Problem 5 Frames

Question Requirements:

Rewrite (5.2) in a frame that rotates relative to the Earth frame, the body frame.

Estimate its moment of inertia matrix and state the assumptions used in the calculations.

Equation used for inertia:

This equation is used to calculate the moment of inertia of some 3D rectangular box with similar dimensions as the drone (equations are in matrix form). Source, Google.

Where the moment of inertia for this object, I, is

I = [I_x, 0, 0; 0, I_y , 0;

0, 0, 1 z;

General Outline for Solution:

- 1. Calculate the moment in the body frame.
- 2. calculate the angular momentum in the body frame using moment of inertia.
- 3. calculate the angular acceleration in the body frame.

Code Solution for Prolem 1:

```
disp('______')

### Implementing this into our problem:

#### Define symbolic variables

### syms p q r real ### Angular velocities in body frame
```

Moment in Body Frame, M_body:

```
disp(M_body);
```

 $\begin{pmatrix} L \\ M \\ N \end{pmatrix}$

```
% Define the mass of the UAV
m = 0.042; % kg // First TIme mass is defined
% Define the dimensions of the UAV (3D square box) using temporary
% variables 'a', 'b', 'c'.
a = 0.11; % m
b = 0.11; \% m
c = 0.029; % m
% Calculate the moment of inertia matrix I
Ixx = (1/12) * m * (b^2 + c^2);
Iyy = (1/12) * m * (a^2 + c^2);
Izz = (1/12) * m * (a^2 + b^2);
% Construct the moment of inertia matrix I
I = [Ixx, 0, 0]
     0, Iyy, 0;
     0, 0, Izz];
% Define the angular momentum of UAV, H:
H = I * w_b_e;
```

```
% Calculate the cross product of omega_b/e and I * omega_b/e
cross_product_term = cross(w_b_e, I * w_b_e);
% Solve for dot_omega_b/e
dot_omega_b_e = I \ (M_body - cross_product_term); % \ is used for matrix division
which is equivalent to multiplying by the inverse
% Define the number of decimal places you want to round to
decimal places = 4;
% Convert to numeric and round off, easier to read format
dot_omega_b_e_numeric = vpa(dot_omega_b_e, decimal_places);
% Convert Angular Momentum H to numeric and round off, easier to read
% format.
H_numeric = vpa(H, decimal_places);
% Display the result
disp('Angular Acceleration in Body Frame, dot_omega_b/e:');
Angular Acceleration in Body Frame, dot_omega_b/e:
disp(dot_omega_b_e_numeric);
 22080.0 L - 0.87 q r
 22080.0 M + 0.87 pr
     11810.0 N
disp('Angular Momentum of UAV, H:');
Angular Momentum of UAV, H:
disp(H_numeric);
(4.529e-5 p)
 4.529e-5 q
 8.47e-5 r
                                                    %
```

Problem 6 Rotational Kinematics

Question Requirements:

Find the Singularities in this equation.

First Implementation:

- 1. Construct Matrix H(Capital Theta), the transformation matrix.
- 2. Determine the determinant of H(Capital Theta).
- 3. Solve the equation where the determinant of H(Capital_Theta) equals zero to find singularities.
- 4. Evaluate and Display Singular Matrices

Code for First Implementation:

```
disp('____')
```

Singularities of Theta are at:

```
disp(singularities_theta);

% Evaluate and Display H(Theta) at the found singularities
for i = 1:length(singularities_theta)
    singular_matrix_postitive = subs(H_theta, theta, singularities_theta(i));
    singular_matrix_negative = subs(H_theta, theta, -singularities_theta(i));
    disp(['H(Theta) is singular at theta = ', char(singularities_theta(i)), ':']);
    disp(singular_matrix_positive);
    disp(singular_matrix_negative);
end
```

Explanation:

There is an absence of explicit solutions from the symbolic solver code above. This is consitent with the known fact that the singularities occur at theta equal to plus or minus pi over two. At these points, the tangent function in the determinant becomes underfines, or in other words, goes to infinity. This makes the matrix H(theta)

non-invertable, or singular. This is further demonstrated with the code below, where the singularity points are explicitly substituted into the calculation. This code is the second implementation of demonstrating the solution to this problem.

Second Implementation:

- 1. Construct Matrix H(Capital Theta), the transformation matrix.
- 2. Define Singular points explicitly of where the determinant is zero.
- 3. Compute the determinant of teh transformation matrix at the identified points.
- 4. Interpret results.

Code for Second Implementation:

```
% Define symbolic variables for roll, pitch, and yaw angles
syms phi theta psi real
% Define the matrix H(Theta) as given in the problem
H_theta = [1, sin(phi)*tan(theta), cos(phi)*tan(theta);
          0, cos(phi), -sin(phi);
          0, sin(phi)/cos(theta), cos(phi)/cos(theta)];
% Check the determinant of H(Theta) at theta = pi/2 and theta = -pi/2
%{
det_pos = det(subs(H_theta, theta, pi/2));
det_neg = det(subs(H_theta, theta, -pi/2));
% Display the determinants at the singular points
disp('Determinant of H(Theta) at theta = pi/2:');
disp(det_pos);
disp('Determinant of H(Theta) at theta = -pi/2:');
disp(det_neg);
% If determinant is zero, then display the singular matrices
if det_pos == 0
    disp('H(Theta) is singular at theta = pi/2:');
    disp(subs(H theta, theta, pi/2));
end
if det neg == 0
    disp('H(Theta) is singular at theta = -pi/2:');
    disp(subs(H_theta, theta, -pi/2));
end
%}
```

Further Explanation:

This code will not run because line 'det_pos = det(subs(H_theta, theta, pi/2));' implementation tries to divide by zero. Meaning that when the singularity points are substituted in, the function 'blows up.' Making it non-invertable, demonstrating that these are the correct singularity points.

