Fluid Mechanics

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Basic Concepts

Heading	Definition	
Viscous Fluid	A fluid is called a Viscous fluid if it has both Normal And shear Force, if non-viscous it doesn't have a shear force value	
Viscosity	Viscosity of a fluid is the property by which it exhibits resistance to the alteration of the form when upper plate moves in x dirn with certain velocity but the lower plate is stationary	
Laminar Flow	A flow in which each particle traverses a definite curve, and the curve traced by any two particles never intersect.	
Steady Flow	A flow in which we have that the properties such as temperature and pressure independent of time is called steady flow	
Langrage Approach	We compare position p_0 at time t_0 with position p_1 at time t_1 i.e $V = f(V_0, t, t_0) \\ \frac{dV}{dt} = \sum_i \left(\frac{dx_i}{dt} \; \hat{x}_i\right)$	
Euler	We fix a point in space and look how fluid is behaving at that point $V, \frac{dV}{dt}, \frac{d^2V}{dt^2}$	

Important Theorems

Heading	Definition
Stokes Law	Let S be an open surface bounded by a closed curve C then $\int_C \vec{F} d\vec{r} = \int \int \int_S (\nabla \times \mathbf{F}) \hat{n} ds$
Gauss Divergence Theorem	Let S be a closed surface bounding a Volume V, and let \hat{n} be a unit vector perpendicular to the surface of V then $\int \int_S \vec{F} \cdot \hat{n} \ dS = \int \int \int_V \vec{\nabla} \cdot \vec{F} \ dV$
Green's theorem	Let ϕ and φ be continuous differentiable function $\int_C \phi \times \frac{d\varphi}{dt} - \varphi \times \frac{d\phi}{dt} \ ds = \int_S \phi \ \nabla^2 \varphi - \varphi \nabla^2 \phi \ dx \ dy$

Important Formulae's

Heading	Definition's	Formulae's
-	Here q_n is the conductive heat per unit area, k is the coefficient	$q_n = -\frac{k\partial T}{\partial n}$

