

Section1.1

线性声波在密度为 ρ_0 的均匀静止理想流体介质中以速度 c_0 传播，声学压力和声学速度用 p' 和 u' 表示，速度势函数用 ϕ 表示，证明：

(1) 声压可以表示为

$$p' = -\rho_0 \frac{\partial \phi}{\partial t}.$$

已知线化声学动量方程：

$$\rho_0 \frac{\partial u'}{\partial t} + \nabla p' = 0 \quad (1)$$

代入势函数：

$$u' = \nabla \phi \quad (2)$$

得到：

$$\begin{aligned} \nabla p' &= -\rho_0 \frac{\partial u'}{\partial t} \\ &= -\rho_0 \frac{\partial (\nabla \phi)}{\partial t} \\ &= \nabla \left(-\rho_0 \frac{\partial \phi}{\partial t} \right) \end{aligned} \quad (3)$$

由上式可得：

$$p' = -\rho_0 \frac{\partial \phi}{\partial t} \quad (4)$$

原式得证。

(2) 势函数和声学速度满足波动方程

$$\frac{1}{c_0^2} \frac{\partial^2 \phi}{\partial t^2} - \nabla^2 \phi = 0, \quad \frac{1}{c_0^2} \frac{\partial^2 u'}{\partial t^2} - \nabla^2 u' = 0.$$

已知声学波动方程：

$$\frac{1}{c_0^2} \frac{\partial^2 p'}{\partial t^2} - \nabla^2 p' = 0 \quad (5)$$

代入(4)式，得：

$$\begin{aligned} \frac{1}{c_0^2} (-\rho_0) \frac{\partial^2}{\partial t^2} \left(\frac{\partial \phi}{\partial t} \right) - (-\rho_0) \nabla^2 \left(\frac{\partial \phi}{\partial t} \right) &= 0 \\ \frac{\partial}{\partial t} \left[\frac{1}{c_0^2} \frac{\partial^2 \phi}{\partial t^2} \right] - \frac{\partial}{\partial t} [\nabla^2 \phi] &= 0 \end{aligned} \quad (6)$$

两边对 t 积分，得：

$$\frac{1}{c_0^2} \frac{\partial^2 \phi}{\partial t^2} - \nabla^2 \phi = 0 \quad (7)$$

第一式得证。

将(7)式两边求梯度，得：

$$\begin{aligned}\nabla \left(\frac{1}{c_0^2} \frac{\partial^2 \phi}{\partial t^2} \right) - \nabla^3 \phi &= 0 \\ \frac{1}{c_0^2} \frac{\partial^2 (\nabla \phi)}{\partial t^2} - \nabla^2 (\nabla \phi) &= 0\end{aligned}\tag{8}$$

代入势函数（式(2)），得：

$$\frac{1}{c_0^2} \frac{\partial^2 u'}{\partial t^2} - \nabla^2 u' = 0\tag{9}$$

第二式得证。

Section1.2

1. 证明自由空间格林函数的偏导数关系:

$$\frac{\partial G_0}{\partial y_i} = \frac{x_i - y_i}{r} \left[\frac{1}{4\pi r c_0} \frac{\partial}{\partial \tau} \delta(t - \tau - r/c_0) + \frac{\delta(t - \tau - r/c_0)}{4\pi r^2} \right].$$

已知自由空间格林函数:

$$G_0 = \frac{1}{4\pi r} \delta\left(t - \tau - \frac{r}{c_0}\right) \quad (10)$$

对 r 求偏导, 得:

$$\begin{aligned} \frac{\partial G_0}{\partial r} &= -\frac{1}{4\pi r^2} \delta\left(t - \tau - \frac{r}{c_0}\right) + \frac{1}{4\pi r} \frac{\partial \delta\left(t - \tau - \frac{r}{c_0}\right)}{\partial r} \\ &= -\frac{1}{4\pi r^2} \delta\left(t - \tau - \frac{r}{c_0}\right) + \frac{1}{4\pi r} \frac{\partial \delta\left(t - \tau - \frac{r}{c_0}\right)}{\partial \tau} \frac{\partial \tau}{\partial r} \end{aligned} \quad (11)$$

由 τ 与 r 的关系式 $\tau = t - \frac{r}{c_0}$ 可得:

$$\frac{\partial \tau}{\partial r} = -\frac{1}{c_0} \quad (12)$$

代入式(11), 得

$$\frac{\partial G_0}{\partial r} = -\frac{1}{4\pi r^2} \delta\left(t - \tau - \frac{r}{c_0}\right) - \frac{1}{4\pi r c_0} \frac{\partial \delta\left(t - \tau - \frac{r}{c_0}\right)}{\partial \tau} \quad (13)$$

根据 r 对 y_i 的偏导数:

$$\frac{\partial r}{\partial y_i} = \frac{\partial \sqrt{\sum (x_i - y_i)^2}}{\partial y_i} = -\frac{x_i - y_i}{r} \quad (14)$$

结合式(13),(14), 得:

$$\begin{aligned} \frac{\partial G_0}{\partial y_i} &= \frac{\partial G_0}{\partial r} \frac{\partial r}{\partial y_i} \\ &= \frac{x_i - y_i}{r} \left[\frac{1}{4\pi r c_0} \frac{\partial}{\partial \tau} \delta(t - \tau - r/c_0) + \frac{\delta(t - \tau - r/c_0)}{4\pi r^2} \right] \end{aligned} \quad (15)$$

原式得证。

2. 利用上述自由空间格林函数的偏导数关系式证明

$$p'(\mathbf{x}, t) = - \int_{-\infty}^{+\infty} \int_S \rho_0 \frac{\partial u_n(\mathbf{y}, \tau)}{\partial \tau} G(\mathbf{x}, \mathbf{y}, t - \tau) dS d\tau - \int_{-\infty}^{+\infty} \int_S p'(\mathbf{y}, \tau) \frac{\partial G(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial y_i} n_i dS d\tau$$

可以改写为

$$p'(\mathbf{x}, t) = - \int_S \left[\rho_0 \frac{\partial u_n}{\partial \tau} \right]_{\tau} \frac{dS(\mathbf{y})}{4\pi r} - \int_S \left[\frac{\partial p'}{\partial \tau} n_i + \frac{p' n_i c_0}{r} \right]_{\tau} \frac{(x_i - y_i) dS(\mathbf{y})}{4\pi r^2 c_0}.$$

原式右侧第一项代入自由格林函数，并对 τ 求积分：

$$\begin{aligned} \text{右侧第一项} &= - \int_{-\infty}^{+\infty} \int_S \rho_0 \frac{\partial u_n(\mathbf{y}, \tau)}{\partial \tau} G_0(\mathbf{x}, \mathbf{y}, t - \tau) dS d\tau \\ &= - \int_S \int_{-\infty}^{+\infty} \rho_0 \frac{\partial u_n(\mathbf{y}, \tau)}{\partial \tau} \frac{1}{4\pi r} \delta(\mathbf{x}, \mathbf{y}, t - \tau) d\tau dS \quad (16) \\ &= - \int_S \left[\rho_0 \frac{\partial u_n}{\partial \tau} \right]_{\tau} \frac{dS(\mathbf{y})}{4\pi r} \end{aligned}$$