Problem 7 Model Gravity

Question Requirements:

Transform the gravity vector from the earth frame to the body frame.

write out the gravity vector in body coordinates as a funciton of psi (ϕ) and theta (θ) .

Explain why the gravity vector resolved in body coordinates does not depend on the yaw angle.

General Outline for Solution:

- 1. Define the Grvaity vector in the Earth Frame.
- 2. Define rotational matrix from earth grame to body frame using psi and theta.
- 3. Transform the gravity vector to the body frame

Code Solution for Prolem 7:

```
disp('____')
```

```
% Rotation matrix about z-axis (yaw)
%{
Wrong Implementation
R_z = [\cos(psi), -\sin(psi), 0]
       sin(psi), cos(psi), 0;
       0, 0, 1];
%}
% Rotation matrix about z-axis (yaw)
% Correct Implementation
R_z = [1, 0, 0; ...
       0, 1, 0; ...
       0, 0, 1];
% Construct the total rotation matrix from Earth frame to Body frame
R_E_B = R_z * R_y * R_x;
% Transform the gravity vector from Earth frame to Body frame
F_gB = R_EB * F_gE;
% Display the gravity vector in the Body frame
disp('Gravity Vector in Body Frame, F_g_B:');
```

Gravity Vector in Body Frame, F_g_B:

```
disp(F_g_B);
```

```
\begin{pmatrix} -\frac{20601\cos(\phi)\sin(\theta)}{50000} \\ \frac{20601\sin(\phi)}{50000} \\ \frac{20601\cos(\phi)\cos(\theta)}{50000} \end{pmatrix}
```

Explanation:

The yaw angle represents a rotation about the z-axis. This is aligned with the direction of gravity, as depicted in the code based on the information given in the assignment. Gavity in this case acts in the vectical direction and the yaw rotation is a rotation in the horizontal plane around the vertical axis. This means that the yaw rotation does not influence the representation of the gravity vector in the body frame because the gravity is acting along the same axis of the yaw rotation. In the code, the yaw component of the rotation matrix represented by R_z does not affect the z-component of the gravity vector. In other words, when you multiply the rotation matrix R_E_B with F_g_E, it leaves the z-component unchanged. Further emphasizing that the yaw angle does not influence the z-component of the gravity vector in the body frame.

Problem 8 Propulsive Motor Force and Moments

Problem Requirements:

Estimate the propeler's thrust coefficient. Assume sea level air density.

General Outline For Solution:

- 1. Create a data set based on values given on the problem pdf.
- 2. Then converted each data value to appropriate unit.
- 3. Defined a matrix variable. First column the set of thurst values. Second column is Capital Phi(n) calculated values usign given equaiton.
- 4. Create a data set of y (Thrust) predictions using the calculated Capital Phi as a funciton of n.
- 5. Ploted both data sets to verify answer.

```
disp('_____')
```

```
% 8(1)
% Define the variable data set initial values to store the initial values from the
data table
% Each row corresponds to a data point, where:
% - The first column is the value of thrust (in grams)
% - The second column is the value of RPM (not converted)
data_set_initial_values = [0.0, 0;
                                      % Row 1: Thrust = 0.0g, RPM = 0.
                           1.6, 4485; % Row 2: Thrust = 1.6g, RPM = 4485.
                           4.8, 7570; % Row 3: Thrust = 4.8g, RPM = 7570.
                           7.9, 9374; % Row 4: Thrust = 7.9g, RPM = 9374.
                           10.9, 10885; % Row 5: Thrust = 10.9g, RPM = 10885.
                           13.9, 12277; % Row 6: Thrust = 13.9g, RPM = 12277.
                           17.3, 13522; % Row 7: Thrust = 17.3g, RPM = 13522.
                           21.0, 14681; % Row 8: Thrust = 21.0g, RPM = 24691.
                           24.4, 15924; % Row 9: Thrust = 24.4g, RPM = 15924.
                           28.6, 17174; % Row 10: Thrust = 28.6g, RPM = 17174.
                           32.8, 18179; % Row 11: Thrust = 32.8g, RPM = 18179.
                           37.3, 19397; % Row 12: Thrust = 37.3g, RPM = 19397.
                           41.7, 20539; % Row 13: Thrust = 41.7g, RPM = 20539.
                           46.0, 21692; % Row 14: Thrust = 46.0g, RPM = 21692.
                           51.9, 22598;]; % Row 15: Thrust = 51.9g, RPM = 22598.
% Display the intial values data set from the provided data table
disp('Initial Data Set before conversion:');
```

Initial Data Set before conversion:

```
disp(data_set_initial_values);
```

```
1.0e+04 *

0 0
0.0002 0.4485
0.0005 0.7570
```

```
0.0014
            1.2277
   0.0017
            1.3522
   0.0021
            1.4681
   0.0024
            1.5924
   0.0029
            1.7174
   0.0033
            1.8179
   0.0037
            1.9397
          2.0539
   0.0042
   0.0046
            2.1692
   0.0052
            2.2598
% Extract the first column (Thrust in g) and convert to kg
Thrust_newtons = ( data_set_initial_values(:, 1) / 1000 ) * 9.8; % 1 g = 0.001 kg,
converting to a force by * by 9.8
% Extract the second column (Speed in RPM) and convert to Hz
Speed_hz = data_set_initial_values(:, 2) / 60; % 1 RPM = 1/60 Hz
% Display the converted data set
disp('Converted Data Set:');
Converted Data Set:
disp('Thurst (N): ');
Thurst (N):
disp([Thrust_newtons]);
   0.0157
   0.0470
   0.0774
   0.1068
   0.1362
   0.1695
   0.2058
   0.2391
   0.2803
   0.3214
   0.3655
   0.4087
   0.4508
   0.5086
disp('Speed (Hz): ');
Speed (Hz):
disp([Speed_hz]);
  74.7500
 126.1667
 156.2333
```

