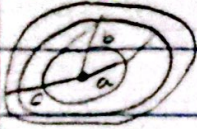


HOMEWORK 7

1. Wangsness 15-7.

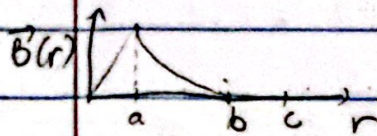


Using Ampere's circular law: $\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}} l$

$$\vec{B}(r) = \frac{\mu_0 I}{2\pi r} \hat{z} \quad (\text{for } r < a)$$

$$\vec{B}(r) = \frac{2\pi a^2}{\mu_0 I} \hat{z} \quad (\text{for } a < r < b) \quad \begin{matrix} \text{Contribution from} \\ \text{2 cylinders} \end{matrix}$$

$$\vec{B}(r) = 0 \quad (\text{for } r > b) = \frac{\mu_0 I}{2\pi r} - \frac{\mu_0 I}{2\pi r}$$



2. Wangsness 15-8. $\vec{B} = 0$ for $0 < r < a$, $\vec{B} = \frac{\mu_0 I}{2\pi r} \frac{r^2 - a^2}{b^2 - a^2} \hat{\phi}$ for $a < r < b$, and $\vec{B} = \mu_0 I \hat{\phi}$ for $b < r$.

$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$. In cylindrical coord: $\frac{1}{r} \frac{\partial}{\partial r} (r \vec{B}) \hat{z} = \mu_0 \vec{J}$

For $a < r < b$: $\frac{1}{r} (\vec{B} + r \frac{\partial \vec{B}}{\partial r}) \hat{z} = \mu_0 \vec{J} = \frac{\mu_0 I}{\pi(b^2 - a^2)} \hat{z}$

$$\vec{B} = \mu_0 I \frac{\partial}{\partial r} \left(\frac{r^2 - a^2}{2\pi(b^2 - a^2)} \right) \hat{\phi} \quad \text{for } a < r < b$$

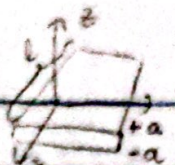
$$\Rightarrow \vec{J} = \frac{1}{\mu_0} (\vec{\nabla} \times \vec{B}) = \hat{z} \frac{I}{\pi(b^2 - a^2)} \frac{\partial}{\partial r} \left[\frac{r^2 - a^2}{2} \right] = \hat{z} \frac{I}{\pi(b^2 - a^2)}$$


For $b < r$: $\vec{J} = 0$ because $\vec{B} = \mu_0 I \hat{\phi}$

$$\Rightarrow \frac{\partial}{\partial r} (r \vec{B}) = \frac{\partial}{\partial r} \left(\frac{\mu_0 I}{2\pi} \right) = 0$$

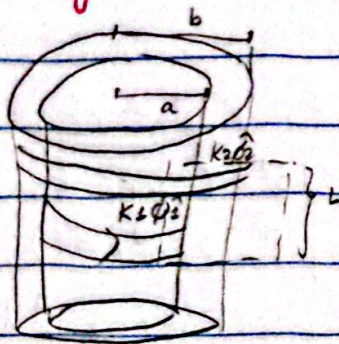
You could produce this kind of field by having coaxial cables carrying current in the opposite direction.

Grading space for 1 & 2:

3.  $\vec{T} = T_0 \hat{x}$ $\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} l$
 Using the right hand rule \vec{B} in $-\hat{y}$ for $z > 0$
 \vec{B} in \hat{y} for $z < 0$
 $I_{enc} l = \int \vec{T} \cdot d\vec{a} = T_0 z l$
 $\oint \vec{B} \cdot d\vec{l} = B \cdot l = \mu_0 T_0 z l \Rightarrow B = \mu_0 z T_0 \Rightarrow \vec{B} = \begin{cases} -\mu_0 T_0 a \hat{y} & (z > a) \\ \mu_0 T_0 a \hat{y} & (z < -a) \end{cases}$
 For $-a < z < a$: $\vec{B} = -\mu_0 z T_0 \hat{y}$

