### 2.2 Helical Gears

# 2.2.1 Anatomy



(a) The three primary planes defining helical gears



(b) The tangential plane only



(c) The transverse plane only



(d) The normal plane only

## 2.2.2 Nomenclature

N = number of teeth

D = pitch diameter (in)

 $p_t = \text{transverse circular pitch (in)}$ 

 $p_n = \text{normal circular pitch (in)}$ 

 $P_d = P_t = \text{diametral pitch (teeth/in)}$ 

 $P_{nd} = P_n = \text{normal diametral pitch (teeth/in)}$ 

 $p_x = \text{axial pitch (in)}$ 

m = metric module

 $m_n = \text{normal metric module}$ 

Face Contact Ratio = number of axial pitches in the face width

F = face width (in)

 $\psi = \text{helix angle}$ 

 $\phi_n = \text{normal pressure angle}$ 

 $\phi_t = \text{transverse pressure angle}$ 

 $T = \text{torque (lbf} \cdot \text{in)}$ 

 $W_t = \text{transmitted load (lbf)}$ 

 $W_a = \text{axial load (lbf)}$ 

 $W_r = \text{radial load (lbf)}$ 

#### 2.2.3 Formulae

I have no clue. Use any of the random fucking formulas below to get an answer.

angle relationship:  $\tan \phi_n = \tan \phi_t \cos \psi$ 

transverse circular pitch:  $p_t = \frac{\pi D_P}{N_P} = \frac{\pi D_G}{N_G} = \frac{\pi}{P_d}$ 

normal circular pitch: 
$$p_n = p_t \cos \psi$$
 axial pitch:  $p_x = \frac{p_t}{\tan \psi} = \frac{\pi P_d}{\tan \psi} = m\pi$ 

Face Contact Ratio  $= \frac{F}{p_x} > 2.0$ 
diametral pitch:  $P_d = \frac{N}{D}$ 

normal diametral pitch:  $P_{nd} = \frac{P_d}{\cos \psi}$ 
 $P_d p_t = \pi$ 
 $P_{nd} p_n = \pi$ 

metric module:  $m = \frac{D}{N}$ 

normal metric module:  $m_n = \frac{1}{P_{nd}} = \frac{\cos \psi}{P_d} = \frac{D \cos \psi}{N} = m \cos \psi$ 
 $W = \frac{W_t}{\cos \phi_n \cos \psi}$ 

Forces and motion:

$$\text{torque: } T = \frac{63000P}{n}$$
 
$$\text{pitch line speed: } v_t = \frac{\pi Dn}{12}$$
 
$$\text{tangential force: } W_t = \frac{33000P}{v_t} = \frac{126000P}{nD}$$
 
$$\text{radial force: } W_r = W_t \tan \phi_t$$
 
$$\text{axial force: } W_x = W_t \tan \psi$$
 
$$\text{bending stress number: } s_t = \frac{W_t P_d}{FJ} K_O K_s K_m K_B K_v$$
 
$$\text{contact stress number: } s_c = C_p \sqrt{\frac{W_t K_O K_s K_m K_v}{FD_p I}}$$
 
$$\text{allowable bending stress: } s_{at} > s_t \frac{(SF)K_R}{Y_N}$$
 
$$\text{allowable contact stress: } s_{ac} > s_c \frac{(SF)K_R}{Z_N}$$

#### 2.2.4 Design Selection

1. Find the type of shock for input and output from this random place in the textbook:

Uniform: Electric motor or constant-speed gas turbine

Light shock: Water turbine, variable-speed drive

Moderate shock: Multicylinder engine

Examples of the roughness of driven machines include the following:

*Uniform:* Continuous-duty generator, paper, and film winders.

Light shock: Fans and low-speed centrifugal pumps, liquid agitators, variable-duty generators, uniformly loaded conveyors, rotary positive displacement pumps, and metal strip processing.

Moderate shock: High-speed centrifugal pumps, reciprocating pumps and compressors, heavy-duty conveyors, machine tool drives, concrete mixers, textile machinery, meat grinders, saws, bucket elevators, freight elevators, escalators, concrete mixers, plastics molding and processing, sewage disposal equipment, winches, and cable reels.

Heavy shock: Rock crushers, punch press drives, pulverizers, processing mills, tumbling barrels, wood chippers, vibrating screens, railroad car dumpers, log conveyors, lumber handling equipment, metal shears, hammer mills, commercial washers, heavy-duty hoists and cranes, reciprocating feeders, dredges, rubber processing, compactors, and plastics extruders.

2. Get the value of  $K_O$  from here

TABLE 9-	1 Sugge	ested Ove	erload Facto	ors, <i>K</i> o	
Driven Machine					
Power source	Uniform	Light shock	Moderate shock	Heavy shock	
Uniform	1.00	1.25	1.50	1.75	
Light shock	1.20	1.40	1.75	2.25	
Moderate shock	1.30	1.70	2.00	2.75	

- 3. Take a wild fucking guess for the value of  $P_{nd}$  and  $N_P$ . The one textbook example used  $P_{nd} = 12$  and  $N_P = 24$  so let's just use those every single time.
- 4. Compute  $P_d$  and  $p_x$

$$P_d = P_{nd}\cos\psi$$

$$p_x = \frac{\pi}{P_d \tan \psi}$$

5. Assume that  $n_G$  is given. If not then refer to the steps in the spur gear design selection guide. Use the speed ratio to get the number of teeth in the gear.

$$VR = \frac{N_G}{N_P} = \frac{n_P}{n_G}$$

6. Compute the tangential pressure angle

$$\phi_t = \arctan\left(\frac{\tan\phi_n}{\cos\psi}\right)$$

7. Compute the diameters of the gears

$$D_P = \frac{N_P}{P_d}$$
$$D_G = \frac{N_G}{P_d}$$

8. Compute the nominal face width

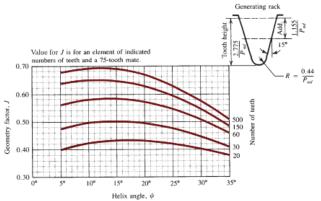
$$F_{\text{nom}} = 2p_x$$

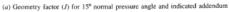
Round it however you want so that the value is convenient.

