

## Technical Documentation for SFINCS with multiple species

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### Introduction

In this document, we detail the equations implemented in SFINCS: the Stellarator Fokker-Planck Iterative Neoclassical Conservative Solver. The normalizations and input and output quantities are also defined.

### Kinetic equation

We begin with the following drift-kinetic equation:

$$\left( \nu_{\parallel} \mathbf{b} + \mathbf{v}_E + \mathbf{v}_{ms} \right) \cdot \nabla_{\mu, W_s} f_{s1} - C_s \{ f_{s1} \} = -\mathbf{v}_{ms} \cdot \nabla_{W_s} f_{sM} + \frac{Z_s e}{T_s} \nu_{\parallel} \frac{\langle E_{\parallel} B \rangle B}{\langle B^2 \rangle} f_{sM} \quad (1)$$

where  $s$  denotes species,  $\mu = \nu_{\perp}^2 / (2B)$ ,

$$W_s = \frac{\nu^2}{2} + \frac{Z_s e \Phi}{m_s} \quad (2)$$

is the total energy,  $Z_s$  is the charge in units of the proton charge  $e$ ,  $T_s$  is the temperature,  $m_s$  is the mass,  $\mathbf{v}_E$  is the  $\mathbf{E} \times \mathbf{B}$  drift,

$$\mathbf{v}_{ms} = \left( \nu_{\parallel} / \Omega \right) \nabla_{\mu, \nu} \times \left( \nu_{\parallel} \mathbf{b} \right) = \frac{\nu_{\perp}^2}{2\Omega_s B^2} \mathbf{B} \times \nabla B + \frac{\nu_{\parallel}^2}{\Omega_s} \nabla \times \mathbf{b} \quad (3)$$

is the magnetic drift,  $\Omega_s = Z_s e B / (m_s c)$  is the gyrofrequency (which is negative for electrons with  $Z = -1$ ), and  $c$  is the speed of light. Subscripts on partial derivatives indicate quantities held fixed in differentiation. We assume the electrostatic potential  $\Phi$  is a flux function to the order of interest. The total distribution function is  $f_s = f_{sM} + f_{s1}$  where

$$f_{sM} = n_s(\psi) \left[ \frac{m_s}{2\pi T_s(\psi)} \right]^{3/2} \exp \left( -\frac{m_s \nu^2}{2T_s(\psi)} \right). \quad (4)$$

In (1),  $C_s$  is the collision operator linearized about the Maxwellian  $f_{sM}$  for each species. We neglect contributions from the inductive electric field to  $\mathbf{v}_E$ , writing  $\mathbf{v}_E = (c / B^2) (d\Phi / d\psi) \mathbf{B} \times \nabla \psi$  where  $2\pi\psi$  is the toroidal flux. Let  $\nu_s = \sqrt{2T_s / m_s}$  be the thermal speed, and let  $x_s = \nu / \nu_s$ .

The independent variables used in SFINCS are  $(\theta, \zeta, x_s, \xi)$  where  $\xi = \nu_{\parallel} / \nu$ . Changing velocity variables to  $(x_s, \xi)$  on the left side of (1),

$$\dot{\mathbf{r}}_s \cdot \nabla_{x_s, \xi} f_{s1} + \dot{x}_s \left( \frac{\partial f_{s1}}{\partial x_s} \right)_{\mathbf{r}, \xi} + \dot{\xi}_s \left( \frac{\partial f_{s1}}{\partial \xi} \right)_{\mathbf{r}, x_s} - C_s \{ f_{s1} \} = -\mathbf{v}_{ms} \cdot \nabla_{W_s} f_{sM} + \frac{Z_s e}{T_s} \nu_{\parallel} \frac{\langle E_{\parallel} B \rangle B}{\langle B^2 \rangle} f_{sM} \quad (5)$$

where

$$\dot{\mathbf{r}}_s = \nu_{\parallel} \mathbf{b} + \mathbf{v}_E + \mathbf{v}_{ms}, \quad (6)$$

$$\dot{x}_s = \left( \nu_{\parallel} \mathbf{b} + \mathbf{v}_E + \mathbf{v}_{ms} \right) \cdot \left( \nabla_{\mu, W_s} x_s \right), \quad (7)$$

and

$$\dot{\xi}_s = (\nu_{\parallel} \mathbf{b} + \mathbf{v}_E + \mathbf{v}_{ms}) \cdot (\nabla_{\mu, W_s} \xi). \quad (8)$$

Applying  $\nabla_{W_s}$  to (2) we find

$$\nabla_{W_s} x_s = -\frac{x_s}{m_s \nu_s^2} \nabla T - \frac{Z_s e}{2T_s x_s} \nabla \Phi, \quad (9)$$

so (7) simplifies to

$$\dot{x}_s = (\mathbf{v}_{ms} \cdot \nabla \psi) \left( -\frac{x_s}{2T_s} \frac{dT_s}{d\psi} - \frac{Z_s e}{2T_s x_s} \frac{d\Phi}{d\psi} \right). \quad (10)$$

Similarly, applying  $\nabla_{\mu, W_s}$  to  $\mu = \nu_s^2 x_s^2 (1 - \xi^2) / (2B)$ , we find

$$\nabla_{\mu, W_s} \xi = -\frac{Z_s e}{2T_s x_s^2 \xi} (1 - \xi^2) \nabla \Phi - \frac{(1 - \xi^2)}{\xi} \frac{1}{2B} \nabla B. \quad (11)$$

Thus, (8) may be written

$$\dot{\xi} = -\frac{Z_s e}{2T_s x_s^2 \xi} (1 - \xi^2) \frac{d\Phi}{d\psi} \mathbf{v}_{ms} \cdot \nabla \psi - \frac{(1 - \xi^2)}{\xi} \frac{1}{2B} (\nu_{\parallel} \mathbf{b} + \mathbf{v}_E + \mathbf{v}_{ms}) \cdot \nabla B. \quad (12)$$