4.  $\vec{E} \cdot d\vec{a} \hat{y}$ $\oint \vec{B} \cdot d\vec{l} = 2Bl = \mu_0 I_{enc} l = \mu_0 K l \Rightarrow B = \frac{\mu_0 K}{2}$
 Above & below the capacitors: B-field = 0 since K points to opposite directions from the 2 plates.
 In between: $\vec{B} = \frac{\mu_0 \sigma_0 \mathcal{V}_0 (-\hat{y})}{2} - \frac{\mu_0 (-\sigma_0) \mathcal{V}_0 (-\hat{y})}{2} = \mu_0 \sigma_0 \mathcal{V}_0 (-\hat{y})$
 b) $\vec{F} = \vec{K} \times \vec{B} = \sigma_0 \frac{\mu_0 \sigma_0 \mathcal{V}_0}{2} = \frac{\mu_0 \sigma_0^2 \mathcal{V}_0^2}{2} \hat{z}$ (using right hand rule)
 c) Electric field @ bottom plate: $E = \frac{\sigma_0}{2\epsilon_0}$; Force on the upper plate:
 $f = \frac{\sigma_0^2}{2\epsilon_0}$ (force/unit area) $F = \frac{\sigma_0^2 A}{2\epsilon_0}$
 $= \frac{\sigma_0^2}{2\epsilon_0} \mu_0 \sigma_0^2 \mathcal{V}_0^2 \Rightarrow \mathcal{V}_0 = \frac{1}{\sqrt{\mu_0 \epsilon_0}} = c \Rightarrow$ forces would never balance.

5. Wangsness 15-10.



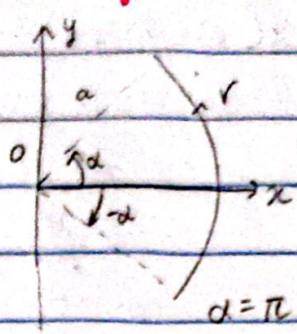
$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} = \mu_0 (K_1 + K_2) l$
 $\Rightarrow \vec{B} = \mu_0 (K_1 + K_2) \hat{z}$ (right hand rule)
 \Rightarrow Magnetic field between 2 cylinders: $\vec{B} = \mu_0 K_2 \hat{z}$
 \Rightarrow Magnetic field outside = 0.
 Magnetic field from loop:

6. Wangsness 15-11.

$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} \Rightarrow B = \frac{\mu_0 I_{enc}}{l}$ At (2) & (4) $\vec{B} = 0$
 $\Rightarrow B_{loop} = B_1 + B_3 = \frac{2\mu_0 I_{enc}}{l} \Rightarrow$ induction cannot drop to 0.
 Change in B is also consistent with capacitor image as current + move parallel in the same direction. Additive B \rightarrow not drop to 0.

Grading space for 3 \rightarrow 6:

7. Wangness 16-10.



$$r = z\hat{z}, r' = a\hat{\rho} \Rightarrow R = z\hat{z} - a\hat{\rho} = \sqrt{z^2 + a^2}$$

$$\vec{A} = \frac{\mu_0 I}{4\pi} \int \frac{d\vec{s}}{R} = \frac{\mu_0 I}{4\pi} \int \frac{a d\theta d\hat{\rho}}{\sqrt{z^2 + a^2}}$$

$$= \frac{\mu_0 I a}{4\pi \sqrt{z^2 + a^2}} \int_{-\alpha}^{\alpha} d\theta \int \hat{\rho} d\theta = \frac{\mu_0 I a}{4\pi \sqrt{z^2 + a^2}} 2\pi \sin \alpha \hat{y}$$

$\alpha = \pi \Rightarrow \vec{A} = 0$ That doesn't make sense, I just don't know why.

8. Wangness 16-14.

Uniform sheet of current in xy plane, carrying current in y direction

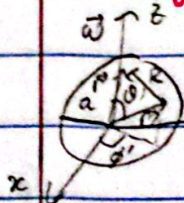
$$\vec{B} = \begin{cases} -\frac{\mu_0 k}{2} x\hat{x} & (z > 0) \\ \frac{\mu_0 k}{2} x\hat{x} & (z < 0) \end{cases}$$

$$\vec{\nabla} \times \vec{A} = \vec{B}, \text{ using Stokes' Theorem: } \oint \vec{A} \cdot d\vec{l} = \int \vec{B} \cdot d\vec{A}$$

$$\Rightarrow \vec{A} = \vec{B} \times \vec{r} = -\frac{\mu_0 k}{2} (z\hat{z} \times \vec{r})$$

$$\Rightarrow \begin{cases} \vec{A} = -\frac{\mu_0 k}{4} (z\hat{y} - k\hat{y}) & \text{for } z > 0 \\ \vec{A} = \frac{\mu_0 k}{4} (z\hat{y} - k\hat{y}) & \text{for } z < 0 \end{cases}$$

