A Methodology to estimate the probability of rare events in the transmission level power system dynamics.

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For more in depth results, check my Github repsository:

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Introduction

We study rare failures associated with cleared faults in the transmission level power system dynamics described by swing equations. Assumptions:

- Prior to a fault the system was in a balanced state.
- Fault is cleared within a few seconds.
- A failure is counted at a power line of the system if during the post-fault transient (before or after the fault is cleared) power flow along the line exceeded a safe limit.

The study aims to address questions such as the expected time to observe a failure and the probability distribution of failures occurring within a specific interval.

Objectives

■ The goal of this project is to develop a procedure to understand, estimate and analyze the dynamics of any given power grid that satisfies the linear swing equations.

- We are looking for a way to determine the distribution of the magnitude of the overloading of the system over time.
- This way we can determine how reliable and stable the system is even if there are failures in the grid for a random period of time.

Motivation

The power system dynamics described by swing equations are crucial for understanding/ensuring the stability/reliability of electrical power systems:

- **System Stability:** Swing equations analyze transient stability, ensuring a power system can recover from disturbances and maintain generation-consumption balance [1].
- **Grid Reliability:** Understanding power system dynamics allows operators to implement preventive measures, avoiding blackouts and ensuring reliable grid operation [2].

Materials and Methods

- A mathematical model simulating phase evolution in a power system, based on swing equations, incorporating post-fault and cleared fault dynamics.
- Implement numerical and analytical solutions to the swing equations using Julia 1.10.4 and the SciMLBase package.
- Estimate failure time, probabilities, and prolonged failure likelihood using brute-force MCMC for statistical analysis.

Swing Equations

We will work with the swing equation in the linear approximation [3]:

$$\forall i \in \mathcal{V}: \ m_i \ddot{\theta}_i(t) + d_i \dot{\theta}_i(t) + \sum_{\{i,j\} \in \mathcal{E}} a_{ij}(\theta_i(t) - \theta_j(t)) = P_i, \quad (1)$$

where \mathcal{V} and \mathcal{E} are the sets of nodes and (undirected) edges of the power system graph $\mathcal{G}=(\mathcal{V},\mathcal{E})$. The set of nodes \mathcal{V} , the vectors of internal voltage angles/phases $\theta(t)=(\theta_i(t)|i\in\mathcal{V})$, inertia $\boldsymbol{m}=(m_i|i\in\mathcal{V})$, damping $\boldsymbol{d}=(d_i|i\in\mathcal{V})$ and the power injection $\boldsymbol{P}=(P_i|i\in\mathcal{V})$ (where $\sum_{i\in\mathcal{V}}P_i=0$) stay constant through out the dynamics considered. We will also define the safety polytope:

$$\mathcal{P}_{\boldsymbol{\vartheta}} \doteq \left(\forall \{i, j\} \in \mathcal{E} : \left| \theta_i - \theta_j \right| \leqslant \vartheta_{ij} \right) : \boldsymbol{\vartheta} \doteq (\vartheta_{ij} | \{i, j\} \in \mathcal{E}). \tag{2}$$

The problem is initialized at the **steady state:**

$$\forall i \in \mathcal{V} : \sum_{\{i,j\} \in \mathcal{E}} a_{ij}(\theta_i(0) - \theta_j(0)) = P_i, \ \ddot{\theta}_i(0) = \dot{\theta}_i(0) = 0.$$
 (3)

Assuming that $\theta(0) \doteq (\theta_i(0)|i \in \mathcal{V}) \in \mathcal{P}_{\vartheta}$.

Simulating Faults

We are interested in the process $\theta(t)$ that follows (1) up to a certain time τ , at that moment we imitate a fault in the system by changing the set of edges/lines $\mathcal E$ removing a pre-selected edge $\alpha \in \mathcal E$ thus transitioning abruptly:

$$\mathcal{E} \to \mathcal{E}_f \doteq \mathcal{E} \backslash \alpha$$
.

The fault lasts for time τ which results in the evolution of $\theta(t)$ according (1) with a different set of edges for $t \in [0, \tau]$:

$$\forall i \in \mathcal{V}: \ m_i \ddot{\theta}_i(t) + d_i \dot{\theta}_i(t) + \sum_{\{i,j\} \in \mathcal{E}_f} a_{ij}(\theta_i(t) - \theta_j(t)) = P_i, \quad \textbf{(4)}$$

Then for $t>\tau$ we fix the fault, that is $\theta(t)$ will follow (1) for $t>\tau$.

Measuring the degree of line overload

To quantify the degree of line overload, given a solution

$$X = \begin{bmatrix} \dot{\bar{\theta}}(t) \\ \bar{\theta}(t) \end{bmatrix}_{t=0}^{t=T}$$

to (1), (2), (3) and (4), (and thus it also satisfies (Ω)) we introduce the following indicator:

$$S(X) \doteq \int_0^T dt \sum_{\{i,j\} \in \mathcal{E}} \mathbb{I}\left(|\beta_{ij}(\theta_i(t) - \theta_j(t))| - \bar{p}_{ij}\right), \tag{5}$$

The indicator function S(X) is the primary characteristic we aim to evaluate across various failure scenarios.