Noting

$$\mathbf{v}_{ms} \cdot \nabla \psi = -\frac{T_s c}{Z_s e B^3} x_s^2 (1 + \xi^2) \mathbf{B} \times \nabla \psi \cdot \nabla B \quad (13)$$

then the two electric field terms in (12) may be combined to give

$$\dot{\xi}_s = -\frac{(1 - \xi^2)}{\xi} \frac{1}{2B} \nu_{\parallel} \mathbf{b} \cdot \nabla B + \xi (1 - \xi^2) \frac{c}{2B^3} \frac{d\Phi}{d\psi} \mathbf{B} \times \nabla \psi \cdot \nabla B - \frac{(1 - \xi^2)}{\xi} \frac{1}{2B} \mathbf{v}_{ms} \cdot \nabla B. \quad (14)$$

In the present implementation of SFINCS, the  $\mathbf{v}_{ms}$  terms in (6) and (14) are neglected, as is the  $dT_s / d\psi$  term in (10). (This last term must be dropped in order to maintain conservation of  $\mu$ .) We are then left with

$$\dot{\mathbf{r}}_s = \nu_{\parallel} \mathbf{b} + \frac{c}{B^2} \frac{d\Phi}{d\psi} \mathbf{B} \times \nabla \psi, \quad (15)$$

$$\dot{x}_s = \frac{c}{2B^3} \frac{d\Phi}{d\psi} x_s (1 + \xi^2) \mathbf{B} \times \nabla \psi \cdot \nabla B, \quad (16)$$

$$\dot{\xi}_s = -x_s (1 - \xi^2) \frac{\nu_s}{2B^2} \mathbf{B} \cdot \nabla B + \xi (1 - \xi^2) \frac{c}{2B^3} \frac{d\Phi}{d\psi} \mathbf{B} \times \nabla \psi \cdot \nabla B. \quad (17)$$

These are the same terms as in the last section of the appendix of Ref. [1].

We can verify that (15)-(17) still conserve  $\mu$ :

$$\begin{aligned} \dot{\mu} &= \frac{d}{dt} \left( \frac{T_s x_s^2 (1 - \xi^2)}{m_s B} \right) = \frac{T_s}{m_s} \frac{d}{dt} \left( \frac{x_s^2 (1 - \xi^2)}{B} \right) \\ &= \frac{T_s}{m_s} \left\{ 2 \frac{1 - \xi^2}{B} x_s \dot{x}_s - 2 \xi \frac{x_s^2}{B} \dot{\xi} - \frac{x_s^2}{B^2} (1 - \xi^2) \dot{\mathbf{r}}_s \cdot \nabla B \right\} \\ &= 0. \end{aligned} \quad (18)$$

As shown in the appendix of Ref. [1], (15)-(17) do not conserve  $W$  because the radial magnetic drift has been dropped. However, in an axisymmetric or quasisymmetric field, (15)-(17) do conserve a combination of energy and canonical momentum.

To compare various effective particle trajectories, the code allows the  $d\Phi/d\psi$  terms in (16) and (17) to be turned off, in which case

$$\dot{x}_s = 0, \quad (19)$$

$$\dot{\xi}_s = -x_s (1 - \xi^2) \frac{v_s}{2B^2} \mathbf{B} \cdot \nabla B. \quad (20)$$

For comparison with DKES, SFINCS allows the option of using

$$\dot{\mathbf{r}}_s = v_{\parallel} \mathbf{b} + \frac{c}{\langle B^2 \rangle} \frac{d\Phi}{d\psi} \mathbf{B} \times \nabla \psi, \quad (21)$$

in place of (15).

One further option allowed in the code is to also include a term

$$-f_{s1} \frac{2c}{B^3} \frac{d\Phi}{d\psi} \mathbf{B} \times \nabla \psi \cdot \nabla B = f_{s1} \nabla \cdot \mathbf{v}_E \quad (22)$$

on the left-hand side of (5). The rationale for including this term is that it allows the left-hand side of (5) to be put into a conservative form when (19)-(20) are used:

$$\nabla_{x_s, \xi} \cdot (f_{s1} \dot{\mathbf{r}}_s) + \left( \frac{\partial}{\partial \xi} \right)_{\mathbf{r}, x_s} [f_{s1} \dot{\xi}_s] - C_s \{f_{s1}\} = -\mathbf{v}_{ms} \cdot \nabla_{w_s} f_{sM} + \frac{Z_s e}{T_s} v_{\parallel} \frac{\langle E_{\parallel} B \rangle B}{\langle B^2 \rangle} f_{sM}. \quad (23)$$

For the rest of these notes, we will include the term (22) multiplied by  $\alpha_{cons}$ , so  $\alpha_{cons}$  will be either 0 or 1.

Now consider the magnetic field in Boozer coordinates:

$$\mathbf{B} = \nabla \psi \times \nabla \theta + \iota \nabla \zeta \times \nabla \psi, \quad (24)$$

where  $\iota = 1/q$  is the rotational transform with  $q$  the safety factor, and

$$\mathbf{B} = \beta \nabla \psi + G \nabla \zeta + I \nabla \theta, \quad (25)$$

where  $G(\psi) = 2i_p / c$ ,  $I(\psi) = 2i_t / c$ ,  $i_p(\psi)$  is the poloidal current outside the flux surface, and  $i_t(\psi)$  is the toroidal current inside the flux surface. Notice  $\mathbf{B} \cdot \nabla \theta = \iota \mathbf{B} \cdot \nabla \zeta$ . The product of (24) with (25) gives the Jacobian

$$\nabla \psi \times \nabla \theta \cdot \nabla \zeta = \frac{B^2}{G + \iota I} = \mathbf{B} \cdot \nabla \zeta. \quad (26)$$

Notice also that

$$\mathbf{B} \cdot \nabla X = \mathbf{B} \cdot \nabla \zeta \left[ \iota \frac{\partial X}{\partial \theta} + \frac{\partial X}{\partial \zeta} \right] \quad (27)$$

for any quantity  $X$ , and

$$\mathbf{B} \times \nabla \psi \cdot \nabla B = \mathbf{B} \cdot \nabla \zeta \left[ G \frac{\partial B}{\partial \theta} - I \frac{\partial B}{\partial \zeta} \right]. \quad (28)$$