0.0008

0.0011

0.9374

1.0885

```
181.4167
204.6167
225.3667
244.6833
265.4000
286.2333
302.9833
323.2833
342.3167
361.5333
376.6333
```

```
% Calculating the data set for thrust and capital_phi to plot
% Equation used: T = p_row * 4 * D^5 * n^2 * C_t

% Define constants
p_row = 1.225; % Density of air in kg/m^3
D = 0.045; % Prop diameter in m, converted from 45 mm

% Calculate Capital_phi for each data point
Capital_phi = 4 * p_row * D^4 * (Speed_hz.^2);

% Display the data points
disp('Data Points with their corresponding values:');
```

Data Points with their corresponding values:

```
disp('Trhust (N), Capital Phi.')
```

Trhust (N), Capital Phi.

disp([Thrust_newtons, Capital_phi]); % this matrix will be used for least squares.

```
0.0157
         0.1123
0.0470
         0.3198
         0.4904
0.0774
         0.6613
0.1068
         0.8413
0.1362
0.1695
         1.0205
0.2058
         1.2030
0.2391
          1.4153
0.2803
          1.6462
0.3214
         1.8445
0.3655
         2.1000
0.4087
         2.3545
0.4508
         2.6263
0.5086
         2.8503
```

```
% Using least squares method to calculate C_t
% least_squares = (phi' * phi) \ phi' * y; % Where phi is the regressor and y is
the output
```

```
% For data_points dataset
% Extracting the regressor (Capital_phi) and output (Thrust) from data_points
phi = Capital_phi; % Regressor
y = Thrust_newtons; % Output

% Calculating the least squares solution for Ct (Coefficient of Thrust)
Ct_least_squares = (phi' * phi) \ phi' * y; % This will give the least squares
solution for Ct

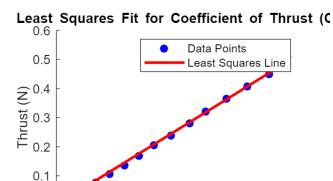
% Display the result
disp('Coefficient of Thrust, Ct (Least Squares):');
```

Coefficient of Thrust, Ct (Least Squares):

```
disp(Ct_least_squares);
```

0.1731

```
% Calculating the predicted y values using the least squares solution
y_pred = phi * Ct_least_squares; % Prediction for Thrust to verify C_t coefficient
% Plotting the original data points
figure;
scatter(phi, y, 'b', 'filled');
hold on;
% Plotting the least squares line
plot(phi, y_pred, 'r', 'LineWidth', 2);
% Adding title and labels to the plot
title('Least Squares Fit for Coefficient of Thrust (C_t)');
xlabel('Regressor (\phi)'); % Capital_phi
ylabel('Thrust (N)');
% Adding a legend to differentiate between the data points and the least squares
line
legend('Data Points', 'Least Squares Line');
% Displaying the plot
hold off;
```



Regressor (ϕ)

Problem Requirements:

0

Estimate the propeller's power coefficient. Assume sea level air density.

3

General Outline For Solution:

- 1. Create a data set based on values given on the problem pdf.
- 2. Then converted each data value to appropriate unit.
- 3. Calculate the Capital phi values using the given equation
- 4. Created a matrix of Power (y outputs) and Capital_phi
- 5. Calculated the power coefficient Cp
- 6. ploted to verify data.

```
disp('_____')
```

```
0.94, 3.88 * (25/100); % Row 5: Current = 0.94A, Voltage =
3.88V * 25%.
                        1.15, 3.84 * (31.25/100); % Row 6: Current = 1.15A, Voltage
= 3.84V * 31.25%.
                        1.37, 3.80 * (37.5/100); % Row 7: Current = 1.37A, Voltage
= 3.80V * 37.5\%.
                        1.59, 3.76 * (43.25/100); % Row 8: Current = 1.59A, Voltage
= 3.76V * 43.25\%.
                        1.83, 3.71 * (50/100); % Row 9: Current = 1.83A, Voltage =
3.71V * 50%.
                        2.11, 3.67 * (56.25/100); % Row 10: Current = 2.11A,
Voltage = 3.67V * 56.25%.
                        2.39, 3.65 * (62.5/100); % Row 11: Current = 2.39A, Voltage
= 3.65V * 62.5\%.
                        2.71, 3.62 * (68.75/100); % Row 12: Current = 2.71A,
Voltage = 3.62V * 68.75%.
                        3.06, 3.56 * (75/100); % Row 13: Current = 3.06A, Voltage =
3.56V * 75%.
                        3.46, 3.48 * (81.25/100); % Row 14: Current = 3.46A,
Voltage = 3.48V * 81.25%.
                        3.88, 3.40 * (87.5/100); ; % Row 15: Current = 3.88A,
Voltage = 3.40V * 87.5%.
% Display the initial values data set from the provided data table
disp('Initial Power Data Set: ');
```

Initial Power Data Set:

disp(power_initial_values);

```
0.2400
0.3700
          0.2487
0.5600
          0.4938
          0.7350
0.7500
0.9400
          0.9700
1.1500
          1.2000
1.3700
          1.4250
1.5900
          1.6262
1.8300
          1.8550
2.1100
          2.0644
2.3900
          2.2812
          2.4888
2.7100
          2.6700
3.0600
3.4600
          2.8275
3.8800
          2.9750
```

```
% Calculate power for each data point
Current_amps = power_initial_values(:, 1);
Voltage_volts = power_initial_values(:, 2);
Power_watts = Current_amps .* Voltage_volts;
% Display Power in watts.
```

```
disp('Power used for each data point:');
```