Case Study 1: Israeli Power Grid

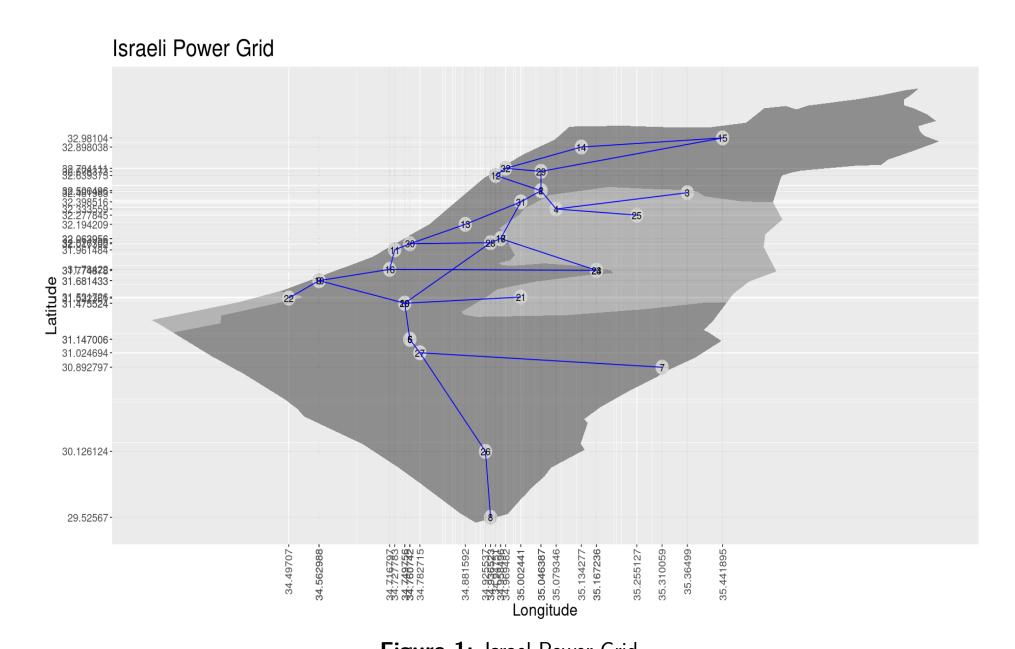


Figure 1: Israel Power Grid.

We will simulate and sample solutions to the system

$$\begin{cases} \Upsilon \cdot \dot{X}(t) = \Xi_2 \cdot X(t) + b \text{ for } t \in [0, \tau], \\ \Upsilon \cdot \dot{X}(t) = \Xi_1 \cdot X(t) + b \text{ for } t > \tau, \\ X(t) = \begin{bmatrix} \dot{\bar{\theta}}(t) \\ \bar{\theta}(t) \end{bmatrix}, \Upsilon = \begin{bmatrix} M & \bar{0}_{n \times n} \\ \bar{0}_{n \times n} & \mathsf{Id}_{n \times n} \end{bmatrix}, \Xi_i = \begin{bmatrix} -D_i & -L_i \\ \mathsf{Id}_{n \times n} & \bar{0}_{n \times n} \end{bmatrix}, \\ \tau \sim \mathsf{Exp}(0.1), b = \begin{bmatrix} \bar{P} \\ \bar{0}_n \end{bmatrix}, \theta(0) = L_1^+ \cdot \bar{P} \in \mathcal{P}_{\vartheta}, \dot{\theta}(0) = \bar{0}, \\ \mathcal{V} = \{1, \dots, 32\}, \mathcal{E} = \{\{1, 2\}, \{1, 4\}, \dots, \{29, 32\}\} : \|\mathcal{E}\| = 36, \end{cases}$$

and estimate the probability of exiting the \mathcal{P}_{ϑ} using S(X).

Statistics of Three Phase Fault Simulation

Distribution of First Exit Time and Distribution of Last Return Time Removed Line(s) = Random [Random Time of Clearance] - Distribution of First Exit Time - Distribution of Last Return Time - Distribution of Last Return Time Survival Function of the Overheating Indicator Removed Line(s) - Random Survival Function of the Overheating Indicator Removed Line(s) - Random

