = m\ddot{x}(t)$$

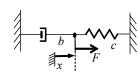
$$F_{cB}(t) = c(x_B(t) - x_A(t))$$

$$F_{bR}(t) = b(\dot{x}_R(t) - \dot{x}_A(t))$$

2) Punkt bilansowania sił







3) Bilans sił [N]

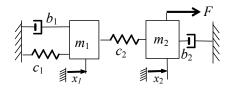
$$m\ddot{x}(t) + b\dot{x}(t) + cx(t) = F(t)$$

$$b\dot{x}(t) + cx(t) = F(t)$$

$$b\dot{x}(t) + cx(t) = F(t)$$

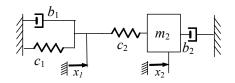
5

Proste układy mechaniczne



$$\begin{cases}
F = m_2 \ddot{x}_2 + b_2 \dot{x}_2 + c_2 (x_2 - x_1) \\
0 = m_1 \ddot{x}_1 + b_1 \dot{x}_1 + c_1 x_1 + c_2 (x_1 - x_2)
\end{cases}$$

(2 punkty, 2 masy)

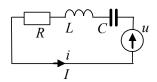


$$\begin{cases} 0 = m_2 \ddot{x}_2 + b_2 \dot{x}_2 + c_2 (x_2 - x_1) \\ 0 = b_1 \dot{x}_1 + c_1 x_1 + c_2 (x_1 - x_2) \end{cases}$$

(2 punkty, 2 masy, bez zewnętrzbej siły)

6

Proste obwody elektryczne



$$\int_{0}^{(1)} j\omega L I + R I + \frac{1}{j\omega C} I = U$$

(2)
$$L\frac{di(t)}{dt} + Ri(t) + \frac{1}{C}\int i(t)dt = u(t)$$
 (3) $L\ddot{q}(t) + R\dot{q}(t) + \frac{1}{C}q(t) = u(t)$

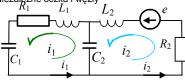
(2)
$$L\frac{di(t)}{dt} + Ri(t) + \frac{1}{C}\int i(t)dt = u(t)$$
 (3) $L\ddot{q}(t) + R\dot{q}(t) + \frac{1}{C}q(t) = u(t)$ (4) $sLi(s) + Ri(s) + \frac{1}{sC}i(s) = u(s)$ (5) $i(s) = \frac{sC}{s^2LC + sRC + 1}u(s)$

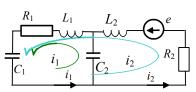
$$u(t) = U\sin(\omega t)$$
 $s = j\omega$ $i(t) = \frac{dq(t)}{dt}$ $i(t) = I\sin(\omega t + \varphi)$ $i(s) = sq(s)$ 7

Proste obwody elektryczne

1) Opis działania układu za pomocą idealnych elementów

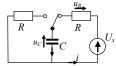
	Opis napięciowo-prądowy $u(i)$		O.prądnapięciowy i(u)	u(q)	Impedancje $Z(s) \mid Z(jm)$	
rezystor (R)	u(t) = Ri(t)	u(s) = Ri(s)	i(t) = Gu(t)	$u(t)=R\dot{q}(t)$	R	R
kondensalor (C)	$u(t) = \frac{1}{C} \int i(t)dt$	$u(s) = \frac{1}{sC}i(s)$	$i(t) = C \frac{du(t)}{dt}$	$u(t) = \frac{1}{C}q(t)$	$\frac{1}{sC}$	1 jecC
eewka (L)	$e_L(t) = -L \frac{di(t)}{dt}$	u(s) - sLi(s)	$i(t) = \frac{1}{L} \int u(t)dt$	$u(t) = L\ddot{q}(t)$	sL	jaL





$$\begin{cases} e = sL_{2}i_{2} + R_{2}i_{2}(s) + \frac{i_{2} - i_{1}}{sC_{2}} \\ 0 = sL_{1}i_{1} + R_{1}i_{1} + \frac{i_{1}}{sC_{1}} + \frac{i_{1} - i_{2}}{sC_{2}} \end{cases} \qquad \begin{cases} e = L_{2}\frac{di_{2}}{dt} + R_{2}i_{2} + \int \frac{i_{2} - i_{1}}{C_{2}} dt \\ 0 = L_{1}\frac{di_{1}}{dt} + R_{1}i_{1} + \int \frac{i_{1}}{C_{1}} dt + \int \frac{i_{1} - i_{2}}{C_{2}} dt \end{cases} \qquad \begin{cases} e = L_{2}\ddot{q}_{2} + R_{2}\dot{q}_{2} + \frac{q_{2} - q_{1}}{C_{2}} \\ 0 = L_{1}\ddot{q}_{1} + R_{1}\dot{q}_{1} + \frac{q_{1}}{C_{1}} + \frac{q_{1} - q_{2}}{C_{2}} \end{cases}$$



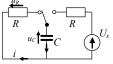


$$u_R(t) + u_C(t) = U_s$$

$$Ri(t) + \frac{q(t)}{g} = U_s$$

$$R\dot{q}(t) + \frac{1}{C}q(t) = U_s$$
 , $q(0) = 0$

r.s.) $R\lambda + \frac{1}{C} = 0 \rightarrow \lambda = -\frac{1}{RC}$



$$u_R(t) + u_C(t) = 0$$

$$Ri(t) + \frac{q(t)}{C} = 0$$

 $\frac{1}{C}q(t) = 0$

 $q_w(t) = 0$

$$R\dot{q}(t) + \frac{1}{C}q(t) = 0$$
 , $q(0) = q_{\text{max}} = CU_s$



$$u_L(t) + u_C(t) = 0$$

$$\begin{aligned} & u_L(t) + u_C(t) = 0 \\ & L \frac{di(t)}{dt} + \frac{1}{C} \int i(t) dt = 0 \\ & L \ddot{q}(t) + \frac{1}{C} q(t) = 0 \end{aligned}$$

$$L\ddot{q}(t) + \frac{1}{C}q(t) = 0$$

$$\ddot{q}(t) + \frac{1}{LC}q(t) = 0$$

$$q_s(t) = Ae^{-\frac{1}{RC}t}$$

$$\mathbf{r.w.}) \frac{1}{C} q(t) = U_s$$

$$q_w(t) = CU_s = q_{\text{max}}$$

r.o.)
$$q(t) = Ae^{-\frac{1}{RC}t} + CU_s$$

w.p.)
$$0 = Ae^{-\frac{1}{RC}0} + CU_s \rightarrow A = -CU_s$$

r.s.) $q(t) = CU_s \left(1 - e^{-\frac{1}{RC}t}\right)$

$$i(t) = \frac{dq(t)}{dt} = \frac{U_s}{R} e^{-\frac{1}{RC}t} , u_C(t) = \frac{q(t)}{C} = \frac{U_s}{RC}$$

$$CU_s = Ae^{\frac{1}{RC}0} {}_s \rightarrow A = CU_s$$

$$q(t) = CU_s e^{\frac{1}{RC}t}$$

$$i(t) = \frac{dq(t)}{dt} = -\frac{U_s}{R}e^{-\frac{1}{RC}t} , u_C(t) = \frac{q(t)}{C} = \frac{U_s}{RC}e^{-\frac{1}{RC}t}$$