原式右侧第二项代入自由格林函数偏导数关系式（式(15)）：

$$\begin{aligned} \text{右侧第二项} &= - \int_{-\infty}^{+\infty} \int_S p'(\mathbf{y}, \tau) \frac{x_i - y_i}{r} \left[\frac{1}{4\pi r c_0} \frac{\partial}{\partial \tau} \delta \left(t - \tau - \frac{r}{c_0} \right) \right. \\ &\quad \left. + \frac{\delta \left(t - \tau - \frac{r}{c_0} \right)}{4\pi r^2} \right] n_i dS d\tau \quad (17) \\ &= - \int_S \left[\int_{-\infty}^{+\infty} p'(\mathbf{y}, \tau) \frac{\partial}{\partial \tau} \delta \left(t - \tau - \frac{r}{c_0} \right) n_i d\tau \right] \frac{(x_i - y_i) dS}{4\pi r^2 c_0} \\ &\quad - \int_S \left[\int_{-\infty}^{+\infty} p'(\mathbf{y}, \tau) \frac{c_0}{r} \delta \left(t - \tau - \frac{r}{c_0} \right) n_i d\tau \right] \frac{(x_i - y_i) dS}{4\pi r^2 c_0} \end{aligned}$$

其中：

$$\begin{aligned} \int_{-\infty}^{+\infty} p'(\mathbf{y}, \tau) \frac{\partial}{\partial \tau} \delta \left(t - \tau - \frac{r}{c_0} \right) n_i d\tau &= -p'(\mathbf{y}, \tau) \delta \left(t - \tau - \frac{r}{c_0} \right) n_i \Big|_{\tau=-\infty}^{\tau=\infty} \\ &\quad - \int_{-\infty}^{+\infty} -\frac{\partial p'(\mathbf{y}, \tau)}{\partial \tau} \delta \left(t - \tau - \frac{r}{c_0} \right) d\tau \quad (18) \end{aligned}$$

根据 t 与 τ 的因果关系，有：

$$-p'(\mathbf{y}, \tau) \delta \left(t - \tau - \frac{r}{c_0} \right) n_i \Big|_{\tau=-\infty}^{\tau=\infty} = 0 \quad (19)$$

因此有：

$$\begin{aligned} \int_{-\infty}^{+\infty} p'(\mathbf{y}, \tau) \frac{\partial}{\partial \tau} \delta \left(t - \tau - \frac{r}{c_0} \right) n_i d\tau &= - \int_{-\infty}^{+\infty} - \frac{\partial p'(\mathbf{y}, \tau)}{\partial \tau} \delta \left(t - \tau - \frac{r}{c_0} \right) d\tau \\ &= \left[\frac{\partial p'}{\partial \tau} n_i \right]_{\tau} \end{aligned} \quad (20)$$

同时，式(17)中：

$$\int_{-\infty}^{+\infty} p'(\mathbf{y}, \tau) \frac{c_0}{r} \delta \left(t - \tau - \frac{r}{c_0} \right) n_i d\tau = \left[\frac{p' n_i c_0}{r} \right]_{\tau} \quad (21)$$

将式(20),(21)代入式(17)，得：

$$\begin{aligned} \text{右侧第二项} &= - \int_S \left[\frac{\partial p'}{\partial \tau} n_i \right]_{\tau} \frac{(x_i - y_i) dS}{4\pi r^2 c_0} - \int_S \left[\frac{p' n_i c_0}{r} \right]_{\tau} \frac{(x_i - y_i) dS}{4\pi r^2 c_0} \\ &= - \int_S \left[\frac{\partial p'}{\partial \tau} n_i + \frac{p' n_i c_0}{r} \right]_{\tau} \frac{(x_i - y_i) dS}{4\pi r^2 c_0} \end{aligned} \quad (22)$$

结合式(16),(22)，得：

$$p'(\mathbf{x}, t) = - \int_S \left[\rho_0 \frac{\partial u_n}{\partial \tau} \right]_{\tau} \frac{dS(\mathbf{y})}{4\pi r} - \int_S \left[\frac{\partial p'}{\partial \tau} n_i + \frac{p' n_i c_0}{r} \right]_{\tau} \frac{(x_i - y_i) dS(\mathbf{y})}{4\pi r^2 c_0} \quad (23)$$

原式得证。

Section1.3

1. 定义任意时域函数 $f(t)$ 和 $h(t)$, 通过 Fourier 变换得到的频域函数分别为 $\tilde{f}(\omega)$ 和 $\tilde{h}(\omega)$, 利用 Fourier 变换定义证明下述关系式成立:

(1) 如果 $f(t) = \int_{-\infty}^{\infty} h(\tau)G(\mathbf{x}, \mathbf{y}, t - \tau)d\tau$, 则有 $\tilde{f}(\omega) = \tilde{h}(\omega)\tilde{G}(\mathbf{x}, \mathbf{y}, \omega)$ 。

根据 Fourier 变换, 有:

$$\begin{aligned}
 \tilde{f}(\omega) &= \int_{-\infty}^{\infty} f(t)e^{i\omega t}dt \\
 &= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} h(\tau)G(\mathbf{x}, \mathbf{y}, t - \tau)d\tau e^{i\omega t}dt \\
 &= \int_{-\infty}^{\infty} h(\tau) \left[\int_{-\infty}^{\infty} G(\mathbf{x}, \mathbf{y}, t - \tau)e^{i\omega(t-\tau)}dt \right] e^{i\omega\tau}d\tau \\
 &= \int_{-\infty}^{\infty} h(\tau)\tilde{G}(\mathbf{x}, \mathbf{y}, \omega)e^{i\omega\tau}d\tau \\
 &= \tilde{G}(\mathbf{x}, \mathbf{y}, \omega) \int_{-\infty}^{\infty} h(\tau)e^{i\omega\tau}d\tau \\
 &= \tilde{h}(\omega)\tilde{G}(\mathbf{x}, \mathbf{y}, \omega)
 \end{aligned} \tag{24}$$

原式得证。

(2) 如果 $f(t) = \int_{-\infty}^{\infty} h(\tau)\frac{\partial G(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial \tau}d\tau$, 则有 $\tilde{f}(\omega) = -i\omega\tilde{h}(\omega)\tilde{G}(\mathbf{x}, \mathbf{y}, \omega)$ 。

根据分步积分, 有:

$$\begin{aligned}
 f(\omega) &= \int_{-\infty}^{\infty} h(\tau)\frac{\partial G(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial \tau}d\tau \\
 &= -h(\tau)G(\mathbf{x}, \mathbf{y}, t - \tau)|_{\tau=-\infty}^{\tau=\infty} - \int_{-\infty}^{\infty} -\frac{\partial h(\tau)}{\partial \tau}G(\mathbf{x}, \mathbf{y}, t - \tau)d\tau
 \end{aligned} \tag{25}$$

根据 t 与 τ 的因果关系, 有:

$$-h(\tau)G(\mathbf{x}, \mathbf{y}, t - \tau)|_{\tau=-\infty}^{\tau=\infty} = 0 \tag{26}$$

因此有:

$$f(\omega) = \int_{-\infty}^{\infty} \frac{\partial h(\tau)}{\partial \tau}G(\mathbf{x}, \mathbf{y}, t - \tau)d\tau \tag{27}$$

根据 Fourier 变换，有：

$$\begin{aligned}
\tilde{f}(\omega) &= \int_{-\infty}^{\infty} f(t) e^{i\omega t} dt \\
&= \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \frac{\partial h(\tau)}{\partial \tau} G(\mathbf{x}, \mathbf{y}, t - \tau) d\tau e^{i\omega t} dt \\
&= \int_{-\infty}^{\infty} \frac{\partial h(\tau)}{\partial \tau} \left[\int_{-\infty}^{\infty} G(\mathbf{x}, \mathbf{y}, t - \tau) e^{i\omega(t-\tau)} dt \right] e^{i\omega\tau} d\tau \quad (28) \\
&= \tilde{G}(\mathbf{x}, \mathbf{y}, \omega) \int_{-\infty}^{\infty} \frac{\partial h(\tau)}{\partial \tau} e^{i\omega\tau} d\tau \\
&= -i\omega \tilde{h}(\omega) \tilde{G}(\mathbf{x}, \mathbf{y}, \omega)
\end{aligned}$$

原式得证。

2. 根据波动方程的时域解，证明频域积分解可以写为

$$\tilde{p}'(\mathbf{x}, \omega) = \int_S i\omega \rho_0 \tilde{u}_n(\mathbf{y}, \omega) \tilde{G}(\mathbf{x}, \mathbf{y}, \omega) dS - \int_S \tilde{p}'(\mathbf{y}, \omega) \frac{\partial \tilde{G}(\mathbf{x}, \mathbf{y}, \omega)}{\partial \mathbf{n}} dS.$$

已知声学波动方程的时域解:

$$\begin{aligned} p'(\mathbf{x}, t) = & - \int_{-\infty}^{+\infty} \int_S \rho_0 \frac{\partial u_n(\mathbf{y}, \tau)}{\partial \tau} G(\mathbf{x}, \mathbf{y}, t - \tau) dS d\tau \\ & - \int_{-\infty}^{+\infty} \int_S p'(\mathbf{y}, \tau) \frac{\partial G(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial \mathbf{n}} dS d\tau \end{aligned} \quad (29)$$

对上式进行 Fourier 变换:

$$\begin{aligned} \tilde{p}'(\mathbf{x}, \omega) = & \int_{-\infty}^{+\infty} \left[- \int_{-\infty}^{+\infty} \int_S \rho_0 \frac{\partial u_n(\mathbf{y}, \tau)}{\partial \tau} G(\mathbf{x}, \mathbf{y}, t - \tau) dS d\tau \right. \\ & \left. - \int_{-\infty}^{+\infty} \int_S p'(\mathbf{y}, \tau) \frac{\partial G(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial \mathbf{n}} dS d\tau \right] e^{i\omega t} dt \\ = & - \int_S \left[\int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \rho_0 \frac{\partial u_n(\mathbf{y}, \tau)}{\partial \tau} G(\mathbf{x}, \mathbf{y}, t - \tau) e^{i\omega t} d\tau dt \right] dS \\ & - \int_S \left[\int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} p'(\mathbf{y}, \tau) \frac{\partial G(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial \mathbf{n}} e^{i\omega t} d\tau dt \right] dS \end{aligned} \quad (30)$$

由第一题中的结论，式(27)、(28)可得:

$$\begin{aligned} & \int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} \rho_0 \frac{\partial u_n(\mathbf{y}, \tau)}{\partial \tau} G(\mathbf{x}, \mathbf{y}, t - \tau) e^{i\omega t} d\tau dt \\ = & - i\omega \rho_0 \tilde{u}_n(\mathbf{y}, \omega) \tilde{G}(\mathbf{x}, \mathbf{y}, \omega) \end{aligned} \quad (31)$$

有第一题中的结论，式(24)可得:

$$\int_{-\infty}^{+\infty} \int_{-\infty}^{+\infty} p'(\mathbf{y}, \tau) \frac{\partial G(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial \mathbf{n}} e^{i\omega t} d\tau dt = \tilde{p}'(\mathbf{y}, \omega) \frac{\partial \tilde{G}(\mathbf{x}, \mathbf{y}, \omega)}{\partial \mathbf{n}} \quad (32)$$

将式(31)、(32)代入式(30)得:

$$\tilde{p}'(\mathbf{x}, \omega) = \int_S i\omega \rho_0 \tilde{u}_n(\mathbf{y}, \omega) \tilde{G}(\mathbf{x}, \mathbf{y}, \omega) dS - \int_S \tilde{p}'(\mathbf{y}, \omega) \frac{\partial \tilde{G}(\mathbf{x}, \mathbf{y}, \omega)}{\partial \mathbf{n}} dS \quad (33)$$

原式得证。

Section 2.1

1. Lighthill 声比拟方程能直接应用于高 Ma 流动诱发的气动噪声问题吗?
不能。(1)Lighthill 声比拟方程假设空气介质是均匀静止的, 但该条件不能适用于高马赫数流动; (2)Lighthill 声比拟方程没有考虑能量输运作用; (3)Lighthill 声比拟方程仅适用于弱可压缩流动, 不适用于高马赫数下的强可压缩流动。
2. 从 Lighthill 声比拟方程出发, 详细证明方程的时域积分为
根据声比拟方程, 有:

$$p'(\mathbf{x}, \tau) = \int_{-\infty}^{\infty} \int_V G \frac{\partial^2 T_{ij}(\mathbf{y}, \tau)}{\partial y_i \partial y_j} dV d\tau \quad (34)$$

根据分部积分, 有:

$$G \frac{\partial^2 T_{ij}}{\partial y_i \partial y_j} = T_{ij} \frac{\partial^2 G}{\partial y_i \partial y_j} + \frac{\partial}{\partial y_i} \left(G \frac{\partial T_{ij}}{\partial y_j} \right) - \frac{\partial}{\partial y_j} \left(T_{ij} \frac{\partial G}{\partial y_i} \right) \quad (35)$$

因此有:

$$\begin{aligned} \int_{-\infty}^{\infty} \int_V G \frac{\partial^2 T_{ij}}{\partial y_i \partial y_j} dV d\tau &= \int_{-\infty}^{\infty} \int_V T_{ij} \frac{\partial^2 G}{\partial y_i \partial y_j} dV d\tau \\ &\quad + \int_{-\infty}^{\infty} \int_V \frac{\partial}{\partial y_i} \left(G \frac{\partial T_{ij}}{\partial y_j} \right) dV d\tau \\ &\quad - \int_{-\infty}^{\infty} \int_V \frac{\partial}{\partial y_j} \left(T_{ij} \frac{\partial G}{\partial y_i} \right) dV d\tau \end{aligned} \quad (36)$$

