

HOMEWORK 7

1. Wangsnass 15-7.

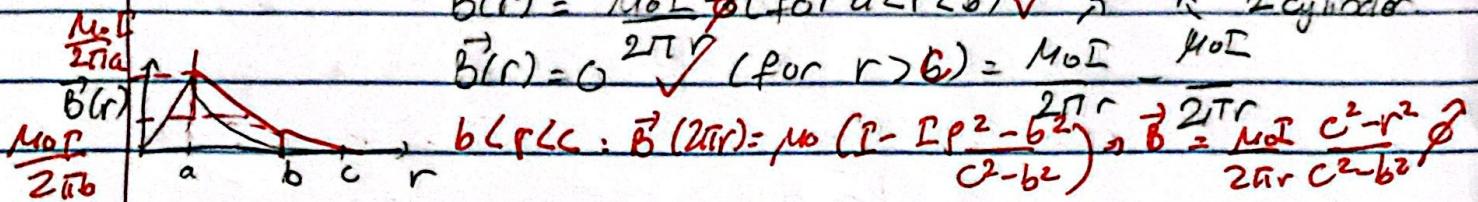


Using Ampere's circular law: $\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}}$

$$\vec{B}(r) = \frac{\mu_0 I r}{2\pi a^2} \hat{\phi} \quad (\text{for } r < a)$$

$$\vec{B}(r) = \frac{2\pi a^2}{\mu_0 I} \hat{\phi} \quad (\text{for } a < r < b) \quad \checkmark \quad \begin{matrix} \text{contribution from} \\ \text{2 cylinder.} \end{matrix}$$

$$\vec{B}(r) = 0 \quad (\text{for } r > b) = \frac{\mu_0 I}{2\pi r} \hat{\phi}$$



2. Wangsnass 15-8. $\vec{B} = 0$ for $0 < r < a$, $\vec{B} = \frac{\mu_0 I}{2\pi r} \frac{r^2 - a^2}{b^2 - a^2} \hat{\phi}$

for $a < r < b$, and $\vec{B} = \frac{\mu_0 I}{2\pi r} \hat{\phi}$ for $b < r$.

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}. \text{ In cylindrical coords: } \frac{1}{r} \frac{\partial}{\partial r} (r \rho \vec{B}) \hat{z} = \mu_0 \vec{J}$$

$$a < r < b: \frac{1}{r} (\vec{B} + \rho \frac{\partial \vec{B}}{\partial r}) \hat{z} = \mu_0 \vec{J} = \frac{\mu_0 I}{2\pi r} \frac{r^2 - a^2}{b^2 - a^2} \hat{z} \Rightarrow \vec{J} = \frac{\vec{I}}{\pi(b^2 - a^2)}$$

$$\vec{B} = \frac{\mu_0 I}{2\pi r} \frac{\rho^2 - a^2}{b^2 - a^2} \hat{\phi} \quad \text{for } a < r < b$$

$$= \frac{1}{r} \vec{I} \cdot (\vec{\nabla} \times \vec{B}) = \vec{z} \cdot \vec{I} \frac{\partial}{\partial r} \left[\frac{r^2 - a^2}{b^2 - a^2} \right] = \vec{z} \cdot \vec{I} \frac{1}{\pi(b^2 - a^2)} \checkmark$$

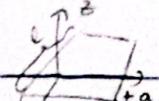
$$b < r \Rightarrow \vec{J} = 0 \text{ because } \vec{B} = \frac{\mu_0 I}{2\pi r} \frac{2\pi r}{b^2 - a^2} \hat{\phi}$$

$$= \frac{\partial}{\partial r} (r \rho \vec{B}) = \frac{\partial}{\partial r} \left(\frac{\mu_0 I}{2\pi} \frac{r^2 - a^2}{b^2 - a^2} \right) = 0 \quad \checkmark$$

There is current I evenly spreading in cylindrical region from $r=a$ to $r=b$

You could produce this kind of field by having coaxial cables carrying current in the opposite direction.

grading space for 1 or 2: I got 1 wrong at the part that I thought there's no field beyond b but there are I between b & c . 2 is correct.