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Viscosity		$\tau = u \times \frac{du}{dy}$
		Where u is constant of proportionality
Density, Velocity, Div		$\rho, \vec{q}, \vec{\nabla} = \frac{\partial}{\partial x} \hat{i} + \frac{\partial}{\partial y} \hat{j} + \frac{\partial}{\partial z} \hat{k}$ $\frac{Df}{Dt} = \left(\frac{\partial}{\partial t} + \vec{\nabla} \cdot \vec{q}\right) f$
Material Derivative		Bt (Ot)
		Where $\frac{Df}{Dt}$ is material derivative and ∂ is local derivative
Streamline Equation	Continuous Line of flow such that the tangent drawn at any point of streamline coincides with the dirn of motion of the fluid	$d\vec{s} = \hat{\imath}dx + \hat{\jmath}dy + \hat{k} dz$ $\vec{q} = u\hat{\imath} + v\hat{\jmath} + w\hat{k}$ $d\vec{s} \times \vec{q} = 0$ $\frac{dx}{u} = \frac{dy}{v} = \frac{dz}{w}$ Last equation is streamline at Point P
Path lines		
		$\vec{r} = \int \vec{q} . dt$
Velocity and Acceleration of fluid particle		$ec{q} = vel = rac{dec{r}}{dt}$ $ec{A} = accn = rac{dec{q}}{dt} = rac{\partial ec{q}}{\partial t} + ec{q} \cdot (ec{\nabla} \cdot ec{q})$
		$A = accn = \frac{1}{dt} = \frac{1}{\partial t} + q.(v.q)$
Equation of Continuity	Normal Form	$\frac{d\rho}{dt} + \vec{\nabla}.\left(\rho\vec{q}\right) = 0$
	LaGrange's form	$ ho_0= ho.J$ where J is Jacobian
Velocity potential (Scalar)		$\vec{q} = -\vec{\nabla} \cdot \phi$
Rotational Flow Vector wz for 2-D		$1/\partial v \partial u$
flow		$\vec{q} = -\vec{\nabla} \cdot \phi$ $\omega_z = \frac{1}{2} \left(\frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \right)$ Where v is velocity in y dirn and u in x
Circulation	Scalar integral indicating measure	
Circulation	of rotation along a closed curve	$\Gamma = \oint \vec{q} \cdot d\vec{r} = \int \vec{w} \cdot \hat{n} ds$
	Flow across closed curve is called	And this integral is >0 for anti-clockwise. W is
	circulation around that curve	the voriticity
Vorticity	Pseudo vector field describing	$\vec{w} = \vec{\nabla} \times \vec{q}$
Volticity	spinning of fluid around a point	
		$\vec{w} = w_1 \hat{\imath} + w_2 \hat{\jmath} + w_3 \hat{k}$ $\vec{w} \times \vec{r} = \vec{0}$
Vortex Line	A vortex Line is a curve drawn	$w \times r = 0$
	such that the tangent drawn at	$\frac{dx}{w_1} = \frac{dy}{w_2} = \frac{dz}{w_3}$
	any point	
Streak Lines	A streak line is defined to be locus	Let at any time t , r be the fixed point
	of different particles passing	$\vec{r} = f(\vec{r}_0, t)$
	through the same point	$\overrightarrow{r_0} = F(\vec{r}, t)$
		Hence, the streak line at time t' would be $\vec{x} = C(\vec{x}, t')$
		$\vec{r} = G(\vec{r}_0, t')$ $\vec{r} = G(\vec{r}_0, t')$
Linear Strain Rule		$\vec{r} = G(F, t')$
Liliear Strain Rule		$Strain_{x} = \frac{\partial u_{x}}{\partial x}$
		$Strain_{y} = \frac{\partial u_{y}}{\partial x}$
		$Strain_y = \frac{1}{\partial x}$
		$Strain_i = \partial u_i/\partial x_i \ \forall i$
		$Total Strain = \sum \frac{\partial u_i}{\partial x_i} = \frac{\partial u_\beta}{\partial x_\beta}$
		$\frac{1}{\partial x_i} - \frac{1}{\partial x_i} - \frac{1}{\partial x_i}$
		Where β is dummy sum convention
Shear Stress or deformation of		$1/\partial u_i - \partial u_j$
fluid element bcoz of Strains		$\epsilon_{ij} = e_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_i} + \frac{\partial u_j}{\partial x_i} \right)$
		ϵ_{ii} denotes principle stress
Change in Density		
		$\frac{1}{\rho} \times \frac{D\rho}{Dt} = \sum \frac{\partial u_i}{\partial x_i}$
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Euler Equation of Motion	$\frac{D\vec{q}}{Dt} = \vec{F}_{ext,per\ unit\ mass} - \frac{1}{\rho}(\nabla \cdot \rho)$
Lamb Hydrodynamics Equation	$\frac{\partial q}{\partial t} + \frac{1}{2} \times \vec{\nabla} \cdot \vec{q}^2 - \vec{q} \times \vec{w} = \vec{F}_{ext} - \frac{1}{\rho} (\nabla \cdot \rho)$
Generic Functions of stress and strain	$Strain = \frac{\delta x}{x}$ $Stress = \frac{F}{A}$ $Shear = \frac{d\theta}{dt} \text{ where } \theta \text{ is the angle}$
Properties of incompressible Liquids	$ec{ abla}. ec{q} = 0 \ ec{ abla}^2 \phi = 0$
Properties of Irrotational Fluids	$ec{ abla} imesec{q}=ec{0}$ Curl of Q $\omega_z=ec{0}$
If force is conservative, we can use force field	$ec{F}=-ec{ extsf{V}}. \phi$ Where ϕ is a force field

