Filter Design #1

EE23BTECH11013 - Avyaaz

1 Introduction

We are supposed to design the equivalent FIR and IIR filter realizations for filter number 1. The filter numbers are calculated using the below code:

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/0 FilterNum.py

This is a bandpass filter whose specifications are available below.

2 Filter Specifications

The sampling rate for the filter has been specified as $F_s = 48$ kHz. If the un-normalized discrete-time (natural) frequency is F, the corresponding normalized digital filter (angular) frequency is given by $\omega = 2\pi \left(\frac{F}{F_s}\right)$.

2.1 The Digital Filter

- i) *Tolerances:* The passband (δ_1) and stopband (δ_2) tolerances are given to be equal, so we let $\delta_1 = \delta_2 = \delta = 0.15$.
- ii) Passband: The passband of filter number j, j going from 0 to 13 is from {4 + 0.6j}kHz to {4 + 0.6(j + 2)}kHz. Since our filter number is 1, substituting j = 1 gives the passband range for our bandpass filter as 4.6 kHz 5.8 kHz. Hence, the un-normalized discrete time filter passband frequencies are:

$$F_{p_1} = 5.8 \text{ kHz}$$
 (2.1.1)

$$F_{p_2} = 4.6 \text{ kHz}$$
 (2.1.2)

The corresponding normalized digital filter passband frequencies are:

$$\omega_{p_1} = 2\pi \frac{F_{p_1}}{F_s} = 0.2416\pi \text{ kHz}$$
 (2.1.3)

$$\omega_{p_2} = 2\pi \frac{F_{p_2}}{F_s} = 0.1916\pi \text{ kHz}$$
 (2.1.4)

The centre frequency is then given by:

$$\omega_c = \frac{\omega_{p_1} + \omega_{p_2}}{2} = 0.2166\pi \tag{2.1.5}$$

iii) Stopband: The transition band for bandpass filters is $\Delta F = 0.3$ kHz on either side of the passband. Hence, the un-normalized stopband frequencies are $F_{s_1} = 5.8 + 0.3 = 6.1$ kHz and $F_{s_2} = 4.6 - 0.3 = 4.3$ kHz. The corresponding normalized frequencies are $\omega_{s_1} = 0.25416\pi$ and $\omega_{s_2} = 0.17916\pi$.

2.2 The Analog filter

In the bilinear transform, the analog filter frequency (Ω) is related to the corresponding digital filter frequency (ω) as:

$$\Omega = \tan \frac{\omega}{2} \tag{2.2.1}$$

Using this relation, we obtain the analog passband and stopband frequencies as $\Omega_{p_1} = 0.399$, $\Omega_{p_2} = 0.311$ and $\Omega_{s_1} = 0.422$, $\Omega_{s_2} = 0.289$ respectively.

3 The IIR Filter Design

Filter Type: We are supposed to design filters whose stopband is monotonic and passband equiripple. Hence, we use the Chebyschev approximation to design our bandpass IIR filter.

3.1 The Analog Filter

1) Low Pass Filter Specifications: If $H_{a,BP}(j\Omega)$ be the desired analog band pass filter, with the specifications provided in Section 2.2, and $H_{a,LP}(j\Omega_L)$ be the equivalent low pass filter, then

$$\Omega_L = \frac{\Omega^2 - \Omega_0^2}{B\Omega} \tag{3.1.1}$$

where.

 $\Omega_0 = \sqrt{\Omega_{p1}\Omega_{p2}} = 0.352$ and $B = \Omega_{p1} - \Omega_{p2} = 0.088$. The low pass filter has the passband edge at $\Omega_{Lp} = 1$ and stopband edges at $\Omega_{Ls_1} = 1.459$ and $\Omega_{Ls_2} = -1.588$. We choose the stopband edge of the analog low pass filter as $\Omega_{Ls} = \min(|\Omega_{Ls_1}|, |\Omega_{Ls_2}|) = 1.459$.

2) The Low Pass Chebyschev Filter Paramters: The magnitude squared of the Chebyschev low pass filter is given by

$$|H_{a,LP}(j\Omega_L)|^2 = \frac{1}{1 + \epsilon^2 c_N^2(\Omega_L/\Omega_{Lp})}$$
 (3.1.2)

where,

$$c_N(x) = \begin{cases} \cosh(N\cosh^{-1}x) & x > 1\\ \cos(N\cos^{-1}x) & |x| \le 1 \end{cases}$$

 $N \in \mathbb{Z}$ which is the order of the filter, and ϵ are design parameters. Since $\Omega_{Lp} = 1$, (3.1.2) may be rewritten as

$$|H_{a,LP}(j\Omega_L)|^2 = \frac{1}{1 + \epsilon^2 c_N^2(\Omega_L)}$$
 (3.1.3)

