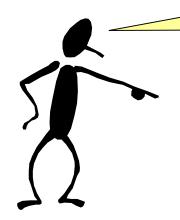


When I complete this chapter, I want to be able to do the following.

- Apply two methods for evaluating control performance: simulation and frequency response
- Apply general guidelines for the effect of
 - feedback dead time
 - disturbance time constant
 - MV variability
 - sensor and final element dynamics

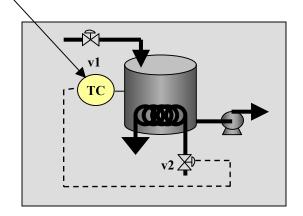


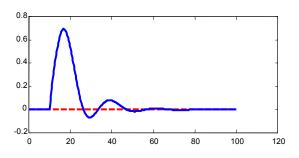
Outline of the lesson.

- Apply dynamic simulation
- Apply frequency response to closedloop performance
- Guidelines for the effects of the process
- Guidelines for the effects of the control system

How do we achieve the performance that we want?

$$MV(t) = K_c \left[E(t) + \frac{1}{T_I} \int_0^t E(t') dt' - T_d \frac{dCV}{dt} \right] + I$$





- Select controlled variable
- Select manipulated variable
- Design process equipment
- Instrumentation
- PID modes and tuning

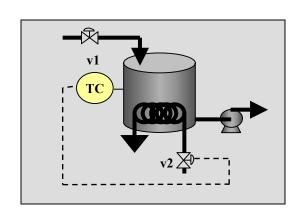


- Is this acceptable?
- Is this the best we can achieve?

Evaluating control performance

- During design, test possible plant changes, and develop principles for guidelines
 - Dynamic simulation
 - Frequency Response
- During plant operation
 - Fine tuning guidelines for set point
 - Complementary guideline for step disturbance
 - Monitor the performance

Dynamic simulation solves the equations describing the process and controller - numerically because of complexity of systems. For example,



Many numerical methods; Euler, Runge-Kutta, and other.



$$V \frac{dC_A}{dt} = F(C_{A0} - C_A) - Vk_0 e^{-E/RT} C_A$$

$$V \rho C_P \frac{dT}{dt} = F \rho C_p (T_0 - T) - (\Delta H_{rxn}) Vk_0 e^{-E/RT} C_A$$

$$-UA(T - (T_{cin} + T_{cout}))$$

$$U \approx h_{in} = aF_c^{0.6} = (v)C_{vmax} \sqrt{\frac{\Delta P}{\rho_c}}$$

$$\tau_{sensor} \frac{dT_m}{dt} = (T_m - T)$$

$$\tau_{valve} \frac{dv}{dt} = (v - MV)$$

$$MV = K_c \left[(T_{SP} - T_m) + \frac{1}{T_I} \int_0^t (T_{SP} - T_m) dt' \right]$$

Dynamic simulation is general and powerful.

Detail for controller and sensors, e.g., valve ___ saturation and sensor non-linearity

All process variables can be predicted, including those not measured

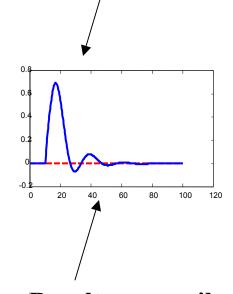
Process
disturbances
can be
essentially
any function,