注意到 $T_{ij} = T_{ji}$, 因此有:

$$\begin{aligned} \int_{-\infty}^{\infty} \int_V G \frac{\partial^2 T_{ij}}{\partial y_i \partial y_j} dV d\tau &= \int_{-\infty}^{\infty} \int_V T_{ij} \frac{\partial^2 G}{\partial y_i \partial y_j} dV d\tau \\ &\quad + \int_{-\infty}^{\infty} \int_V \frac{\partial}{\partial y_j} \left[G \frac{\partial T_{ij}}{\partial y_i} - T_{ij} \frac{\partial G}{\partial y_i} \right] dV d\tau \end{aligned} \quad (37)$$

应用高斯散度定理, 有:

$$\begin{aligned} \int_{-\infty}^{\infty} \int_V G \frac{\partial^2 T_{ij}}{\partial y_i \partial y_j} dV d\tau &= \int_{-\infty}^{\infty} \int_V T_{ij} \frac{\partial^2 G}{\partial y_i \partial y_j} dV d\tau \\ &\quad + \int_{-\infty}^{\infty} \int_S \left[G \frac{\partial T_{ij}}{\partial y_i} - T_{ij} \frac{\partial G}{\partial y_i} \right] n_i dS d\tau \end{aligned} \quad (38)$$

对于 Lighthill 声比拟方程, S 为无穷大, 因此有:

$$\int_{-\infty}^{\infty} \int_S \left[G \frac{\partial T_{ij}}{\partial y_i} - T_{ij} \frac{\partial G}{\partial y_i} \right] n_i dS d\tau = 0 \quad (39)$$

因此:

$$\begin{aligned} p'(\mathbf{x}, \tau) &= \int_{-\infty}^{\infty} \int_V G \frac{\partial^2 T_{ij}(\mathbf{y}, \tau)}{\partial y_i \partial y_j} dV d\tau \\ &= \int_{-\infty}^{\infty} \int_V T_{ij}(\mathbf{y}, \tau) \frac{\partial^2 G}{\partial y_i \partial y_j} dV d\tau \end{aligned} \quad (40)$$

代入自由空间格林函数 G_0 , 有:

$$p'(\mathbf{x}, \tau) = \int_{-\infty}^{\infty} \int_V T_{ij}(\mathbf{y}, \tau) \frac{\partial^2 G_0(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial y_i \partial y_j} dV d\tau \quad (41)$$

自由空间格林函数 G_0 满足:

$$\frac{\partial^2 G_0}{\partial y_i \partial y_j} = \frac{\partial^2 G_0}{\partial x_i \partial x_j} \quad (42)$$

因此有:

$$\begin{aligned} p'(\mathbf{x}, \tau) &= \int_{-\infty}^{\infty} \int_V T_{ij}(\mathbf{y}, \tau) \frac{\partial^2 G_0(\mathbf{x}, \mathbf{y}, t - \tau)}{\partial x_i \partial x_j} d^3 \mathbf{y} d\tau \\ &= \frac{\partial^2}{\partial x_i \partial x_j} \int_V \int_{-\infty}^{\infty} T_{ij}(\mathbf{y}, \tau) G_0(\mathbf{x}, \mathbf{y}, t - \tau) d\tau d^3 \mathbf{y} \\ &= \frac{\partial^2}{\partial x_i \partial x_j} \int_V \int_{-\infty}^{\infty} T_{ij}(\mathbf{y}, \tau) \frac{\delta(t - \tau - r/c_0)}{4\pi r} d\tau d^3 \mathbf{y} \\ &= \frac{1}{4\pi} \frac{\partial^2}{\partial x_i \partial x_j} \int_V \frac{T_{ij}(\mathbf{y}, t - r/c_0)}{r} d^3 \mathbf{y} \end{aligned} \quad (43)$$

原式得证。

Section 2.2

1. 已知三维频域自由空间格林函数为 $G_0(\mathbf{x}, \mathbf{y}, \omega) = \frac{e^{ikr}}{4\pi r}$ ，推导 $\frac{\partial G_0}{\partial y_i}$ 和 $\frac{\partial^2 G_0}{\partial y_i \partial y_j}$ 的解析表达式。

已知，在三维频域下：

$$r = \sqrt{\sum_{i=1}^{n=3} (x_i - y_i)^2} \quad (44)$$

因此有：

$$\begin{aligned} \frac{\partial G_0}{\partial y_i} &= \frac{\partial}{\partial r} \left(\frac{e^{ikr}}{4\pi r} \right) \frac{\partial r}{\partial y_i} \\ &= \frac{ikr e^{ikr} - e^{ikr}}{4\pi r^2} \frac{\partial \sqrt{\sum_{i=1}^{n=3} (x_i - y_i)^2}}{\partial y_i} \\ &= \left(\frac{ik}{4\pi r} - \frac{1}{4\pi r^2} \right) e^{ikr} \left(-\frac{x_i - y_i}{r} \right) \\ &= \frac{x_i - y_i}{r} \left(\frac{e^{ikr}}{4\pi r^2} - \frac{ike^{ikr}}{4\pi r} \right) \end{aligned} \quad (45)$$

同理有：

$$\begin{aligned} \frac{\partial^2 G_0}{\partial y_i \partial y_j} &= \frac{\partial}{\partial y_j} \left(\frac{\partial G_0}{\partial y_i} \right) \\ &= \frac{\partial}{\partial r} \left(\frac{\partial G_0}{\partial y_i} \right) \frac{\partial r}{\partial y_j} \\ &= \frac{x_i - y_i}{r^2} \left(-\frac{3e^{ikr}}{4\pi r^2} + \frac{3ike^{ikr}}{4\pi r} + \frac{k^2 e^{ikr}}{4\pi} \right) \left(-\frac{x_j - y_j}{r} \right) \\ &= \frac{(x_i - y_i)(x_j - y_j)}{r^3} \left(\frac{3e^{ikr}}{4\pi r^2} - \frac{3ike^{ikr}}{4\pi r} - \frac{k^2 e^{ikr}}{4\pi} \right) \end{aligned} \quad (46)$$

综上，

$$\frac{\partial G_0}{\partial y_i} = \frac{x_i - y_i}{r} \left(\frac{e^{ikr}}{4\pi r^2} - \frac{ike^{ikr}}{4\pi r} \right) \quad (47)$$

$$\frac{\partial^2 G_0}{\partial y_i \partial y_j} = \frac{(x_i - y_i)(x_j - y_j)}{r^3} \left(\frac{3e^{ikr}}{4\pi r^2} - \frac{3ike^{ikr}}{4\pi r} - \frac{k^2 e^{ikr}}{4\pi} \right) \quad (48)$$

2. 假设静止固体表面是可穿透的，并忽略粘性的贡献，写出 Curle 方程的频域积分公式。

已知忽略粘性贡献的 Curle 方程为：

$$\begin{aligned} c_0^2 \rho'(\mathbf{x}, t) = & \int_V \int_{-\infty}^{+\infty} T_{ij} \frac{\partial^2 G}{\partial y_i \partial y_j} d^3 \mathbf{y} d\tau \\ & - \int_S \int_{-\infty}^{+\infty} (\rho u_i u_j + p_{ij}) n_j \frac{\partial G}{\partial y_i} d^2 \mathbf{y} d\tau \\ & - \int_S \int_{-\infty}^{+\infty} G \frac{\partial (\rho u_j n_j)}{\partial \tau} d^2 \mathbf{y} d\tau \end{aligned} \quad (49)$$