The kinetic equation (5) with (15)-(17) is thus equivalent to

$$\begin{aligned}
& \dot{\theta}_s \frac{\partial f_{s1}}{\partial \theta} + \dot{\zeta}_s \frac{\partial f_{s1}}{\partial \zeta} + \dot{x}_s \frac{\partial f_{s1}}{\partial x_s} + \dot{\xi}_s \frac{\partial f_{s1}}{\partial \xi} - C_s \{f_{s1}\} - \alpha_{cons} f_{s1} \frac{2c}{B^3} \frac{d\Phi}{d\psi} \mathbf{B} \cdot \nabla \zeta \left[ G \frac{\partial B}{\partial \theta} - I \frac{\partial B}{\partial \zeta} \right] \\
& = \frac{T_s c}{Z_s e B^3} x_s^2 (1 + \xi^2) \mathbf{B} \cdot \nabla \zeta \left[ G \frac{\partial B}{\partial \theta} - I \frac{\partial B}{\partial \zeta} \right] f_{sM} \left[ \frac{1}{n_s} \frac{dn_s}{d\psi} + \frac{Z_s e}{T_s} \frac{d\Phi}{d\psi} + \left( x_s^2 - \frac{3}{2} \right) \frac{1}{T_s} \frac{dT_s}{d\psi} \right] + \frac{Z_s e}{T_s} v_{\parallel} \frac{\langle E_{\parallel} B \rangle B}{\langle B^2 \rangle} f_{sM}
\end{aligned} \tag{29}$$

where

$$\dot{\theta}_s = \left[ \frac{v_s x_s \xi}{B} \iota + \frac{cG}{B^2} \frac{d\Phi}{d\psi} \right] \mathbf{B} \cdot \nabla \zeta, \tag{30}$$

$$\dot{\zeta}_s = \left[ \frac{v_s x_s \xi}{B} - \frac{Ic}{B^2} \frac{d\Phi}{d\psi} \right] \mathbf{B} \cdot \nabla \zeta, \tag{31}$$

$$\dot{x}_s = \frac{c}{2B^3} \frac{d\Phi}{d\psi} x_s (1 + \xi^2) \mathbf{B} \cdot \nabla \zeta \left[ G \frac{\partial B}{\partial \theta} - I \frac{\partial B}{\partial \zeta} \right], \tag{32}$$

$$\dot{\xi}_s = -x_s (1 - \xi^2) \frac{v_s}{2B^2} \mathbf{B} \cdot \nabla \zeta \left[ \iota \frac{\partial B}{\partial \theta} + \frac{\partial B}{\partial \zeta} \right] + \xi (1 - \xi^2) \frac{c}{2B^3} \frac{d\Phi}{d\psi} \mathbf{B} \cdot \nabla \zeta \left[ G \frac{\partial B}{\partial \theta} - I \frac{\partial B}{\partial \zeta} \right]. \tag{33}$$

## Normalizations

Let's suppose we are given  $T_s$ ,  $dT_s/d\psi_N$ ,  $n_s$ ,  $dn_s/d\psi_N$ ,  $d\Phi/d\psi_N$ ,  $B(\theta, \zeta)$ ,  $\iota$ ,  $G$ ,  $I$ ,  $\psi_a = \psi(\psi_N = 1)$ , and  $\langle E_{\parallel} B \rangle$  where  $\psi_N$  is the normalized toroidal flux. The flux at the last closed flux surface is  $\psi_a$ , so the dimensional flux  $\psi$  is related to  $\psi_N$  by  $\psi = \psi_N \psi_a$ . The input quantities are specified in terms of some species-independent dimensions  $\bar{T}$  (e.g. eV),  $\bar{n}$  (e.g.  $10^{20}/\text{m}^3$ ),  $\bar{\Phi}$  (e.g. kV),  $\bar{B}$  (e.g. T),  $\bar{R}$  (e.g. m), and  $\bar{m}$  (typically the proton or deuteron mass). In other words, the quantities we are actually given are

$$\hat{m}_s = m_s / \bar{m}, \tag{34}$$

$$\hat{T}_s = T_s / \bar{T}, \tag{35}$$

$$\hat{n}_s = n_s / \bar{n}, \tag{36}$$

$$d\hat{T}_s / d\psi_N = (dT_s / d\psi_N) / \bar{T}, \tag{37}$$

$$d\hat{n}_s / d\psi_N = (dn_s / d\psi_N) / \bar{n}, \tag{38}$$

$$d\hat{\Phi} / d\psi_N = (d\Phi / d\psi_N) / \bar{\Phi}, \tag{39}$$

$$\hat{B} = B / \bar{B}, \tag{40}$$

$$\hat{G} = G / (\bar{R}\bar{B}), \tag{41}$$

$$\hat{I} = I / (\bar{R}\bar{B}), \tag{42}$$

$$\hat{\psi}_a = \psi_a / (\bar{B}\bar{R}^2), \tag{43}$$

and

$$\hat{E} = \langle E_{\parallel} B \rangle \frac{\bar{R}}{\bar{\Phi}\bar{B}}. \tag{44}$$

Notice  $\psi = \psi_N \hat{\psi}_a \bar{R}^2 \bar{B}$ , and so

$$\frac{dX}{d\psi} = \frac{1}{\hat{\psi}_a \bar{R}^2 \bar{B}} \frac{dX}{d\psi_N} \quad (45)$$

for any flux function  $X$ .

It will be useful to define the following combinations of normalization constants:

$$\bar{v} = \sqrt{2\bar{T} / \bar{m}}, \quad (46)$$

$$\Delta = \frac{\bar{m}c\bar{v}}{e\bar{B}\bar{R}} \quad (47)$$

(which resembles  $\rho_* = \rho / R$ ),

$$\alpha = \frac{e\bar{\Phi}}{\bar{T}}, \quad (48)$$

$$\omega = \frac{c\bar{\Phi}}{\bar{v}\bar{R}\bar{B}} = \frac{\Delta\alpha}{2}, \quad (49)$$

and a normalized collisionality

$$\nu_n = \bar{\nu}\bar{R} / \bar{v} \quad (50)$$

where  $\bar{\nu}$  is the dimensional collisionality at the reference parameters:

$$\bar{\nu} = \frac{4\sqrt{2\pi}\bar{n}e^4 \ln \Lambda}{3\bar{m}^{1/2}\bar{T}^{3/2}}. \quad (51)$$

We assume  $\ln \Lambda$  has the same value for all species. It will be useful to notice

$$\mathbf{B} \cdot \nabla \zeta = \frac{\bar{B}}{\bar{R}} \frac{\hat{B}^2}{\hat{G} + \iota \hat{I}}. \quad (52)$$

We define a normalized distribution function  $\hat{f}_s$  as follows:

$$f_{s1} = \frac{\bar{n}}{\bar{v}^3} \hat{f}_s. \quad (53)$$

Notice the normalization is the same for each species. Also notice that the normalization is different than in the original 1-species version of SFINCS.