• step

• sine

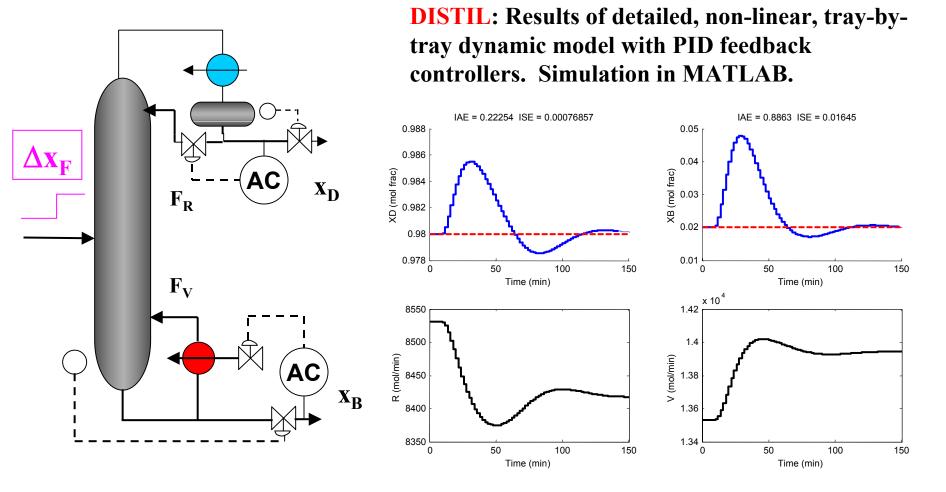
• ~~~//

Process models can be linearized or detailed non-linear



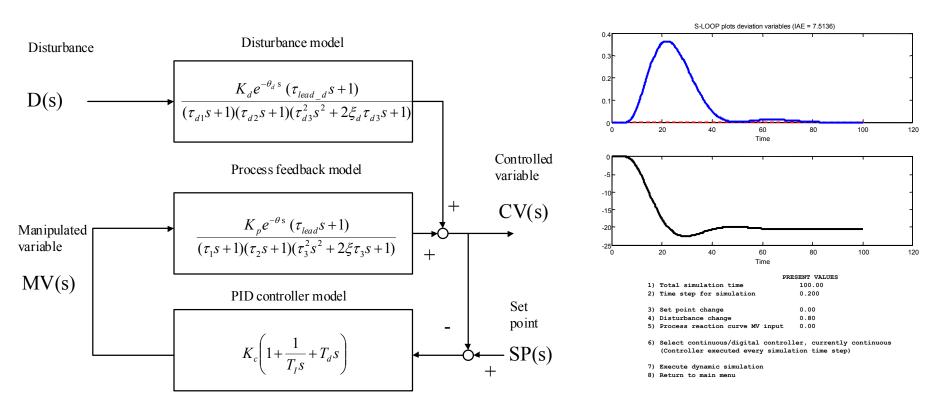
Results are easily interpreted, entire transient available

Dynamic simulation is general and powerful.



Dynamic simulation is general and powerful.

Simulation of single-loop linear systems is easily achieved using the **S_LOOP** program in MATLAB. Cases are possible for systems with and without control for step inputs



Frequency Response: determines the response of systems variables to a sine input.

Why do we study frequency response?

- Professors want to ruin the semester for students
- Perfect sine disturbances occur frequently in plants
- We want another case for dynamic simulation
- We use sine to characterize time-varying inputs, especially disturbances
- We can learn useful generalizations about control performance

Are you sure of this answer?

Response: determines the response of systems to a sine input.

10!

ves!

Yes!

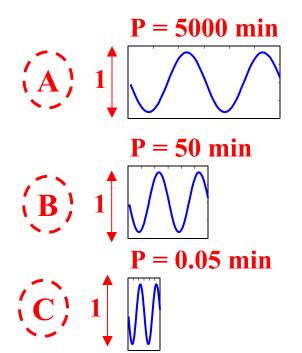
Why do we study frequency response?



- Professors want to ruin the semester for students 🔨
- Perfect sine disturbances occur frequently in plants
- We want another case for dynamic simulation
- We use sine to characterize time-varying inputs, especially disturbances
- We can learn useful generalizations about control performance

Frequency Response : Sine in \Rightarrow sine out without control

Three cases with amplitude 1 K and different T_{in} sine periods, P.

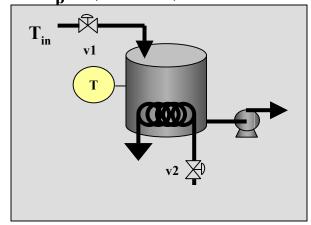


Process dynamics for disturbance T_{in} to T

$$K_d = 1.5; \theta = 0; \tau = 5$$

Process dynamics for MV v₂ to T

$$K_{n}=1; \theta = 5; \tau = 5 \text{ min}$$



For each case, what is the output amplitude?

Let's do a thought experiment, without calculating!



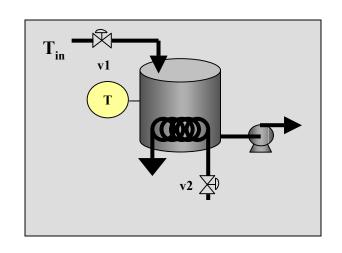
Frequency Response : Sine in \Rightarrow sine out without control

Process dynamics for disturbance T_{in} to T

$$K_d = 1.5; \theta = 0; \tau = 5 \text{ min}$$

Process dynamics for MV v₂ to T

$$K_p = 1$$
; $\theta = 5$ min; $\tau = 5$ min

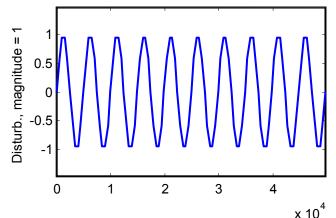


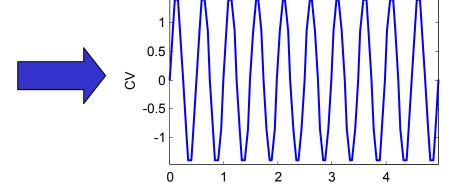
x 10⁴



P = 5000 min

FREQUENCY =0.0012629 rad/time & AMP RATIO =1.4678





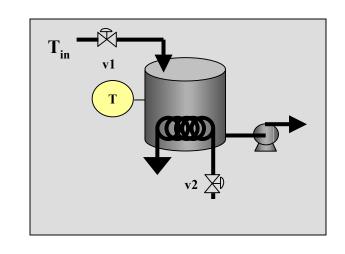
Frequency Response : Sine in \Rightarrow sine out without control

Process dynamics for disturbance T_{in} to T

$$K_d = 1.5; \theta = 0; \tau = 5 \text{ min}$$

Process dynamics for MV v_2 to T

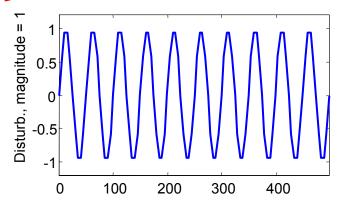
$$K_p=1$$
; $\theta = 5$ min; $\tau = 5$ min