Power used for each data point:

```
disp(Power_watts);
```

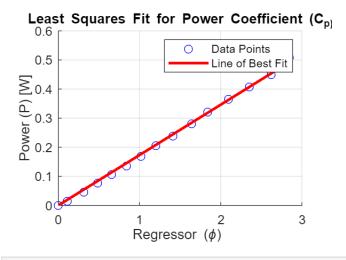
```
0.0920
0.2765
0.5513
0.9118
1.3800
1.9522
2.5857
3.3946
4.3558
5.4522
6.7445
8.1702
9.7832
```

```
% Calculating the data set for thrust and capital_phi to plot
% Equation used: P = p_row * 4 * D^5 * n^3 * Cp = V * I
%
                 P = V * I = thrust * w
% Define constants
p_row = 1.225; % Density of air in kg/m^3
D = 0.045; % Prop diameter in m, converted from 45 mm
% Calculate Capital_phi values using the given equation
Capital_phi_power = 4 * p_row * D^5 * ((Voltage_volts) * 2 * pi).^3; % Convert n
from RPM to rad/s
% Calculate the least squares solution for Cp (Power Coefficient)
Cp_least_squares = (Capital_phi_power' * Capital_phi_power) \ Capital_phi_power' *
Power_watts;
% Calculating the predicted y values using the least squares solution
Power_predicted = Capital_phi_power * Cp_least_squares;
% Display the calculated Power Coefficient
disp(['The estimated Power Coefficient (C_p) is: ', num2str(Cp_least_squares)]);
```

The estimated Power Coefficient (C_p) is: 1979.0226

```
% Plotting the data points and the line of best fit
figure;
scatter(phi, y, 'b'); % Plot the data points in blue
hold on;
```

```
plot(phi, y_pred, 'r','LineWidth', 2); % Plot the line of best fit in red
xlabel('Regressor (\phi) ');
ylabel('Power (P) [W]');
title('Least Squares Fit for Power Coefficient (C_p)');
legend('Data Points', 'Line of Best Fit');
grid on;
hold off;
```



Problem Requirements:

Estimate the propeller's torque coefficient. Assume sea level air density.

General Outline For Solution:

- 1. Create a data set based on values given on the problem pdf and from the previous two sections.
- 2. Calculate the torque given the relationships of the equations based on the data values created.
- 3. Calculate Capital phi from the equations provided. This will be used in the least squares method.
- 4. Use the least squares method to calculate the torque coefficient C m.
- 5. Create a prediction method of the torque.
- 6. Plot the data values against each other to verify calculations.

```
disp('_____')
```

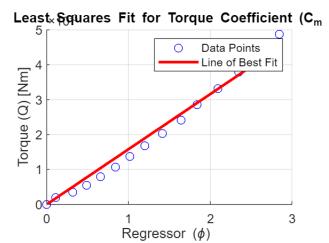
```
% 8(3)
% Equations used in this problem:
% P = Q * w
% Q = Cm * p_row * D^4 * n^2 * 4 , where Q is torque
% w = 2 * pi * n , where n is motor speed in Hz, and w is angular velocity
% Estimating the propeller's torque coefficient (C_m) using the least squares method.
```

```
% Define constants
p row = 1.225; % Density of air in kg/m<sup>3</sup> at sea level
D = 0.045; % Prop diameter in m, converted from 45 mm
% Extracting motor speed (n) from 'Thrust_Hz' defined in 8(1)
n values = Speed hz;
% Extracting power (P) from 'Power_watts' calculated in 8(2)
P values = Power_watts; % Power in Watts
% Calculate the torque (Q) for each data point using Q = P / w
% w (angular velocity) is calculated as w = 2 * pi * n
% Set the first row of the first column of torque_data_points to zero to handle the
division by zero.
Torque_Nm = zeros(size(n_values));
Torque Nm(1) = 0; % Torque is zero when n is zero
% Calculate the torque (Q) for each data point from the second row onwards using Q
= P / W
Torque_Nm(2:end) = P_values(2:end) ./ (2 * pi * n_values(2:end));
% Calculate the regressor (Phi) values using the given equation
Regressor phi = 4 * p row * D^4 * (n values.^2);
% Calculate the least squares solution for C_m (Torque Coefficient)
Cm_least_squares = (Regressor_phi' * Regressor_phi) \ Regressor_phi' * Torque_Nm;
% Calculating the predicted y values using the least squares solution
Torque_predicted = Regressor_phi * Cm_least_squares;
% Display the calculated Torque Coefficient
disp(['The estimated Torque Coefficient (C m) is: ', num2str(Cm least squares)]);
```

The estimated Torque Coefficient (C_m) is: 0.0015791

```
% Plotting the data points and the line of best fit
figure;
scatter(Regressor_phi, Torque_Nm, 'b'); % Plot the data points in blue
hold on;
plot(Regressor_phi, Torque_predicted, 'r', 'LineWidth', 2);%% Plot the line of best
fit in red
xlabel('Regressor (\phi) ');
ylabel('Torque (Q) [Nm]');
title('Least Squares Fit for Torque Coefficient (C_m)');
legend('Data Points', 'Line of Best Fit');
grid on;
```

hold off;



Problem Requirements:

Determine pitching moment produced by each motor as a function of motor speed.