The kinetic equation (29) for each species is made dimensionless by multiplying through by

$$\frac{\bar{v}^3}{\bar{n}} \frac{\bar{B}}{\bar{v} \mathbf{B} \cdot \nabla \zeta}. \quad (54)$$

(this normalization too is slightly different than in the 1-species version of SFINCS.) We then obtain

$$\begin{aligned}
& \left[ \frac{\hat{T}_s^{1/2} x_s \xi}{\hat{m}_s^{1/2} \hat{B}} \iota + \frac{\alpha \Delta \hat{G}}{2 \hat{\psi}_a \hat{B}^2} \frac{d\hat{\Phi}}{d\psi_N} \right] \frac{\partial \hat{f}_s}{\partial \theta} \\
& \left[ \frac{\hat{T}_s^{1/2} x_s \xi}{\hat{m}_s^{1/2} \hat{B}} - \frac{\alpha \Delta \hat{I}}{2 \hat{\psi}_a \hat{B}^2} \frac{d\hat{\Phi}}{d\psi_N} \right] \frac{\partial \hat{f}_s}{\partial \zeta} \\
& + \frac{\alpha \Delta}{4 \hat{\psi}_a \hat{B}^3} \frac{d\hat{\Phi}}{d\psi_N} x_s (1 + \xi^2) \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \frac{\partial \hat{f}_s}{\partial x_s} \\
& + \left\{ -x_s (1 - \xi^2) \frac{\hat{T}_s^{1/2}}{2 \hat{m}_s^{1/2} \hat{B}^2} \left[ \iota \frac{\partial \hat{B}}{\partial \theta} + \frac{\partial \hat{B}}{\partial \zeta} \right] + \xi (1 - \xi^2) \frac{\alpha \Delta}{4 \hat{\psi}_a \hat{B}^3} \frac{d\hat{\Phi}}{d\psi_N} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \right\} \frac{\partial \hat{f}_s}{\partial \xi} \\
& - \frac{\hat{G} + \iota \hat{I}}{\hat{B}^2} v_n \frac{1}{\bar{V}} C_s \{ \hat{f}_s \} - \alpha_{cons} \frac{d\hat{\Phi}}{d\psi_N} \frac{\Delta \alpha}{\hat{\psi}_a \hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \hat{f}_s \\
& = \frac{\Delta \hat{n}_s \hat{T}_s}{2 \pi^{3/2} \hat{\psi}_a Z_s \hat{B}^3} \left( \frac{\hat{m}_s}{\hat{T}_s} \right)^{3/2} x_s^2 (1 + \xi^2) \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] e^{-x_s^2} \left[ \frac{1}{\hat{n}_s} \frac{d\hat{n}_s}{d\psi_N} + \frac{\alpha Z_s}{\hat{T}_s} \frac{d\hat{\Phi}}{d\psi_N} + \left( x_s^2 - \frac{3}{2} \right) \frac{1}{\hat{T}_s} \frac{d\hat{T}_s}{d\psi_N} \right] \\
& + \alpha \frac{\hat{G} + \iota \hat{I}}{\hat{B}} \frac{Z_s}{\hat{T}_s^2} x_s \xi \hat{E} \frac{1}{\langle \hat{B}^2 \rangle} \frac{\hat{n}_s \hat{m}_s}{\pi^{3/2}} e^{-x_s^2}
\end{aligned} \tag{55}$$

where  $\hat{C}_s \{ \hat{f}_s \} = \bar{V}^{-1} C_s \{ \hat{f}_s \}$ .

## Legendre discretization

SFINCS uses a collocation discretization in the  $x_s$ ,  $\theta$ , and  $\zeta$  coordinates, but a modal discretization in the  $\xi$  coordinate. In other words, the distribution function is known at certain grid points in  $x_s$ ,  $\theta$ , and  $\zeta$ , but it is expanded as modes in  $\xi$ . We employ the following modal expansion in terms of Legendre polynomials  $P_\ell(\xi)$ :

$$\hat{f}_s = \sum_{\ell} f_{s,\ell} P_\ell(\xi). \tag{56}$$

We discretize the kinetic equation (55) by applying

$$\frac{2L+1}{2} \int_{-1}^1 d\xi P_L(\xi) ( \cdot ). \tag{57}$$

To evaluate the various integrals that result, the following identities may be used:

$$\frac{2L+1}{2} \int_{-1}^1 d\xi \xi P_L(\xi) P_\ell(\xi) = \frac{L+1}{2L+3} \delta_{L+1,\ell} + \frac{L}{2L-1} \delta_{L-1,\ell}, \tag{58}$$

$$\begin{aligned}
\frac{2L+1}{2} \int_{-1}^1 d\xi (1 + \xi^2) P_L(\xi) P_\ell(\xi) &= \frac{2[3L^2 + 3L - 2]}{(2L+3)(2L-1)} \delta_{L,\ell} \\
&+ \frac{L-1}{2L-3} \frac{L}{2L-1} \delta_{L-2,\ell} + \frac{L+2}{2L+5} \frac{L+1}{2L+3} \delta_{L+2,\ell},
\end{aligned} \tag{59}$$

$$\frac{2L+1}{2} \int_{-1}^1 d\xi (1 - \xi^2) P_L(\xi) \frac{dP_\ell}{d\xi} = \frac{(L+1)(L+2)}{2L+3} \delta_{L+1,\ell} - \frac{(L-1)L}{2L-1} \delta_{L-1,\ell}, \tag{60}$$

$$\begin{aligned} \frac{2L+1}{2} \int_{-1}^1 d\xi (1-\xi^2) \xi P_L(\xi) \frac{dP_\ell}{d\xi} &= \frac{(L+1)L}{(2L-1)(2L+3)} \delta_{L,\ell} \\ &+ \frac{(L+3)(L+2)(L+1)}{(2L+5)(2L+3)} \delta_{L+2,\ell} - \frac{L(L-1)(L-2)}{(2L-3)(2L-1)} \delta_{L-2,\ell}, \end{aligned} \quad (61)$$

$$\frac{2L+1}{2} \int_{-1}^1 d\xi P_L(\xi) \xi = \delta_{L,1}, \quad (62)$$

and

$$\frac{2L+1}{2} \int_{-1}^1 d\xi P_L(\xi) (1+\xi^2) = \frac{4}{3} \delta_{L,0} + \frac{2}{3} \delta_{L,2}. \quad (63)$$