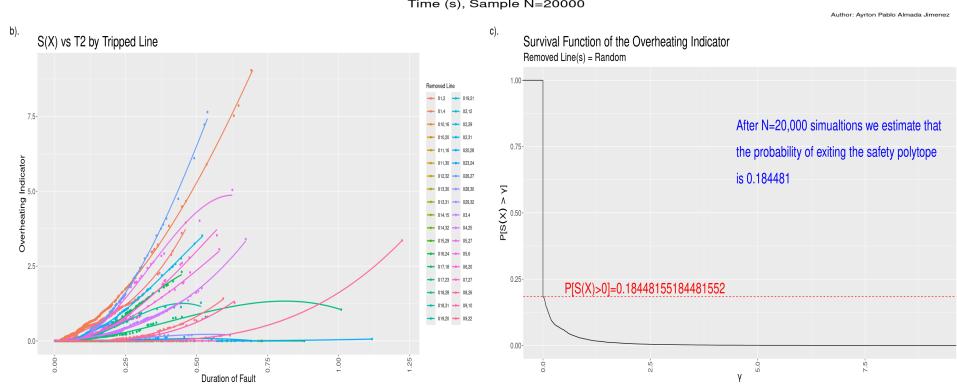


Figure 2: a). Distribution of First Exit Time and Distribution of Last Return Time, d). Cubic Regression: Overheating indicator vs Duration of Fault, c). Survival Function of Overheating Indicator.

Statistics of Single Phase Fault Simulation

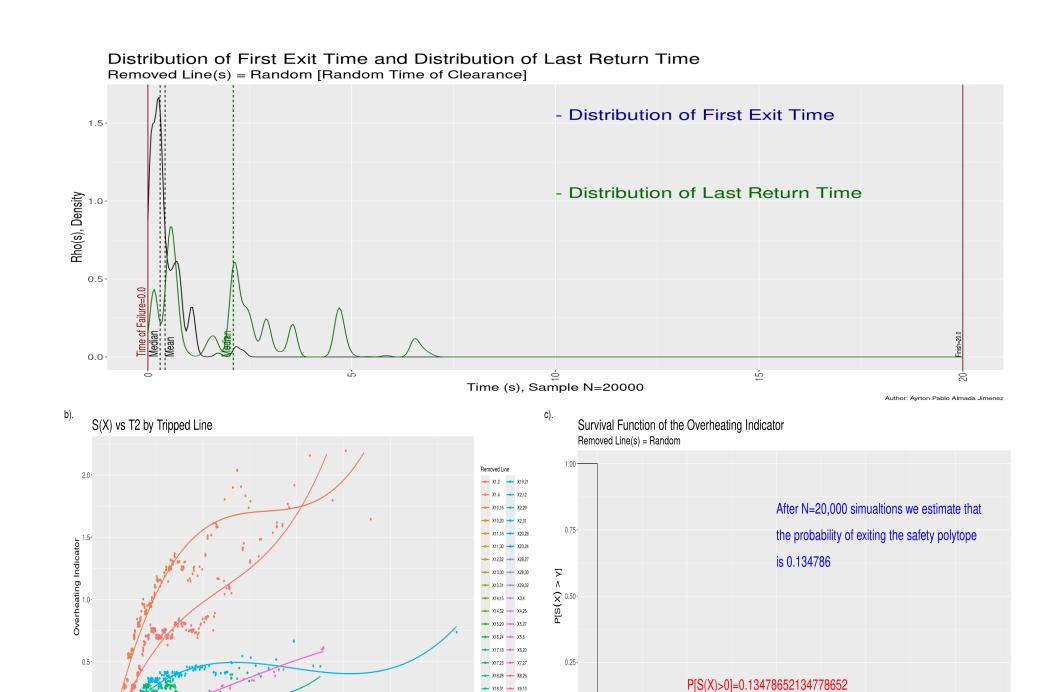


Figure 3: a). Distribution of First Exit Time and Distribution of Last Return Time, b). Quadratic Regression: Overheating indicator vs Duration of Fault, c). Survival Function of Overheating Indicator

Future Directions

- Apply sampling techniques, such as cross-entropy, adaptive importance sampling, and quasi-Monte Carlo, to enhance efficiency and results.
- Analyze and sample from a stochastic model to add noise and simulate a realistic power grid:

$$m_i D^2 \theta_i(t) + d_i D \theta_i(t) + \sum_{\{i,j\} \in \mathcal{E}} a_{ij}(\theta_i(t) - \theta_j(t)) Dt = P_i Dt + DW_i(t),$$

where D is the derivative operator, Dt is the differential w.r.t. t and $DW(t) = (DW_i(t)|i \in \mathcal{V})$ is a vector of Brownian noise.

 Perform statistical analysis of large power systems to improve methodology efficiency (e.g. Texas Interconnection, Mexico's National Power System, or the UCTE grid)

References

- [1] Leonard L Grigsby. *Power system stability and control*. CRC press,
- [2] Prabha Kundur. Power system stability. *Power system stability and control*, 10:7–1, 2007.
- [3] D Ruiz-Vega, D Olguín Salinas, and M Pavella. Simultaneous optimization of transient stability-constrained transfer limits of multi-area power systems. In *Proceedings of Med Power 2002 Conference*, 2002.