

This form must be completed and submitted by all teams no later than the date specified in the Action Deadlines on specific event website. The FSAE Technical Committee will review all submissions which deviate from the FSAE® rules and reply with a decision about the requested deviation. All requests will have a confirmation of receipt sent to the team. Impact Attenuator Data (IAD) and supporting calculations must be submitted electronically in Adobe Acrobat Format (*.pdf). The submissions must be named as follows: schoolname_IAD.pdf using the complete school name. Submit the IAD report as instructed on the event website. For Michigan and Lincoln events submit through fsaeonline.com.

*In the event that the FSAE Technical Committee requests additional information or calculations, teams have **one** week from the date of the request to submit the requested information or ask for a deadline extension.

University Name:	Yale Univeristy	Car Number:	<u>E228</u>
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Faculty Advisor: _	Joseph Zinter	E-mail Address:	joseph.zinter@yale.edu

Material(s) Used	Aluminum	
Description of form/shape	Honeycomb 5052 5.7pcf 3/16" 4"x8"x10.7"	
IA to Anti-Intrusion Plate	WEST SYSTEM® Six10® Thickened Epoxy Adhesive	
mounting method		
Anti-Intrusion Plate to Front	4, 5/16 Grade 8 Bolts	
Bulkhead mounting method		
Peak deceleration (<= 40 g's)	18.8 g's	
Average deceleration (<= 20 g's)	16.3g's	

Confirm that the attenuator contains the minimum volume 200mm wide x 100mm high x 200mm long

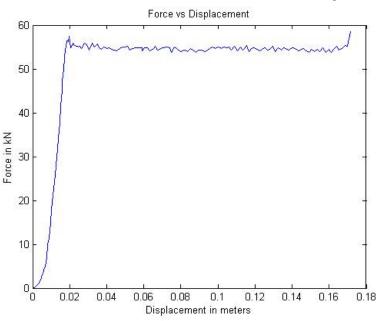


Figure 1: Force-Displacement Curve (dynamic tests must show displacement during collision and after the point v=0 and until force becomes =0)

DP 3-	TECHNICAL COMMIT	TEE DECISION/COM			
Approved by	Joseph Zinter	Da	ate	2/5/16	

NOTE: THIS FORM AND THE APPROVED COPY OF THE SUBMISSION MUST BE PRESENTED AT TECHNICAL INSPECTION AT EVERY FORMULA SAE EVENT ENTERED

University Name: __Yale University ____ Car Number(s) & Event(s): _E228: FSAE Electric__

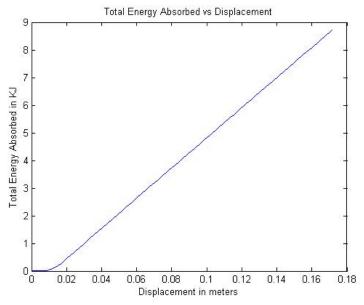


Figure 2: Energy-Displacement Curve (dynamic tests must show displacement during collision and after v=0)



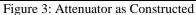




Figure 4: Attenuator after Impact

*See appended photos for Anti-intrusion plate deformation measurement

Energy Absorbed (J):	8,720	Vehicle includes front wing	Yes/No
Must be $\geq 7350 \text{ J}$		in front of front bulkhead?	
IA Max. Crushed Displacement	171.5	Wing structure included in	N/A
(mm):		test?	
IA Post Crush Displacement -	-18.0	Test Type: (e.g. barrier test,	Quasi-static crush
demonstrating any return (mm):		drop test, quasi-static crush)	
Anti-Intrusion Plate	9	Test Site: (must be from	Yale University,
Deformation (mm)		approved test site list on	Schroers's Lab
		website for dynamic tests)	Instron 5569



University Name: __Yale University____ Car Number(s) & Event(s): _E228: FSAE Electric__

Test Data Calculations:

The Rules require that our impact attenuator, "when mounted on the front of a vehicle with a total mass of 300 kg (661 lbs.) and run into a solid, non-yielding impact barrier with a velocity of impact of 7.0 meters/second (23.0 ft/sec), would give an average deceleration of the vehicle not to exceed 20 g's, with a peak deceleration less than or equal to 40 g's. Total energy absorbed must meet or exceed 7350 Joules."