As a result, (55) may be written

$$\sum_{\ell} M_{s,L,\ell} \hat{f}_{s,\ell} = R_{s,L} \quad (64)$$

where

$$M_{s,L,\ell} = \dot{\theta}_{s,L,\ell} \frac{\partial}{\partial \theta} + \dot{\zeta}_{s,L,\ell} \frac{\partial}{\partial \zeta} + M_{s,L,\ell}^{(\xi)} + \dot{x}_{s,L,\ell} \frac{\partial}{\partial x_s} - \nu_n \frac{(\hat{G} + i\hat{I})}{\hat{B}^2} \hat{C}_{s,L} \delta_{L,\ell} + \alpha_{cons} \delta_{L,\ell} Y, \quad (65)$$

$$\dot{\theta}_{s,L,\ell} = \frac{\hat{T}_s^{1/2} x_s}{\hat{m}_s^{1/2} \hat{B}} l \left[ \frac{L+1}{2L+3} \delta_{L+1,\ell} + \frac{L}{2L-1} \delta_{L-1,\ell} \right] + \frac{\alpha \Delta \hat{G}}{2\hat{\psi}_a \hat{B}^2} \frac{d\hat{\Phi}}{d\psi_N} \delta_{L,\ell} \quad (66)$$

$$\dot{\zeta}_{s,L,\ell} = \frac{\hat{T}_s^{1/2} x_s}{\hat{m}_s^{1/2} \hat{B}} \left[ \frac{L+1}{2L+3} \delta_{L+1,\ell} + \frac{L}{2L-1} \delta_{L-1,\ell} \right] - \frac{\alpha \Delta \hat{I}}{2\hat{\psi}_a \hat{B}^2} \frac{d\hat{\Phi}}{d\psi_N} \delta_{L,\ell} \quad (67)$$

$$\begin{aligned} M_{s,L,\ell}^{(\xi)} &= -x_s \frac{\hat{T}_s^{1/2}}{2\hat{m}_s^{1/2} \hat{B}^2} \left[ \iota \frac{\partial \hat{B}}{\partial \theta} + \frac{\partial \hat{B}}{\partial \zeta} \right] \left[ \frac{(L+1)(L+2)}{2L+3} \delta_{L+1,\ell} - \frac{(L-1)L}{2L-1} \delta_{L-1,\ell} \right] \\ &+ \frac{\alpha \Delta}{4\hat{\psi}_a \hat{B}^3} \frac{d\hat{\Phi}}{d\psi_N} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \left[ \frac{(L+1)L}{(2L-1)(2L+3)} \delta_{L,\ell} \right. \\ &\quad \left. + \frac{(L+3)(L+2)(L+1)}{(2L+5)(2L+3)} \delta_{L+2,\ell} - \frac{L(L-1)(L-2)}{(2L-3)(2L-1)} \delta_{L-2,\ell} \right] \end{aligned} \quad (68)$$

$$\dot{x}_{s,L,\ell} = \frac{\alpha \Delta}{4\hat{\psi}_a \hat{B}^3} \frac{d\hat{\Phi}}{d\psi_N} x_s \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \left[ \frac{2[3L^2 + 3L - 2]}{(2L+3)(2L-1)} \delta_{L,\ell} \right. \\ \left. + \frac{L-1}{2L-3} \frac{L}{2L-1} \delta_{L-2,\ell} + \frac{L+2}{2L+5} \frac{L+1}{2L+3} \delta_{L+2,\ell} \right], \quad (69)$$

$$Y = -\frac{d\hat{\Phi}}{d\psi_N} \frac{\Delta \alpha}{\hat{\psi}_a \hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right], \quad (70)$$

and

$$R_{s,L} = \frac{\Delta \hat{n}_s \hat{T}_s}{2\pi^{3/2} \hat{\psi}_a Z_s \hat{B}^3} \left( \frac{\hat{m}_s}{\hat{T}_s} \right)^{3/2} x_s^2 \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] e^{-x_s^2} \left[ \frac{1}{\hat{n}_s} \frac{d\hat{n}_s}{d\psi_N} + \frac{\alpha Z_s}{\hat{T}_s} \frac{d\hat{\Phi}}{d\psi_N} + \left( x_s^2 - \frac{3}{2} \right) \frac{1}{\hat{T}_s} \frac{d\hat{T}_s}{d\psi_N} \right] \left[ \frac{4}{3} \delta_{L,0} + \frac{2}{3} \delta_{L,2} \right] \\ + \alpha \frac{\hat{G} + \hat{I}}{\hat{B}} \frac{Z_s}{\hat{T}_s^2} x_s \xi \hat{E} \frac{1}{\langle \hat{B}^2 \rangle} \frac{\hat{n}_s \hat{m}_s}{\pi^{3/2}} e^{-x_s^2} \delta_{L,1} \quad (71)$$