Stress and Strain

Heading	Definition's	Formulae's
Cauchy stress tensor	2nd order tensor defining a stress at a point inside the material	Let Stress Vector be \vec{T}_n and \hat{n} be the unit vector in direction of T then $\vec{T}_n = \vec{\sigma}.\hat{n} = \sigma_{ij}n_i$
Moment of Force(torque)	It is the rotational equivalent of linear force and is equivalent to magnitude of Force and the perpendicular distance between force and axis	$\tau = \vec{r} \vec{F} \sin\theta$ Where θ is the angle between r and F $\vec{\tau} = \vec{r} \times \vec{F}$ $\vec{\tau} = \frac{d\vec{L}}{dt}$
Angular Momentum		$ec{L}=ec{r} imesec{p}$ Where $ec{p}=mec{v}$ $ ightarrowec{L}=mec{r} imesec{v}$
Moment of Inertia (analogy mass)	Defined to be as angular momentum by angular Velocity	$I = rac{L}{\omega}$ Where L is the angular momentum
Stress Tensor and vector		$\sigma = \begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix}$ $T^{n} = \hat{n}.\vec{\sigma}$ $T_{i} = \sigma_{ij}n_{j}$
Levi-Civia System		$\epsilon_{i1,i2,\dots,in}=(-1)^p\epsilon_{1234\dots n}$ Where LHS has distinct and in ordered fashion
Cauchy First Law of Motion		$\frac{\partial(\sigma_{ji})}{\partial j} + F_i = 0$
Principal Stress		$\sigma = \begin{bmatrix} \sigma'_{11} & 0 & 0 \\ 0 & \sigma'_{22} & 0 \\ 0 & 0 & \sigma'_{33} \end{bmatrix}$ where $\sigma'_{11} = \max(\lambda_1, \lambda_2, \lambda_3)$ $\sigma'_{33} = \min(\lambda_1, \lambda_2, \lambda_3)$ $\sigma'_{22} = I_1 - \sigma'_{11} - \sigma'_{33}$ Where

		$\det \sigma_{ij} - \lambda \delta_{ij} = 0$ $-\lambda^3 + I_1 \lambda^2 - I_2 \lambda + I_3 = 0$ $I_1 = \sigma_{kk}$ $I_2 = \frac{1}{2} (\sigma_{ii} \sigma_{kk} - \sigma_{ik} \sigma_{ki})$ $I_3 = \det(\sigma)$
Stress Derivative Tensor	S_{ij} is derivative stress tensor which tends to distort the body. $\pi \delta_{ij}$ tends to change its volume.	$\sigma_{ij} = \pi \delta_{ij} + S_{ij}$ $\pi = \frac{1}{3} (\sigma_{11} + \sigma_{22} + \sigma_{33})$
Bernoulli Equation	Here $\vec{F}_{ext} = -\vec{\nabla} \cdot V$ $\vec{q} = velocity$ $\phi = Velocity potential$ $P = Pressure$ $\rho = Density$	$\varphi(t) = -\frac{d\phi}{dt} + \frac{\vec{q}^2}{2} + \int \frac{dP}{\rho} + V$
Bernoulli Equation with no velocity potential & conservative force		$\frac{\vec{q}^2}{2} + V + \int \frac{dP}{\rho} = Const$

Energy Equations

Heading	Definition's	Formulae's
Basic Statement	The rate of change of total energy (kinetic, potential etc) on a given segment of a compressible inviscid fluid as it moves is equal to the total work done by the pressure on the boundary provided	Let T=Kinetic Energy, P=Potential, I=internal, W=work done, P=pressure Ω =Potenital field $\frac{dT}{dt} + \frac{dP}{dt} + \frac{dI}{dt} = \int P(\vec{q}.\hat{n}) ds = W$ where $T = \int_v \rho \vec{q} ^2 dV$ $P = \int_v \rho \Omega \mathrm{d}V$ $E = \int P dV$ $I = \int_v E \rho dV$

2-D Flow

Heading	Definition's	Formulae's
Stream Function	Stream function signifies that the difference of its values across two points represent the flow across any line joining the points (inform of flux)	$ec{q}=(u,v)$ is velocity vector. Let $arphi$ be the potential $u=rac{\partial \psi}{\partial y}$ $v=-rac{\partial \psi}{\partial x}$
Flux		Flux flowing is equal to $Total\ flux = \Phi_1 - \Phi_2$ Flux across a small segment $Flux_{\delta s} = \delta s \times normal_{vel}$ $Velocity_{normal} = \frac{\delta \varphi}{\delta s}$
Velocity in Polar Coordinates		$q_r = \frac{1}{r} \times \frac{d\psi}{d\theta} = \frac{d\phi}{dr}$ $q_{\theta} = -\frac{d\psi}{dr} = \frac{d\phi}{rd\theta}$