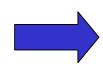


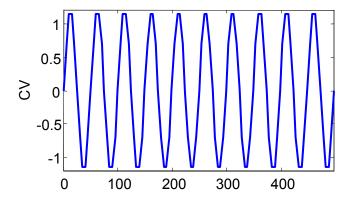


P = 50 min

FREQUENCY =0.12629 rad/time & AMP RATIO =1.2115







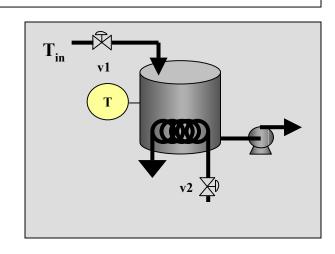
Frequency Response : Sine in \Rightarrow sine out without control

Process dynamics for disturbance T_{in} to T

$$K_d = 1.5; \theta = 0; \tau = 5 \text{ min}$$

Process dynamics for MV v₂ to T

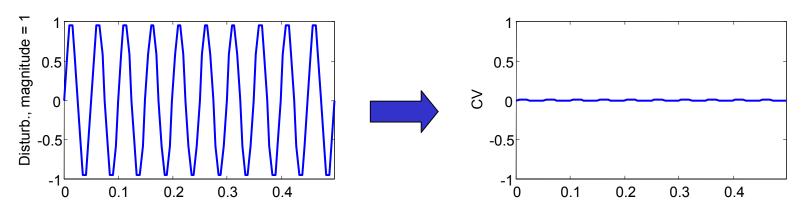
$$K_p = 1$$
; $\theta = 5$ min; $\tau = 5$ min





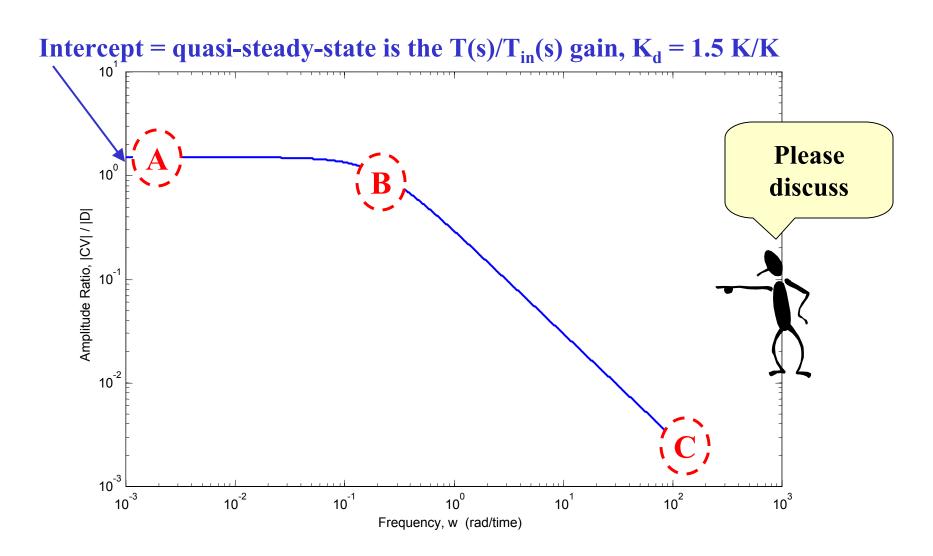
P = .05 min

FREQUENCY =126.2939 rad/time & AMP RATIO =0.0021544



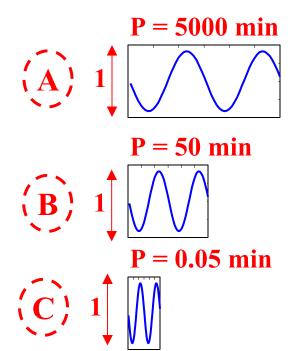
Frequency Response : Sine in \Rightarrow sine out without control

Summarize the results for many frequencies in a Bode Plot



Frequency Response : Sine in \Rightarrow sine out with control

Three cases with amplitude 1 K and different T_{in} sine periods, P.

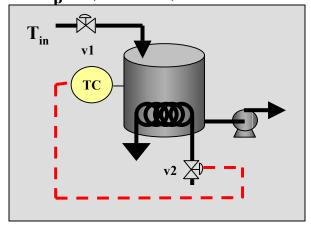


Process dynamics for disturbance T_{in} to T

$$K_d = 1.5; \theta = 0 \text{ min } ; \tau = 5 \text{ min}$$

Process dynamics for MV v₂ to T

$$K_{n}=1; \theta = 5; \tau = 5 \text{ min}$$



For each case, what is the output amplitude?

Let's do a thought experiment, without calculating!



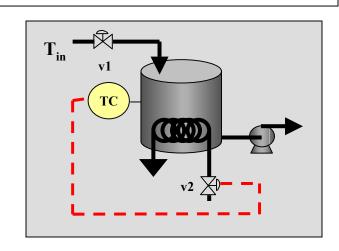
Frequency Response : Sine in \Rightarrow sine out with control

Process dynamics for disturbance T_{in} to T

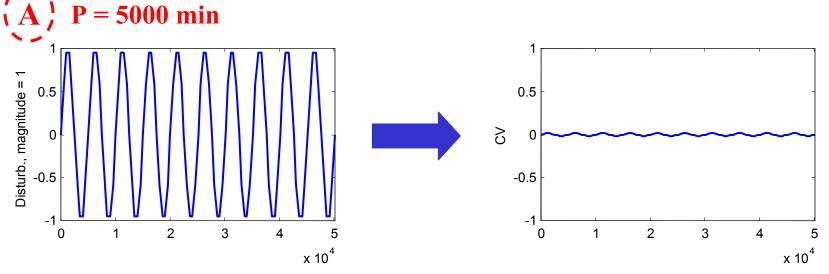
$$K_d = 1.5; \theta = 0 \text{ min } ; \tau = 5 \text{ min}$$