不妨设：

$$F_i(\mathbf{y}, \tau) = (\rho u_i u_j + p_{ij}) n_j \quad (50)$$

$$Q(\mathbf{y}, \tau) = \rho u_j n_j \quad (51)$$

代入自由格林函数 G_0 ，根据 G_0 的性质：

$$\frac{\partial G_0}{\partial y_i} = -\frac{\partial G_0}{\partial x_i} \quad (52)$$

$$\frac{\partial^2 G_0}{\partial y_i \partial y_j} = \frac{\partial^2 G_0}{\partial x_i \partial x_j} \quad (53)$$

可以得到：

$$\begin{aligned} c_0^2 \rho'(\mathbf{x}, t) = & \frac{\partial^2}{\partial x_i \partial x_j} \int_{-\infty}^{+\infty} \int_V T_{ij}(\mathbf{y}, \tau) G_0 d^3 \mathbf{y} d\tau \\ & + \frac{\partial}{\partial x_i} \int_{-\infty}^{+\infty} \int_S F_i(\mathbf{y}, \tau) G_0 d^2 \mathbf{y} d\tau \\ & - \int_{-\infty}^{+\infty} \int_S \frac{\partial Q(\mathbf{y}, \tau)}{\partial \tau} G_0 d^2 \mathbf{y} d\tau \\ = & \frac{\partial^2}{\partial x_i \partial x_j} \int_V [T_{ij}(\mathbf{y}, t - r/c_0)]_{\tau=t-r/c_0} \frac{d^3 \mathbf{y}}{4\pi r} \\ & + \frac{\partial}{\partial x_i} \int_S [F_i(\mathbf{y}, t - r/c_0)]_{\tau=t-r/c_0} \frac{d^2 \mathbf{y}}{4\pi r} \\ & - \int_S \left[\frac{\partial}{\partial \tau} Q(\mathbf{y}, t - r/c_0) \right]_{\tau=t-r/c_0} \frac{d^2 \mathbf{y}}{4\pi r} \end{aligned} \quad (54)$$

根据 Fourier 变换，可得：

$$\begin{aligned}
(c_0^2 \tilde{\rho}'(\mathbf{x}, \omega))_{quadrupole} &= \frac{\partial^2}{\partial x_i \partial x_j} \int_V \int_{-\infty}^{+\infty} T_{ij}(\mathbf{y}, t - r/c_0) e^{i\omega t} dt \frac{d^3 \mathbf{y}}{4\pi r} \\
&= \frac{\partial^2}{\partial x_i \partial x_j} \int_V \widetilde{T}_{ij}(\mathbf{y}, \omega) e^{i\omega r/c_0} \frac{d^3 \mathbf{y}}{4\pi r}
\end{aligned} \tag{55}$$

同理有：

$$\begin{aligned}
(c_0^2 \tilde{\rho}'(\mathbf{x}, \omega))_{dipole} &= \frac{\partial}{\partial x_i} \int_S \int_{-\infty}^{+\infty} F_i(\mathbf{y}, t - r/c_0) e^{i\omega t} dt \frac{d^2 \mathbf{y}}{4\pi r} \\
&= \frac{\partial}{\partial x_i} \int_S \widetilde{F}_i(\mathbf{y}, \omega) e^{i\omega r/c_0} \frac{d^2 \mathbf{y}}{4\pi r}
\end{aligned} \tag{56}$$

根据 Fourier 变换的偏分性质，可得：

$$\begin{aligned}
(c_0^2 \tilde{\rho}'(\mathbf{x}, \omega))_{monopole} &= \int_S \int_{-\infty}^{+\infty} \frac{\partial}{\partial \tau} [Q(\mathbf{y}, t - r/c_0)] e^{i\omega t} dt \frac{d^2 \mathbf{y}}{4\pi r} \\
&= \int_S -i\omega \widetilde{Q}(\mathbf{y}, \omega) e^{i\omega r/c_0} \frac{d^2 \mathbf{y}}{4\pi r}
\end{aligned} \tag{57}$$

综上，curle 方程的频域积分表达式为：

$$\begin{aligned}
c_0^2 \tilde{\rho}'(\mathbf{x}, \omega) &= \frac{\partial^2}{\partial x_i \partial x_j} \int_V \widetilde{T}_{ij}(\mathbf{y}, \omega) e^{i\omega r/c_0} \frac{d^3 \mathbf{y}}{4\pi r} \\
&+ \frac{\partial}{\partial x_i} \int_S \widetilde{F}_i(\mathbf{y}, \omega) e^{i\omega r/c_0} \frac{d^2 \mathbf{y}}{4\pi r} \\
&+ \int_S i\omega \widetilde{Q}(\mathbf{y}, \omega) e^{i\omega r/c_0} \frac{d^2 \mathbf{y}}{4\pi r}
\end{aligned} \tag{58}$$

Section2.3

1. 针对声学远场，证明近似表达式：

$$\frac{\partial^2}{\partial x_i \partial x_j} \left[\frac{T_{ij}(\mathbf{y})}{r} \right] \approx \frac{1}{c_0^2} \frac{(x_i - y_i)(x_j - y_j)}{r^3} \left[\frac{\partial^2 T_{ij}(\mathbf{y})}{\partial \tau^2} \right].$$

根据偏分法则可以得到：

$$\begin{aligned} \frac{\partial^2}{\partial x_i \partial x_j} \left[\frac{T_{ij}(\mathbf{y})}{r} \right] &= \left[\frac{\partial^2 T_{ij}(\mathbf{y})}{\partial \tau^2} \right] \frac{1}{r} \frac{\partial \tau}{\partial x_i} \frac{\partial \tau}{\partial x_j} \\ &+ 2 \left[\frac{\partial T_{ij}(\mathbf{y})}{\partial \tau} \right] \frac{\partial \tau}{\partial x_i} \frac{\partial(1/r)}{\partial x_i} + [T_{ij}(\mathbf{y})] \frac{\partial(1/r)}{\partial x_i \partial x_j} \end{aligned} \quad (59)$$

对于声学远场，可以将忽略上式中的 r^{-2} 和 r^{-3} 项，因此有：

$$\frac{\partial^2}{\partial x_i \partial x_j} \left[\frac{T_{ij}(\mathbf{y})}{r} \right] \approx \left[\frac{\partial^2 T_{ij}(\mathbf{y})}{\partial \tau^2} \right] \frac{1}{r} \frac{\partial \tau}{\partial x_i} \frac{\partial \tau}{\partial x_j} \quad (60)$$

其中，

$$\frac{\partial \tau}{\partial x_i} = \frac{\partial \tau}{\partial r} \frac{\partial r}{\partial x_i} \quad (61)$$

根据 τ 与 r 关系式：

$$\tau = t - \frac{r}{c_0} \quad (62)$$

有：

$$\frac{\partial \tau}{\partial r} = -\frac{1}{c_0} \quad (63)$$

又因为：

$$\frac{\partial r}{\partial x_i} = \frac{\partial \sqrt{\sum (x_i - y_i)^2}}{\partial x_i} = \frac{x_i - y_i}{r} \quad (64)$$