Also, the design paramters have the following constraints

$$\frac{\sqrt{D_2}}{c_N(\Omega_{Ls})} \le \epsilon \le \sqrt{D_1},$$

$$N \ge \left[\frac{\cosh^{-1} \sqrt{D_2/D_1}}{\cosh^{-1} \Omega_{Ls}} \right],$$
(3.1.4)

where $D_1 = \frac{1}{(1-\delta)^2} - 1$ and $D_2 = \frac{1}{\delta^2} - 1$. After appropriate substitutions, we obtain:

$$0.337 \le \epsilon \le 0.6197 \tag{3.1.5}$$

$$N \ge 4 \tag{3.1.6}$$

$$D_1 = 0.3841 \tag{3.1.7}$$

$$D_2 = 43.444 \tag{3.1.8}$$

Below is the code which plots the Fig. 1:

wget https://github.com/Avyaaz13/Audio-Filtering/ blob/main/Filter%20Design/codes/1 epsilon.py

In Fig. 1, we plot $|H(j\Omega)|$ for a range of values of ϵ , for N=4. We find that for larger values of ϵ , $|H(j\Omega)|$ decreases in the transition band. We choose $\epsilon=0.4$ for our IIR filter design.

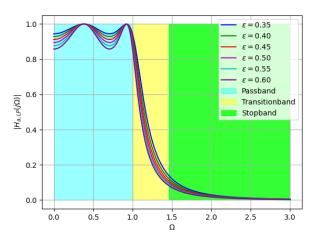


Fig. 1: The Analog Low-Pass Frequency Response for $0.35 \le \epsilon \le 0.6$

3) The Low Pass Chebyschev Filter: Thus, we obtain

$$|H_{a,LP}(j\Omega_L)|^2 = \frac{1}{1 + 0.16c_4^2(\Omega_L)}$$
 (3.1.9)

where

$$c_4(x) = 8x^4 - 8x^2 + 1.$$
 (3.1.10)

The poles of the frequency response in (3.1.2) are general obtained as $r_1 \cos \phi_k + jr_2 \sin \phi_k$, where

$$\phi_k = \frac{\pi}{2} + \frac{(2k+1)\pi}{2N}, k = 0, 1, \dots, 2N - 1$$

$$r_1 = \frac{\beta^2 - 1}{2\beta}, r_2 = \frac{\beta^2 + 1}{2\beta}, \beta = \left[\frac{\sqrt{1 + \epsilon^2} + 1}{\epsilon}\right]^{\frac{1}{N}} (3.1.11)$$

Thus, for N even, the low-pass stable Chebyschev filter, with a gain G has the form

$$H_{a,LP}(s_L) = \frac{G_{LP}}{\prod_{k=0}^{\frac{N}{2}-1} (s_L^2 - 2r_1 \cos \phi_k s_L + r_1^2 \cos^2 \phi_k + r_2^2 \sin^2 \phi_k)}$$
(3.1.12)

Substituting N=4, $\epsilon=0.4$ and $H_{a,LP}(j)=\frac{1}{\sqrt{1+\epsilon^2}}$, from (3.1.11) and (3.1.12), we obtain

$$H_{a,LP}(s_L) = \frac{0.3125}{s_L^4 + 1.1068s_L^3 + 1.6125s_L^2 + 0.9140s_L + 0.3366}$$
(3.1.13)

Below is the code which plots the Fig. 2:

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/2_design.py

In Fig. 2 we plot $|H(j\Omega)|$ using (3.1.9) and (3.1.13), thereby verifying that our low-pass Chebyschev filter design meets the specifications.

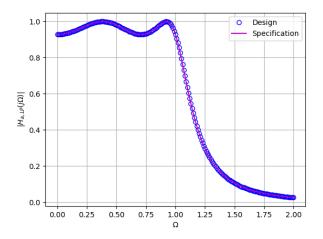


Fig. 2: The magnitude response plots from the specifications in Equation 3.1.9 and the design in Equation 3.1.13

Below is the code of pole-zero plot of the (3.1.9):