Process dynamics for MV v₂ to T

$$K_p = 1; \theta = 5; \tau = 5 \text{ min}$$



FREQUENCY =0.0012496 rad/time & AMP RATIO =0.016156



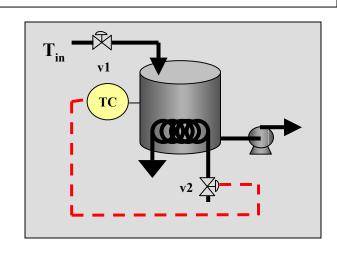
Frequency Response : Sine in \Rightarrow sine out with control

Process dynamics for disturbance T_{in} to T

$$K_d = 1.5; \theta = 0 \text{ min } ; \tau = 5 \text{ min}$$

Process dynamics for MV v₂ to T

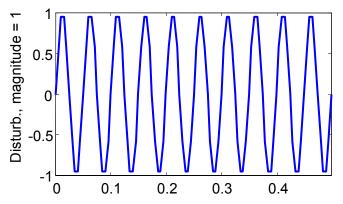
$$K_p = 1; \theta = 5; \tau = 5 \text{ min}$$



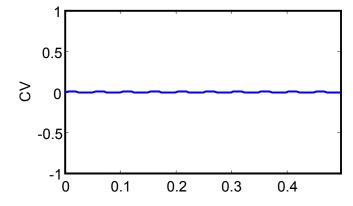


P = 0.050 min

FREQUENCY =126.2939 rad/time & AMP RATIO =0.0021544







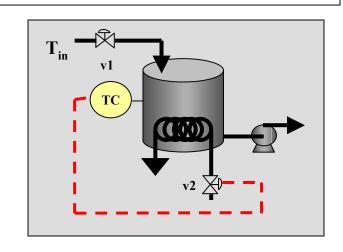
Frequency Response : Sine in \Rightarrow sine out with control

Process dynamics for disturbance T_{in} to T

$$K_d = 1.5; \theta = 0 \text{ min } ; \tau = 5 \text{ min}$$

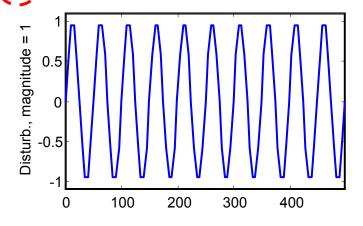
Process dynamics for MV v₂ to T

$$K_p = 1; \theta = 5; \tau = 5 \text{ min}$$

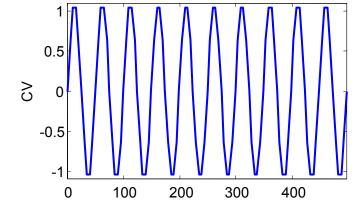




FREQUENCY =0.12629 rad/time & AMP RATIO =1.1007

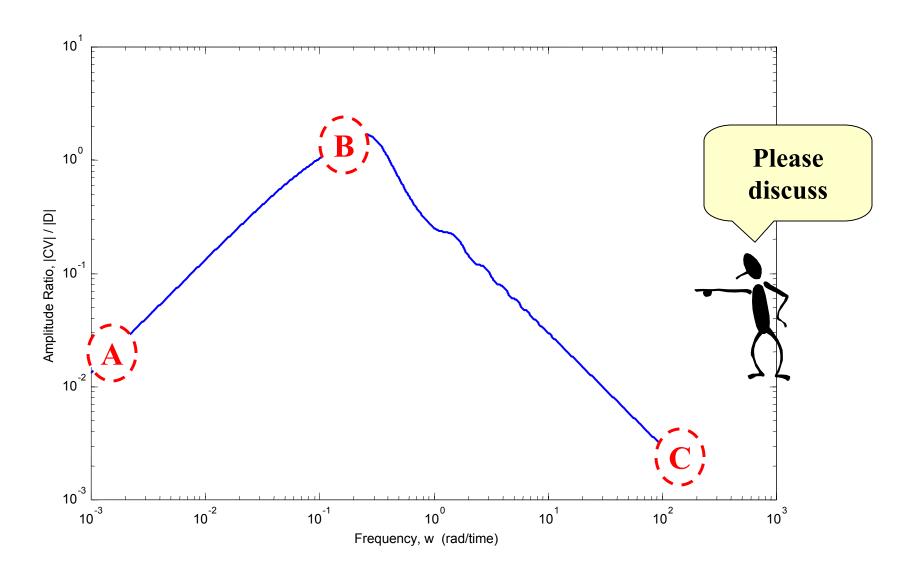






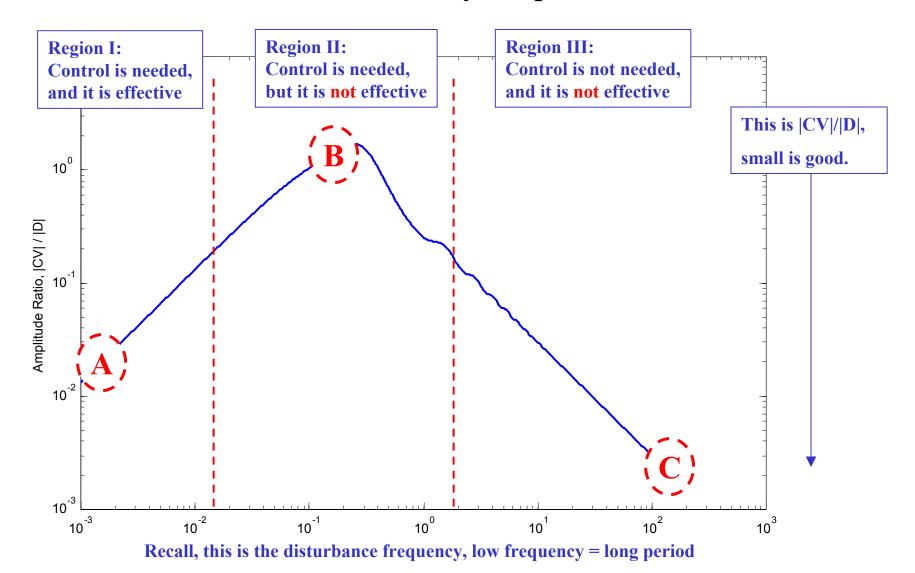
Frequency Response : Sine in \Rightarrow sine out with control

Summarize the results for many frequencies in a Bode Plot

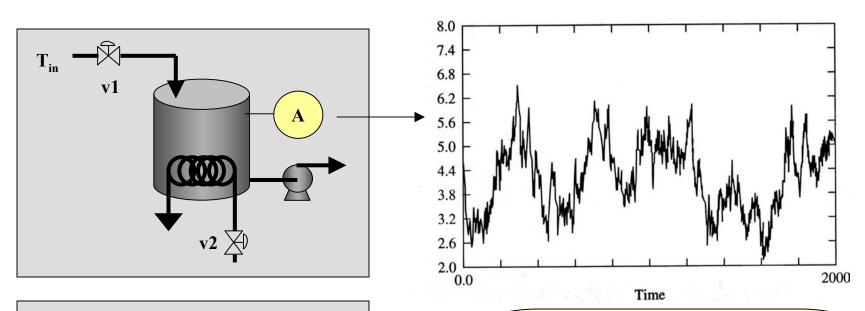


Frequency Response : Sine in \Rightarrow sine out with control

Summarize the results for many frequencies in a Bode Plot



Let's apply frequency response concepts to a practical example. Can we reduce this open-loop variation?



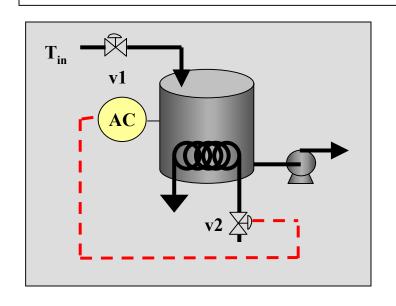
Feedback dynamics are:

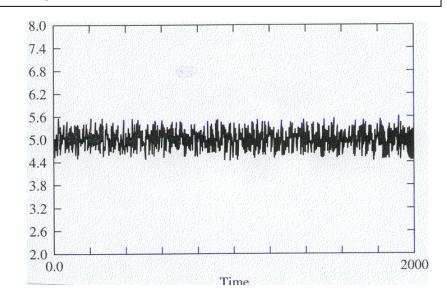
$$\frac{\mathbf{A(s)}}{\mathbf{v(s)}} = \frac{1.0\mathrm{e}^{-2\mathrm{s}}}{2\mathrm{s} + 1}$$



We note that the variation has many frequencies, some much slower than the feedback dynamics.

Yes, we can we reduce the variation substantially because of the dominant low frequency of the disturbance effects.





Feedback dynamics are:

$$\frac{\mathbf{A(s)}}{\mathbf{v(s)}} = \frac{1.0\mathrm{e}^{-2\mathrm{s}}}{2\mathrm{s} + 1}$$



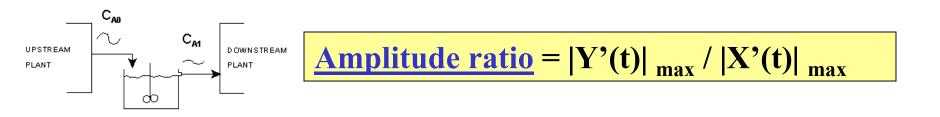
Low frequencies reduced <u>a lot</u>. Higher frequencies remain!

Frequency Response : Sine in \Rightarrow sine out

How do we calculate the frequency response?

- We could use dynamic simulation
 - Lots of cases at every frequency
 - Can be done for non-linear systems
- For linear models, we can use the transfer function
 - Remember that the frequency response can be calculated by setting $s = j \omega$

Frequency Response : Sine in \Rightarrow sine out

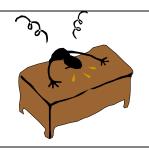


For linear systems, we can evaluate directly using transfer function! Set $s = j\omega$, with $\omega =$ frequency and j = complex variable.