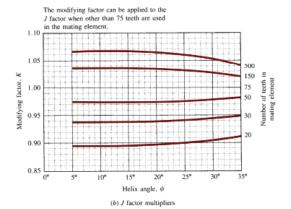
9. Compute the center distance, pitch line speed, and transmitted load

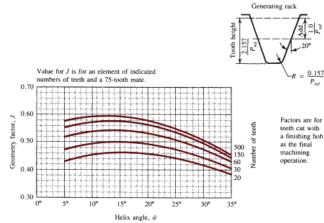
$$C = \frac{N_P + N_G}{2P_d}$$
 
$$v_t = \frac{\pi}{12} D_P n_P$$
 
$$W_t = \frac{33000P}{v_t}$$

- 10. Choose a material (steel) and follow the rest of the steps from the spur gear design selection to get values for  $C_p$ ,  $A_v$ ,  $K_v$ ,  $C_{pf}$ ,  $C_{ma}$ ,  $K_m$ ,  $K_s$ ,  $K_B$ , SF,  $K_R$ ,  $N_c$ ,  $Y_N$ ,  $Z_N$ . The only different constants will be J and I which can be gotten from the following steps.
- 11. Choose the  $J_P$  and  $J_G$  values from one of the graphs depending on the normal pressure angle  $\phi_n$ . (this is different from spur gears)

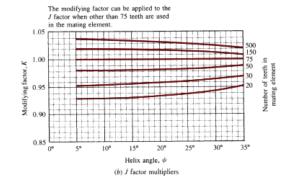


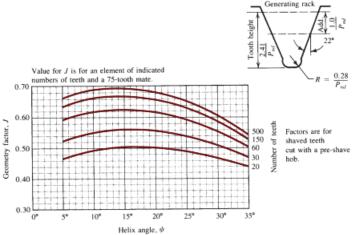




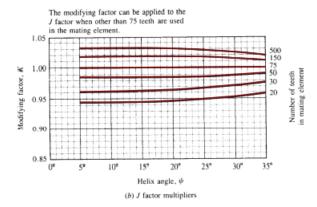


(a) Geometry factor (J) for 20° normal pressure angle, standard addendum, and finishing hob





(a) Geometry factor (I), for 22° normal pressure angle, standard addendum, and pre-shave hob



12. Choose the pitting geometry factor, I, from one of these tables.

	e ψ = 15.0°							
Gear		Pinion teeth						
teeth	17	21		26	35	55		
17	0.124							
21	0.139	0.128						
26	0.154	0.143	0	.132				
35	0.175	0.165	0	.154	0.137			
55	0.204	0.196	0	.187	0.171	0.143		
135	0.244	0.241	0	.237	0.229	0.209		
			Pinion	teeth				
Gear					25	55		
	14	17	21	26	35	33		
	0.123	17	21	26	35	- 55		
teeth		0.126	21	26	35	33		
teeth 14	0.123		0.130	26	35			
14 17	0.123 0.137	0.126		0.134	35	33		
14 17 21	0.123 0.137 0.152	0.126 0.142	0.130		0.138	33		
14 17 21 26	0.123 0.137 0.152 0.167	0.126 0.142 0.157	0.130 0.146	0.134		0.14		

A. Helix ar	ngle ψ = 15.0°							
Gear	Pinion teeth							
teeth	14	17	21	26	35	55		
14	0.130							
17	0.144	0.133						
21	0.160	0.149	0.137					
26	0.175	0.165	0.153	0.140				
35	0.195	0.186	0.175	0.163	0.143			
55	0.222	0.215	0.206	0.195	0.178	0.14		
105	0.257	0.255	0.251	0.246	0.236	0.21		
	ngle ψ = 25.0°	0.233	0.231	0.240	0.230	0.2.		
B. Helix ar		0.233	Pinion to		0.230	0.21		
B. Helix ar		14			35			
B. Helix ar	ngle $\psi=25.0^\circ$		Pinion to	eeth		55		
Gear teeth	ngle $\psi=25.0^\circ$		Pinion to	eeth				
B. Helix ar Gear teeth	ngle $\psi = 25.0^{\circ}$ 12  0.129	14	Pinion to	eeth				
B. Helix ar Gear teeth	ngle $\psi = 25.0^{\circ}$ 12  0.129  0.141	14 0.132	Pinion to	eeth 26				
B. Helix ar Gear teeth 12 14 17	ngle $\psi = 25.0^{\circ}$ 12  0.129  0.141  0.155	14 0.132 0.146	Pinion to 21 0.135	26				
B. Helix ar Gear teeth 12 14 17 21	ngle $\psi = 25.0^{\circ}$ 12  0.129  0.141  0.155  0.170	14 0.132 0.146 0.162	Pinion to  17 21  0.135  0.151 0.138	26 3 4 0.141				
Gear teeth 12 14 17 21 26	ngle $\psi = 25.0^{\circ}$ 12  0.129  0.141  0.155  0.170  0.185	0.132 0.146 0.162 0.177	0.135 0.151 0.166 0.154	26 3 0.141 5 0.163	35			

13. Compute  $s_{tP}$  and  $s_{tG}$  and follow the remaining steps in the spur gear design selection guide.