因此有：

$$\frac{\partial \tau}{\partial x_i} = -\frac{1}{c_0} \frac{x_i - y_i}{r} \quad (65)$$

同理：

$$\frac{\partial \tau}{\partial x_j} = -\frac{1}{c_0} \frac{x_j - y_j}{r} \quad (66)$$

代入式(60)，得：

$$\frac{\partial^2}{\partial x_i \partial x_j} \left[\frac{T_{ij}(\mathbf{y})}{r} \right] \approx \frac{1}{c_0^2} \frac{(x_i - y_i)(x_j - y_j)}{r^3} \left[\frac{\partial^2 T_{ij}(\mathbf{y})}{\partial \tau^2} \right] \quad (67)$$

原式得证。

2. 对于等熵流动, $\frac{\partial^2}{\partial \tau^2} (p' - c_0^2 \rho') = 0$ 一定成立吗?

不一定。 $p' = c_0^2 \rho'$ 成立的前提是均匀介质, 对于梯度较大的介质, $p' \neq c_0^2 \rho'$, 因此, $\frac{\partial^2}{\partial \tau^2} (p' - c_0^2 \rho') = 0$ 不一定成立。

3. 参数 p' 和 ρ' 哪一个更适合描述非稳态低速燃烧流动产生的噪声?

p' 更适合。非稳态低速燃烧流动涉及到能量方程, 而参数 p' 主要就源于能量方程, 因此 p' 更适合。

Section 2.5

1. 在 FW-H 方程中, $f = 0$ 的面在运动过程中形状能发生改变吗?

不能。FW-H 方程的前提假设为刚体运动, $f = 0$ 的面不能发生形变。

2. 如果 $|\nabla f| \neq 1$, 试推导 FW-H 方程, 并求其积分表达式。

对于表面, 有:

$$\begin{aligned}\frac{DH(f)}{Dt} &= \frac{\partial H(f)}{\partial t} + v_j \frac{\partial H(f)}{\partial x_j} = 0 \\ \frac{\partial H(f)}{\partial x_j} &= \frac{\partial H(f)}{\partial f} |\nabla f| n_j = |\nabla f| n_j \delta(f)\end{aligned}\quad (68)$$

由上式可得:

$$\frac{\partial H(f)}{\partial t} = -v_j \frac{\partial H(f)}{\partial x_j} = -v_j |\nabla f| n_j \delta(f) \quad (69)$$

于是有:

$$\begin{aligned}\frac{\partial [\phi H(f)]}{\partial t} &= H(f) \frac{\partial \phi}{\partial t} + \phi \frac{\partial H(f)}{\partial t} = H(f) \frac{\partial \phi}{\partial t} - \phi v_j |\nabla f| n_j \delta(f) \\ \frac{\partial [\phi H(f)]}{\partial x_i} &= H(f) \frac{\partial \phi}{\partial x_i} + \phi \frac{\partial H(f)}{\partial x_i} = H(f) \frac{\partial \phi}{\partial x_i} + \phi |\nabla f| n_i \delta(f)\end{aligned}\quad (70)$$

代入连续方程有:

$$\begin{aligned}\frac{\partial [\rho' H(f)]}{\partial t} + \frac{\partial [\rho u_j H(f)]}{\partial x_j} &= \rho u_j |\nabla f| n_j \delta(f) - \rho' v_j |\nabla f| n_j \delta(f) \\ &= [\rho (u_j - v_j) + \rho_0 v_j] |\nabla f| n_j \delta(f)\end{aligned}\quad (71)$$

代入动量方程有:

$$\begin{aligned}\frac{\partial [H(f) \rho u_i]}{\partial t} + c_0^2 \frac{\partial [H(f) \rho']}{\partial x_i} &= -H(f) \frac{\partial T_{ij}}{\partial x_j} + (c_0^2 \rho' \delta_{ij} - \rho u_i v_j) |\nabla f| n_j \delta(f) \\ &= -\frac{\partial [H(f) T_{ij}]}{\partial x_j} + (T_{ij} + c_0^2 \rho' \delta_{ij} - \rho u_i v_j) |\nabla f| n_j \delta(f) \\ &= -\frac{\partial [H(f) T_{ij}]}{\partial x_j} + [\rho u_i (u_j - v_j) + p_{ij}] |\nabla f| n_j \delta(f)\end{aligned}\quad (72)$$

于是有:

$$\frac{\partial^2 [\rho' H(f)]}{\partial t^2} - c_0^2 \frac{\partial^2 [H(f) \rho']}{\partial x_i^2} = \frac{\partial^2 [H(f) T_{ij}]}{\partial x_i \partial x_j} - \frac{\partial [F_i \delta(f)]}{\partial x_i} + \frac{\partial [Q \delta(f)]}{\partial t} \quad (73)$$

其中,

$$Q = [\rho(u_j - v_j) + \rho_0 v_j] |\nabla f| n_j$$

$$F_i = [\rho u_i (u_j - v_j) + p_{ij}] |\nabla f| n_j$$

其积分表达式可以表示为:

$$H(f) c_0^2 \rho'(\mathbf{x}, t) = \int_V \int_{-\infty}^{+\infty} G \left\{ \frac{\partial^2 [H(f) T_{ij}]}{\partial y_i \partial y_j} - \frac{\partial [F_i \delta(f)]}{\partial y_i} + \frac{\partial [Q \delta(f)]}{\partial \tau} \right\} d\tau d^3 \mathbf{y} \quad (74)$$

对于四极子项:

$$G \frac{\partial^2 [T_{ij} H(f)]}{\partial y_i \partial y_j} = [T_{ij} H(f)] \frac{\partial^2 G}{\partial y_i \partial y_j} + \frac{\partial}{\partial y_i} \left(G \frac{\partial [T_{ij} H(f)]}{\partial y_j} \right) - \frac{\partial}{\partial y_j} \left([T_{ij} H(f)] \frac{\partial G}{\partial y_i} \right) \quad (75)$$

其中,

$$\int_{\Sigma+\Omega} \int_{-\infty}^{+\infty} \frac{\partial}{\partial y_i} \left(G \frac{\partial [T_{ij} H(f)]}{\partial y_j} \right) d\tau d^3 \mathbf{y} = \int_{S_\infty} \int_{-\infty}^{+\infty} G \frac{\partial [T_{ij} H(f)]}{\partial y_j} n_i d\tau d^2 \mathbf{y} = 0$$

$$\int_{\Sigma+\Omega} \int_{-\infty}^{+\infty} \frac{\partial}{\partial y_j} \left(T_{ij} H(f) \frac{\partial G}{\partial y_i} \right) d\tau d^3 \mathbf{y} = \int_{S_\infty} \int_{-\infty}^{+\infty} T_{ij} H(f) \frac{\partial G}{\partial y_j} n_j d\tau d^2 \mathbf{y} = 0$$