Amp. Ratio =
$$AR = |G(j\omega)| = \sqrt{\text{Re}(G(j\omega))^2 + \text{Im}(G(j\omega))^2}$$

In most programming languages, the absolute value gives the magnitude of a complex number

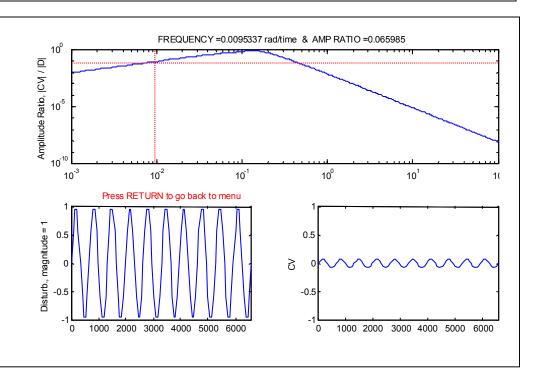
Frequency Response : Sine in \Rightarrow sine out



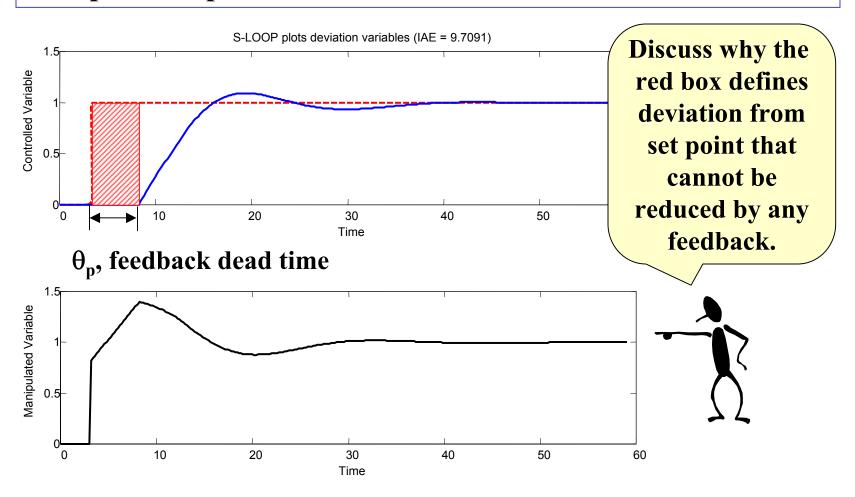
Caution: Do not perform these calculations by hand - too complex!

S_LOOP

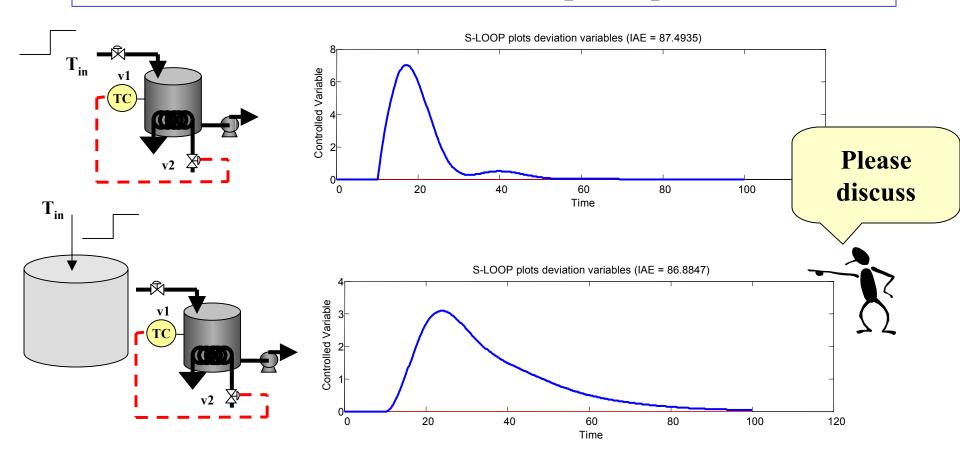
For linear systems, sub-menu 7 gives
Bode plot and sines at user-selected frequency



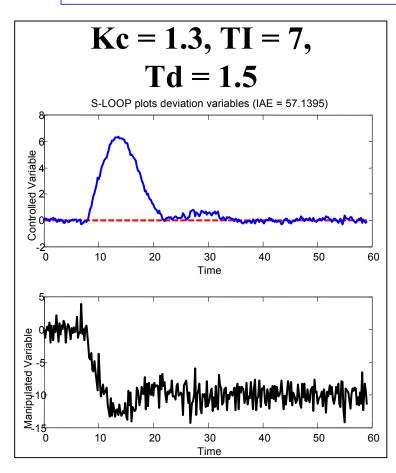
Performance Observation #1. Feedback dead time limits best possible performance

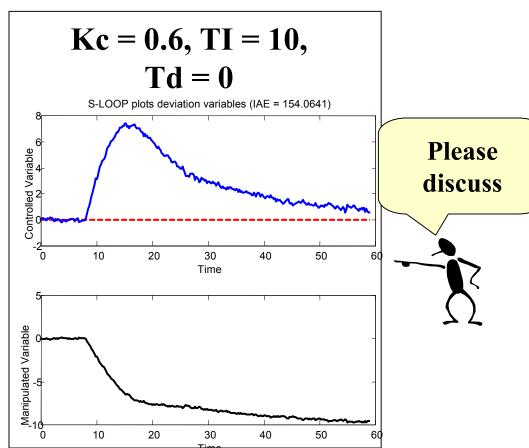


Performance Observation #2. Large disturbance time constants slow disturbances and improve performance.

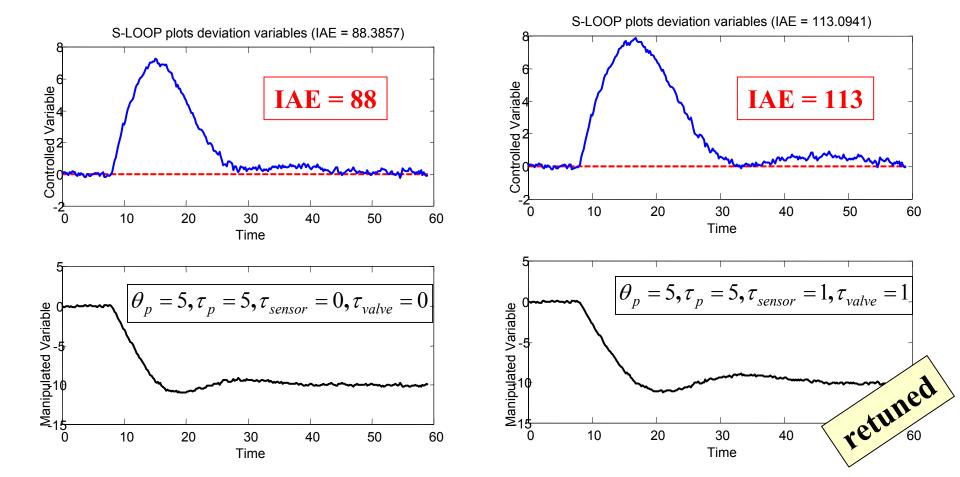


Performance Observation #3. Feedback must change the MV aggressively to improve performance.





Performance Observation #4. Sensor and final element dynamics also degrade performance.



QUICK SUMMARY OF KEY POINTS

Important general insights!!

Class exercise:

The importance of disturbance dynamics

The importance of feedback dynamics

Please complete & discuss



The importance of the disturbance frequency

QUICK SUMMARY OF KEY POINTS

Important general insights!!

- The importance of disturbance dynamics
 - Large time constants decrease the effect of the disturbance on the controller variable
 - Dead time has no effect
- The importance of feedback dynamics
 - Large dead times and time constants are bad!!
- The importance of the disturbance frequency
 - Low frequencies are easy to control. Critical frequency cannot be controlled.

Please discuss



KEY CONCLUSION ABOUT FEEDBACK CONTROL!!

Class exercise: We can achieve the desired control performance by a judicious selection of controller algorithms and tuning.

True

False

Please answer and explain your response



KEY CONCLUSION ABOUT FEEDBACK CONTROL!!

FALSE!

FEEDBACK CONTROL PERFORMANCE IS LIMITED

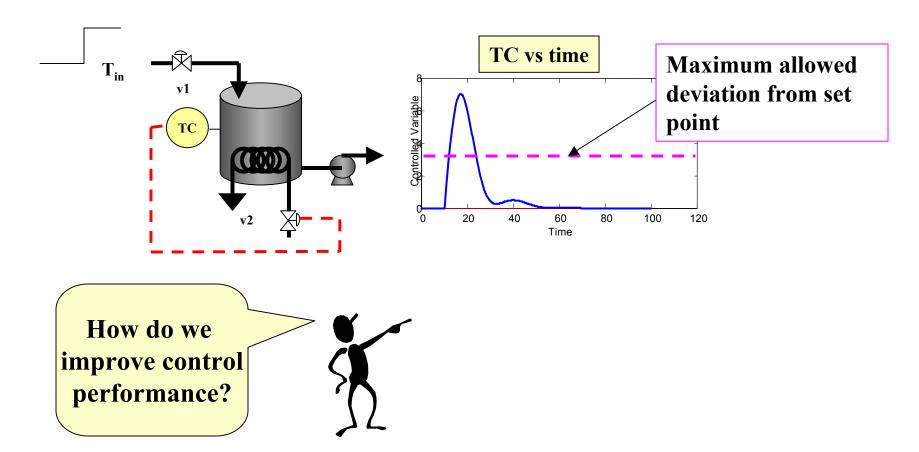
• The <u>process dynamics</u> introduce limits on the best achievable feedback performance

Please discuss

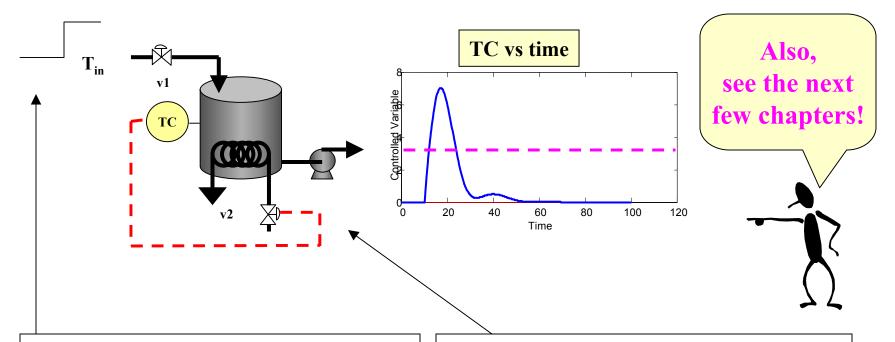
- No controller algorithm can do better (same CV-MV)
- Controller tuning cannot overcome this limitation
- The PID often performs well for single-loop systems
- If we need better performance, we must change the process or the control structure (See upcoming chapters)

STEPS TO IMPROVE FEEDBACK PERFORMANCE!!

Class exercise:



STEPS TO IMPROVE FEEDBACK PERFORMANCE!!



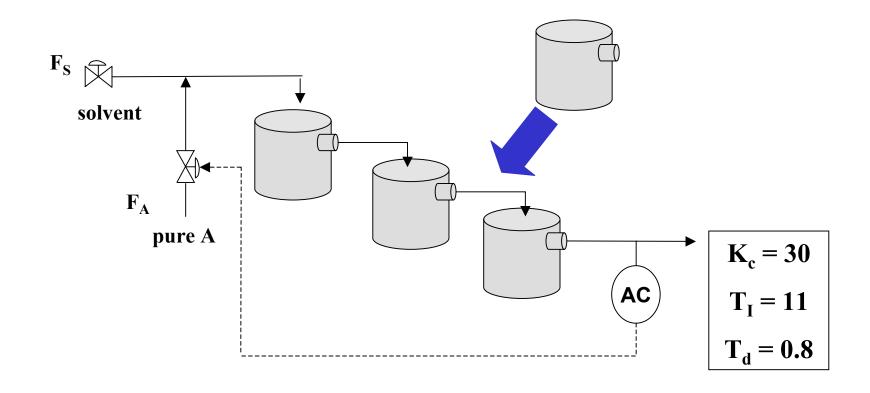
Reduce disturbance effect by looking "upstream", if possible

- Reduce the magnitude
- Increase time constant (tank)

Improve feedback dynamics, if possible

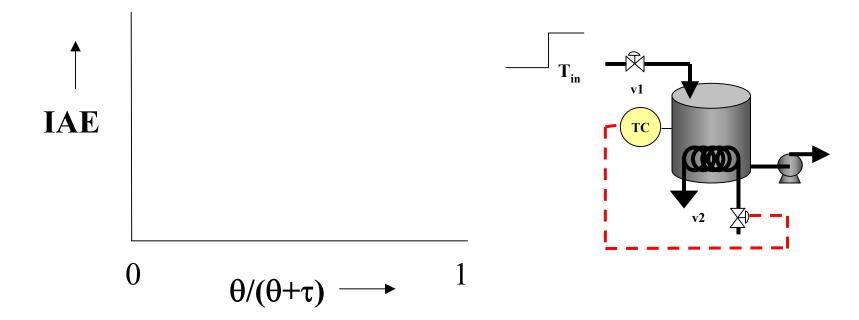
Reduce dead time & time constants

The PID controller has been applied to a three-tank mixer. We have decided to include another mixing tank in the process. How will the performance be changed?



Sketch the shape of feedback control performance vs. the feedback fraction dead time, $\theta/(\theta+\tau)$. Assume disturbance time constant is the same as the feedback time constant.

- 1. The performance with the best PID tuning
- 2. The best possible feedback



The transfer function below gives the behavior of the controlled variables, CV, in response to a disturbance. As we increase the controller gain to a large number, the controlled variable deviation can be made as small as desired in the frequency response calculation.

Is this result reasonable? Why?

Disturbance Response

$$\frac{CV(s)}{D(s)} = \frac{G_d(s)}{1 + K_c G_p(s) G_v(s) G_S(s)}$$

Determine a rough estimate of the dynamics for the following control-loop elements.

- Thermocouple in a steel thermowell
- Globe valve with pneumatic actuator
- Pressure sensor
- Gas chromatograph on a sample from a gas stream
- Signal transmission for 400 m
- Typical commercial digital controller execution period

CHAPTER 13: PERFORMANCE



When I complete this chapter, I want to be able to do the following.

- Apply two methods for evaluating control performance: simulation and frequency response
- Apply general guidelines for the effect of
 - feedback dead time
 - disturbance time constant
 - MV variability
 - sensor and final element dynamics



Lot's of improvement, but we need some more study!

- Read the textbook
- Review the notes, especially learning goals and workshop
- Try out the self-study suggestions
- Naturally, we'll have an assignment!

CHAPTER 13: LEARNING RESOURCES

SITE PC-EDUCATION WEB

- Instrumentation Notes
- Interactive Learning Module (Chapter 13, not yet available)
- Tutorials (Chapter 13)

S_LOOP

- Dynamic simulation of linear system
- Easy evaluation of frequency response for open and closed-loop systems. Compare Bode plot with sine plots!

CHAPTER 13: SUGGESTIONS FOR SELF-STUDY

- 1. Carefully review the summary in textbook Table 13.3. Do not memorize, but understand!
- 2. Use **S_LOOP** to simulate the system in Workshop Question #1.
- 3. Derive a mathematical expression for the minimum IAE for a feedback loop responding to a single step set point change. Hint: See textbook equation (13.8) and associated discussion.
- 4. Discuss the information that you need to know to be able to predict the performance, i.e., the behavior of the CV and MV.

CHAPTER 13: SUGGESTIONS FOR SELF-STUDY

- 5. S_LOOP: Consider the system used in Performance Observation #1 ($K_p = 1$, $\theta_p = 5$, $\tau_p = 5$; $K_d = 1.5$ $\tau_d = 5$). Simulate the closed-loop dynamic response for a <u>step</u> disturbance of magnitude 1.
 - How did you tune the PID controller?
 - Sketch the best possible CV control performance on the plot of the transient response.
 - What steps are required to improve the CV performance?
- 6. Develop two more Performance Observations and prepare one visual aids (slide) per observation to explain them to your class.