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/pole-zero.py

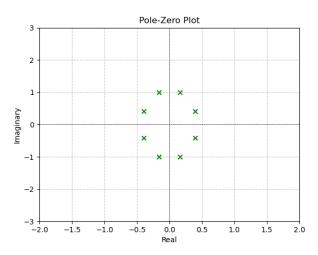


Fig. 3: Pole-Zero plot of $H_{a,LP}(j\Omega_L)$

4) The Band Pass Chebyschev Filter: The analog bandpass filter is obtained from (3.1.13) by substituting $s_L = \frac{s^2 + \Omega_0^2}{Bs}$. Hence

$$H_{a,BP}(s) = G_{BP}H_{a,LP}(s_L)|_{\substack{s_L = \frac{s^2 + \Omega_0^2}{Bs}}},$$
 (3.1.14)

where G_{BP} is the gain of the bandpass filter. After appropriate substitutions, and evaluating the gain such that $H_{a,BP}(j\Omega_{p1})=1$, we obtain

$$H_{a,BP}(s) = \frac{1.908 \times 10^{-5} s^4}{s^8 + 0.0979 s^7 + 0.5081 s^6 + 0.0370 s^5 + 0.0952 s^4 + 0.0046 s^3 + 0.0078 s^2 + 0.0002 s + 0.0002}$$
(3.1.15)

$$G_{BP} = 1.048 \times 10^{-5}$$
 (3.1.16)

Below is the code which plots the Fig. 4:

In Fig. 4, we plot $|H_{a,BP}(j\Omega)|$ as a function of Ω for both positive as well as negative frequencies. We find that the passband and stopband frequencies in the figure match well with those obtained analytically through the bilinear transformation.

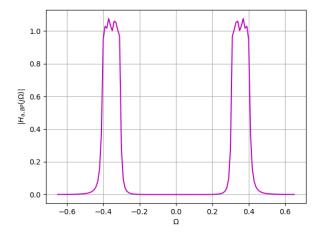


Fig. 4: The analog bandpass magnitude response plot from Equation 3.1.15

3.2 The Digital Filter

From the bilinear transformation, we obtain the digital bandpass filter from the corresponding analog filter as

$$H_{d,BP}(z) = GH_{a,BP}(s)|_{s=\frac{1-z^{-1}}{1+z^{-1}}}$$
 (3.2.1)

where G is the gain of the digital filter. From (3.1.15) and (3.2.1), we obtain

$$H_{d,BP}(z) = G\frac{N(z)}{D(z)}$$
(3.2.2)

where $G = 1.908 \times 10^{-5}$,

$$N(z) = 1 - 4z^{-2} + 6z^{-4} - 4z^{-6} + z^{-8}$$
 (3.2.3)

and

$$D(z) = 1.7511 - 10.6506z^{-1} + 30.9794z^{-2} - 55.1588z^{-3} + 65.4285z^{-4}$$
$$-52.8121z^{-5} + 28.3995z^{-6} - 9.3484z^{-7} + 1.4717z^{-8}3.2.4$$

The plot of $|H_{d,BP}(z)|$ with respect to the normalized angular frequency (normalizing factor π) is available in Fig. 5. Again we find that the passband and stopband frequencies meet the specifications well enough.

Below is the code which plots the Fig. 5:

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/4 iir d.py

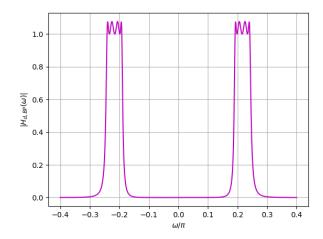


Fig. 5: The magnitude response of the bandpass digital filter designed to meet the given specifications

4 The FIR Filter

We design the FIR filter by first obtaining the (non-causal) lowpass equivalent using the Kaiser window and then converting it to a causal bandpass filter.

4.1 The Equivalent Lowpass Filter

The lowpass filter has a passband frequency ω_l and transition band $\Delta\omega = 2\pi \frac{\Delta F}{F_s} = 0.0125\pi$. The stopband tolerance is δ .

1) The passband frequency ω_l is defined as:

$$\omega_l = \frac{\omega_{p1} - \omega_{p2}}{2} \tag{4.1.1}$$

Substituting the values of ω_{p1} and ω_{p2} from Section 2.1, we obtain $\omega_l = 0.025\pi$.

2) The impulse response $h_{lp}(n)$ of the desired lowpass filter with cutoff frequency ω_l is given by

$$h_l(n) = \frac{\sin(n\omega_l)}{n\pi} w(n), \tag{4.1.2}$$

where w(n) is the Kaiser window obtained from the design specifications.

3) The impulse response of ideal Low Pass Filter is given by :

$$h(n) = \begin{cases} \frac{\sin(w_l n)}{n\pi}, & n \neq 0\\ \frac{w_l}{\pi}, & n = 0 \end{cases}$$
 (4.1.3)

From (4.1.3) we conclude that h(n) for an ideal Low Pass Filter is not causal and can neither be made causal by introducing a finite delay. And h(n) do not converge and hence the system is unstable.

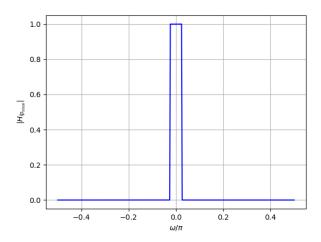


Fig. 6: Frequency plot of the ideal low pass filter

4.2 The Kaiser Window

The Kaiser window is defined as

$$w(n) = \begin{cases} \frac{I_0 \left[\beta N \sqrt{1 - \left(\frac{n}{N}\right)^2}\right]}{I_0(\beta N)}, & -N \le n \le N, \quad \beta > 0 \\ 0 & \text{otherwise,} \end{cases}$$
 (4.2.1)

where $I_0(x)$ is the modified Bessel function of the first kind of order zero in x and β and N are the window shaping factors. In the following, we find β and N using the design parameters in 2.1

1) N is chosen according to

$$N \ge \frac{A - 8}{4.57\Delta\omega},\tag{4.2.2}$$

where $A = -20 \log_{10} \delta$. Substituting the appropriate values from the design specifications, we obtain A = 16.4782 and $N \ge 48$.

2) β is chosen according to

$$\beta N = \begin{cases} 0.1102(A - 8.7) & A > 50\\ 0.5849(A - 21)^{0.4} + 0.07886(A - 21) & 21 \le A \le 500\\ 0 & A < 21 \end{cases}$$

In our design, we have A = 16.4782 < 21. Hence, from (4.2.3) we obtain $\beta = 0$.

3) We choose N = 100, to ensure the desired low pass filter response. Substituting in (4.2.1) gives us the rectangular window

$$w(n) = \begin{cases} 1, -100 \le n \le 100 \\ 0 \text{ otherwise} \end{cases}$$
 (4.2.4)

From (4.1.2) and (4.2.4), we obtain the desired lowpass filter impulse response

$$h_{lp}(n) = \begin{cases} \frac{\sin(\frac{n\pi}{40})}{n\pi} & -100 \le n \le 100\\ 0, & \text{otherwise} \end{cases}$$
 (4.2.5)

Below is the code which plots Fig. 7:

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/hlp.py

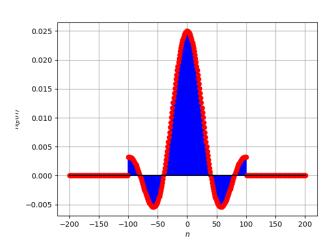


Fig. 7: Impulse response of low pass FIR filter

Below is the code which plots Fig. 8:

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/5 fir lp.py

The magnitude response of the filter in (4.2.5) is shown in Fig. 8.

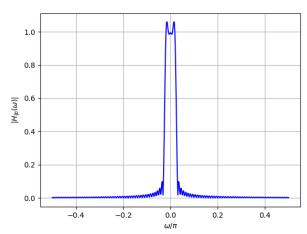


Fig. 8: The magnitude response of the FIR lowpass digital filter designed to meet the given specifications

4.3 The FIR Bandpass Filter

The centre of the passband of the desired bandpass filter was found to be $\omega_c = 0.2166\pi$ in Section 2.1. The impulse response of the desired bandpass filter is obtained from the impulse response of the corresponding lowpass filter as

$$h_{bp}(n) = 2h_{lp}(n)cos(n\omega_c)$$
 (4.3.1)

Thus, from (4.2.5), we obtain

$$h_{bp}(n) = \begin{cases} \frac{2\sin(\frac{n\pi}{40})\cos(\frac{13n\pi}{60})}{n\pi} & -100 \le n \le 100\\ 0, & \text{otherwise} \end{cases}$$

Below is the code which plots Fig. 9:

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/hbp.py

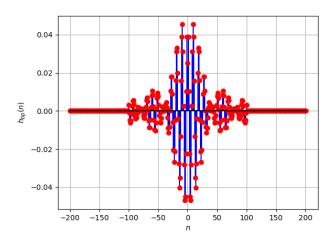


Fig. 9: Impulse response of BandPass FIR filter

Below is the code which plots Fig. 10:

wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/6_fir_bp.py

The magnitude response of the FIR bandpass filter designed to meet the given specifications is plotted in Fig. 10.

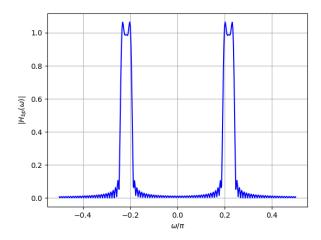


Fig. 10: The magnitude response of the FIR bandpass digital filter designed to meet the given specifications