Weight:

We estimate our vehicle will have a mass of mass of about 683 lbs. As this weight is greater than the 300 kg weight specified in the rules, we will show calculations for both the hypothetical 300kg vehicle and our 683 lbs (309 kg) vehicle when the weight is rounded off to the next one-hundred (i.e., 700 lbs or 317.5 kg).

Peak deceleration:

Our compression testing yielded a maximum force of 58.5 kN. Generally, acceleration may be calculated as:

1.
$$a = F/m$$

For a Force "F" and Mass "m"

Case 1: m=317.5 kg

For our mass of 317.5 kg, equation 1 yields a maximum acceleration:

$$a_{max} = \frac{F_{max}}{m} = \frac{58,500N}{317.5 \, kg} = 184.3 \, \frac{m}{s^2} = 18.8 \, g's$$

Case 2: m = 300 kg

For a mass of 300 kg, this yields

$$a_{max} = \frac{F_{max}}{m} = \frac{58,500N}{300 \, kg} = 195 \frac{m}{s^2} = 19.9 \, g's$$

In both cases, $a_{max} < 40$ g's.

Average deceleration:

We used Matlab to calculate a displacement-averaged-force of 50.7 kN over our testing curve. For each displacement unit, we multiplied the differential displacement by the average force over that distance. Finally, we summed each of these products and divided by total displacement to generate a total average force.

Case 1: m=317.5 kg

For our mass of 317.5 kg, this yields an average acceleration:

$$a_{average} = \frac{F_{average}}{m} = \frac{50,700 \text{ N}}{317.5 \text{ kg}} = 159.7.3 \frac{m}{s^2} = 16.3 \text{ g/s}$$



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Case 2: m=300kg

For a mass of 300 kg, this yields

$$a_{average} = \frac{F_{average}}{m} = \frac{51,200 \text{ N}}{300 \text{ kg}} = 170.7 \frac{m}{s^2} = 17.4 \text{ g/s}$$

In both cases, $a_{average} < 20$ g's.

Total Absorbed Energy:

The Rules require that our impact attenuator decelerate our vehicle from 7 m/s, absorbing more than 7,350 Joules.

Generally, work done on a system at is given by:

3.
$$W = F * D$$

for a force "F", over a distance "D".

Thus, for a Force vs. Displacement curve, the work done on the attenuator is equivalent to the area under the curve. By conservation of energy, this total work is equivalent to total absorbed KE. We used Matlab to approximate this area as a sum of trapezoidal areas. For our total test displacement of 0.17 meters, we calculated:

Total Energy absorbed = 8,720 Joules

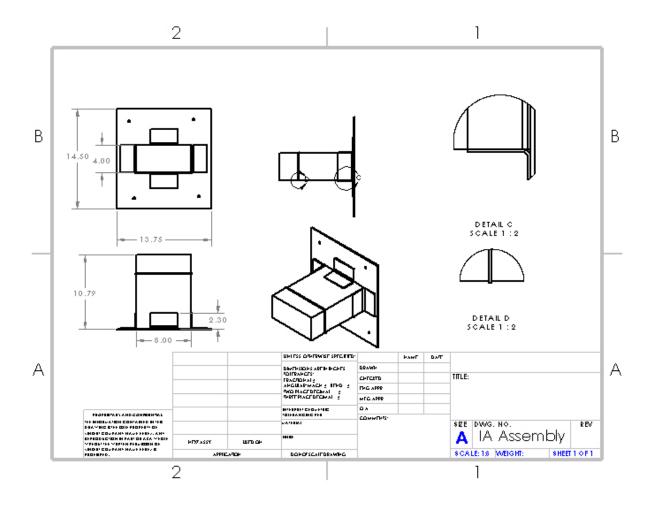
At 317.5 kg, our vehicle has Kinetic Energy given by:

2.
$$KE = \frac{1}{2}mv^2 = \frac{1}{2}(317.5 \text{ kg})\left(7\frac{m}{s}\right)^2 = 7,779 \text{ Joules}.$$

And 8,720J > 7779J > 7350J, so we can absorb enough energy.