Complex Potential	Complex potential is potential function + I * stream function	$\omega = f(z) = \phi(x, y) + i\psi(x, y)$ $z = x + iy$ $\frac{\partial \phi}{\partial x} = \frac{\partial \psi}{\partial y}; \frac{\partial \varphi}{\partial x} = -\frac{\partial \psi}{\partial y}$ $\Omega = \frac{1}{2} Curl \vec{q} = \frac{1}{2} (\vec{\nabla} \times \vec{q})$
Spin Component of q		$\Omega = \frac{1}{2} Curl \ \vec{q} = \frac{1}{2} (\vec{\nabla} \times \vec{q})$
Velocity in complex plane		$\frac{d\omega}{dz} = -u + iv$
Strength Source and Sink	A source of strength m in 2D is such that the flow across any small curve surrounding it is $2\pi m$	$m = rq_r$ $\psi = -m\theta$ $\phi = -m \log r$ $\omega = -m \log z$
Dipole	A combination of source and sink. μ is the strength of the doublet represented as m δ s, δ s is the distance	$\omega = \frac{\mu}{z}$ Doublets At point z_1, z_2 $\omega = \frac{\mu_1}{z - z_1} + \frac{\mu_2}{z - z_2} + \cdots$
Image of a source	In a fluid, if there exists a surface S where there is no flow, then the system of sources, sinks and doublets on opposite sides of S is known as the system with regards to that curve	i) For St line Direct image ii) For circle Source at inverse point and sink at centre
Milne Thompson Theorem	Let f(z) be the complex potential in a flow having no rigid boundaries such that there are no singularities inside circle z =a. Then if we introduce a solid cylinder at z =a, then the new complex potential would be	$\omega = f(z) + f\left(\frac{z^2}{a}\right)$ $ z \ge a$
Blasius Theorem	In steady 2D Irrotational flow of an incompressible liquid with complex potential w=f(z), the pressure thrust of a cylinder of any shape is represented by Force(X,Y) and the moment M	$X - iY = \frac{i\rho}{2} \int_{c} \left(\frac{d\omega}{dz}\right)^{2} dz$ $M = real \left(-\frac{i\rho}{2} \int_{c} z \left(\frac{d\omega}{dz}\right)^{2} dz\right)$ Where C is contour.
Flow	Value of integral $\int_a^b u dx + v dy + w dz$ is called flow from a to b.	
Kelvin Circulation Theorem	When the external forces are conservative and derived from single valued potential function and density is a function of pressure only. Then the circulation in a particular closed circuit is constant all the time.	
Green's Theorem	Let two single valued continuous function φ and φ'	$\int_{v} \nabla \phi. \nabla \phi' dV = \int_{s} \phi \times \frac{d\phi'}{dt} ds$ $- \int_{v} \phi \nabla^{2} \phi' dV$ $= \int_{v} \phi' \times \frac{d\phi}{dt} ds$ $- \int_{v} \phi' \nabla^{2} \phi dV$
Kelvin Minimum Energy Theorem	The Irrotational motion of a liquid occupying a simply connected region would have less kinetic	, and the second

energy than any other motion	
having same normal velocity at	
the boundary.	

Motion of Cylinders

Heading	Definition's	Formulae's
Stream function for pure rotational motion		$\Psi = vx - uy + \frac{\omega}{2}(x^2 + y^2) + C$ where ω is the angular velocity
Kinetic Energy		$KE = \frac{\rho}{2} \int_{s} \frac{\phi \partial \phi}{\partial n} ds$
When cylinder is moving in an infinite mass of liquid in x dirn		$\frac{\partial^2 \phi}{\partial r^2} + \frac{1}{r} \frac{\partial \phi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2} = 0$ Solution of the form $\phi(r, \theta) = Ar \cos \theta + \frac{B}{r} \cos \theta$ $\omega = \frac{Ua^2}{z}$
Fluid flowing at vel=-U		$\omega = \frac{Ua^2}{z} + Uz$
Cylinder moving with velocity U		$\omega = \frac{Ua^2}{z} + Uz$ $\omega = \frac{Ua^2}{z - Ut}$
Complex potential due to circulation		$\omega = i \frac{k}{2\pi} \log z$
Streaming & Circulation around a fixed cylinder		$\omega = \frac{ik}{2\pi} \log z + \frac{Ua^2}{z} + Uz$