因此有:

$$\int_V \int_{-\infty}^{+\infty} G \frac{\partial^2 [H(f) T_{ij}]}{\partial y_i \partial y_j} d\tau d^3 \mathbf{y} = \int_V \int_{-\infty}^{+\infty} H(f) T_{ij} \frac{\partial^2 G}{\partial y_i \partial y_j} d\tau d^3 \mathbf{y} \quad (76)$$

对于偶极子项:

$$\int_V \int_{-\infty}^{+\infty} G \frac{\partial [F_i \delta(f)]}{\partial y_i} d\tau d^3 \mathbf{y} = \int_V \int_{-\infty}^{+\infty} \frac{\partial [G F_i \delta(f)]}{\partial y_i} d\tau d^3 \mathbf{y} - \int_V \int_{-\infty}^{+\infty} F_i \delta(f) \frac{\partial G}{\partial y_i} d\tau d^3 \mathbf{y} \quad (77)$$

对于无边界区域, 有:

$$\int_V \frac{\partial [G F_i \delta(f)]}{\partial y_i} d^3 \mathbf{y} = \int_{\Sigma+\Omega} \frac{\partial [G F_i \delta(f)]}{\partial y_i} d^3 \mathbf{y} = \int_{S_\infty} G F_i \delta(f) n_i d^2 \mathbf{y} = 0 \quad (78)$$

因此有：

$$\int_V \int_{-\infty}^{+\infty} G \frac{\partial [F_i \delta(f)]}{\partial y_i} d\tau d^3\mathbf{y} = - \int_V \int_{-\infty}^{+\infty} F_i \delta(f) \frac{\partial G}{\partial y_i} d\tau d^3\mathbf{y} \quad (79)$$

对于单极子项：

$$\begin{aligned} \int_V \int_{-\infty}^{+\infty} G \frac{\partial [Q \delta(f)]}{\partial \tau} d\tau d^3\mathbf{y} &= \int_V \int_{-\infty}^{+\infty} \frac{\partial [GQ \delta(f)]}{\partial \tau} d\tau d^3\mathbf{y} \\ &\quad - \int_V \int_{-\infty}^{+\infty} Q \delta(f) \frac{\partial G}{\partial \tau} d\tau d^3\mathbf{y} \end{aligned} \quad (80)$$

根据 $G = \frac{\partial G}{\partial \tau} = 0 (t < \tau)$, 有：

$$\int_{-\infty}^{+\infty} \frac{\partial [GQ \delta(f)]}{\partial \tau} d\tau = GQ \delta(f) \Big|_{\tau=-\infty}^{\tau=+\infty} = 0 \quad (81)$$

因此有：

$$\int_V \int_{-\infty}^{+\infty} G \frac{\partial [Q \delta(f)]}{\partial \tau} d\tau d^3\mathbf{y} = - \int_V \int_{-\infty}^{+\infty} Q \delta(f) \frac{\partial G}{\partial \tau} d\tau d^3\mathbf{y} \quad (82)$$

综上，FW-H 方程的积分表达式可表示为：

$$\begin{aligned} H(f) c_0^2 \rho'(\mathbf{x}, t) &= \int_V \int_{-\infty}^{+\infty} H(f) T_{ij} \frac{\partial^2 G}{\partial y_i \partial y_j} d\tau d^3\mathbf{y} \\ &\quad + \int_V \int_{-\infty}^{+\infty} F_i \delta(f) \frac{\partial G}{\partial y_i} d\tau d^3\mathbf{y} \\ &\quad - \int_V \int_{-\infty}^{+\infty} Q \delta(f) \frac{\partial G}{\partial \tau} d\tau d^3\mathbf{y} \end{aligned} \quad (83)$$

3. 如果 $f = 0$ 的面不是固体表面，而是流体区域任意选择的可穿透封闭面，FW-H 方程还成立吗？

成立。FW-H 方程仅假设 $f = 0$ 为移动的刚体表面，并没有假设表面是否可穿透。因此 FW-H 方程对可穿透表面成立。对于不可穿透表面，FW-H 方程可以进一步简化，简化后的方程对可穿透表面不成立。

Section 2.6

1. 对均匀静止介质中以攻数 M_i 运动的声源, 证明

$$\frac{\partial M_r}{\partial \tau} = \frac{1}{r} \left\{ r_i \frac{\partial M_i}{\partial \tau} + c_0 (M_r^2 - M^2) \right\}, M = \sqrt{M_1^2 + M_2^2 + M_3^2}$$

已知:

$$M_r = \frac{r_i M_i}{r} \quad (84)$$

根据微分公式, 有:

$$\begin{aligned} \frac{\partial M_r}{\partial \tau} &= \frac{\partial}{\partial \tau} \left(\frac{r_i M_i}{r} \right) \\ &= \frac{r_i}{r} \frac{\partial M_i}{\partial \tau} + \frac{M_i}{r} \frac{\partial r_i}{\partial \tau} - \frac{r_i M_i}{r^2} \frac{\partial r}{\partial \tau} \end{aligned} \quad (85)$$

其中:

$$\frac{M_i}{r} \frac{\partial r_i}{\partial \tau} = \frac{M_i}{r} (-v_i) = -\frac{M_i^2 c_0}{r} \quad (86)$$

$$\frac{r_i M_i}{r^2} \frac{\partial r}{\partial \tau} = \frac{M_r}{r} (-M_r c_0) = -\frac{M_r^2 c_0}{r} \quad (87)$$

带入式(85), 得:

$$\begin{aligned} \frac{\partial M_r}{\partial \tau} &= \frac{r_i}{r} \frac{\partial M_i}{\partial \tau} + \frac{M_i}{r} \frac{\partial r_i}{\partial \tau} - \frac{r_i M_i}{r^2} \frac{\partial r}{\partial \tau} \\ &= \frac{r_i}{r} \frac{\partial M_i}{\partial \tau} - \frac{M_i^2 c_0}{r} + \frac{M_r^2 c_0}{r} \\ &= \frac{1}{r} \left\{ r_i \frac{\partial M_i}{\partial \tau} + c_0 (M_r^2 - M_i^2) \right\} \\ &= \frac{1}{r} \left\{ r_i \frac{\partial M_i}{\partial \tau} + c_0 (M_r^2 - M^2) \right\}, M = \sqrt{M_1^2 + M_2^2 + M_3^2} \end{aligned} \quad (88)$$

2. 证明偶极子噪声的积分表达式

$$\begin{aligned} \pi p_D(\mathbf{x}, t) &= \int_S \left[\frac{r_i}{r^2 c_0 (1 - M_r)^2} \left\{ \frac{\partial F_i}{\partial \tau} + \frac{F_i}{1 - M_r} \left(\frac{r_j}{r} \frac{\partial M_j}{\partial \tau} \right) \right\} \right] d^2 \mathbf{y} \\ &\quad + \int_S \left[\frac{1}{r^2 (1 - M_r)^2} \left\{ \frac{F_i r_i}{r} \frac{1 - M^2}{1 - M_r} - F_i M_i \right\} \right] d^2 \mathbf{y} \end{aligned}$$