General Outline For Solution:

- 1. Calculated the distance between a motor and the center of gravity of the drone.
- 2. Calculated the pitching moment for each motor speed as a function of n and thrust(n).
- 3. Plotted data to verify method used.

```
disp('____')
```

```
% 8(4)
% Define the distance from the center of mass to the motor (r) in meters
r = (92 / 2) / 1000; % Convert from mm to m

% Assuming Speed_hz is already defined as the array of motor speeds in Hz
% and Thrust_newtons is already defined as the array of thrust values in Newtons

% Calculate the pitching moment for each motor speed
M_pitching_values = r .* Thrust_newtons; % Element-wise multiplication of r and thrust for each motor speed

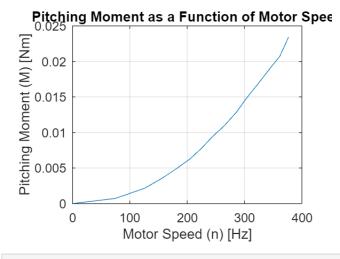
disp('Pitching Moment for each data point in Newton-meters');
```

Pitching Moment for each data point in Newton-meters

```
disp(M_pitching_values);
```

```
0.0007
0.0022
0.0036
0.0049
0.0063
0.0078
0.0095
0.0110
0.0129
0.0148
0.0168
0.0188
0.0207
0.0234
```

```
% Plot the pitching moment as a function of motor speed
figure;
plot(Speed_hz, M_pitching_values);
xlabel('Motor Speed (n) [Hz]');
ylabel('Pitching Moment (M) [Nm]');
title('Pitching Moment as a Function of Motor Speed');
grid on;
```



Problem Requirements:

Determine the rolling moment produced by each motor as a function of motor speed.

General Outline For Solution:

- 1. Calculated the distance is the perpendicular distance from the motor to the roll axis.
- 2. Calculated the pitching moment for each motor speed as a function of n and thrust(n).

3. Plotted data to verify method used

```
disp('____')
```

% 8(5)
% Define constants
distance_between_motors_m = 0.092; % 92 mm converted to meters
distance_to_roll_axis_m = distance_between_motors_m * sqrt(2)/2; % Distance from
each motor to the roll axis

% Calculate the rolling moment for each data point
RollingMoment_Nm = Thrust_newtons .* distance_to_roll_axis_m; % Rolling moment in

Newton-meters, using element-wise multiplication

% Display the calculated rolling moments

Rolling Moment for each data point in Newton-meters:

disp('Rolling Moment for each data point in Newton-meters:');

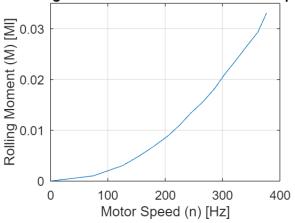
```
disp(RollingMoment_Nm);
```

0.0010 0.0031 0.0050 0.0069 0.0089 0.0110 0.0134 0.0156 0.0182 0.0209 0.0238 0.0266 0.0293

0.0331

```
figure;
plot(Speed_hz, RollingMoment_Nm);
xlabel('Motor Speed (n) [Hz]');
ylabel('Rolling Moment (M) [M1]');
title('Rolling Moment as a Function of Motor Speed');
grid on;
```

Rolling Moment as a Function of Motor Spee



Problem Requirements:

Determine yawing moment produced by each motor as a function of motor speed.

General Outline For Solution:

- 1. Calculated the distance is the perpendicular distance from the motor to the roll axis.
- 2. Calculated the pitching moment for each motor speed as a function of n and thrust(n).
- 3. Plotted data to verify method used

```
disp('_____')
```

```
% 8(6)
% Extract power values and motor speeds from the data set
Power_W = Power_watts; % Power in Watts, using the variable name established in 8(2)
Speed_Hz = Speed_hz; % Motor speed in Hz, using the variable name established
previously
% Initialize YawingMoment_Nm and Speed_rad_s variables
YawingMoment Nm = zeros(size(Power W)); % Initialize with zeros
Speed rad_s = zeros(size(Power_W)); % Initialize with zeros
% Define the first element of yawing_moment_Nm as zero
YawingMoment Nm(1) = 0; % As the first element of Speed hz is zero, leading to
division by zero
Speed_rad_s(1) = 0;
% Convert motor speed from Hz to rad/s for the remaining elements starting from the
second row
Speed_rad_s(2:end) = 2 * pi * Speed_Hz(2:end);
% Calculate the torque for each data point starting from the second row
```

```
Torque_Nm = Power_W(2:end) ./ Speed_rad_s(2:end); % Torque in Newton-meters

% Assign the calculated torque values to the YawingMoment_Nm variable starting from
the second row
YawingMoment_Nm(2:end) = Torque_Nm; % Yawing moment in Newton-meters

% Display the calculated yawing moments
disp('Yawing Moment for each data point in Newton-meters:');
```

Yawing Moment for each data point in Newton-meters:

```
disp(YawingMoment_Nm);

0
0.0002
0.0003
0.0006
0.0008
```

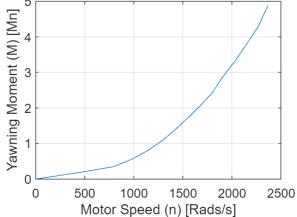
0.0011 0.0014 0.0017 0.0020

0.0024 0.0029 0.0033

0.0038 0.0043 0.0049

```
figure;
plot(Speed_rad_s, YawingMoment_Nm);
xlabel('Motor Speed (n) [Rads/s]');
ylabel('Yawning Moment (M) [Mn]');
title('Yawning Moment as a Function of Motor Speed');
grid on;
```

Yawning Moment as a Function of Motor Speed



Problem Requirements:

Estimate the angular velocity of the four propellers (assuming they all maintain the same constant speed) to produce a thrust equal and opposite to gravity (trim to 1g).

