

# Filter Design #1

EE23BTECH11013 - Avyaaz

## 1 Introduction

We are supposed to design the equivalent FIR and IIR filter realizations for filter number 1. The filter numbers are calculated using the below code:

```
wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/0_FilterNum.py
```

This is a bandpass filter whose specifications are available below.

## 2 Filter Specifications

The sampling rate for the filter has been specified as  $F_s = 48$  kHz. If the un-normalized discrete-time (natural) frequency is  $F$ , the corresponding normalized digital filter (angular) frequency is given by  $\omega = 2\pi\left(\frac{F}{F_s}\right)$ .

### 2.1 The Digital Filter

- i) *Tolerances*: The passband ( $\delta_1$ ) and stopband ( $\delta_2$ ) tolerances are given to be equal, so we let  $\delta_1 = \delta_2 = \delta = 0.15$ .
- ii) *Passband*: The passband of filter number  $j$ ,  $j$  going from 0 to 13 is from  $\{4 + 0.6j\}$  kHz to  $\{4 + 0.6(j + 2)\}$  kHz. Since our filter number is 1, substituting  $j = 1$  gives the passband range for our bandpass filter as 4.6 kHz - 5.8 kHz. Hence, the un-normalized discrete time filter passband frequencies are:

$$F_{p1} = 5.8 \text{ kHz} \quad (2.1.1)$$

$$F_{p2} = 4.6 \text{ kHz} \quad (2.1.2)$$

The corresponding normalized digital filter passband frequencies are:

$$\omega_{p1} = 2\pi \frac{F_{p1}}{F_s} = 0.2416\pi \text{ kHz} \quad (2.1.3)$$

$$\omega_{p2} = 2\pi \frac{F_{p2}}{F_s} = 0.1916\pi \text{ kHz} \quad (2.1.4)$$

The centre frequency is then given by:

$$\omega_c = \frac{\omega_{p1} + \omega_{p2}}{2} = 0.2166\pi \quad (2.1.5)$$

- iii) *Stopband*: The *transition band* for bandpass filters is  $\Delta F = 0.3$  kHz on either side of the passband. Hence, the un-normalized *stopband* frequencies are  $F_{s1} = 5.8 + 0.3 = 6.1$  kHz and  $F_{s2} = 4.6 - 0.3 = 4.3$  kHz. The corresponding normalized frequencies are  $\omega_{s1} = 0.25416\pi$  and  $\omega_{s2} = 0.17916\pi$ .

## 2.2 The Analog filter

In the bilinear transform, the analog filter frequency ( $\Omega$ ) is related to the corresponding digital filter frequency ( $\omega$ ) as:

$$\Omega = \tan \frac{\omega}{2} \quad (2.2.1)$$

Using this relation, we obtain the analog passband and stopband frequencies as  $\Omega_{p1} = 0.399$ ,  $\Omega_{p2} = 0.311$  and  $\Omega_{s1} = 0.422$ ,  $\Omega_{s2} = 0.289$  respectively.

## 3 The IIR Filter Design

*Filter Type*: We are supposed to design filters whose stopband is monotonic and passband equiripple. Hence, we use the *Chebyshev approximation* to design our bandpass IIR filter.

### 3.1 The Analog Filter

- 1) *Low Pass Filter Specifications*: If  $H_{a,BP}(j\Omega)$  be the desired analog band pass filter, with the specifications provided in Section 2.2, and  $H_{a,LP}(j\Omega_L)$  be the equivalent low pass filter, then

$$\Omega_L = \frac{\Omega^2 - \Omega_0^2}{B\Omega} \quad (3.1.1)$$

where,

$\Omega_0 = \sqrt{\Omega_{p1}\Omega_{p2}} = 0.352$  and  $B = \Omega_{p1} - \Omega_{p2} = 0.088$ . The low pass filter has the passband edge at  $\Omega_{Lp} = 1$  and stopband edges at  $\Omega_{Ls1} = 1.459$  and  $\Omega_{Ls2} = -1.588$ . We choose the stopband edge of the analog low pass filter as  $\Omega_{Ls} = \min(|\Omega_{Ls1}|, |\Omega_{Ls2}|) = 1.459$ .

- 2) *The Low Pass Chebyshev Filter Parameters*: The magnitude squared of the Chebyshev low pass filter is given by

$$|H_{a,LP}(j\Omega_L)|^2 = \frac{1}{1 + \epsilon^2 c_N^2(\Omega_L/\Omega_{Lp})} \quad (3.1.2)$$

where,

$$c_N(x) = \begin{cases} \cosh(N \cosh^{-1} x) & |x| > 1 \\ \cos(N \cos^{-1} x) & |x| \leq 1 \end{cases}$$

$N \in \mathbb{Z}$  which is the order of the filter, and  $\epsilon$  are design parameters. Since  $\Omega_{Lp} = 1$ , (3.1.2) may be rewritten as

$$|H_{a,LP}(j\Omega_L)|^2 = \frac{1}{1 + \epsilon^2 c_N^2(\Omega_L)} \quad (3.1.3)$$

Also, the design parameters have the following constraints

$$\begin{aligned} \frac{\sqrt{D_2}}{c_N(\Omega_{Ls})} &\leq \epsilon \leq \sqrt{D_1}, \\ N &\geq \left\lceil \frac{\cosh^{-1} \sqrt{D_2/D_1}}{\cosh^{-1} \Omega_{Ls}} \right\rceil, \end{aligned} \quad (3.1.4)$$

where  $D_1 = \frac{1}{(1-\delta)^2} - 1$  and  $D_2 = \frac{1}{\delta^2} - 1$ . After appropriate substitutions, we obtain:

$$0.337 \leq \epsilon \leq 0.6197 \quad (3.1.5)$$

$$N \geq 4 \quad (3.1.6)$$

$$D_1 = 0.3841 \quad (3.1.7)$$

$$D_2 = 43.444 \quad (3.1.8)$$

Below is the code which plots the Fig. 1:

```
wget https://github.com/Avyaaz13/Audio-Filtering/
blob/main/Filter%20Design/codes/1_epsilon.py
```

In Fig. 1, we plot  $|H(j\Omega)|$  for a range of values of  $\epsilon$ , for  $N = 4$ . We find that for larger values of  $\epsilon$ ,  $|H(j\Omega)|$  decreases in the transition band. We choose  $\epsilon = 0.4$  for our IIR filter design.

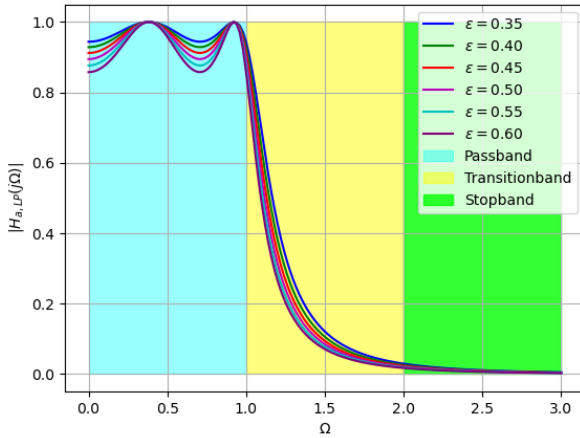


Fig. 1: The Analog Low-Pass Frequency Response for  $0.35 \leq \epsilon \leq 0.6$

3) *The Low Pass Chebyshev Filter:* Thus, we obtain

$$|H_{a,LP}(j\Omega_L)|^2 = \frac{1}{1 + 0.16c_4^2(\Omega_L)} \quad (3.1.9)$$

where

$$c_4(x) = 8x^4 - 8x^2 + 1. \quad (3.1.10)$$

The poles of the frequency response in (3.1.2) are general obtained as  $r_1 \cos \phi_k + jr_2 \sin \phi_k$ , where

$$\phi_k = \frac{\pi}{2} + \frac{(2k+1)\pi}{2N}, k = 0, 1, \dots, 2N-1$$

$$r_1 = \frac{\beta^2 - 1}{2\beta}, r_2 = \frac{\beta^2 + 1}{2\beta}, \beta = \left[ \frac{\sqrt{1 + \epsilon^2} + 1}{\epsilon} \right]^{\frac{1}{N}} \quad (3.1.11)$$

Thus, for  $N$  even, the low-pass stable Chebyshev filter, with a gain  $G$  has the form

$$H_{a,LP}(s_L) = \frac{G_{LP}}{\prod_{k=0}^{\frac{N}{2}-1} (s_L^2 - 2r_1 \cos \phi_k s_L + r_1^2 \cos^2 \phi_k + r_2^2 \sin^2 \phi_k)} \quad (3.1.12)$$

Substituting  $N = 4$ ,  $\epsilon = 0.4$  and  $H_{a,LP}(j) = \frac{1}{\sqrt{1+\epsilon^2}}$ , from (3.1.11) and (3.1.12), we obtain

$$H_{a,LP}(s_L) = \frac{0.3125}{s_L^4 + 1.1068s_L^3 + 1.6125s_L^2 + 0.9140s_L + 0.3366} \quad (3.1.13)$$

Below is the code which plots the Fig. 2:

```
wget https://github.com/Avyaaz13/Audio-Filtering/
blob/main/Filter%20Design/codes/2_design.py
```

In Fig. 2 we plot  $|H(j\Omega)|$  using (3.1.9) and (3.1.13), thereby verifying that our low-pass Chebyshev filter design meets the specifications.

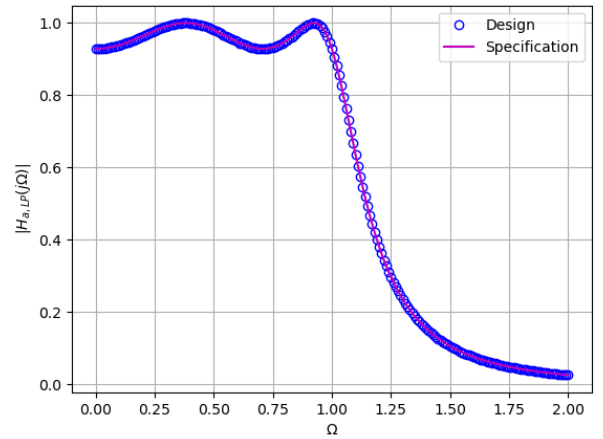


Fig. 2: The magnitude response plots from the specifications in Equation 3.1.9 and the design in Equation 3.1.13

Below is the code of pole-zero plot of the (3.1.9):

```
wget https://github.com/Avyaaz13/Audio-Filtering/
blob/main/Filter%20Design/codes/pole-zero.py
```

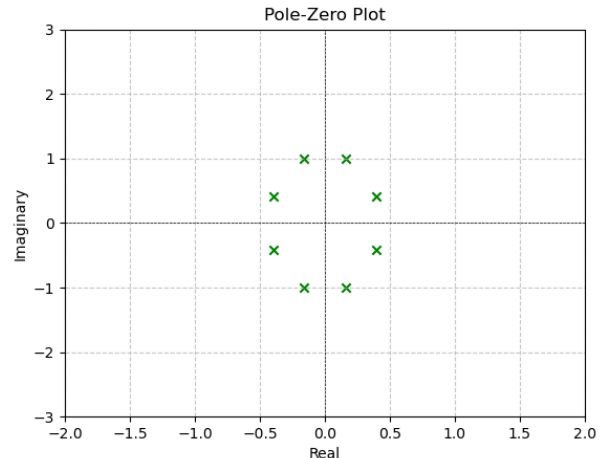


Fig. 3: Pole-Zero plot of  $H_{a,LP}(j\Omega_L)$

- 4) *The Band Pass Chebyshev Filter*: The analog bandpass filter is obtained from (3.1.13) by substituting  $s_L = \frac{s^2 + \Omega_0^2}{Bs}$ . Hence

$$H_{a,BP}(s) = G_{BP}H_{a,LP}(s_L) \Big|_{s_L = \frac{s^2 + \Omega_0^2}{Bs}}, \quad (3.1.14)$$

where  $G_{BP}$  is the gain of the bandpass filter. After appropriate substitutions, and evaluating the gain such that  $H_{a,BP}(j\Omega_{p1}) = 1$ , we obtain

$$H_{a,BP}(s) = \frac{2.0601 \times 10^{-5} s^4}{s^8 + 0.0979s^7 + 0.5081s^6 + 0.0370s^5 + 0.0952s^4 + 0.0046s^3 + 0.0078s^2 + 0.0002s + 0.0002} \quad (3.1.15)$$

$$G_{BP} = 2.0601 \times 10^{-5} \quad (3.1.16)$$

Below is the code which plots the Fig. 4:

```
wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/3_iir_1.py
```

In Fig. 4, we plot  $|H_{a,BP}(j\Omega)|$  as a function of  $\Omega$  for both positive as well as negative frequencies. We find that the passband and stopband frequencies in the figure match well with those obtained analytically through the bilinear transformation.

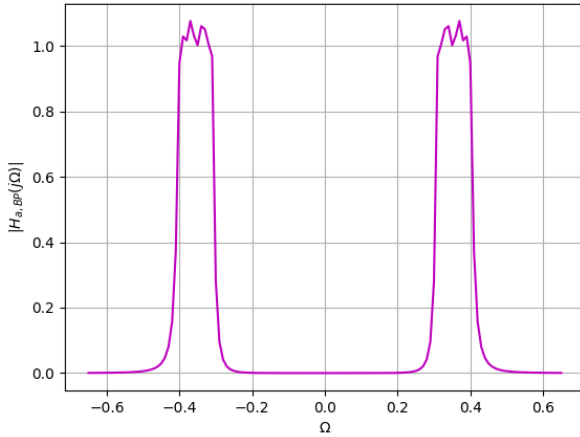


Fig. 4: The analog bandpass magnitude response plot from Equation 3.1.15

### 3.2 The Digital Filter

From the bilinear transformation, we obtain the digital bandpass filter from the corresponding analog filter as

$$H_{d,BP}(z) = GH_{a,BP}(s) \Big|_{s = \frac{1-z^{-1}}{1+z^{-1}}} \quad (3.2.1)$$

where  $G$  is the gain of the digital filter. From (3.1.15) and (3.2.1), we obtain

$$H_{d,BP}(z) = G \frac{N(z)}{D(z)} \quad (3.2.2)$$

where  $G = 2.0601 \times 10^{-5}$ ,

$$N(z) = 1 - 4z^{-2} + 6z^{-4} - 4z^{-6} + z^{-8} \quad (3.2.3)$$

and

$$D(z) = 1.7511 - 10.6506z^{-1} + 30.9794z^{-2} - 55.1588z^{-3} + 65.4285z^{-4} - 52.8121z^{-5} + 28.3995z^{-6} - 9.3484z^{-7} + 1.4717z^{-8} \quad (3.2.4)$$

The plot of  $|H_{d,BP}(z)|$  with respect to the normalized angular frequency (normalizing factor  $\pi$ ) is available in Fig. 5. Again we find that the passband and stopband frequencies meet the specifications well enough.

Below is the code which plots the Fig. 5:

```
wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/4_iir_d.py
```

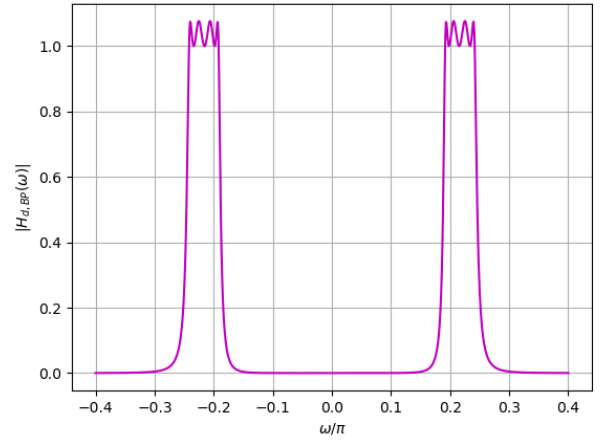


Fig. 5: The magnitude response of the bandpass digital filter designed to meet the given specifications

## 4 The FIR Filter

We design the FIR filter by first obtaining the (non-causal) lowpass equivalent using the Kaiser window and then converting it to a causal bandpass filter.

### 4.1 The Equivalent Lowpass Filter

The lowpass filter has a passband frequency  $\omega_l$  and transition band  $\Delta\omega = 2\pi \frac{\Delta F}{F_s} = 0.0125\pi$ . The stopband tolerance is  $\delta$ .

- 1) The *passband frequency*  $\omega_l$  is defined as:

$$\omega_l = \frac{\omega_{p1} - \omega_{p2}}{2} \quad (4.1.1)$$

Substituting the values of  $\omega_{p1}$  and  $\omega_{p2}$  from Section 2.1, we obtain  $\omega_l = 0.025\pi$ .

- 2) The *impulse response*  $h_l(n)$  of the desired lowpass filter with cutoff frequency  $\omega_l$  is given by

$$h_l(n) = \frac{\sin(n\omega_l)}{n\pi} w(n), \quad (4.1.2)$$

where  $w(n)$  is the Kaiser window obtained from the design specifications.

- 3) The impulse response of ideal Low Pass Filter is given by :

$$h(n) = \begin{cases} \frac{\sin(\omega_l n)}{n\pi}, & n \neq 0 \\ \frac{\omega_l}{\pi}, & n = 0 \end{cases} \quad (4.1.3)$$

From (4.1.3) we conclude that  $h(n)$  for an ideal Low Pass Filter is not causal and can neither be made causal by introducing a finite delay. And  $h(n)$  do not converge and hence the system is unstable.

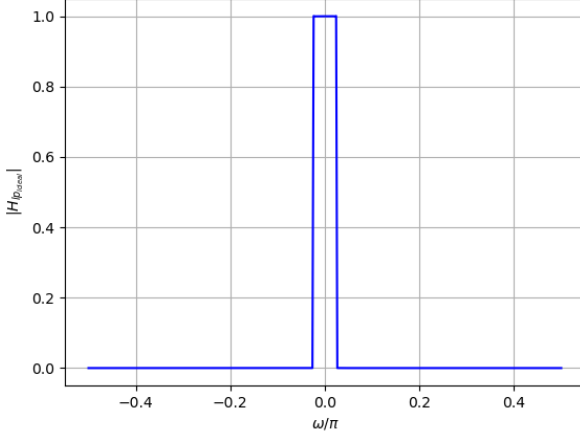


Fig. 6: Frequency plot of the ideal low pass filter

## 4.2 The Kaiser Window

The Kaiser window is defined as

$$w(n) = \begin{cases} \frac{I_0\left[\beta N \sqrt{1 - \left(\frac{n}{N}\right)^2}\right]}{I_0(\beta N)}, & -N \leq n \leq N, \quad \beta > 0 \\ 0 & \text{otherwise,} \end{cases} \quad (4.2.1)$$

where  $I_0(x)$  is the modified Bessel function of the first kind of order zero in  $x$  and  $\beta$  and  $N$  are the window shaping factors. In the following, we find  $\beta$  and  $N$  using the design parameters in 2.1

- 1)  $N$  is chosen according to

$$N \geq \frac{A - 8}{4.57\Delta\omega}, \quad (4.2.2)$$

where  $A = -20 \log_{10} \delta$ . Substituting the appropriate values from the design specifications, we obtain  $A = 16.4782$  and  $N \geq 48$ .

- 2)  $\beta$  is chosen according to

$$\beta N = \begin{cases} 0.1102(A - 8.7) & A > 50 \\ 0.5849(A - 21)^{0.4} + 0.07886(A - 21) & 21 \leq A \leq 50 \\ 0 & A < 21 \end{cases}$$

In our design, we have  $A = 16.4782 < 21$ . Hence, from (4.2.3) we obtain  $\beta = 0$ .

- 3) We choose  $N = 100$ , to ensure the desired low pass filter response. Substituting in (4.2.1) gives us the rectangular window

$$w(n) = \begin{cases} 1, & -100 \leq n \leq 100 \\ 0 & \text{otherwise} \end{cases} \quad (4.2.4)$$

From (4.1.2) and (4.2.4), we obtain the desired lowpass filter impulse response

$$h_{lp}(n) = \begin{cases} \frac{\sin(\frac{n\pi}{40})}{n\pi} & -100 \leq n \leq 100 \\ 0, & \text{otherwise} \end{cases} \quad (4.2.5)$$

Below is the code which plots Fig. 7:

```
wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/hlp.py
```

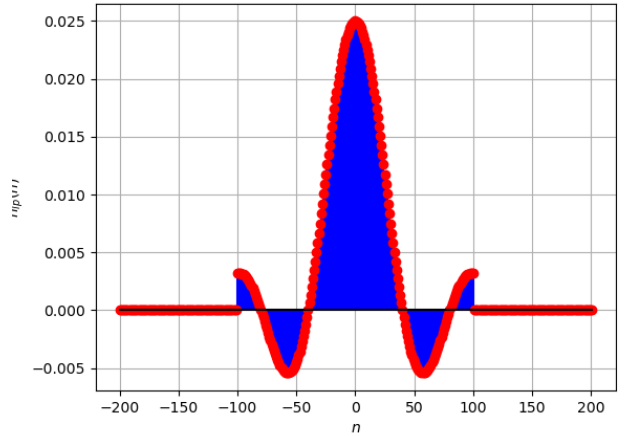


Fig. 7: Impulse response of low pass FIR filter

Below is the code which plots Fig. 8:

```
wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/5_fir_lp.py
```

The magniude response of the filter in (4.2.5) is shown in Fig. 8.

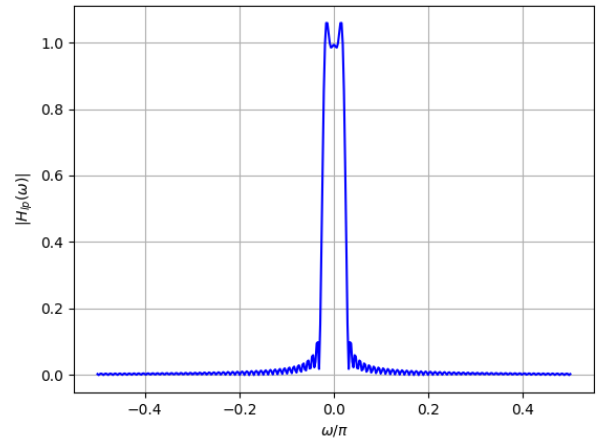


Fig. 8: The magniude response of the FIR lowpass digital filter designed to meet the given specifications

### 4.3 The FIR Bandpass Filter

The centre of the passband of the desired bandpass filter was found to be  $\omega_c = 0.2166\pi$  in Section 2.1. The impulse response of the desired bandpass filter is obtained from the impulse response of the corresponding lowpass filter as

$$h_{bp}(n) = 2h_l(n)\cos(n\omega_c) \quad (4.3.1)$$

Thus, from (4.2.5), we obtain

$$h_{bp}(n) = \begin{cases} \frac{2 \sin(\frac{n\pi}{40}) \cos(\frac{13n\pi}{60})}{n\pi} & -100 \leq n \leq 100 \\ 0, & \text{otherwise} \end{cases}$$

Below is the code which plots Fig. 9:

```
wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/hbp.py
```

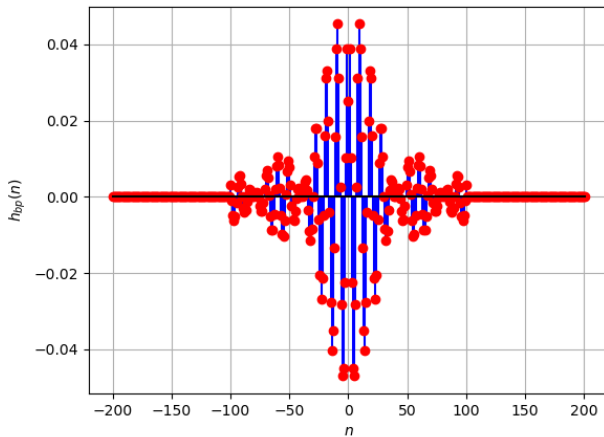


Fig. 9: Impulse response of BandPass FIR filter

Below is the code which plots Fig. 10:

```
wget https://github.com/Avyaaz13/Audio-Filtering/blob/main/Filter%20Design/codes/6_fir_bp.py
```

The magnitude response of the FIR bandpass filter designed to meet the given specifications is plotted in Fig. 10.

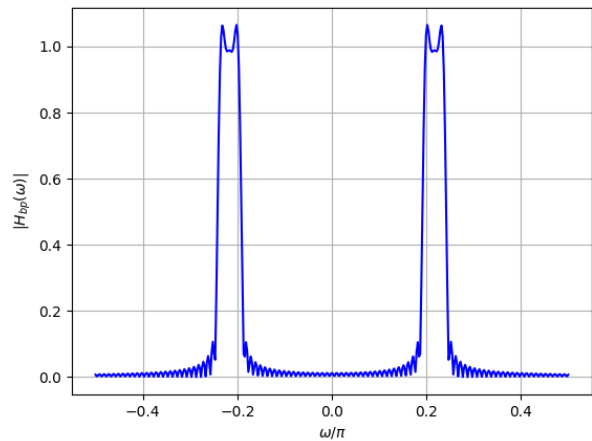


Fig. 10: The magnitude response of the FIR bandpass digital filter designed to meet the given specifications