9. Wangness 16-15.



Assuming $\vec{\omega} = \omega\hat{z}$

$$\vec{r}' = r \sin\theta' \cos\phi' \hat{x} + r \sin\theta' \sin\phi' \hat{y} + r \cos\theta' \hat{z}$$

$$\vec{\omega} \times \vec{r}' = (-\omega r \sin\theta' \sin\phi') \hat{x} - (\omega r \sin\theta' \cos\phi') \hat{y}$$

$$\vec{A}(\vec{r}) = \frac{\mu_0}{4\pi} \int \frac{\vec{J}(\vec{r}')}{R} d\tau, \text{ where } \vec{J}(\vec{r}') = \rho \vec{v} = \rho (\vec{\omega} \times \vec{r}')$$

$$= \frac{\mu_0}{4\pi} \int_0^R \int_0^\pi \int_0^{2\pi} (-\omega r' \sin\theta' \sin\phi' \hat{x} + \omega r \sin\theta' \cos\phi' \hat{y}) r'^2 \sin\theta' dr' d\theta' d\phi'$$

But since $\int_0^{2\pi} \sin\phi' d\phi' = 0 = \int_0^{2\pi} \cos\phi' d\phi'$

$$\Rightarrow \vec{A} = 0$$

Grading space for 7-9,

10. $L = \int \frac{dL}{dt} dt = \int T dt = \int (r \times F) dt$ (Angular momentum of particle).

Initial velocity: $\vec{v}_0 = v_0 \hat{p}$. Since the particle is moving in B-field

$\vec{F} = q(\vec{v} \times \vec{B}) \Rightarrow L = \int r \times q(\vec{v} \times \vec{B}) dt = \int r \times q(d\vec{r} \times \vec{B}) = q \int (r \cdot \vec{B}) d\vec{r} - \int B(r \cdot d\vec{r})$

$r \cdot d\vec{r} = r \cdot dr = \frac{1}{2} d(r^2) = r dr = \frac{1}{2} (2\pi r dr)$ $\vec{B} \perp \vec{r}$

$\Rightarrow L = -\frac{q}{2\pi} \int_0^R B 2\pi r dr = -\frac{q}{2\pi} \int B da = -\frac{q}{2\pi} \cdot \Phi \Rightarrow \text{flux} = \int B da$

1 If $\Phi = 0 \Rightarrow L = 0 \Rightarrow \iint B da = 0$. Therefore, we can conclude that the charge leave the region pretty radially.

11. Wangsness 16-5.

$\vec{B} = B\hat{z} = \nabla \times \vec{A} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{z} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_x & A_y & A_z \end{vmatrix} \Rightarrow \begin{cases} \frac{\partial A_z}{\partial y} - \frac{\partial A_y}{\partial z} = 0 & (1) \\ \frac{\partial A_x}{\partial z} - \frac{\partial A_z}{\partial x} = 0 & (2) \\ \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} = B & (3) \end{cases}$

From section 16-3:

(a) $A_x = 0, A_y = Bx, A_z = \text{const.}$ From (2) $\Rightarrow \frac{\partial A_z}{\partial x} = 0, \frac{\partial A_y}{\partial z} = 0$

$\frac{\partial A_x}{\partial z} = 0, \frac{\partial A_z}{\partial x} = 0; \frac{\partial A_y}{\partial x} = B \Rightarrow \frac{\partial A_y}{\partial x} = B \Rightarrow A_y = Bx$
 $\Rightarrow \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} = B - 0 = B \Rightarrow \nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = 0 + 0 + 0 = 0$ $\begin{cases} A_x = 0 \\ A_y = Bx \\ A_z = \text{const} \end{cases}$