Aerofoils & Naiver Stokes Equation

Heading	Definition's	Formulae's
Conformal Mapping	Preserves angle and side ratios	$\zeta = f(z)$ $z = x + iy$ $\zeta = \xi + i\eta$ $f'(z) = \frac{d\zeta}{dz}$ Area Ratio (\xi to z) equals to f'(z) ^2 Velocity Ratio equals to 1/ f'(z) Kinetic Energy Preserved Complex potential preserved
Differentiation		$f'(z) = \frac{d\zeta}{dz} = \frac{d\xi}{dx} + i\frac{d\eta}{dx} = \frac{d\eta}{dy} - i\frac{d\xi}{dy}$
Joukowski's Transformation		$f(z) = \zeta = z + \frac{a^2}{z}$
Kutta- Joukowski Theorem	When a cylinder of any shape is placed in uniform stream of speed U then the resultant thrust on the cylinder is KpU per unit length normal to the cylinder, where K is the circulation.	$X-iY=-i\rho KUe^{-i\alpha}$ $\omega=Az+\frac{B}{z^2}+Uze^{-i\alpha}+i\frac{k\log z}{2\pi}$ $\alpha=dir^n \text{ with the positive x axis, other }$ variables have their usual meanings

Flow past a circle		$\alpha = d$ irn with the -ive x axis
		$\omega = Ue^{i\alpha}(z - z_0) + \frac{Ub^2e^{-i\alpha}}{z - z_0}$
		$\omega = Ue^{\omega}(z - z_0) + {z - z_0}$
		$+i\frac{k}{2\pi}\log z-z_0$
Flow past an aerofoil		$\frac{d\omega}{d\zeta} = \frac{\frac{d\omega}{dz}}{1 - \frac{a^2}{z^2}}$
		$\frac{d\omega}{dz} = \frac{dz}{dz}$
		$d\zeta = 1 - \frac{a^2}{2}$
		$X - iY = -i\rho K e^{i\alpha} U$
		$N = 2\pi\rho U^{2} [2bc \sin(\alpha + \beta) \cos \alpha + \gamma]$
		$N = 2\pi\rho\sigma \left[2\rho\sigma \sin(\alpha + \rho)\cos\alpha + \gamma\right]$
Naiver Stokes Equation		$\frac{-\rho du}{dt} = \rho F_x - \frac{\partial P}{\partial x}$
Naiver Stokes Equation		$\frac{\rho uu}{dt} = \rho F_x - \frac{\sigma r}{\partial x}$
		$\begin{bmatrix} a_1 & b_2 \\ b_1 & b_2 \end{bmatrix} = 2u \partial (\overrightarrow{\nabla} \overrightarrow{a})$
		$+ \left[2\mu \times \frac{\partial^2 u}{\partial x^2} - \frac{2\mu}{3} \frac{\partial (\overrightarrow{\nabla} \cdot \overrightarrow{q})}{\partial x} \right]$
		$+\mu\left(\frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 v}{\partial x \partial y}\right)$
		$\left[\left(\partial^2 u - \partial^2 w \right) \right]$
		$+\mu\left(\frac{\partial^2 u}{\partial z^2} + \frac{\partial^2 w}{\partial x \partial z}\right)$
Constitutive law of Newtonian		$\sigma_{ii} = 2\mu \frac{\partial q_i}{\partial i} - \frac{2\mu}{3} \vec{\nabla} \cdot \vec{q} - P$
compressible flow		
		$\sigma_{ij} = \mu \left(\frac{\partial q_i}{\partial i} + \frac{\partial q_j}{\partial i} \right)$
		$O_{ij} = \mu \left(\frac{\partial}{\partial j} + \frac{\partial}{\partial i} \right)$
		Where i, j= x,,y,z
Naiver Stokes for incompressible		$\frac{d\vec{q}}{dt} = \vec{F} - \frac{\vec{\nabla}p}{\rho} + \frac{\mu}{\rho} \vec{\nabla}^2 \vec{q}$ $D = -\int_{v} \mu \Omega ^2 dV$
fluid		$\frac{1}{dt} = F - \frac{1}{Q} + \frac{1}{Q} \nabla^2 \vec{q}$
Dissipation of energy	ρς	ρ ρ [
2.00.60.00.00.00	$TKE = \frac{\rho}{2} \int_{V} q^2 dV$	$D = - \int \mu \Omega ^2 dV$
	_ J _V	$\Omega = \overrightarrow{\nabla} \times \overrightarrow{q}$
		$12L - V \wedge Q$

Solving Differential Equations

Heading	Definition's	Formulae's
Generic Way to find PI		$\frac{X}{D-\alpha} = e^{\alpha x} \int X e^{-ax} dx$

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