General Outline For Solution:

- 1. Convert the thrust of the individual propeller to 1/4th.
- 2. Calculate the angular velocity using given equation.
- 3. Display the results for calculation verification.

```
disp('____')
```

```
% 8(7)
% Define constants
p row = 1.225; % Density of air in kg/m<sup>3</sup>
D = 0.045; % Prop diameter in m, converted from 45 mm
g = 9.81; % Acceleration due to gravity in m/s^2s
% The total thrust needed to counteract gravity for all four propellers is equal to
the gravitational force acting on the drone.
% Since there are four propellers, the thrust produced by each propeller is 1/4th
of the total thrust needed.
T_per_propeller_N = g / 4; % Thrust per propeller in Newtons to balance out 1g of
gravitational acceleration
% Calculate the angular velocity needed for each propeller to produce the required
thrust
n rad s = sqrt(T per propeller N / (Ct least squares * p row * D^4)); % Angular
velocity in rad/s
Speed_n_Hz = n_rad_s / (2 * pi); % Convert angular velocity to Hz
% Display the calculated angular velocity
disp(['The estimated angular velocity of the four propellers to produce']);
```

The estimated angular velocity of the four propellers to produce

```
disp(['thrust equal and opposite to gravity (1g) is: ', num2str(Speed_n_Hz), '
Hz']);
```

thrust equal and opposite to gravity (1g) is: 267.3249 Hz

Problem 9 Translational Kinematics

```
% Given Information in the probelm

% Velocity of the vehicle in an earth frame
% v_E = [V_n, V_E, V_D];
```

```
% Ground Speed of the UAV
% V_b = [u, v, w]; = R_b_E * V_E
```

Problem Requirements:

Derive the expression for R E B in terms of the euler angles ϕ , θ , and ψ .

General Outline For Solution:

- 1. Define the rotational matrix for the euler angles.
- 2. Computer the roation multiplicaiton calculation.
- 3. Display Results for calculation verification.

```
% Define symbolic variables for Euler angles
syms phi theta psi real
% Define the Roll rotation matrix
R_{phi} = [1, 0, 0;
         0, cos(phi), -sin(phi);
         0, sin(phi), cos(phi)];
% Define the Pitch rotation matrix
R theta = [cos(theta), 0, sin(theta);
           0, 1, 0;
           -sin(theta), 0, cos(theta)];
% Define the Yaw rotation matrix
R_{psi} = [cos(psi), -sin(psi), 0;
         sin(psi), cos(psi), 0;
         0, 0, 1];
% Compute the combined rotation matrix R_E_B
R_EB = R_phi * R_theta * R_psi;
% Display the combined rotation matrix R_E_B
disp('The combined rotation matrix R E B is:');
```

The combined rotation matrix R_E_B is:

```
disp(R_E_B);
```

```
\begin{pmatrix}
\cos(\psi)\cos(\theta) & -\cos(\theta)\sin(\psi) & \sin(\theta) \\
\cos(\phi)\sin(\psi) + \cos(\psi)\sin(\phi)\sin(\theta) & \cos(\phi)\cos(\psi) - \sin(\phi)\sin(\psi)\sin(\theta) & -\cos(\theta)\sin(\phi) \\
\sin(\phi)\sin(\psi) - \cos(\phi)\cos(\psi)\sin(\theta) & \cos(\psi)\sin(\phi) + \cos(\phi)\sin(\psi)\sin(\theta) & \cos(\phi)\cos(\theta)
\end{pmatrix}
```

```
%____Going Backwards to provide proof of the implementation on top____%
% Given the property of orthonormal matrices, the inverse is the transpose
```

```
R_B_E_transpose = R_E_B'; % This is the transpose of R_E_B

% Display the matrix R_B_E
disp('The rotation matrix R_B_E (going backwards) is:');
```

The rotation matrix R_B_E (going backwards) is:

```
disp(R_B_E_transpose);
```

```
\begin{pmatrix}
\cos(\psi)\cos(\theta) & \cos(\phi)\sin(\psi) + \cos(\psi)\sin(\phi)\sin(\theta) & \sin(\phi)\sin(\psi) - \cos(\phi)\cos(\psi)\sin(\theta) \\
-\cos(\theta)\sin(\psi) & \cos(\phi)\cos(\psi) - \sin(\phi)\sin(\psi)\sin(\theta) & \cos(\psi)\sin(\phi) + \cos(\phi)\sin(\psi)\sin(\theta) \\
\sin(\theta) & -\cos(\theta)\sin(\phi) & \cos(\phi)\cos(\theta)
\end{pmatrix}
```

```
% Further Proof:
% Applying the transpose operator to the formula
R_E_B_backwards = R_phi' * R_theta' * R_psi';

% Display the matrix R_E_B_backwards
disp('The matrix R_E_B_backwards is:');
```

The matrix R E B backwards is:

```
disp(R_E_B_backwards);
```

```
\begin{pmatrix}
\cos(\psi)\cos(\theta) & \cos(\theta)\sin(\psi) & -\sin(\theta) \\
\cos(\psi)\sin(\phi)\sin(\theta) - \cos(\phi)\sin(\psi) & \cos(\phi)\cos(\psi) + \sin(\phi)\sin(\psi)\sin(\theta) & \cos(\theta)\sin(\phi) \\
\sin(\phi)\sin(\psi) + \cos(\phi)\cos(\psi)\sin(\theta) & \cos(\phi)\sin(\psi)\sin(\theta) - \cos(\psi)\sin(\phi) & \cos(\phi)\cos(\theta)
\end{pmatrix}
```

Problem 10 The Equation Of Motion

Requirements of Matrix A:

The elements of matrix A are the coefficients of the linearized differential equations of motion. Matrix AA encapsulates the inherent dynamics of the UAV, excluding any external control inputs.

```
% Define symbolic variables
syms phi theta psi p q r F_t u v w pn pe pd Z_T_c L_T_c M_T_c N_T_c My Mx My p_dot
w_dot theta_dot nFL nFR nRL nRR real

% Context for variables:
% p_row = 1.225; % Density of air in kg/m^3 at sea level
% D = 0.045; % Prop diameter in m, converted from 45 mm

% K_p = Cp_least_squares; % Power Coefficient
% k_t = Ct_least_squares; % Coefficient of Thrust
% distance_to_roll_axis_m
% K_p = Cp_least_squares;
omega = [p; q; r]; % omega_B_E, angular velocity
```

```
v b = [u; v; w];
x = [pn; pe; pd; u; v; w; phi; theta; psi; p; q; r];
V_b = [u; v; w]; % Velocity in body frame
n_motors = [nFL; nFR; nRL; nRR]; % For B Matrix
% inertia matrix
I = [Ixx, 0, 0]
     0, Iyy, 0;
     0, 0, Izz];
% inertia matrix inverse
I inv = inv(I);
% Calculate moment
K p = Cp least squares ; % Power Coefficient
k_t = Ct_least_squares; % Coefficient of Thrust
distance roll = distance to roll axis m;
Distance_to_pitch_axis = distance_to_roll_axis_m;
% Define the Roll rotation matrix
% Order of rotation Z, Y, X
R_{phi} = [1, 0, 0;
         0, cos(phi), -sin(phi);
         0, -sin(phi), cos(phi)];
% Define the Pitch rotation matrix
R_theta = [cos(theta), 0, -sin(theta);
           0, 1, 0;
           sin(theta), 0, cos(theta)];
% Define the Yaw rotation matrix
R psi = [cos(psi), sin(psi), 0;
         -sin(psi), cos(psi), 0;
         0, 0, 1];
% Matrix A:
% Compute the combined rotation matrix R E B
R_EB = R_phi * R_theta * R_psi;
R_B_E = R_E_B'; % Going backward
F_gb = R_EB' * [0; 0; m*g]; % force of gravity acting on the UAV in the body
frame
% Define Moments:
% Mx = Roll Moment, My = Pitch Moment, Mz = Yaw Moment
% Creating Rolling Function
```

```
Rolling_function = @(x) p_row * Ct_least_squares * D^4 * x^2 *
distance_to_roll_axis_m;
% Mx
M_x_FR = -Rolling_function(nFR);
M_x_FL = Rolling_function(nFL);
M x RL = Rolling function(nRL);
M_x_RR = -Rolling_function(nRR);
% My
% Creating Pitching Function
Pitching_function = @(x) p_row * Ct_least_squares * D^4 * x^2 *
Distance_to_pitch_axis;
M_y_FR = Pitching_function(nFR);
M y FL = Pitching function(nFL);
M_y_RL = -Pitching_function(nRL);
M_y_RR = -Pitching_function(nRR);
% Mz
% Creating Yawing Function
Yawing_Function = @(x) ((p_row * Cp_least_squares * D^5) / 2 * pi ) * x^2;
M_z_FR = Yawing_Function(nFR);
M z FL = -Yawing Function(nFL);
M_z_RL = Yawing_Function(nRL);
M_z_RR = -Yawing_Function(nRR);
Mx = vpa(M_xFR + M_xFL + M_xRL + M_xRR);
My = vpa(M_y_FR + M_y_FL + M_y_RL + M_y_RR);
Mz = vpa(M_z_FR + M_z_FL + M_z_RL + M_z_RR);
% Moment Vector
M t = [Mx;...]
        My;...
        Mz;]
```

 $M_t =$

```
% Extract coefficients and terms from the symbolic expressions
[coeffs_Mx, terms_Mx] = coeffs(Mx, n_motors);
[coeffs_My, terms_My] = coeffs(My, n_motors);
[coeffs_Mz, terms_Mz] = coeffs(Mz, n_motors);
% Equation for Thrust
```

```
Thrust_general = @(x) Ct_least_squares * p_row * D^4 * x^2;
% Calculate thrust for each motor
thrust f nFR = Thrust general(nFR);
thrust_f_nFL = Thrust_general(nFL);
thrust_f_nRR = Thrust_general(nRR);
thrust f nRL = Thrust general(nRL);
% Sum total thrust from all motors
Forces_w_Components_F_Z_B = [thrust_f_nFR + thrust_f_nFL + thrust_f_nRR +
thrust_f_nRL];
% VEctor form of Thrust
F_t = [0;0; Forces w Components F Z B]; % Vector form of Thrust
% Extract coefficients and terms from the thrust expressions
[coeffs_F_nFR, terms_F_nFR] = coeffs(thrust_f_nFR, nFR);
[coeffs_F_nFL, terms_F_nFL] = coeffs(thrust_f_nFL, nFL);
[coeffs F nRR, terms F nRR] = coeffs(thrust f nRR, nRR);
[coeffs_F_nRL, terms_F_nRL] = coeffs(thrust_f_nRL, nRL);
% Combine all force coefficients
All F coeffs = vpa([coeffs F nFR, coeffs F nFL, coeffs F nRR, coeffs F nRL]);
% Create matrix M combining all coefficients
M = [All_F_coeffs;...
    coeffs Mx;...
    coeffs_My;...
    coeffs_Mz];
M_{inv} = inv(M);
W_c_t = [Z_T_c; L_T_c; M_T_c; N_T_c];
motor_speeds_squared = M_inv * W_c_t;
motor_speeds = sqrt(abs(motor_speeds_squared));
w_g_t = M * motor_speeds_squared;
eqn_omega_dot = inv(I) * (M_t - cross(omega, I*omega) ); % angular acceleration of
UAV
% Define angular equations of motion
% Define equation for roll_dot, pitch_dot, yaw_dot
H_inv = [1, sin(phi)*tan(theta), cos(phi)*tan(theta);...
                0, cos(phi), -sin(phi);...
                0, sin(phi)/cos(theta), cos(phi)/cos(theta)];
```

```
% Define equation for roll_dot, pitch_dot, yaw_dot
dot_angles = H_inv * omega;
% Define translational equations of motion
eqn_u_dot = (1/m) * (F_t + F_g_b(1)) - r*v + q*w;
eqn_v_dot = (1/m) * F_g_b(2) + r*u - p*w;
eqn_w_dot = (1/m) * F_g_b(3) - q*u + p*v;
translational_equations = [eqn_u_dot; eqn_v_dot; eqn_w_dot];
% Equation of position
eqn_p_n_dot = R_E_B(1, :) * v_b;
eqn_p_e_dot = R_E_B(2, :) * v_b;
eqn_p_d_dot = R_E_B(3, :) * v_b;
position_equation = [eqn_p_n_dot; eqn_p_e_dot; eqn_p_d_dot];
% Define translational equations of motion
V_{dot} = 1/m * (F_t + F_g_b - cross(omega, m * V_b));
% Equation of
f = [position equation;...
    translational_equations
    eqn_omega_dot;...
    dot_angles;...
    1;
disp(f); % demonstrate function f
```

```
u \in v (\cos(\phi)\cos(\psi) - \sin(\phi)\sin(\psi)u (\sin(\phi)\sin(\psi) + \cos(\phi)\cos(\psi)
```