(b) $A_x = -By, A_y = 0, A_z = \text{const.} \Rightarrow \frac{\partial A_z}{\partial y} = -B, \frac{\partial A_x}{\partial z} = 0, \frac{\partial A_y}{\partial z} = 0 = \frac{\partial A_y}{\partial z}$
 $\frac{\partial A_z}{\partial y} = -B, \frac{\partial A_z}{\partial x} = 0 \Rightarrow$ (1) & (2) satisfied \Rightarrow (3) $\Rightarrow \frac{\partial A_y}{\partial x} - \frac{\partial A_x}{\partial y} = 0 - (-B) = B$
 $\nabla \cdot \vec{A} = \frac{\partial A_x}{\partial x} + \frac{\partial A_y}{\partial y} + \frac{\partial A_z}{\partial z} = -B \frac{\partial y}{\partial y} + 0 + \frac{\partial \text{const}}{\partial z} = 0$

(c) $A_x = -\frac{1}{2} By, A_y = \frac{1}{2} Bx, A_z = \text{const}$

$\Rightarrow \nabla \cdot \vec{A} = -\frac{1}{2} B \frac{\partial y}{\partial y} + \frac{1}{2} B \frac{\partial x}{\partial x} + \frac{\partial \text{const}}{\partial z} = 0$

$\Rightarrow \frac{\partial A_x}{\partial y} = -\frac{1}{2} B, \frac{\partial A_y}{\partial x} = \frac{1}{2} B, \text{ else } = 0. \text{ Satisfied (1) \& (2) \& (3)}$

From Gauge transformation of $\vec{A}' = (0, Bx, \text{const})$

$\vec{A}' = (-By, 0, \text{const}) = \vec{A} + \nabla \chi_{12}$

$\Rightarrow (-By, 0, \text{const}) = (0, Bx, c) + (\frac{\partial \chi_{12}}{\partial x}, \frac{\partial \chi_{12}}{\partial y}, \frac{\partial \chi_{12}}{\partial z}) = (\frac{\partial \chi_{12}}{\partial x}, Bx + \frac{\partial \chi_{12}}{\partial y}, c + \frac{\partial \chi_{12}}{\partial z})$

$\Rightarrow \int \frac{\partial \chi_{12}}{\partial x} = -By \Rightarrow \chi_{12} = -Bxy + C'$

$\frac{\partial \chi_{12}}{\partial y} = -Bx$

$\frac{\partial \chi_{12}}{\partial z} = 0$

$$\vec{A}_2 \rightarrow \vec{A}_3 \Rightarrow \vec{A}_3 = \vec{A}_2 + \vec{\nabla} X_{23}$$

$$\Rightarrow \left(-\frac{1}{2} B_y, \frac{1}{2} B_x, c\right) = (-B_y, 0, c) + \left(\frac{\partial X_{23}}{\partial x}, \frac{\partial X_{23}}{\partial y}, \frac{\partial X_{23}}{\partial z}\right)$$

$$\Rightarrow \left(-\frac{1}{2} B_y, \frac{1}{2} B_x, c\right) = \left(-B_y + \frac{\partial X_{23}}{\partial x}, \frac{\partial X_{23}}{\partial y}, c + \frac{\partial X_{23}}{\partial z}\right)$$

$$\Rightarrow -\frac{1}{2} B_y = -B_y + \frac{\partial X_{23}}{\partial x} \Rightarrow \frac{\partial X_{23}}{\partial x} = \frac{1}{2} B_y \Rightarrow X_{23} = \frac{1}{2} B_x y + c''$$

$$\vec{A}_3 \rightarrow \vec{A}_1 \Rightarrow \vec{A}_1 = \vec{A}_3 + \vec{\nabla} X_{13}$$

$$\Rightarrow (0, B_x, c) = \left(-\frac{1}{2} B_y, \frac{\partial X_{13}}{\partial x}, \frac{1}{2} B_x + \frac{\partial X_{13}}{\partial y}, c + \frac{\partial X_{13}}{\partial z}\right)$$

$$\Rightarrow -\frac{1}{2} B_y + \frac{\partial X_{13}}{\partial x} = 0 \Rightarrow \frac{\partial X_{13}}{\partial x} = \frac{1}{2} B_y \Rightarrow X_{13} = \frac{1}{2} B_x y + c''$$

Grading space for $L_0 + L_1$:

Conclusion: