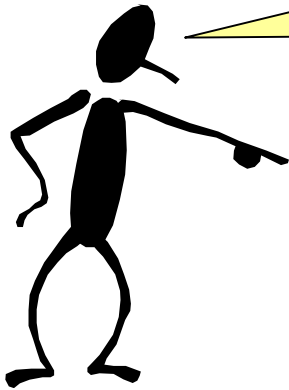


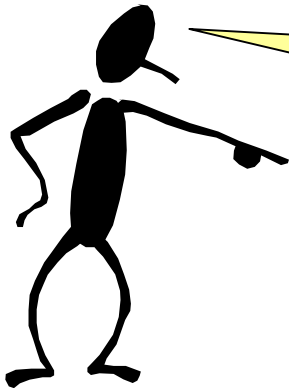
CHAPTER 8: THE PID CONTROLLER



When I complete this chapter, I want to be able to do the following.

- **Understand the strengths and weaknesses of the three modes of the PID**
- **Determine the model of a feedback system using block diagram algebra**
- **Establish general properties of PID feedback from the closed-loop model**

CHAPTER 8: THE PID CONTROLLER



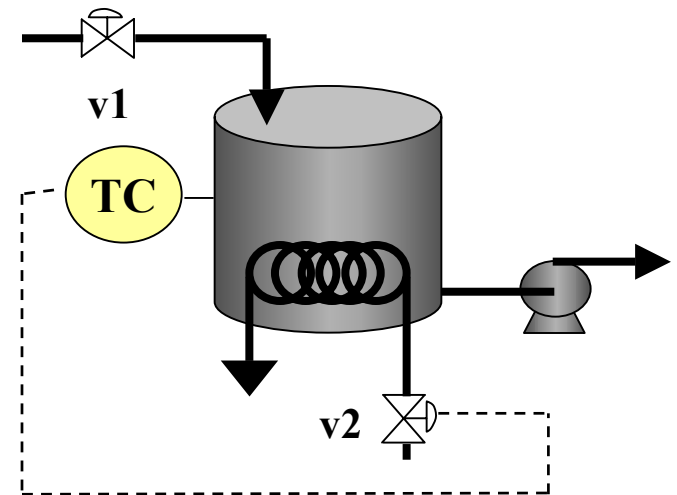
Outline of the lesson.

- **General Features and history of PID**
- **Model of the Process and controller - the Block Diagram**
- **The Three Modes with features**
 - **Proportional**
 - **Integral**
 - **Derivative**
- **Typical dynamic behavior**

CHAPTER 8: THE PID CONTROLLER

PROPERTIES THAT WE SEEK IN A CONTROLLER

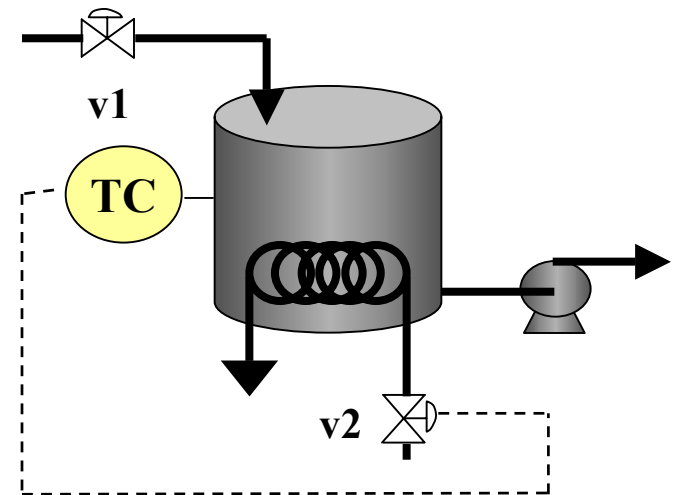
- **Good Performance** - feedback measures from Chapter 7
- **Wide applicability** - adjustable parameters
- **Timely calculations** - avoid convergence loops
- **Switch to/from manual** - bumplessly
- **Extensible** - enhanced easily



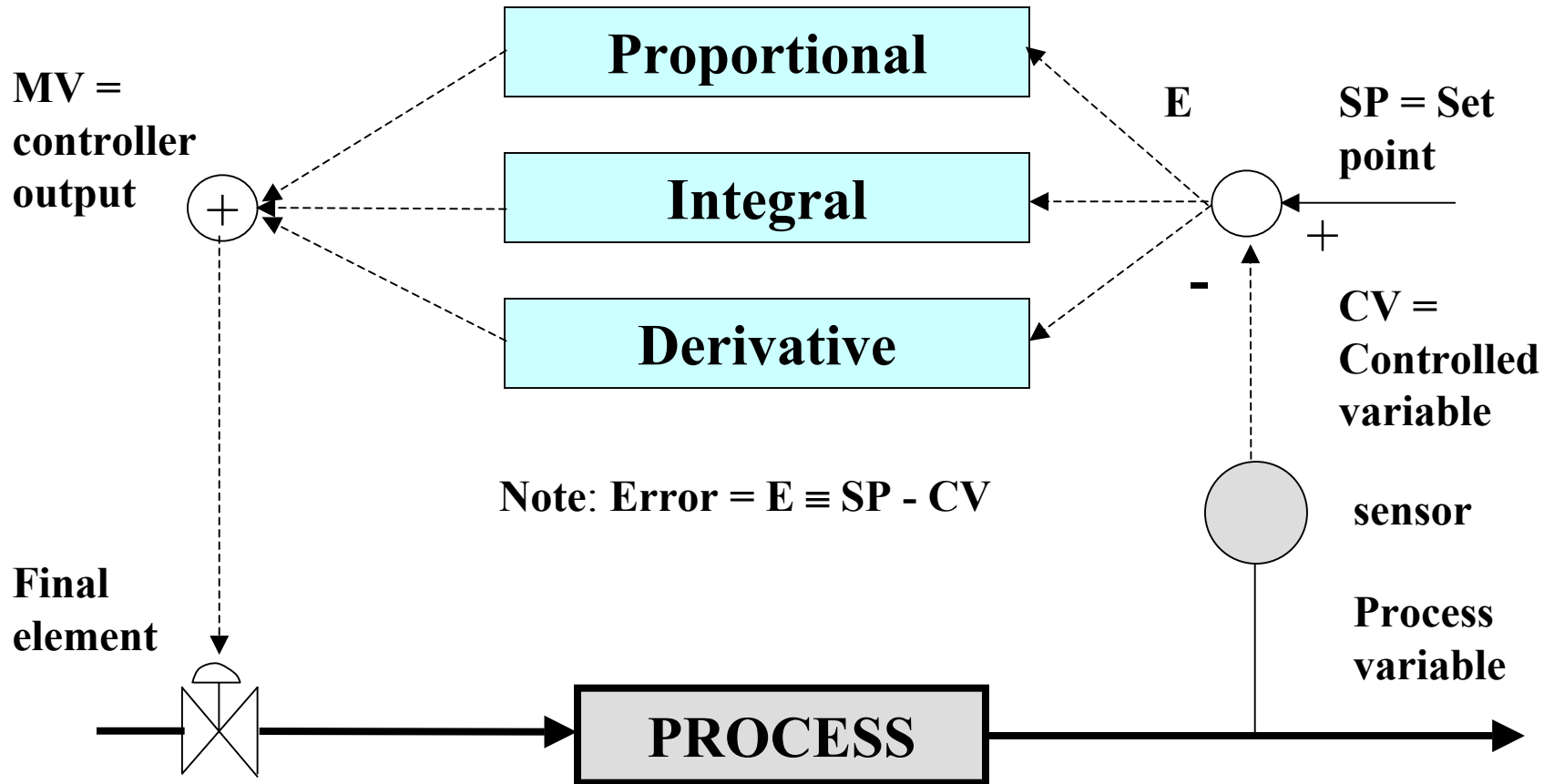
CHAPTER 8: THE PID CONTROLLER

SOME BACKGROUND IN THE CONTROLLER

- Developed in the **1940's**, remains workhorse of practice
- **Not “optimal”**, based on good properties of each mode
- Programmed in digital control equipment
- **ONE** controlled variable (CV) and **ONE** manipulated variable (MV). Many PID's used in a plant.



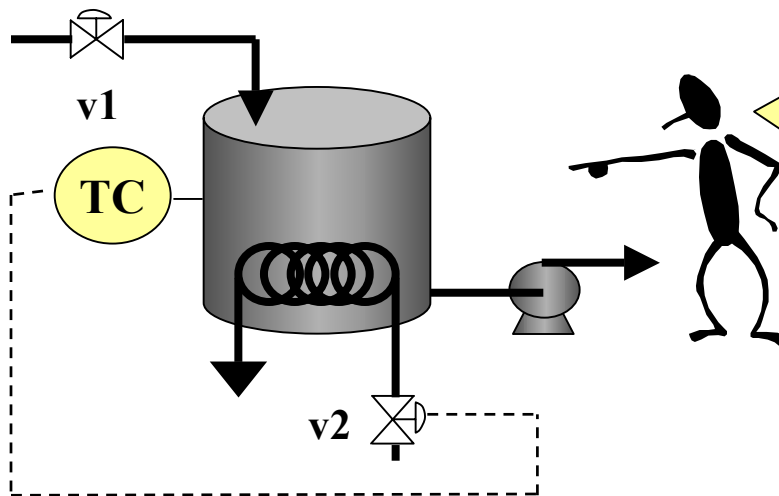
CHAPTER 8: THE PID CONTROLLER



Three “modes”: Three ways of using the time-varying behavior of the measured variable

CHAPTER 8: THE PID CONTROLLER

Closed-Loop Model: Before we learn about each calculation, we need to develop a general dynamic model for a **closed-loop system** - that is the process and the controller working as an integrated system.

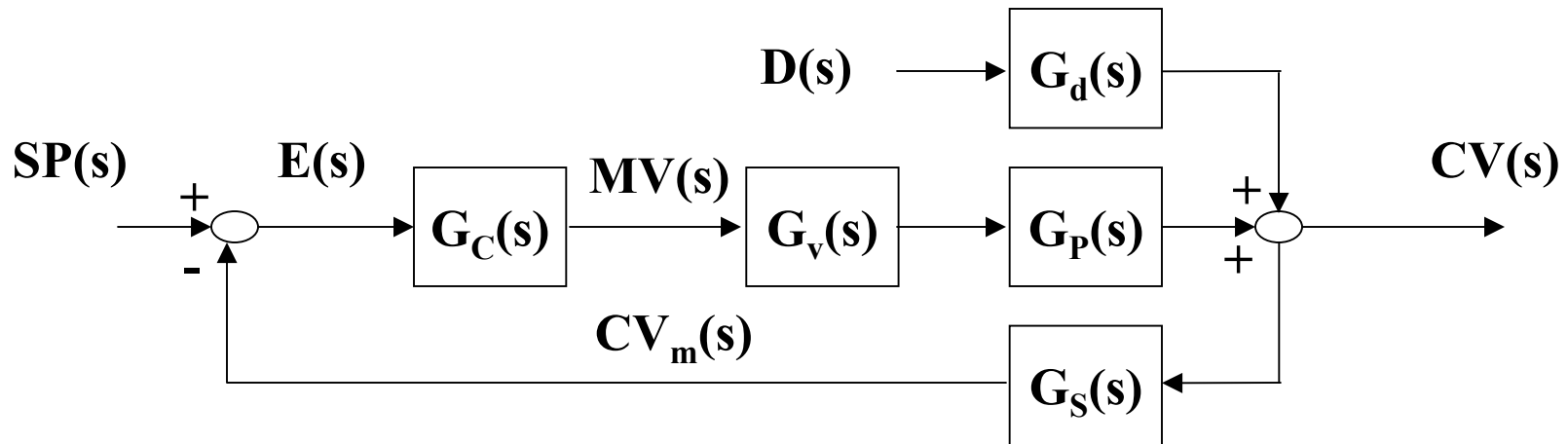


This is an example; how can we generalize?