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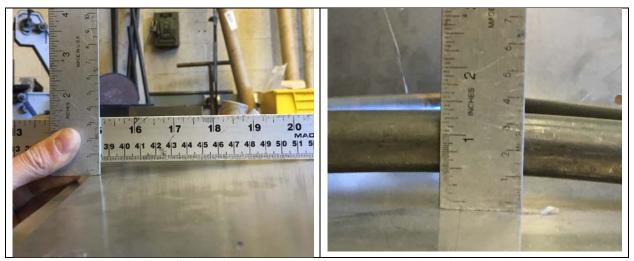
See attached drawings for improved size and quality.

Length (fore/aft direction): ___274.1_ mm (>=200mm) Width (lateral direction): __203.2_ mm (>=200mm) Height (vertical direction): __101.6_ mm (>=100mm)

Attenuator is at least 200mm wide by 100mm high for at least 200mm: **Yes**/No *Attach additional information below this point and/or on additional sheets*

Test schematic, photos of test, design report including reasons for selection and advantages/disadvantages, etc. Additional information shall be kept concise and relevant.

Additional Post-Test Photos



Figures 4a and 4b: (left) Deflection of Anti-intrusion plate, (right) Deflection of Bulkhead Diagonal Member

Design Selection:

We decided to use the same Aluminum honeycomb from our 2014 vehicle, as that attenuator performed well. Again, we opted for the industry standard pre-crushed 8*8*4 in aluminum 5052 5.7pcf 3/16" honeycomb because of its abundance and low-cost compared to a custom-built honeycomb.

To calculate the necessary length of our impact attenuator, we used the equation:

1.
$$W = F * D$$

The data sheet for our aluminum honeycomb states that the honeycomb crumples at a minimum pressure of 2.327 MPa. Multiplying this pressure by our cross-sectional area of 0.021 m² yields a minimum compression force of 48.9 kN. For this force, equation 1 yields a necessary minimum length of 0.16 m. After accounting for the roughly 75% stroke efficiency of the honeycomb (see attached data sheet) and 1 cm pre-crushed region, we concluded that we our impact attenuator must be at least 0.236 meters, or 9.3 inches long.

After adding a 15% safety margin we decided to stack another 2.6 in honeycomb with identical properties on top of the 8*8*4 block, thereby giving rise to our new impact attenuator with dimensions 10.6*8*4. This safety margin allows our car to strike a wall at 20 degrees and still absorb all of the vehicle's Kinetic Energy.

We bonded these pieces with WEST SYSTEM® Six10® Thickened Epoxy Adhesive. To increase surface area and improve resistance to shearing forces, we placed a 0.1 inch thick aluminum plate between the honeycomb pieces. Detailed information regarding the equivalency of the epoxy to the (4) 5/16 Grade 5 bolts stated in the rules T3.20.3 can be found in our SES rev1.

To attach the honeycomb system and the aluminum L brackets that help support the honeycomb on the anti-intrusion plate we again used WEST SYSTEM® Six10® Thickened Epoxy Adhesive. The aluminum L brackets provide an additional level of protection against shearing forces and enhances stability in the event of a linear impact.

We used 4 mm-thick aluminum for our anti-intrusion plate to facilitate bonding with the honeycomb and the L brackets, since they are aluminum as well.

In summary, the impact attenuator we designed for our 2016 car was optimized in terms of cost, weight and use of materials. We emphasized safety as a key point and thus over-engineered both our honeycomb system and our anti-intrusion plate to outperform the criteria of Formula SAE, as we believe that a few pounds and a few dollars are well spent to protect a human life.



CERTIFICATE OF CONFORMANCE

Date:

February 28, 2011

PURCHASE ORDER INFORMATION

Work Order Number:

276806

Size:

8.000" x 8.000" x 4.000"

Plascore Part Number:

IMPACT_ATTENUATOR

CORE INFORMATION

Core Type: Foil Type:

PAMG-XR1-5.7-3/16-P-5052

0.0020"

Measured Cell Size:

0.1875 inches

Measured Density:

5.7 pcf

Block Number:

005B0307

SAMPLE ONLY

(ACTUAL TEST RESULTS MAY VARY)

This is to certify that the aluminum honeycomb core supplied, meets the crush requirements of 375 psi +/- 10% per ASTM D 7336.