3.  $\vec{J} = J \hat{x}$ $\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}}$

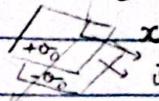
Using the right hand rule \vec{B} is $-\hat{y}$ for $z > 0$

$$I_{\text{enc}} = \int \vec{J} \cdot d\vec{a} = J a b$$

\vec{B} in \hat{y} for $z < 0$

$$\oint \vec{B} \cdot d\vec{l} = B \cdot l = \mu_0 I_{\text{enc}} \Rightarrow B = \mu_0 z \frac{J a}{l} \quad (z > a) \quad \checkmark$$

$$\therefore \text{For } -a < z < a: \vec{B} = -\mu_0 z \frac{J a}{l} \hat{y} \quad (z < -a) \quad \checkmark$$

4.  $\vec{R} = \sigma \vec{r}$

$$\vec{r} = \sigma_0 \vec{r} \quad \Rightarrow \oint \vec{B} \cdot d\vec{l} = 2Bl = \mu_0 I_{\text{enc}} = \mu_0 K l \Rightarrow B = \frac{\mu_0 K}{2} l$$

Above & below the capacitors: B -field = 0 since K points to opposite directions from the 2 plates.

In between: $B = \frac{\mu_0 \sigma_0 V_0 (\hat{y})}{2} - \frac{\mu_0 (-\sigma_0) V_0 (-\hat{y})}{2} = \frac{\mu_0 \sigma_0 V_0 (+\hat{y})}{2} \quad \checkmark$

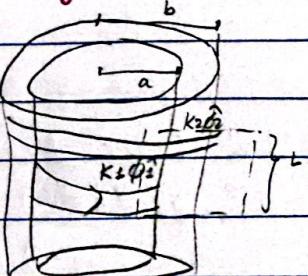
b) $\vec{F} = \vec{R} \times \vec{B} = \sigma_0 \frac{2}{2} \mu_0 \sigma_0 V_0 = \frac{2}{2} \mu_0 \sigma_0^2 V_0^2 \vec{z}$ (using right hand rule) \checkmark

c) Electric field @ bottom plate: $E = \frac{\sigma_0}{2\varepsilon_0}$; Force on the upper plate:

$$f = \sigma_0^2 \quad (\text{Force/unit area}) \quad F = \frac{\sigma_0^2 A}{2\varepsilon_0}$$

$$= \frac{2\varepsilon_0}{2\varepsilon_0} \mu_0 \sigma_0^2 \sigma_0^2 \Rightarrow \frac{2\varepsilon_0}{\sqrt{\mu_0 \sigma_0}} = c \quad \text{forces would never balance}$$

5. Wangsness 15-10.



$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}} = \mu_0 (K_1 + K_2) L$$

$$\Rightarrow \vec{B} = \mu_0 (K_1 + K_2) \hat{z} \quad \checkmark \quad (\text{right-hand rule})$$

Magnetic field between 2 cylinders: $\vec{B} = \mu_0 k_2 \hat{z}$

Magnetic field outside = 0. \checkmark

Magnetic field from loop

6. Wangsness 15-11.

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}} \quad \checkmark \quad B_L > 0 \quad \oint \vec{B} \cdot d\vec{s} = 0$$

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}} \Rightarrow B = \mu_0 I_{\text{enc}} \quad \text{At } \vec{r} \text{ & } \vec{r}' \Rightarrow B = 0 \quad B_L > 0$$

$$\Rightarrow B_{\text{loop}} = B_1 + B_2 = 2\mu_0 I_{\text{enc}} \quad \Rightarrow \text{induction cannot drop to 0.}$$

Change in B is also consistent with capacitor image as current more parallel in the same direction. Additive B → not drop to 0.

grading space for 3→6: I forgot Z fors. Correct 4&5. I think I am wrong for 6, I got the sign for B incorrectly & I think my explanation is also wrong.

7. Wengness 16-10.

$$r = z\hat{z}, r' = a\hat{\phi} \Rightarrow R = \sqrt{z^2 + a^2}$$

$$\vec{A} = \frac{\mu_0 I}{4\pi} \int \frac{ds}{R} = \frac{\mu_0 I}{4\pi} \int \frac{a d\phi d\theta}{\sqrt{z^2 + a^2}}$$

$$= \frac{\mu_0 I a}{2\pi} \sin \hat{y} = \frac{\mu_0 I a \sin \hat{y}}{2\pi \sqrt{z^2 + a^2}}$$

$a = \pi \Rightarrow \vec{A} = 0$, that doesn't make sense, I just don't know why.

8. Wengness 16-14.

Uniform ∞ sheet of current in xy plane, carrying current in y -direct
ion. $\vec{B} = \begin{cases} -\frac{\mu_0 k}{2} \hat{x} & (z > 0) \\ \frac{\mu_0 k}{2} \hat{x} & (z < 0) \end{cases}$

$$\vec{\nabla} \times \vec{A} = \vec{B}, \text{ using Stok's Theorem: } \oint \vec{A} \cdot d\vec{l} = \iint \vec{B} \cdot d\vec{A}$$

$$\Rightarrow A = \frac{\mu_0 k}{2} \left(z\hat{y} - \hat{x} \right) \quad \text{for } z > 0$$

$$\Rightarrow \oint A = -\frac{\mu_0 k}{2} (z\hat{y} - \hat{x}) \quad \text{for } z > 0$$

$$A = \frac{\mu_0 k}{2} (z\hat{y} - \hat{x}) \quad \text{for } z < 0$$

9. Wengness 16-15.

Assuming $\vec{\omega} = \omega \hat{z}$

$$\vec{r}' = r \sin \theta \cos \phi' \hat{x} + r \sin \theta \sin \phi' \hat{y} + r \cos \theta \hat{z}$$

$$\vec{\omega} = \vec{\omega} \times \vec{r} = (-\omega r \sin \theta \sin \phi') \hat{x} - (\omega r \sin \theta \cos \phi') \hat{y}$$

$$\vec{A}(r) = \frac{\mu_0}{4\pi} \int \vec{j}(\vec{r}') d\vec{l}, \text{ where } \vec{j}(\vec{r}') = \rho \vec{v} = \rho (\vec{\omega} \times \vec{r}')$$

$$= \frac{\mu_0}{4\pi} \int_0^R \int_0^{2\pi} (-\omega r \sin \theta \sin \phi' \hat{x} + \omega r \sin \theta \cos \phi' \hat{y}) \dots r^2 \sin \theta dr d\phi$$

But since $\int_0^{2\pi} \sin \phi' d\phi' = 0 = \int_0^{2\pi} \cos \phi' d\phi'$ $d\phi$ vanishes.

$$\Rightarrow \vec{A} = 0 \quad \text{on axis.}$$

Grade space for 7-9: I got 7&9 correct, I am correct
for finding \vec{B} in 8, but I messed up \vec{A} .
I did the reverse order for compared to the
answer. I should find \vec{A} first so $\vec{\nabla} \times \vec{A} = \vec{B}$
can be easier.

$$10. L = \int \frac{d\vec{r}}{dt} dt = \int \vec{T} dt = \int (r \times \vec{F}) dt \quad (\text{Angular momentum of particle})$$

Initial velocity: $\vec{v}_0 = v_0 \hat{\phi}$. Since the particle is moving in B -field

$$\rightarrow \vec{F} = q(\vec{E} + \vec{v} \times \vec{B}) \rightarrow L = \int r \times q(\vec{v} \times \vec{B}) dt = \int r \times q(d\vec{r} \times \vec{B}) = q \int r \times \vec{B} d\vec{r} - \int \vec{B} (r d\vec{r})$$

$$r \cdot dr = r \cdot dr = \frac{1}{2} d(r^2) = r dr = \frac{1}{2} (2\pi r dr) \quad \text{Osmar} \checkmark$$

$$\therefore L = -\frac{q}{2\pi} \int_0^{2\pi} B 2\pi r dr = -\frac{q}{2\pi} \int B da = \left[-\frac{q}{2\pi} \cdot \phi \right] \checkmark \quad \text{flux} = \int B da$$

If $\phi = C$ $\rightarrow L = 0$ $\rightarrow \int B da = 0$. Therefore, we can conclude that the charge leave the region pretty radially.

11. Wangsnass 16-5.

$$\vec{B} = B \hat{z} = \nabla \times \vec{A} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix} \quad \begin{cases} \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} = 0 \quad (1) \\ \frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} = 0 \quad (2) \\ \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} = B \quad (3) \end{cases}$$

From section 16-3:

$$(1) A_x = 0, A_y = Bx, A_z = \text{const.} \quad \text{From } (1) \rightarrow \frac{\partial A_z}{\partial y} = 0, \frac{\partial A_y}{\partial z} = 0$$

$$\frac{\partial A_x}{\partial z} = 0, \frac{\partial A_z}{\partial x} = 0 ; \quad \frac{\partial A_y}{\partial x} = B \frac{\partial x}{\partial x} = B ; \quad \frac{\partial A_x}{\partial y} = 0$$

$$\rightarrow \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} = B - 0 = B \rightarrow \nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = \begin{cases} Ax = 0 \\ Ay = Bx \\ Az = \text{const} \end{cases}$$

I just
proof
some
textbook
stuff
in
section
16-3

$$(2) A_x = -By, A_y = 0, A_z = \text{const.} \rightarrow \frac{\partial A_z}{\partial y} = -B, \frac{\partial A_x}{\partial z} = 0, \frac{\partial A_y}{\partial x} = 0 = \frac{\partial A_y}{\partial x}$$

$$\frac{\partial A_z}{\partial y} = 0, \frac{\partial A_x}{\partial z} = 0 \rightarrow (1) \& (2) \text{ satisfied} \rightarrow (3) \rightarrow \frac{\partial A_y}{\partial z} - \frac{\partial A_z}{\partial y} = 0 - (-B) = B$$

$$\frac{\partial A_y}{\partial z} - \frac{\partial A_z}{\partial y} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = -B \frac{\partial y}{\partial z} + 0 + \frac{\partial \text{const}}{\partial z} \frac{\partial y}{\partial z} = 0$$

$$(3) A_x = -\frac{1}{2} By, A_y = \frac{1}{2} Bx, A_z = \text{const}$$

$$\Rightarrow \nabla \cdot \vec{A} = -\frac{1}{2} B \frac{\partial y}{\partial x} + \frac{1}{2} B \frac{\partial z}{\partial z} + \frac{\partial \text{const}}{\partial z} = 0$$

$$\Rightarrow \frac{\partial A_x}{\partial y} = -\frac{1}{2} B, \quad \frac{\partial A_y}{\partial x} = \frac{1}{2} B, \quad \text{else} = 0. \quad \text{Satisfied } (1) \& (2) \& (3)$$

From Gauge transformation of $\vec{A} = (A_x, A_y, A_z)$

$$\vec{A}' = (-By, 0, \text{const}) = \vec{A} + \vec{\chi}_{12}$$

$$\rightarrow (-By, 0, \text{const}) = (0, Bx, c) + \left(\frac{\partial \chi_{12}}{\partial x}, \frac{\partial \chi_{12}}{\partial y}, \frac{\partial \chi_{12}}{\partial z} \right) = \left(\frac{\partial \chi_{12}}{\partial x}, Bx + \frac{\partial \chi_{12}}{\partial y}, c + \frac{\partial \chi_{12}}{\partial z} \right)$$

$$\Rightarrow \int \frac{\partial \chi_{12}}{\partial x} = -By \Rightarrow \chi_{12} = -Bxy + c' \quad \checkmark$$

$$\frac{\partial \chi_{12}}{\partial y} = -Bx$$

$$\frac{\partial \chi_{12}}{\partial z} = 0$$

$$\vec{A_2} \rightarrow \vec{t_3} = \vec{r_2} = \vec{r_2} + \vec{j}x_{23}$$

$$\Rightarrow \left(-\frac{1}{2}By, \frac{1}{2}Bx, c \right) = (-By, 0, c) + \left(\frac{\partial X_{23}}{\partial x}, \frac{\partial X_{23}}{\partial y}, \frac{\partial X_{23}}{\partial z} \right)$$

$$\Rightarrow \left(-\frac{1}{2}By, \frac{1}{2}Bx, c \right) = (-By + \frac{\partial X_{23}}{\partial x}, \frac{\partial X_{23}}{\partial y}, c + \frac{\partial X_{23}}{\partial z})$$

$$\Rightarrow -\frac{1}{2}By = -By + \frac{\partial X_{23}}{\partial x} \Rightarrow \frac{\partial X_{23}}{\partial x} = \frac{1}{2}By \Rightarrow X_{23} = \frac{1}{2}By + c" \quad \checkmark$$

$$\vec{A_3} \rightarrow \vec{A_2} \Rightarrow \vec{A_2} = \vec{r_3} + \vec{j}X_{23}$$

$$\Rightarrow (0, Bx, c) = \left(-\frac{1}{2}By, \frac{\partial X_{23}}{\partial x}, \frac{1}{2}Bx + \frac{\partial X_{23}}{\partial y}, c + \frac{\partial X_{23}}{\partial z} \right)$$

$$\Rightarrow -\frac{1}{2}By + \frac{\partial X_{13}}{\partial x} = 0 \Rightarrow \frac{\partial X_{13}}{\partial x} = \frac{-1}{2}By \Rightarrow X_{13} = -\frac{1}{2}Bxy + c"$$

Trading space for 10+11: All correct for 10+11.

Conclusion: I guess I did relatively well this homework.

My mistakes would be about not be able to find correct \vec{A}' in defined the region(sign) of \vec{t}' wrong. That just proof I didn't understand what was going on (which I admit, I didn't) so I need to work on my understanding more.