- What if we measured pressure, or flow, or ...?
- What if the process were different?
- What if the valve were different?

CHAPTER 8: THE PID CONTROLLER

GENERAL CLOSED-LOOP MODEL BASED ON BLOCK DIAGRAM



Transfer functions

$G_C(s)$ = controller

$G_v(s)$ = valve +

$G_P(s)$ = feedback process

$G_S(s)$ = sensor

$G_d(s)$ = disturbance process

Variables

$CV(s)$ = controlled variable

$CV_m(s)$ = measured value of $CV(s)$

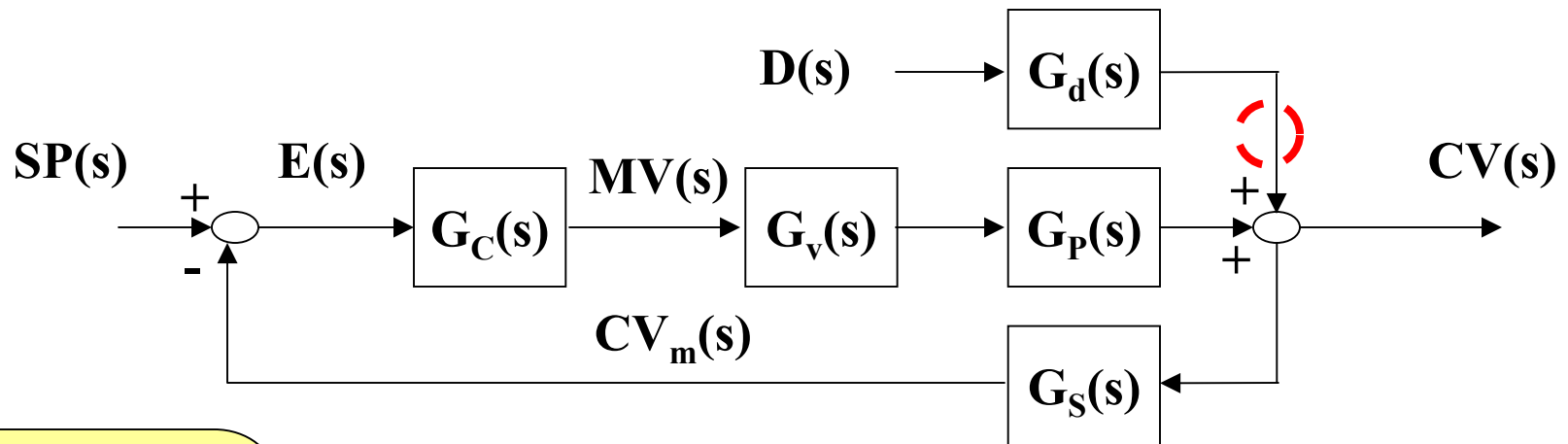
$D(s)$ = disturbance

$E(s)$ = error

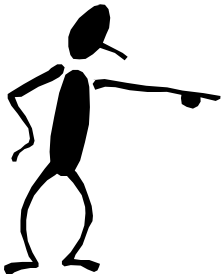
$MV(s)$ = manipulated variable

$SP(s)$ = set point

CHAPTER 8: THE PID CONTROLLER

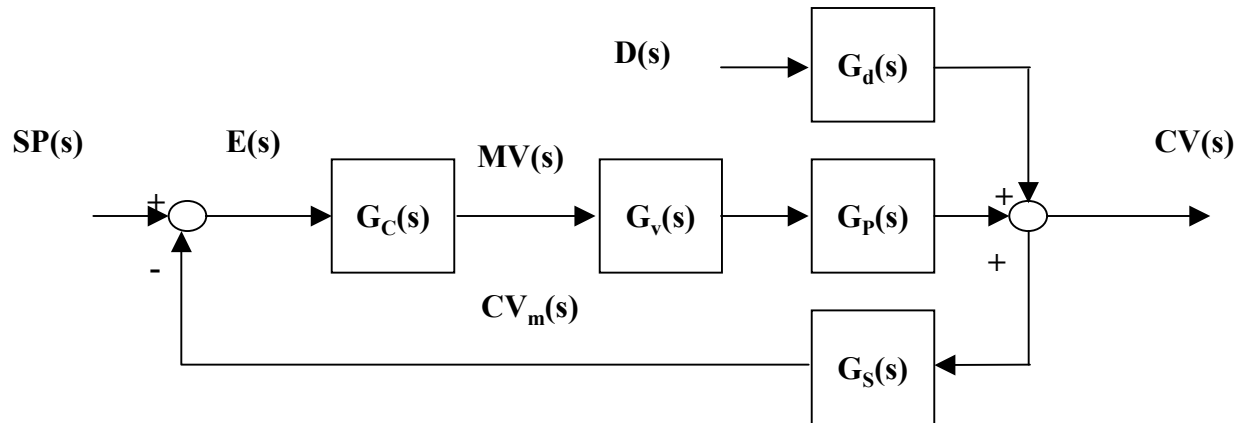


Let's audit
our
understanding



- Where are the models for the transmission, and signal conversion?
- What is the difference between $CV(s)$ and $CV_m(s)$?
- What is the difference between $G_P(s)$ and $G_d(s)$?
- How do we measure the variable whose line is indicated by the red circle?
- Which variables are determined by a person, which by computer?

CHAPTER 8: THE PID CONTROLLER



Set point response

$$\frac{CV(s)}{SP(s)} = \frac{G_p(s)G_v(s)G_c(s)}{1 + G_p(s)G_v(s)G_c(s)G_s(s)}$$

Disturbance Response

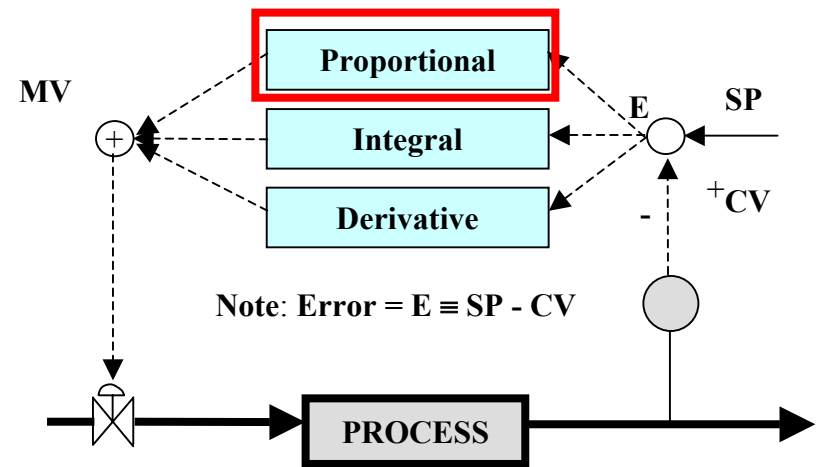
$$\frac{CV(s)}{D(s)} = \frac{G_d(s)}{1 + G_p(s)G_v(s)G_c(s)G_s(s)}$$



- Which elements in the control system affect system stability?
- Which elements affect dynamic response?

CHAPTER 8: THE PID CONTROLLER, The Proportional Mode

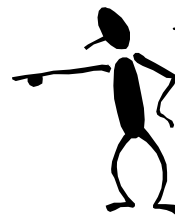
“correction proportional to error.”



Time domain : $MV(t) = K_c E(t) + I_p$

Transfer function : $G_C(s) = \frac{MV(s)}{E(s)} = K_C$

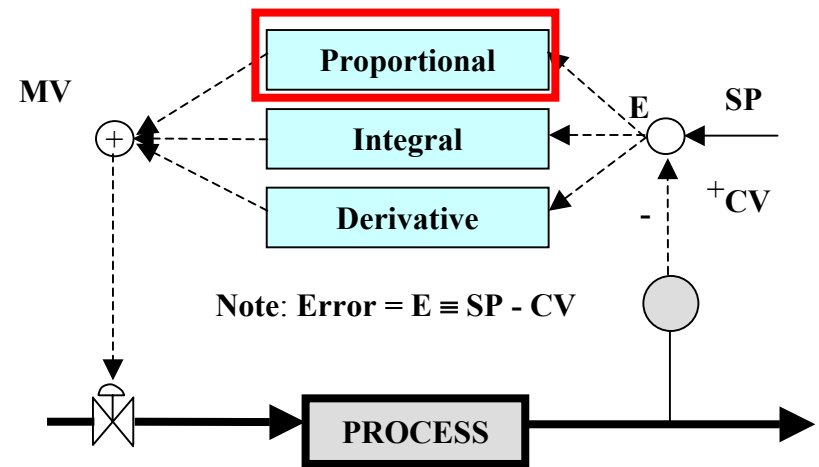
K_C = controller gain



How does this differ from the process gain, K_p ?

CHAPTER 8: THE PID CONTROLLER, The Proportional Mode

“correction proportional to error.”



Time domain : $MV(t) = K_c E(t) + I_p$

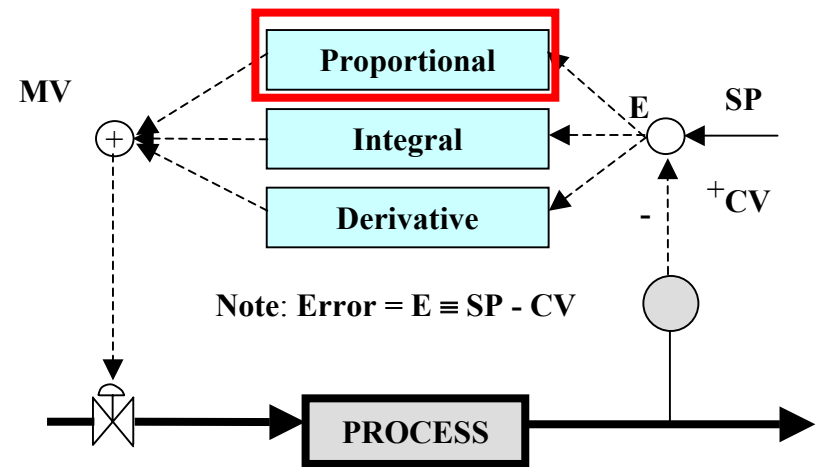
K_C = controller gain

How does this differ from the process gain, K_p ?