## Collision operator

The total collision operator for species  $a$  is a sum of collision operators with each species:

$$C_a = \sum_b C_{ab}. \quad (72)$$

The linearized Fokker-Planck collision operator for each pair of species may be written

$$C_{ab} = C_{ab}^L + C_{ab}^E + C_{ab}^F, \quad (73)$$

where the Lorentz part of the collision term is

$$C_{ab}^L = \frac{\nu_{Dab}}{2} \frac{\partial}{\partial \xi} (1 - \xi^2) \frac{\partial f_{a1}}{\partial \xi} \quad (74)$$

with

$$\nu_{Dab} = \frac{\Gamma_{ab} n_b}{\nu^3} [\text{erf}(x_b) - \Psi(x_b)], \quad (75)$$

$$\Gamma_{ab} = \frac{4\pi Z_a^2 Z_b^2 e^4 \ln \Lambda}{m_a^2}, \quad (76)$$

$$\Psi(x_b) = \frac{\text{erf}(x_b) - x_b \text{erf}'(x_b)}{2x_b^2}. \quad (77)$$

The energy scattering contribution is

$$C_{ab}^E = \nu_{\parallel ab} \left[ \frac{\nu^2}{2} \frac{\partial^2 f_{a1}}{\partial \nu^2} - x_b^2 \left( 1 - \frac{m_a}{m_b} \right) \nu \frac{\partial f_{a1}}{\partial \nu} \right] + \nu_{Dab} \nu \frac{\partial f_{a1}}{\partial \nu} + 4\pi \Gamma_{ab} \frac{m_a}{m_b} f_{Mb} f_{a1} \quad (78)$$

where

$$\nu_{\parallel ab} = 2 \frac{\Gamma_{ab} n_b}{\nu^3} \Psi(x_b). \quad (79)$$

The field term is

$$C_{ab}^F = \Gamma_{ab} f_{Ma} \left[ \frac{2\nu^2}{\nu_a^4} \frac{\partial^2 G_{b1}}{\partial \nu^2} - \frac{2\nu}{\nu_a^2} \left( 1 - \frac{m_a}{m_b} \right) \frac{\partial H_{b1}}{\partial \nu} - \frac{2}{\nu_a^2} H_{b1} + 4\pi \frac{m_a}{m_b} f_{b1} \right] \quad (80)$$

where the potentials are defined by

$$\nabla_\nu^2 H_{b1} = -4\pi f_{b1} \quad (81)$$

and

$$\nabla_\nu^2 G_{b1} = 2H_{b1}. \quad (82)$$

We write the field term as

$$C_{ab}^F = C_{ab}^H + C_{ab}^G + C_{ab}^D \quad (83)$$

where



$$C_{ab}^G = \Gamma_{ab} f_{Ma} \frac{2\nu^2}{\nu_a^4} \frac{\partial^2 G_{b1}}{\partial \nu^2} \quad (84)$$

$$C_{ab}^H = \Gamma_{ab} f_{Ma} \left[ -\frac{2\nu}{\nu_a^2} \left( 1 - \frac{m_a}{m_b} \right) \frac{\partial H_{b1}}{\partial \nu} - \frac{2}{\nu_a^2} H_{b1} \right] \quad (85)$$

$$C_{ab}^D = \Gamma_{ab} f_{Ma} 4\pi \frac{m_a}{m_b} f_{b1} = \frac{\Gamma_{ab} n_a}{\nu_a^3} \exp(-x_a^2) \frac{4}{\pi^{1/2}} \frac{m_a}{m_b} f_{b1} \quad (86)$$

The Poisson equations that define the potentials are (for Legendre mode  $P_\ell(\xi)$ )

$$\frac{\partial}{\partial x_b} x_b^2 \frac{\partial H_{b1}}{\partial x_b} - \ell(\ell+1) H_{b1} = -4\pi \nu^2 f_{b1} \quad (87)$$

$$\frac{\partial}{\partial x_b} x_b^2 \frac{\partial G_{b1}}{\partial x_b} - \ell(\ell+1) G_{b1} = 2\nu^2 H_{b1}. \quad (88)$$

Let us define

$$\hat{H}_{b1} = H_{b1} / \nu_b^2 \quad (89)$$

$$\hat{G}_{b1} = G_{b1} / \nu_b^4 \quad (90)$$

so the defining equations for the potentials become

$$\frac{\partial}{\partial x_b} x_b^2 \frac{\partial \hat{H}_{b1}}{\partial x_b} - \ell(\ell+1) \hat{H}_{b1} = -4\pi x_b^2 f_{b1} \quad (91)$$

$$\frac{\partial}{\partial x_b} x_b^2 \frac{\partial \hat{G}_{b1}}{\partial x_b} - \ell(\ell+1) \hat{G}_{b1} = 2x_b^2 \hat{H}_{b1}. \quad (92)$$

Next, recall that in the kinetic equation (65), we need to evaluate

$$\hat{C}_{ab} = \frac{1}{\bar{\nu}} C_{ab} \quad (93)$$

where  $\bar{\nu}$  is defined in (51). It is convenient to note

$$\frac{\Gamma_{ab}}{\bar{\nu}} = \frac{3\sqrt{\pi}}{4} \frac{1}{\bar{n}} \frac{Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \nu_a^3 \quad (94)$$

Expanding  $\hat{C}_{ab} = \hat{C}_{ab}^L + \hat{C}_{ab}^E + \hat{C}_{ab}^F$  as before,

$$\hat{C}_{ab}^L = \frac{\hat{\nu}_{Dab}}{2} \frac{\partial}{\partial \xi} (1 - \xi^2) \frac{\partial f_{a1}}{\partial \xi} \quad (95)$$

where

$$\hat{\nu}_{Dab} = \frac{3\sqrt{\pi}}{4} \frac{\hat{n}_b Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \frac{1}{x_a^3} [\text{erf}(x_b) - \Psi(x_b)] \quad (96)$$

The energy scattering component is

$$\hat{C}_{ab}^E \{f_{a1}\} = \frac{3\sqrt{\pi}}{4} \frac{\hat{n}_b Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \left[ \frac{1}{x_a} \Psi(x_b) \frac{\partial^2 f_{a1}}{\partial x_a^2} + \left\{ -2 \frac{\hat{T}_a}{\hat{T}_b} \frac{\hat{m}_b}{\hat{m}_a} \Psi(x_b) \left( 1 - \frac{\hat{m}_a}{\hat{m}_b} \right) + \frac{1}{x_a^2} [\text{erf}(x_b) - \Psi(x_b)] \right\} \frac{\partial f_{a1}}{\partial x_a} + \frac{4}{\sqrt{\pi}} \left( \frac{\hat{T}_a}{\hat{T}_b} \right)^{3/2} \left( \frac{\hat{m}_b}{\hat{m}_a} \right)^{1/2} e^{-x_b^2} f_{a1} \right] \quad (97)$$

The diagonal term is

$$\hat{C}_{ab}^D = 3 \frac{\hat{n}_a Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \frac{\hat{m}_a}{\hat{m}_b} \exp(-x_a^2) f_{b1} \quad (98)$$

In the cross-species case, this term is no longer identical to the  $f_{a1}$  term in energy scattering (as it is in the same-species case).