$$\frac{342096732324972875 \text{ nFL}^2}{16528282690043758247936} + \frac{34209673232497287}{165282826900437582} \\ r \, u - p \, w$$

where

$$\sigma_1 = \sigma_3 + q w - r v + \sigma_2$$

$$\sigma_2 = \frac{981\cos(\phi)\cos(\psi)\sin(\theta)}{100}$$

$$\sigma_3 = \frac{981 \sin(\phi) \sin(\psi)}{100}$$

```
% Calculate the A matrix from the jacobian
df_dx = jacobian(f, [x]);
A = subs(df_dx, x, zeros(12, 1) );
disp(A); % demonstrate Matrix A
```

```
(0 \ 0 \ 0 \ 1 \ 0 \ 0)
                    0 \quad 0 \quad 0 \quad 0 \quad 0
0 0 0 0 1 0
                    0 0 0 0 0
                        0 0 0 0
0 0 0 0 0 1
                        0 0 0 0
0 0 0 0 0 0
0 0 0 0 0 0
                        0 0 0 0
0 0 0 0 0 0
                        0 0 0 0
                981
0 0 0 0 0 0
                        0 0 0 0
0 0 0 0 0 0
                0
                       0 0 0 0
0 0 0 0 0 0
                    0 0 0 0 0
0 0 0 0 0 0
                    0 0 0 0 0
0 0 0 0 0 0
                   0 0 0 0 0
0 0 0 0 0 0
                   0 0 1 0 0
0 0 0 0 0 0
                   0 0 0 1 0
0 \ 0 \ 0 \ 0 \ 0
                    0 0 0 0 1
```

```
% Calculate Matrix B:
% function of f with added equations
f = [position_equation;...
   V_dot;...
    eqn omega dot;... %
    dot_angles;...
    1; % added v dot
% Take the Jacobian of f with respect to the motors
df dn = jacobian(f, n motors);
% Calculate Matrix B
B = vpa(subs(df_dn, n_motors, ones(4, 1) * Speed_n_Hz));
% matlabFunction(f, 'File', 'DroneDynamics', 'Outputs', {'z_dot'},'Vars',{'pn' 'pe'
'pd' 'u' 'v' 'w' 'p' 'q' 'r' 'phi' 'theta' 'psi' 'nFR' 'nFL' 'nRR' 'nRL'}); %
should not expect motor speed
matlabFunction(f, 'File', 'FunctionSimulation', 'Outputs', {'z_dot'}, 'Vars',{'pn'
'pe' 'pd' 'u' 'v' 'w' 'p' 'q' 'r' 'phi' 'theta' 'psi' 'Z_T_c' 'L_T_c' 'M_T_c'
'N_T_c'});
```

Error using sym/matlabFunction>checkVarsSubset
Free variables 'nFL,nFR,nRL,nRR' must be included in 'Vars' value.

```
Error in sym/matlabFunction>checkVars (line 251)
checkVarsSubset(vexpanded,funvars);

Error in sym/matlabFunction (line 158)
vars = checkVars(funvars,opts);
```

Related documentation

```
forces
% [t, z] = ode45(@(t, x) droneDynamics( x(1), x(2), x(3), x(4), x(5), x(6), x(7),
x(8), x(9), x(10), x(11), x(12), 50, 50, 50, 50), [0, 0.1], zeros(12,1)); % should
not expect motor speed.

% plot(t, z(:,3));

disp(f);
disp(df_dn);
disp(B);
```

Are the nonlinear dynamics locally stable around this reference condition?

First take the eigenvalues of matrix A. Local stability is analyzed using linearization and the properties of the linear system through the eigenvalues of the system.

Hence:

```
eigenvalues = eig(A);
disp(eigenvalues);
```

The system has already been linearized using the dynamics around the reference condition. Overall, the system shows a mix of stable and potentially unstable behaviors. The presence of eight zero eigenvalues suggests that the system may have some neutral stability characteristics, meaning certain state variables neither diverge nor converge but remain constant over time. The last two eigenvalues shown in this 12 x 1 vector are complex, indicating oscillatory dynamics. Such dynamics suggest that the system's response will have a sinusoidal component. Furthermore, the negative part of these eigenvalues means that the oscillations are damped, implying that the oscillations will decrease in amplitude over time, which actually contributes to the system's stability. The two middle eigenvalues, the remaining ones, are real and not complex (they lack the imaginary unit). The first of these (in row 9) has a negative real part, indicated by the minus sign at the front, making the expression overall negative. The opposite is true for the next eigenvalue (in row 10), meaning this eigenvalue has a positive real part. This is concerning because a positive real part indicates that disturbances will grow exponentially over time, potentially leading to an unstable system. Conversely, the negative real part suggests that disturbances within that state will decay exponentially over time, contributing to the stability of the system. Overall, the system is largely stable over time, with only one component that seems to be contributing instability to the system's performance. This might be intentional, but I personally believe the instability factor is

	itions or coding process. Further investigation is required
to identify where this mistake occurred if the instability	component is unintended.