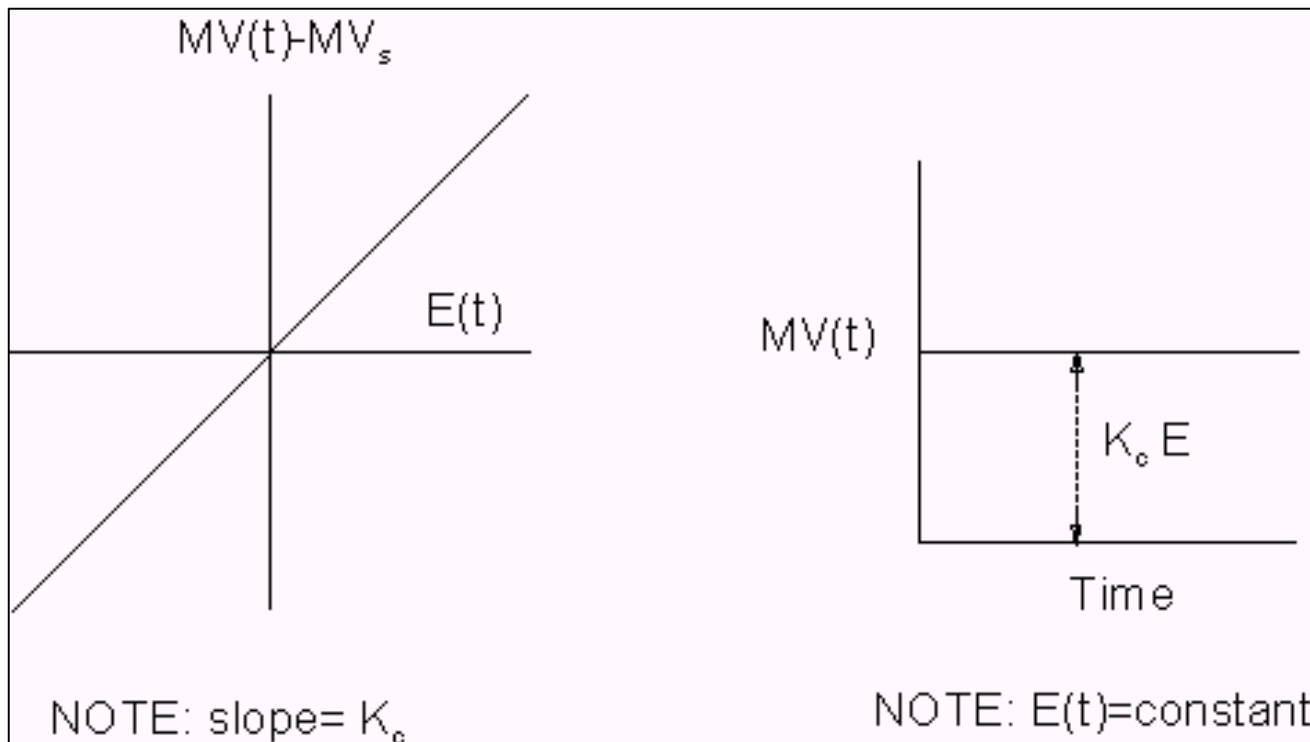
K_p depends upon the process (e.g., reactor volume, flows, temperatures, etc.)

K_C is a number we select; it is used in the computer each time the controller equation is calculated

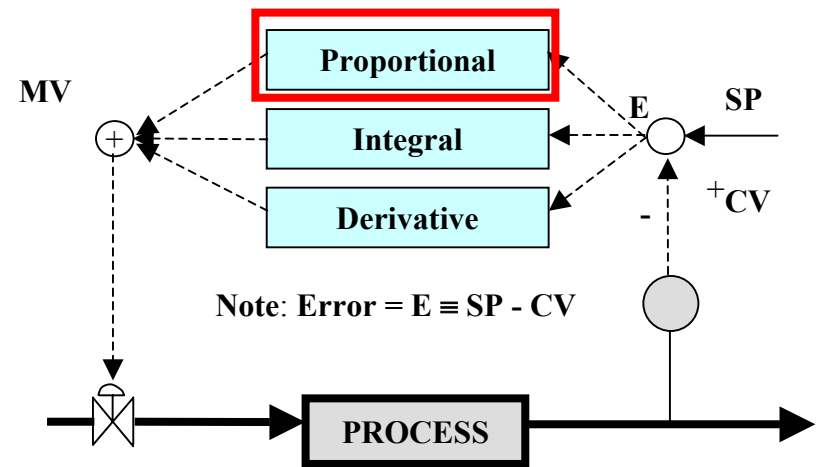
CHAPTER 8: THE PID CONTROLLER, The Proportional Mode



Time domain : $MV(t) = K_c E(t) + I_p$

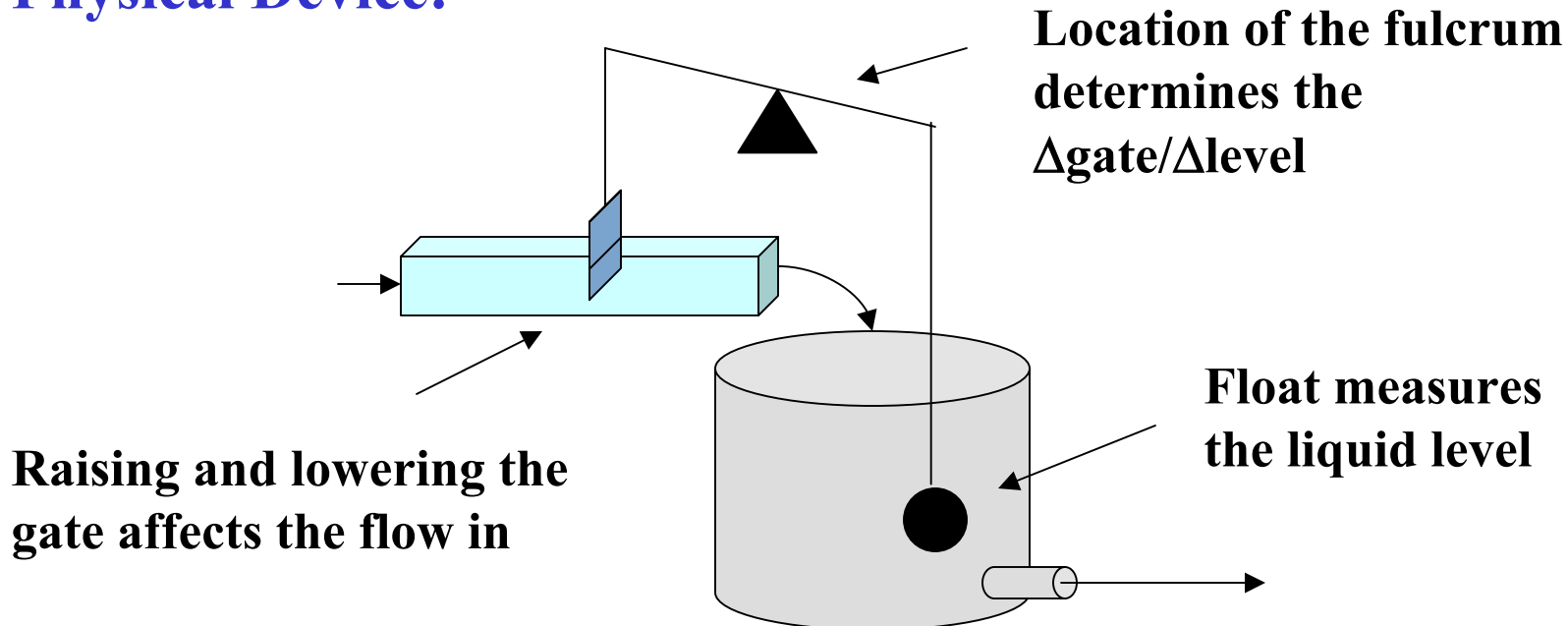


CHAPTER 8: THE PID CONTROLLER, The Proportional Mode

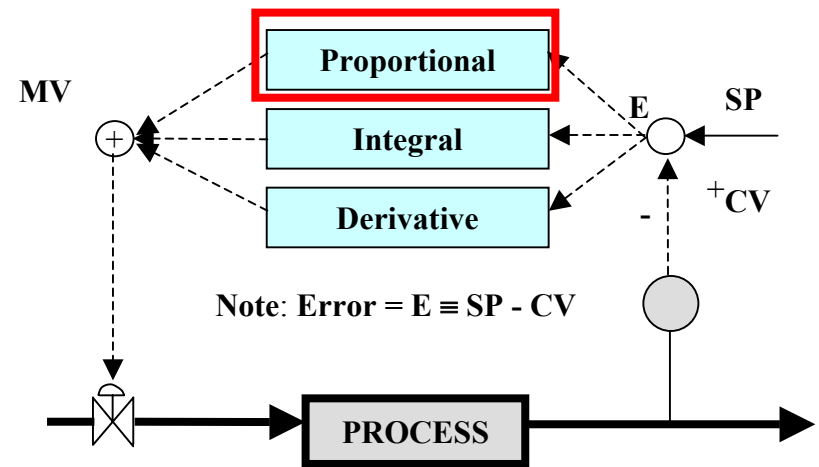


Time domain : $MV(t) = K_c E(t) + I_p$

Physical Device:



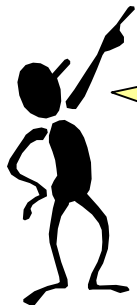
CHAPTER 8: THE PID CONTROLLER, The Proportional Mode