The  $G$  term in the collision operator is

$$\begin{aligned} \hat{C}_{ab}^G &= \frac{3}{2\pi} \frac{\hat{n}_a Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \left( \frac{\hat{T}_b}{\hat{T}_a} \frac{\hat{m}_a}{\hat{m}_b} \right)^2 e^{-x_a^2} x_b^2 \frac{\partial^2 \hat{G}_{b1}}{\partial x_b^2} \\ &= \frac{3}{2\pi} \frac{\hat{n}_a Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \left( \frac{\hat{T}_b}{\hat{T}_a} \frac{\hat{m}_a}{\hat{m}_b} \right) e^{-x_a^2} x_a^2 \frac{\partial^2 \hat{G}_{b1}}{\partial x_b^2}. \end{aligned} \quad (99)$$

Although in principle we would also be free to write

$$\hat{C}_{ab}^G = \frac{3}{2\pi} \frac{\hat{n}_a Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \left( \frac{\hat{T}_b}{\hat{T}_a} \frac{\hat{m}_a}{\hat{m}_b} \right)^2 e^{-x_a^2} \textcolor{red}{x}_a^2 \frac{\partial^2 \hat{G}_{b1}}{\partial \textcolor{red}{x}_a^2} \quad (100)$$

(i.e. replacing  $x_b \rightarrow x_a$  in two places), the resulting expression is less convenient because we compute  $\hat{G}_{b1}$  on the  $x_b$  grid, and so it is easier to differentiate with respect to  $x_b$ .

The  $H$  collision term is

$$\hat{C}_{ab}^H = -\frac{3}{2\pi} \frac{\hat{n}_a Z_a^2 Z_b^2}{\hat{T}_a^{3/2} \hat{m}_a^{1/2}} \frac{\hat{T}_b}{\hat{T}_a} \frac{\hat{m}_a}{\hat{m}_b} e^{-x_a^2} \left[ \left( 1 - \frac{\hat{m}_a}{\hat{m}_b} \right) x_b \frac{\partial \hat{H}_{b1}}{\partial x_b} + \hat{H}_{b1} \right] \quad (101)$$

## Output quantities

### Flux surface average:

For any quantity  $X$ , the flux surface average can be computed from

$$\langle X \rangle = \frac{1}{\hat{V}'} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{X}{\hat{B}^2} \quad (102)$$

where

$$\text{VPrimeHat} = \hat{V}' = \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{1}{\hat{B}^2}. \quad (103)$$

Notice

$$\text{FSABHat2} = \langle \hat{B}^2 \rangle = \frac{4\pi^2}{\hat{V}'} . \quad (104)$$

### Density perturbation

SFINCS returns the density carried in  $\hat{f}_{s1}$ :

$$\text{densityPerturbation} = \frac{1}{\bar{n}} \int d^3v f_{s1} = 4\pi \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^{3/2} \int_0^\infty dx_s x_s^2 \hat{f}_{s,L=0} . \quad (105)$$

Upon flux surface averaging, we obtain

$$\begin{aligned} \text{FSADensityPerturbation} &= \left\langle \frac{1}{\bar{n}} \int d^3v f_{s1} \right\rangle \\ &= \frac{1}{\hat{V}'} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{\text{densityPerturbation}}{\hat{B}^2} . \end{aligned} \quad (106)$$

### Pressure perturbation

SFINCS also returns the pressure in  $\hat{f}_{s1}$ , normalized to the reference pressure  $\bar{n}\bar{T}$ :

$$\begin{aligned} \text{pressurePerturbation} &= \frac{1}{\bar{n}\bar{T}} \frac{m_s}{3} \int d^3v v^2 f_{s1} \\ &= \frac{8\pi\hat{m}_s}{3} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^{5/2} \int_0^\infty dx_s x_s^4 \hat{f}_{s,L=0} . \end{aligned} \quad (107)$$

Upon flux surface averaging, we obtain

$$\begin{aligned} \text{FSAPressurePerturbation} &= \left\langle \frac{1}{\bar{n}\bar{T}} \frac{m_s}{3} \int d^3v v^2 f_{s1} \right\rangle \\ &= \frac{1}{\hat{V}'} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{\text{pressurePerturbation}}{\hat{B}^2} . \end{aligned} \quad (108)$$

### Flow

We choose to normalize the parallel flow at each point as follows:

$$\text{flow} = \frac{1}{\bar{n}\bar{v}} \int d^3v v_{\parallel} f_{s1} = \frac{4\pi}{3} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^2 \int_0^\infty dx_s x_s^3 \hat{f}_{s,L=1} . \quad (109)$$

Both numerical and analytic calculations often employ the weights average flow  $\langle V_{\parallel} B \rangle$ . In SFINCS, this quantity is normalized in the following way:

$$\text{FSABFlow} = \frac{1}{\bar{n}\bar{v}\bar{B}} \langle B \int d^3v v_{\parallel} f \rangle = \frac{1}{\hat{V}'} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{\text{flow}}{\hat{B}} . \quad (110)$$

### Particle flux

The following expression is useful for evaluating the radial fluxes:

$$\mathbf{v}_{ms} \cdot \nabla \psi = -\bar{v}\bar{R}\bar{B} \frac{\Delta \hat{T}_s}{2Z_s \hat{B}} x_s^2 (1 + \xi^2) \frac{1}{\hat{G} + \hat{U}} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{U} \frac{\partial \hat{B}}{\partial \zeta} \right] . \quad (111)$$