SAMPLE ONLY

٩M

ASTM D7336

(ACTUAL TEST RESULTS MAY VARY)

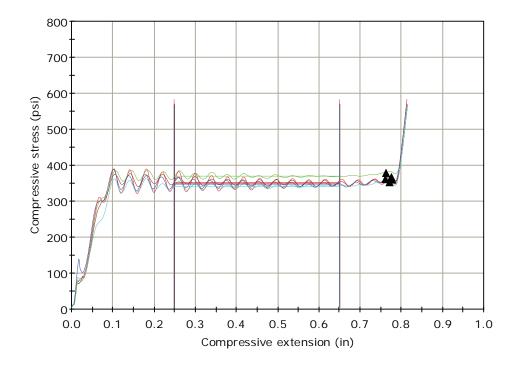
Sample file name: QC005B0307_CR

Honeycomb Type	Aluminum
Part Number	A57316P5052
Block Number	005B0307
Slice Location	27.750
Plascore Visual	Yes
Instron	1
Operator	JT
Room Temp (F)	70.0
Humidity (%)	50.0
Rate 1	1.00 in/min

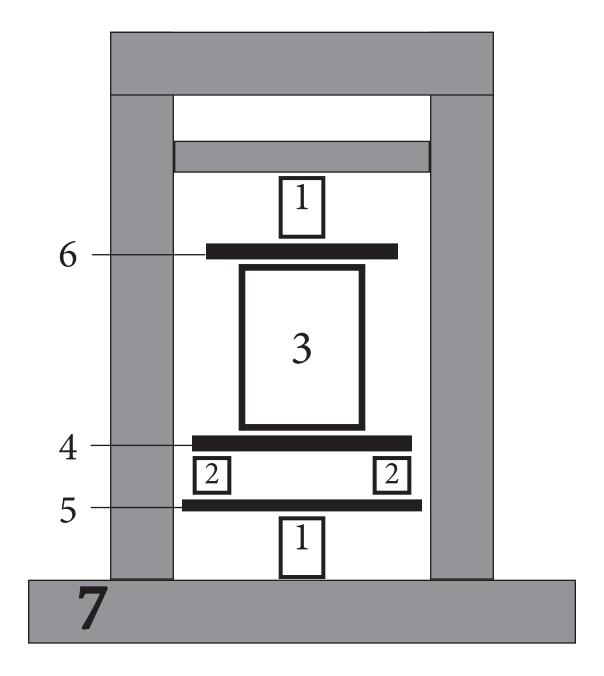
	Measured Cell (in)	Average Crush Strength (psi)	Stroke (%)	Test Result
1	0.203	351.0	77.7	Pass
2	0.196	352.8	77.5	Pass
3	0.190	370.5	76.2	Pass
4	0.210	342.3	77.0	Pass
5	0.200	348.3	76.0	Pass

Sample note 1 0.190"-0.210"

Stress vs Displacement Curve (English)







- 1: Platens
- 2: Spacers with h>2" to raise the IA system
- 3: IA Aluminum Honeycomb
- 4: Mock-up of Front Bulkhead
- 5: 0.75" thick T6 6061 aluminum support plate
- 6: Precision ground 1" thick aluminum plate to homogenize the force
- 7: Instron 5569 Dual Column Tabletop Universal Testing System

^{*}Parts 3, 4, 5, 6 drawn to 1:6 scale

Matlab Scripts: Test Data Processing

```
name = 'ImpactAttenuatorTestData.xlsx';
Data=xlsread(name);
%Displacement in meters, force in kN
Disp = Data(:,1) *.001;
Force = Data(:,2);
%totalE in kJ
TotalE=zeros(length(Force),1);
for i = 2:length(Force)
               TotalE(i) = TotalE(i-1) + ((Disp(i)-Disp(i-1))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((Force(i)+Force(i-1)))*((For
1))/2));
end
%distance averaged force
sumForce=0;
for i=1:length(Force)-1
                sumForce=sumForce+(Force(i)*(Disp(i+1)-Disp(i)));
end
%Fav in kN
Fav=sumForce/Disp(i+1);
figure
plot(Disp, Force);
title('Force vs Displacement')
xlabel('Displacement in meters')
ylabel('Force in kN')
figure
plot(Disp, TotalE);
title('Total Energy Absorbed vs Displacement')
xlabel('Displacement in meters')
ylabel('Total Energy Absorbed in KJ')
```