Key feature of closed-loop performance with P-only

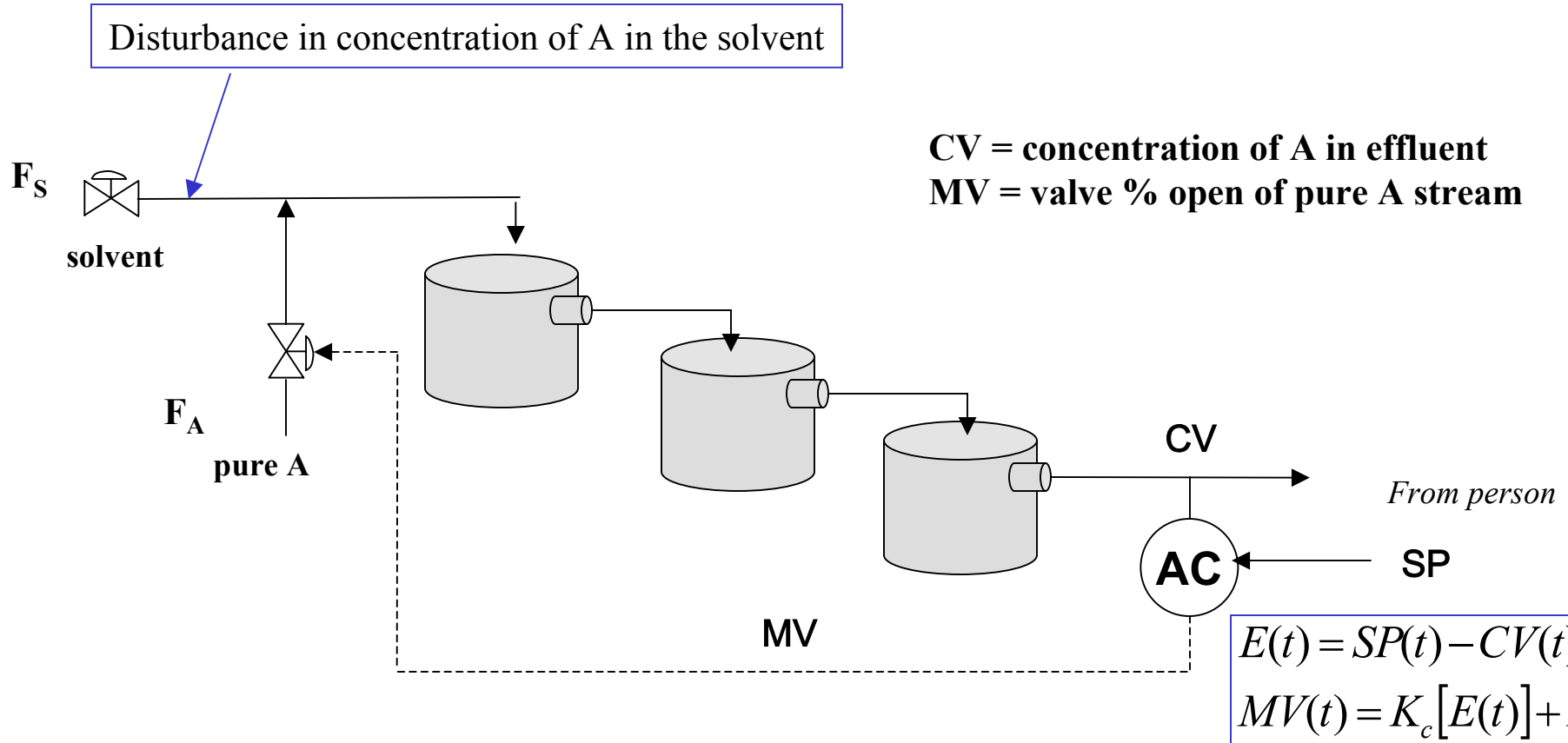
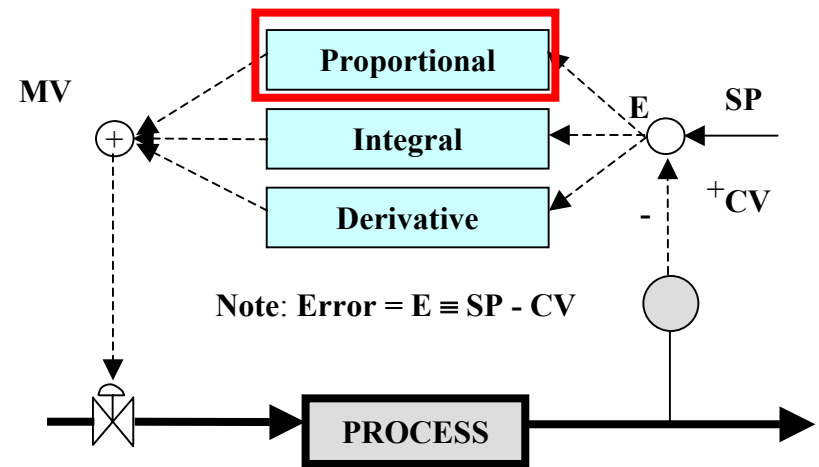
**Final value
after
disturbance:**

$$CV(t)\Big|_{t \rightarrow \infty} = \lim_{s \rightarrow 0} s \frac{\Delta D}{s} \frac{K_d}{1 + K_c K_p} = \frac{\Delta D K_d}{1 + K_c K_p} \neq 0$$

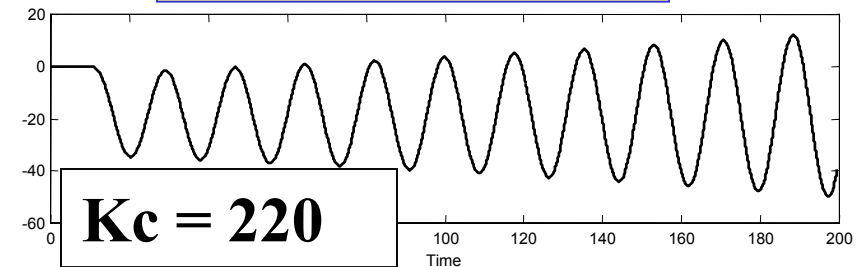
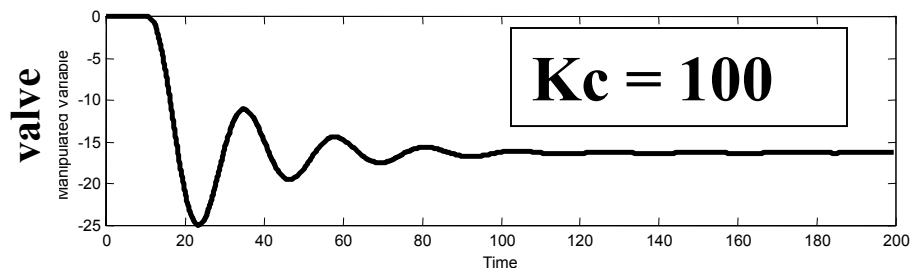
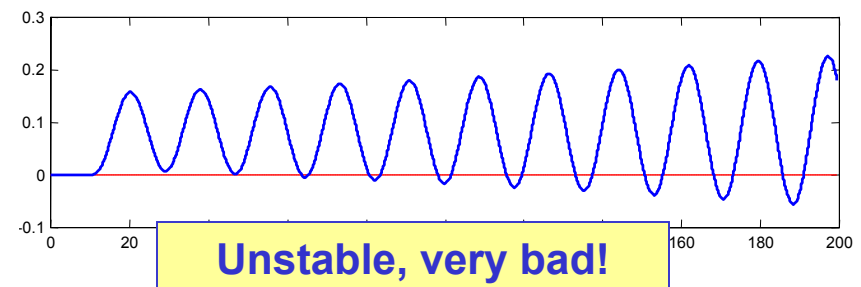
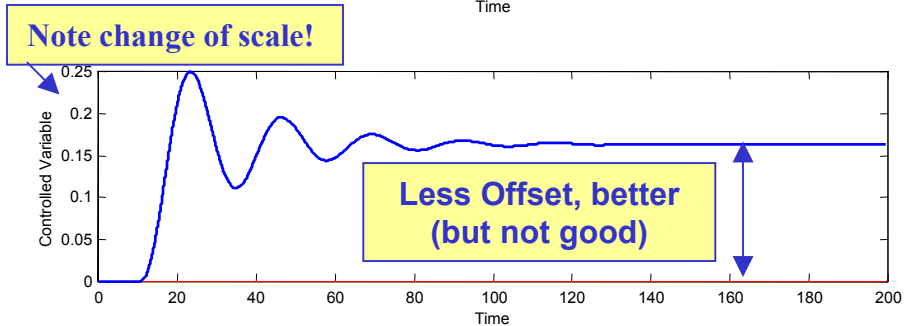
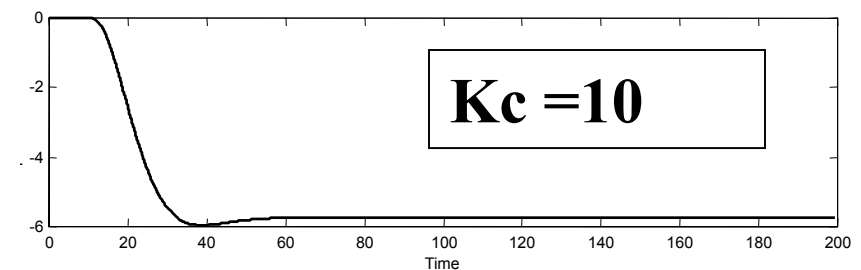
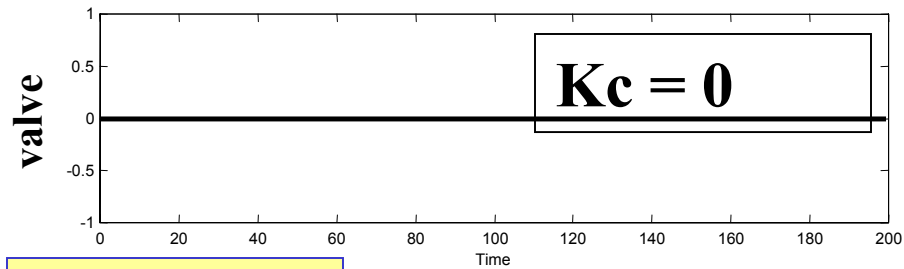
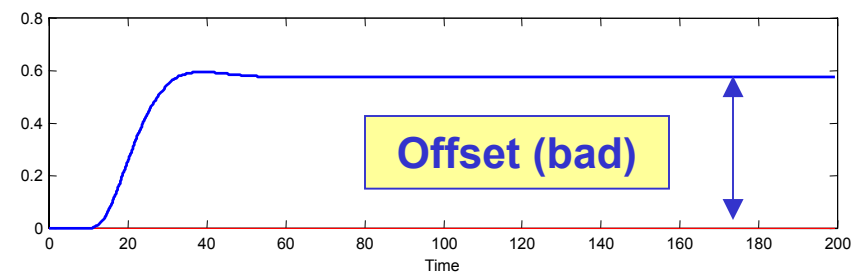
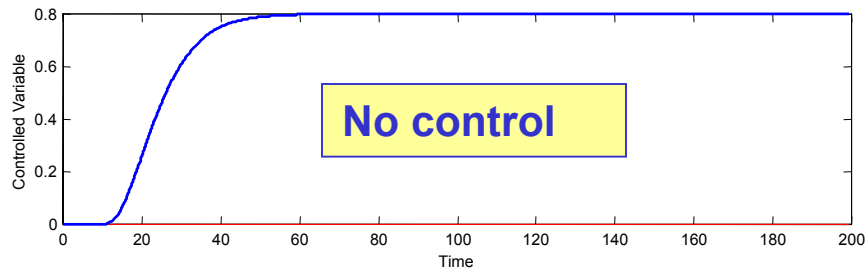


- We do not achieve zero offset; **don't return to set point!**
- How can we get very close by changing a controller parameter?
- Any possible problems with suggestion?

CHAPTER 8: THE PID CONTROLLER, The Proportional Mode

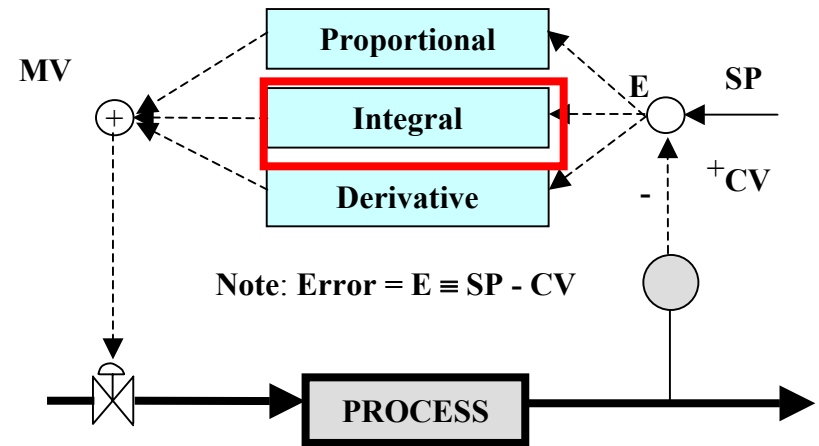


THE PID CONTROLLER, The Proportional Mode



CHAPTER 8: THE PID CONTROLLER, The Integral Mode

“The persistent mode”

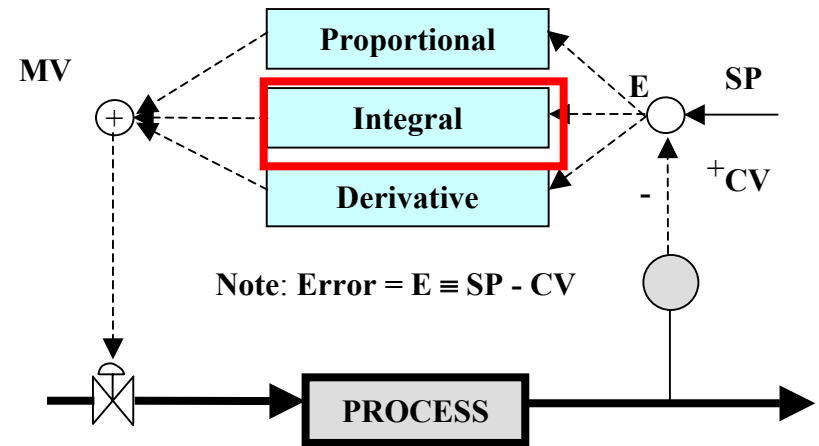


Time domain :
$$MV(t) = \frac{K_c}{T_I} \int_0^t E(t') dt' + I_I$$

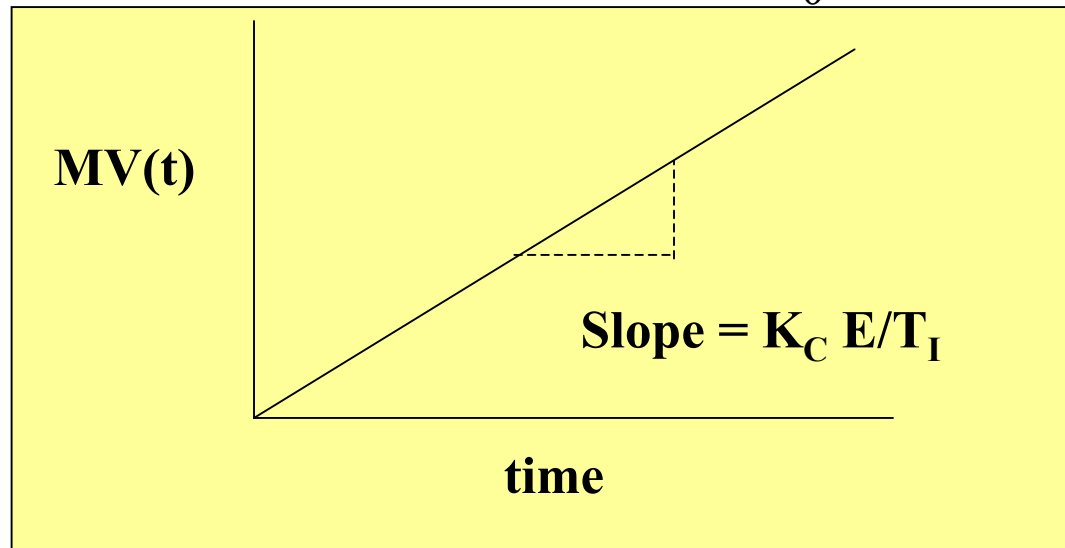
Transfer function :
$$G_C(s) = \frac{MV(s)}{E(s)} = \frac{K_C}{T_I} \frac{1}{s}$$

T_I = controller integral time (in denominator)

CHAPTER 8: THE PID CONTROLLER, The Integral Mode

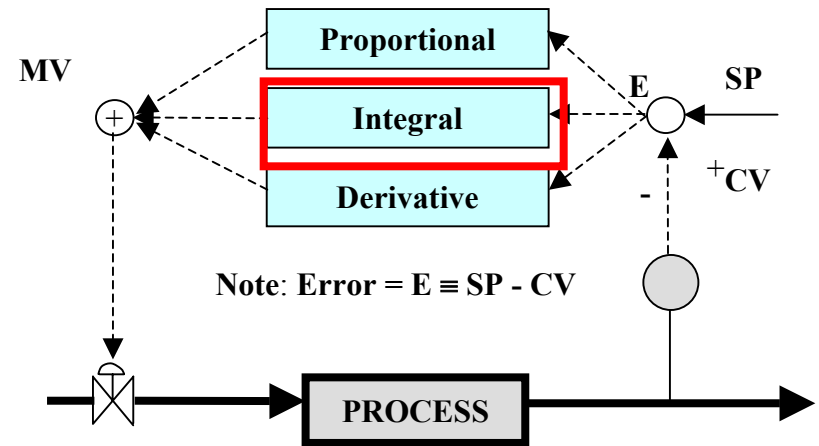


Time domain :
$$MV(t) = \frac{K_c}{T_I} \int_0^t E(t') dt' + I_I$$



Behavior when $E(t) = \text{constant}$

CHAPTER 8: THE PID CONTROLLER, The Integral Mode



Key feature of closed-loop performance with I mode

**Final value
after
disturbance:**

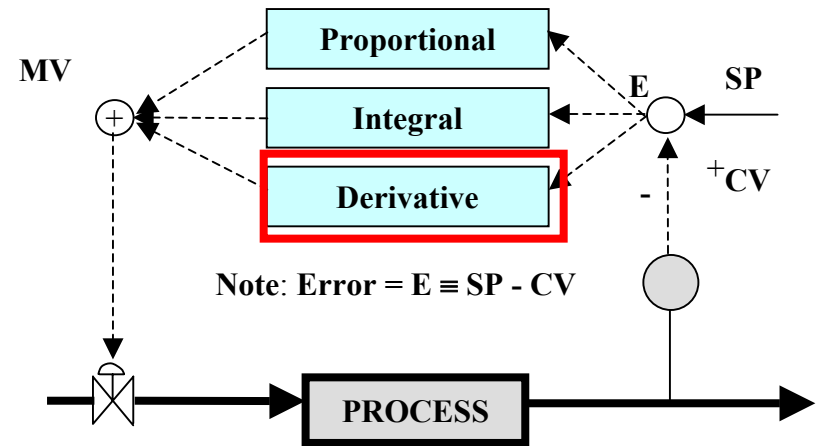
$$CV(t)\Big|_{t \rightarrow \infty} = \lim_{s \rightarrow 0} s \frac{\Delta D}{s} \frac{K_d}{1 + \frac{K_c K_p}{s T_I}} = 0$$



- We achieve zero offset for a step disturbance;
return to set point!
- Are there other scenarios where we do not?

CHAPTER 8: THE PID CONTROLLER, The Derivative Mode

“The predictive mode”

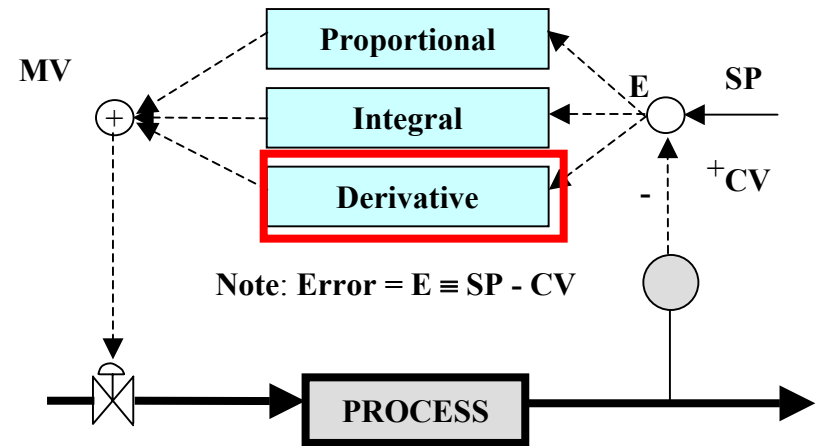


Time domain : $MV(t) = K_c T_D \frac{dE(t)}{dt} + I_D$

Transfer function : $G_C(s) = \frac{MV(s)}{E(s)} = K_c T_d s$

T_D = controller derivative time

CHAPTER 8: THE PID CONTROLLER, The Derivative Mode



Key features using closed-loop dynamic model

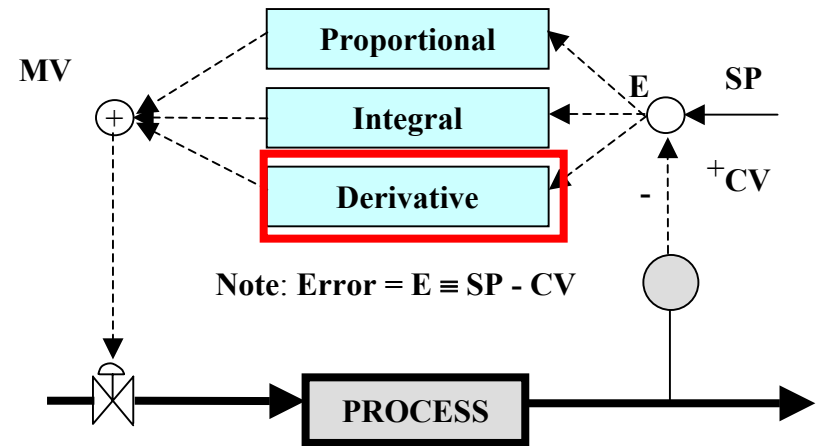
Final value
after
disturbance:

$$CV(t)\Big|_{t \rightarrow \infty} = \lim_{s \rightarrow 0} s \frac{\Delta D}{s} \frac{K_d}{1 + K_c T_d s} = \Delta D K_d$$



We do not achieve zero offset; do not return to set point!

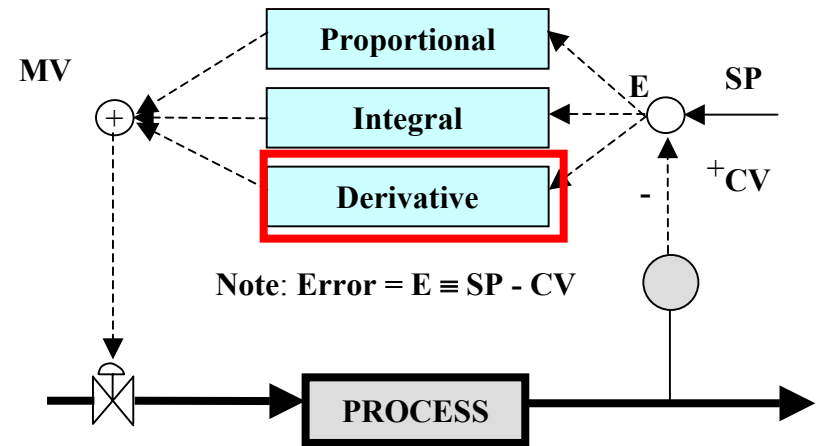
CHAPTER 8: THE PID CONTROLLER, The Derivative Mode



Time domain : $MV(t) = K_c T_D \frac{dE(t)}{dt} + I_D$

- What would be the behavior of the manipulated variable when we enter a step change to the set point?
- How can we modify the algorithm to improve the performance?

CHAPTER 8: THE PID CONTROLLER, The Derivative Mode

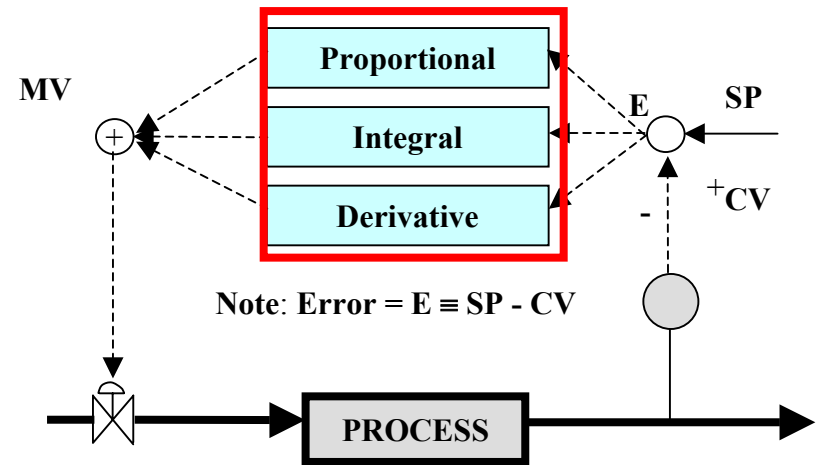


Time domain : $MV(t) = \cancel{K_c} T_D \frac{dE(t)}{dt} + I_D$

We do not want to take the derivative of the set point; therefore, we use only the CV when calculating the derivative mode.

Time domain : $MV(t) = -K_c T_D \frac{d CV(t)}{dt} + I_D$

CHAPTER 8: THE PID CONTROLLER



Let's combine the modes to formulate the PID Controller!

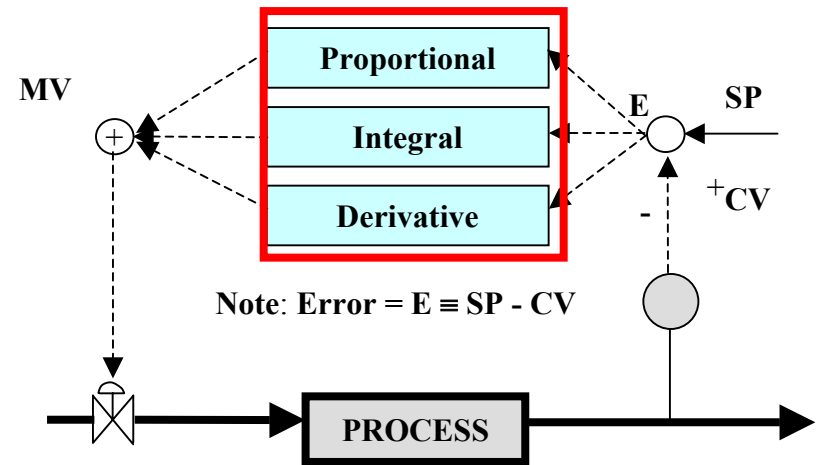
$$E(t) = SP(t) - CV(t)$$

$$MV(t) = K_c \left[E(t) + \frac{1}{T_I} \int_0^t E(t') dt' - T_d \frac{d CV}{dt} \right] + I$$



Please explain every term and symbol.

CHAPTER 8: THE PID CONTROLLER



Let's combine the modes to formulate the PID Controller!

$$E(t) = SP(t) - CV(t) \quad \left. \vphantom{E(t)} \right\} \text{Error from set point}$$

$$MV(t) = K_c \left[\underbrace{E(t)}_{\text{proportional}} + \underbrace{\frac{1}{T_I} \int_0^t E(t') dt'}_{\text{integral}} - \underbrace{T_d \frac{d CV}{dt}}_{\text{derivative}} \right] + I$$

Constant (bias) for bumpless transfer

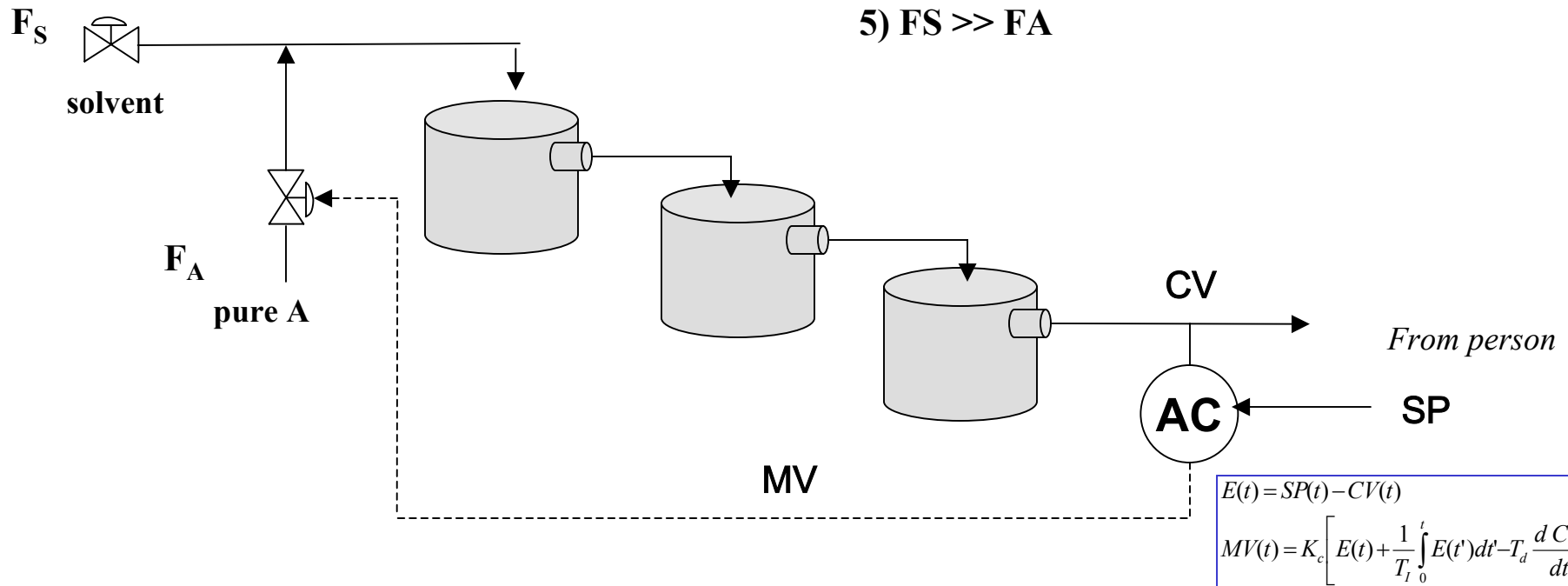
CHAPTER 8: THE PID CONTROLLER

Let's apply the controller to the three-tank mixer (no rxn).

CV = concentration of A in effluent
MV = valve % open of pure A stream

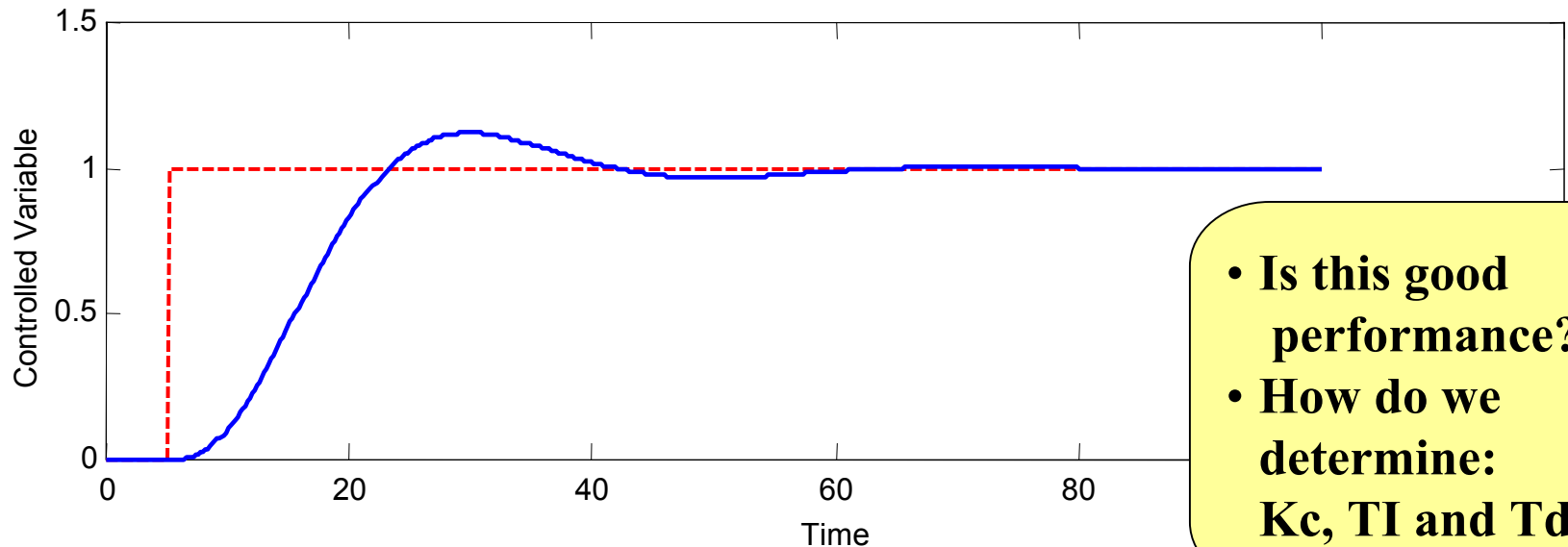
Notes:

- 1) tanks are well mixed
- 2) liquid volumes are constant
- 3) sensor and valve dynamics are negligible
- 4) $F_A = K_v (v)$, with $v = \% \text{ opening}$
- 5) $F_S \gg F_A$

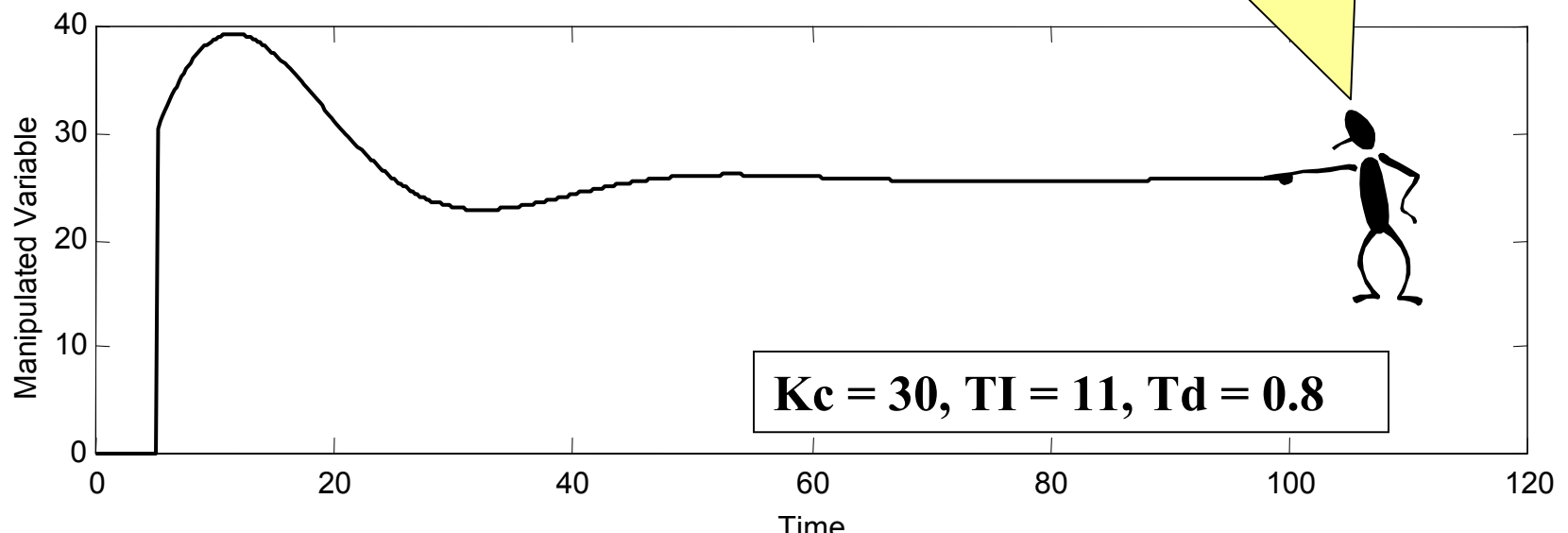


CHAPTER 8: THE PID CONTROLLER

S-LOOP plots deviation variables (IAE = 12.2869)



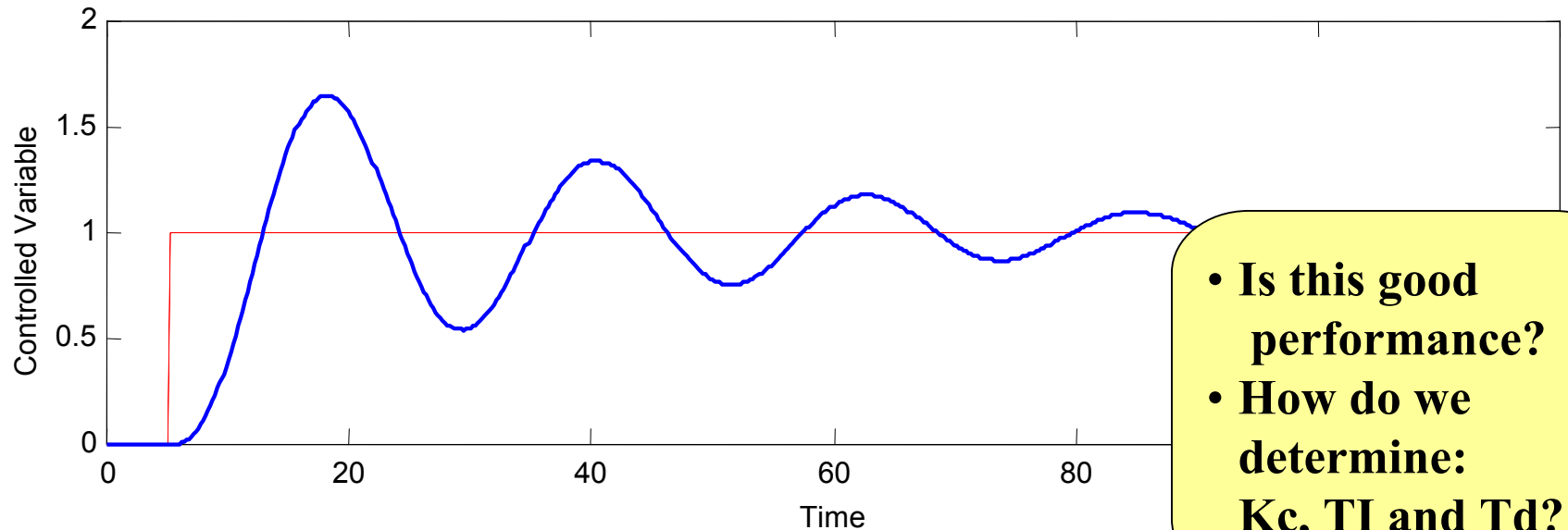
- Is this good performance?
- How do we determine: K_c , T_I and T_d ?



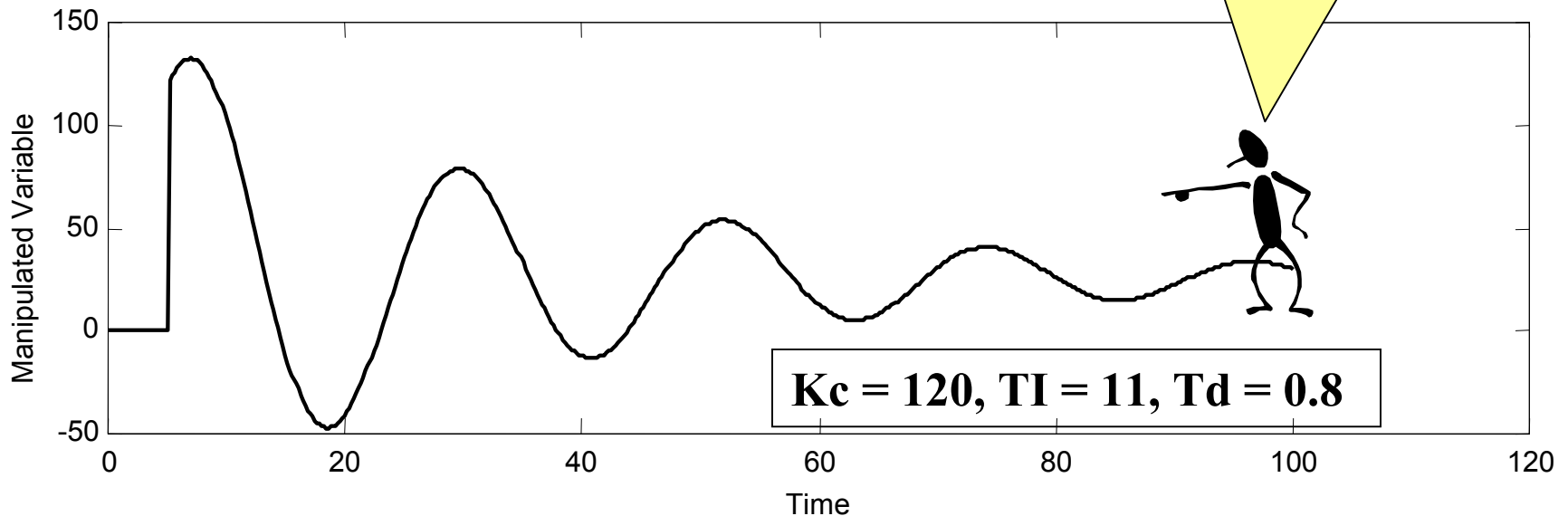
$K_c = 30, T_I = 11, T_d = 0.8$

CHAPTER 8: THE PID CONTROLLER

S-LOOP plots deviation variables (IAE = 20.5246)



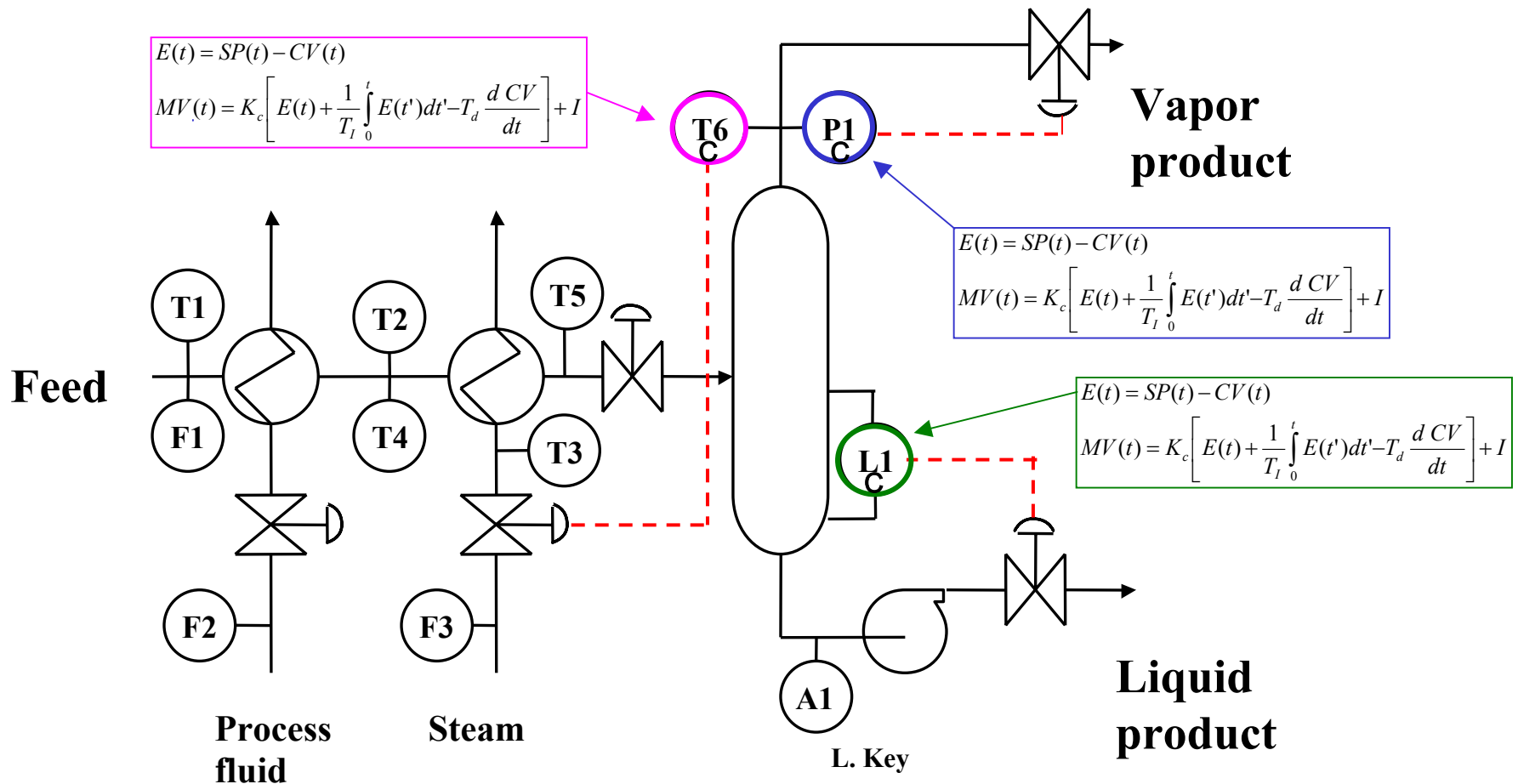
- Is this good performance?
- How do we determine: K_c , T_I and T_d ?



$K_c = 120, T_I = 11, T_d = 0.8$

CHAPTER 8: THE PID CONTROLLER

Lookahead: We can apply **many PID controllers** when we have many variables to be controlled!



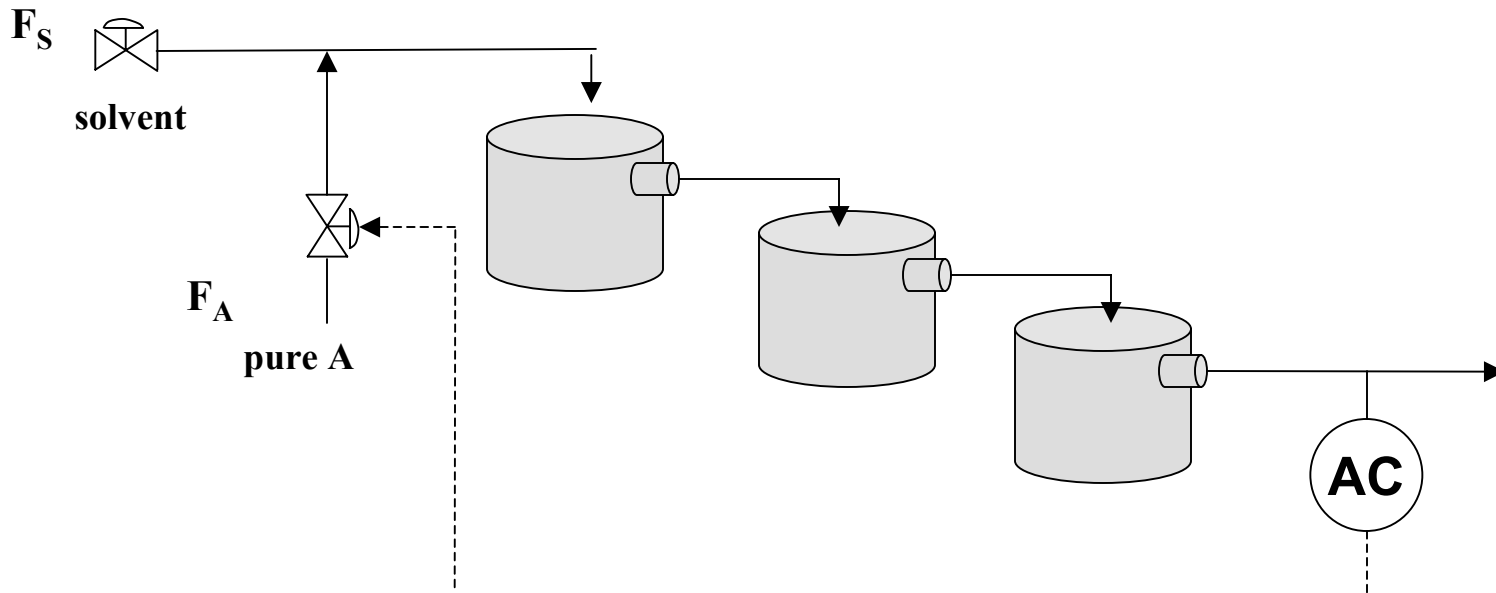
CHAPTER 8: THE PID CONTROLLER

HOW DO WE EVALUATE THE DYNAMIC RESPONSE OF THE CLOSED-LOOP SYSTEM?

- **In a few cases, we can do this analytically
(See Example 8.5)**
- **In most cases, we must solve the equations numerically. At each time step, we integrate**
 - The differential equations for the process**
 - The differential equation for the controller**
 - Any associated algebraic equations**
- **Many numerical methods are available**
- **“S_LOOP” does this from menu-driven input**

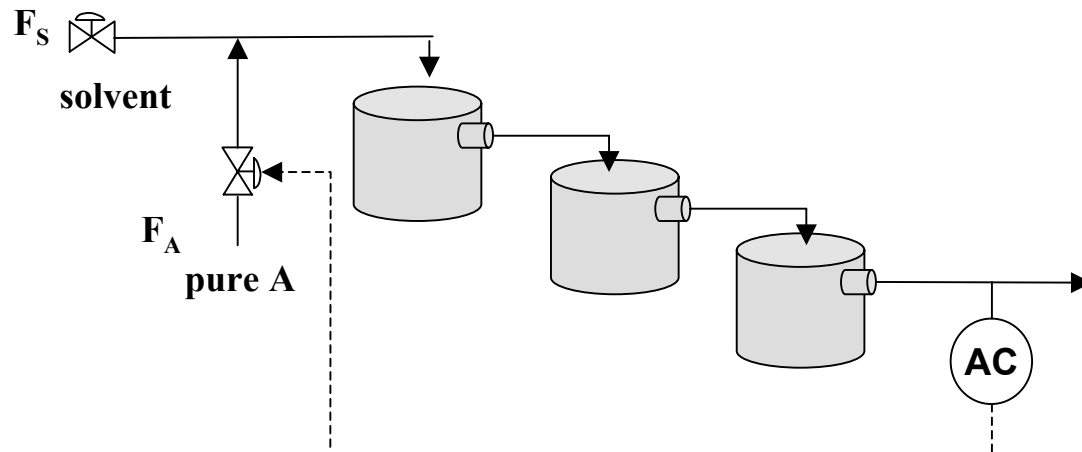
CHAPTER 8: THE PID, WORKSHOP 1

- **Model formulation:** Develop the equations that describe the dynamic behavior of the three-tank mixer and PID controller.
- **Numerical solution:** Develop the equations that are solved at each time step for the simulated control system (process and controller).



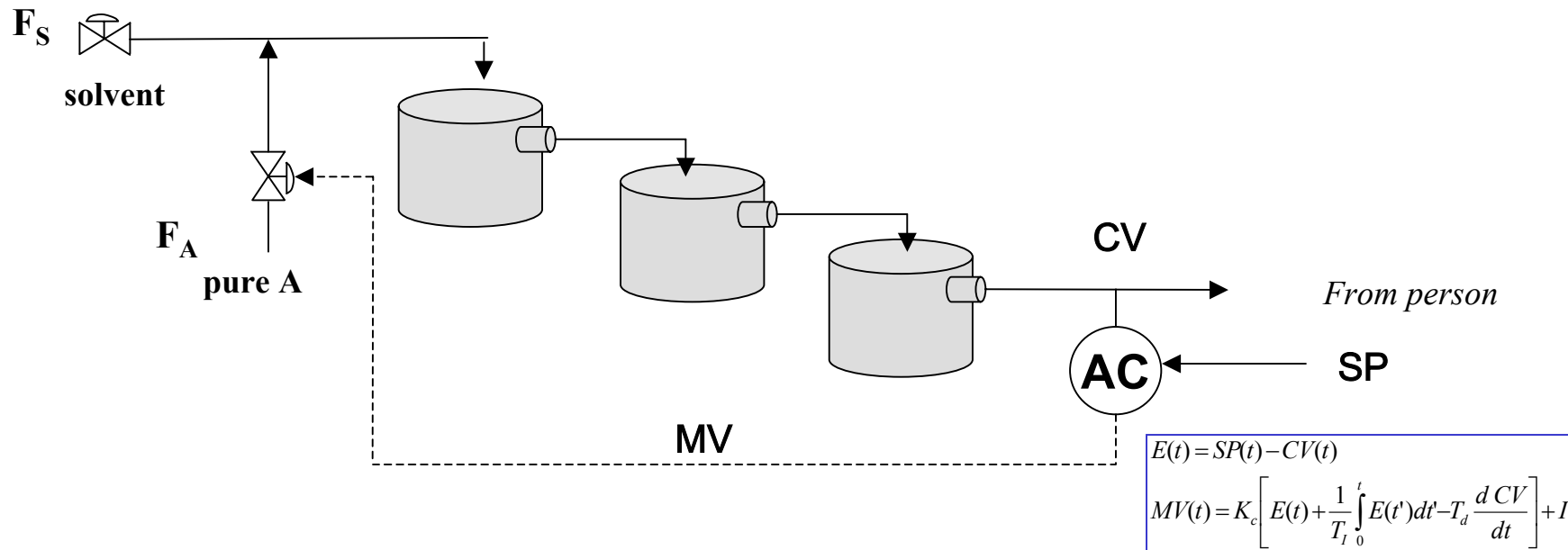
CHAPTER 8: THE PID, WORKSHOP 2

- The PID controller is applied to the three-tank mixer. Prove that the PID controller will provide zero steady-state offset when the set point is changed in a step, ΔSP .
- The three-tank process is stable. If we add a controller, could the closed-loop system become unstable?



CHAPTER 8: THE PID, WORKSHOP 3

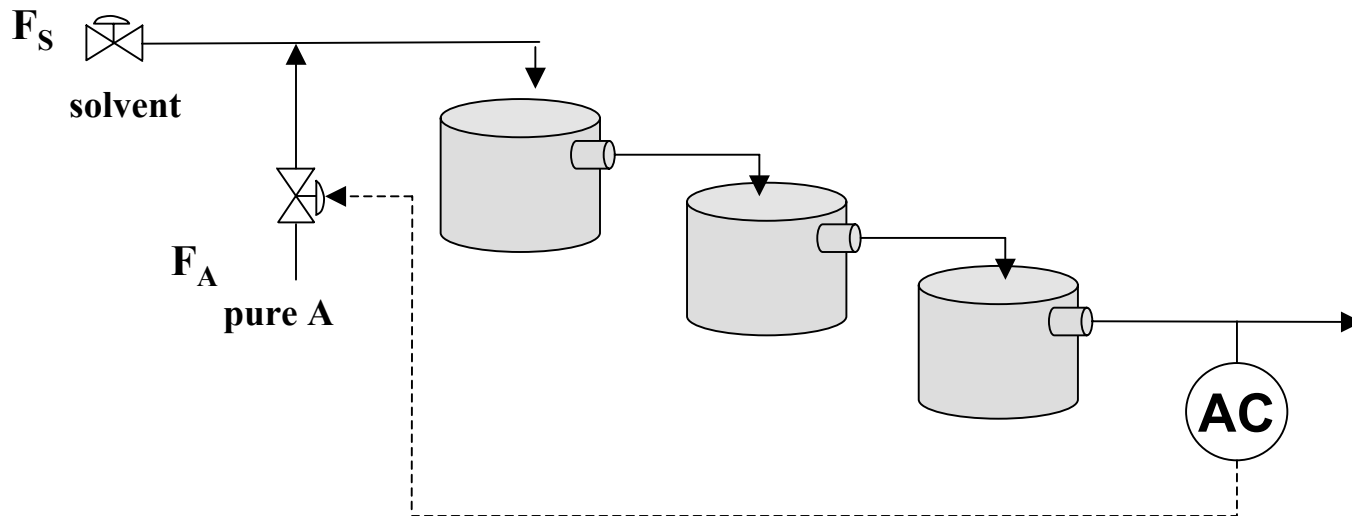
- Determine the engineering units for the controller tuning parameters in the system below.
- Explain how the initialization constant (I) is calculated. This is sometimes called the “bias”.



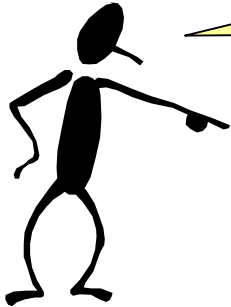
CHAPTER 8: THE PID, WORKSHOP 4

The PID controller must be displayed on a computer console for the plant operator. Design a console display and define values that

- **The operator needs to see to monitor the plant**
- **The operator can change to “run” the plant**
- **The engineer can change**



CHAPTER 8: THE PID CONTROLLER



When I complete this chapter, I want to be able to do the following.

- **Understand the strengths and weaknesses of the three modes of the PID**
- **Determine the model of a feedback system using block diagram algebra**
- **Establish general properties of PID feedback from the closed-loop model**



Lot's of improvement, but we need some more study!

- **Read the textbook**
- **Review the notes, especially learning goals and workshop**
- **Try out the self-study suggestions**
- **Naturally, we'll have an assignment!**

CHAPTER 8: LEARNING RESOURCES

- **SITE PC-EDUCATION WEB**
 - **Instrumentation Notes**
 - **Interactive Learning Module (Chapter 8)**
 - **Tutorials (Chapter 8)**

CHAPTER 8: SUGGESTIONS FOR SELF-STUDY

- 1. In your own words, explain each of the PID modes. Give at least one advantage and disadvantage for each.**
- 2. Repeat the simulations for the three-tank mixer with PID control that are reported in these notes. You may use the MATLAB program “S_LOOP”.**
- 3. Select one of the processes modelled in Chapters 3 or 4. Add a PID controller to the numerical solution of the dynamic response in the MATLAB m-file.**
- 4. Derive the transfer function for the PID controller.**