We may write the radial particle flux as

$$\begin{aligned} \left\langle \int d^3v f_{s1} \mathbf{v}_{ms} \cdot \nabla \psi \right\rangle &= -\bar{n}\bar{v}\bar{R}\bar{B} \frac{\pi\Delta\hat{T}_s}{Z_s\hat{V}'} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^{3/2} \frac{1}{\hat{G} + i\hat{I}} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{1}{\hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \\ &\times \int_{-1}^1 d\xi \int_0^\infty dx_s \hat{f}_s x_s^4 (1 + \xi^2). \end{aligned} \quad (112)$$

Using

$$\int_{-1}^1 d\xi P_L(\xi) (1 + \xi^2) = \frac{8}{3} \delta_{L,0} + \frac{4}{15} \delta_{L,2} \quad (113)$$

then

$$\left\langle \int d^3v f_{s1} \mathbf{v}_{ms} \cdot \nabla \psi \right\rangle = \bar{n}\bar{v}\bar{R}\bar{B} (\text{particleFlux}) \quad (114)$$

where

$$\begin{aligned} \text{particleFlux} &= -\frac{\pi\Delta\hat{T}_s}{Z_s\hat{V}'} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^{3/2} \frac{1}{\hat{G} + i\hat{I}} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{1}{\hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \\ &\times \int_0^\infty dx_s x_s^4 \left[ \frac{8}{3} \hat{f}_{s,L=0} + \frac{4}{15} \hat{f}_{s,L=2} \right]. \end{aligned} \quad (115)$$

### Momentum flux

We may write a radial momentum flux as

$$\begin{aligned} \left\langle \int d^3v f_{s1} m_s v_{\parallel} \mathbf{v}_{ms} \cdot \nabla \psi \right\rangle &= -\bar{n}\bar{m}\bar{v}^2\bar{R}\bar{B} \frac{\pi\Delta\hat{T}_s}{Z_s\hat{V}'} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^2 \frac{\hat{m}_s}{\hat{G} + i\hat{I}} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{1}{\hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \\ &\times \int_{-1}^1 d\xi \int_0^\infty dx_s \hat{f}_s x_s^5 \xi (1 + \xi^2). \end{aligned} \quad (116)$$

Using

$$\int_{-1}^1 d\xi P_L(\xi) \xi (1 + \xi^2) = \frac{16}{15} \delta_{L,1} + \frac{4}{35} \delta_{L,3} \quad (117)$$

then

$$\left\langle \int d^3v f_{s1} v_{\parallel} \mathbf{v}_{ms} \cdot \nabla \psi \right\rangle = \bar{n}\bar{m}\bar{v}^2\bar{R}\bar{B} (\text{momentumFlux}) \quad (118)$$

where

$$\begin{aligned} \text{momentumFlux} &= -\frac{\pi\Delta\hat{T}_s}{Z_s\hat{V}'} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^2 \frac{\hat{m}_s}{\hat{G} + i\hat{I}} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{1}{\hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \\ &\times \int_0^\infty dx_s x_s^5 \left[ \frac{16}{15} \hat{f}_{s,L=1} + \frac{4}{35} \hat{f}_{s,L=3} \right]. \end{aligned} \quad (119)$$

### Heat flux

We may write the radial energy flux as

$$\left\langle \int d^3v f_{s1} \frac{m_s v^2}{2} \mathbf{v}_{ms} \cdot \nabla \psi \right\rangle = -\bar{n}\bar{m}\bar{v}^3 \bar{R}\bar{B} \frac{\pi \Delta \hat{T}_s \hat{m}_s}{2Z_s \hat{V}'} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^{5/2} \frac{1}{\hat{G} + i\hat{I}} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{1}{\hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \times \int_{-1}^1 d\xi \int_0^\infty dx_s \hat{f}_s x_s^6 (1 + \xi^2). \quad (120)$$

Using (113), then

$$\left\langle \int d^3v f_{s1} \frac{m_s v^2}{2} \mathbf{v}_{ms} \cdot \nabla \psi \right\rangle = \bar{n}\bar{m}\bar{v}^3 \bar{R}\bar{B} (\text{heatFlux}) \quad (121)$$

where

$$\begin{aligned} \text{heatFlux} = & -\frac{\pi \Delta \hat{T}_s \hat{m}_s}{2Z_s \hat{V}'} \left( \frac{\hat{T}_s}{\hat{m}_s} \right)^{5/2} \frac{1}{\hat{G} + i\hat{I}} \int_0^{2\pi} d\theta \int_0^{2\pi} d\zeta \frac{1}{\hat{B}^3} \left[ \hat{G} \frac{\partial \hat{B}}{\partial \theta} - \hat{I} \frac{\partial \hat{B}}{\partial \zeta} \right] \\ & \times \int_0^\infty dx_s \hat{f}_s x_s^6 \left[ \frac{8}{3} \hat{f}_{s,L=0} + \frac{4}{15} \hat{f}_{s,L=2} \right]. \end{aligned} \quad (122)$$

### Parallel current

The current is normalized as follows:

$$j_{\parallel} = \sum_s Z_s e n_s V_{\parallel s} = \sum_s Z_s e \int d^3v f_{s1} v_{\parallel} = e \bar{n} \bar{v} (\text{jHat}) \quad (123)$$

so

$$\text{jHat} = \frac{1}{e \bar{n} \bar{v}} \sum_s Z_s e \int d^3v f_{s1} v_{\parallel} = \sum_s Z_s (\text{flow}_s). \quad (124)$$

We also form the average  $\langle \mathbf{B} \cdot \mathbf{j} \rangle$  which is associated with the bootstrap current:

$$\langle \mathbf{B} \cdot \mathbf{j} \rangle = \left\langle \sum_s Z_s e n_s B V_{\parallel s} \right\rangle = \left\langle B \sum_s Z_s e \int d^3v f_{s1} v_{\parallel} \right\rangle = e \bar{n} \bar{v} \bar{B} (\text{FSAB jHat}) \quad (125)$$

where

$$\text{FSAB jHat} = \frac{1}{e \bar{n} \bar{v} \bar{B}} \left\langle B \sum_s Z_s e \int d^3v f_{s1} v_{\parallel} \right\rangle = \sum_s Z_s (\text{FSAB flow}_s). \quad (126)$$