已知:

$$\pi p_D(\mathbf{x}, t) = -\frac{\partial}{\partial x_i} \int_S \left[\frac{F_i}{r (1 - M_r)} \right] d^2 \mathbf{y} \quad (89)$$

根据微分公式，有：

$$\frac{\partial}{\partial x_i} \left[\frac{F_i}{r(1-M_r)} \right] = \left[\frac{\partial}{\partial x_i} \left\{ \frac{F_i}{r(1-M_r)} \right\} \right] + \left[\frac{\partial \tau}{\partial x_i} \frac{\partial}{\partial \tau} \left\{ \frac{F_i}{r(1-M_r)} \right\} \right] \quad (90)$$

Section 2.7

1. 将 Fourier 变换对定义为 $\tilde{f}(\omega) = \int_{-\infty}^{\infty} f(t) e^{-i\omega t} dt$, $f(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} \tilde{f}(\omega) e^{i\omega t} d\omega$, 证明时域格林函数 $G_0(\mathbf{x}, \mathbf{y}, t - \tau) = \frac{\delta(t - \tau - R/c_0)}{4\pi\Re}$ 的频域表达式为 $\tilde{G}_0(\mathbf{x}, \mathbf{y}, \omega) = \frac{\exp(-ikR)}{4\pi\Re}$ 。

根据 Fourier 变换的定义, 有:

$$\begin{aligned}
 \tilde{G}_0(\mathbf{x}, \mathbf{y}, \omega) &= \int_{-\infty}^{\infty} G_0(\mathbf{x}, \mathbf{y}, t - \tau) e^{-i\omega(t - \tau)} dt - \tau \\
 &= \int_{-\infty}^{\infty} \frac{\delta(t - \tau - R/c_0)}{4\pi\Re} e^{-i\omega(t - \tau)} dt - \tau \\
 &= \frac{1}{4\pi\Re} \int_{-\infty}^{\infty} \delta(t - \tau - R/c_0) e^{-i\omega(t - \tau - R/c_0)} e^{-i\omega R/c_0} dt - \tau \\
 &= \frac{e^{-i\omega R/c_0}}{4\pi\Re} \int_{-\infty}^{\infty} \delta(t - \tau - R/c_0) e^{-i\omega(t - \tau - R/c_0)} dt - \tau
 \end{aligned} \tag{91}$$

对于 Dirac Function, 有:

$$\int_{-\infty}^{\infty} \delta(t) e^{-i\omega t} dt = 1 \tag{92}$$

因此有:

$$\begin{aligned}
 \tilde{G}_0(\mathbf{x}, \mathbf{y}, \omega) &= \frac{e^{-i\omega R/c_0}}{4\pi\Re} \int_{-\infty}^{\infty} \delta(t - \tau - R/c_0) e^{-i\omega(t - \tau - R/c_0)} dt - \tau \\
 &= \frac{e^{-i\omega R/c_0}}{4\pi\Re} \\
 &= \frac{e^{-ikR}}{4\pi\Re}
 \end{aligned} \tag{93}$$

其中, $k = \frac{\omega}{c_0}$ 。

2. 对均匀平均流中的静止点源 $Q(\mathbf{y}, \tau) = \exp(i\omega\tau)$, 其辐射的声场用 $\phi(\mathbf{x}, t)$ 表示, 利用上题中的格林函数, 证明 $\phi(\mathbf{x}, t) = \frac{\exp[i\omega(t - R/c_0)]}{4\pi\Re}$

$$\begin{aligned}
 \phi(\mathbf{x}, t) &= \int_{-\infty}^{\infty} Q(\mathbf{y}, \tau) G_0(\mathbf{x}, \mathbf{y}, \tau) d\tau \\
 &= \int_{-\infty}^{\infty} e^{i\omega\tau} \frac{\delta(t - \tau - R/c_0)}{4\pi\Re} d\tau \\
 &= \frac{e^{i\omega(t - R/c_0)}}{4\pi\Re} \int_{-\infty}^{\infty} \delta(t - \tau - R/c_0) e^{-i\omega(t - \tau - R/c_0)} d\tau \\
 &= \frac{e^{i\omega(t - R/c_0)}}{4\pi\Re}
 \end{aligned} \tag{94}$$

Section 2.8

1. 假设亚声速均匀流沿 x_1 轴正向运动, 在 \mathbf{y} 点有一静止声源辐射声波, 如果已知观察点 \mathbf{x} 的时间 t , 如何确定延迟时间 τ ?
2. 假设均匀静止介质中有一点源以恒定速度 v (亚声速) 沿 x_1 轴正向运动, 其初始位置为 \mathbf{y}_0 , 如果已知观察点 \mathbf{x} 的时间 t , 如何确定延迟时间 τ ?
3. 均匀静止介质中, 一强度为 $q(t)$ 的点源以恒定速度 \mathbf{v} 亚声速直线运动, 且 $t = 0$ 时刻恰好经过坐标原点, 辐射声场的速度势函数 $\phi(\mathbf{x}, t)$ 满足方程 $\frac{1}{c_0^2} \frac{\partial^2 \phi}{\partial t^2} - \nabla^2 \phi = q(t) \delta(\mathbf{x} - \mathbf{v}t)$, 证明

$$\phi(\mathbf{x}, t) = \frac{q(t - R/c_0)}{4\pi R(1 - M \cos \theta)}, \quad M = \frac{|\mathbf{v}|}{c_0}$$

其中, R 为观察点 \mathbf{x} 与声源辐射声波时所在位置间的距离, θ 为声源运动方向与声传播方向的夹角。

Section 3.1

1. 对无黏、均熵可压缩流动, 证明涡运动方程的表达形式可写为

$$\frac{D}{Dt} \left(\frac{\boldsymbol{\omega}}{\rho} \right) = \frac{\boldsymbol{\omega}}{\rho} \cdot \nabla \mathbf{u}$$

已知:

$$\frac{\partial \mathbf{u}}{\partial t} + \nabla H + \boldsymbol{\omega} \times \mathbf{u} - T \nabla s - \mathbf{e} = 0 \quad (95)$$

两边求旋度得:

$$\nabla \times \left(\frac{\partial \mathbf{u}}{\partial t} + \nabla H + \boldsymbol{\omega} \times \mathbf{u} - T \nabla s - \mathbf{e} \right) = 0 \quad (96)$$

因为 $\nabla \times \nabla H \equiv 0$, 因此有:

$$\frac{\partial \boldsymbol{\omega}}{\partial t} + \nabla \times (\boldsymbol{\omega} \times \mathbf{u}) - \nabla T \times \nabla s - \nabla \times \mathbf{e} = 0 \quad (97)$$

又因为:

$$\begin{aligned} \nabla \times (\boldsymbol{\omega} \times \mathbf{u}) &= \boldsymbol{\omega}(\nabla \cdot \mathbf{u}) - \mathbf{u}(\nabla \cdot \boldsymbol{\omega}) + (\mathbf{u} \cdot \nabla) \boldsymbol{\omega} - (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} \\ \nabla \times \mathbf{e} &= \nu \nabla^2 \boldsymbol{\omega} \end{aligned} \quad (98)$$

结合 $\nabla \cdot \boldsymbol{\omega} = \nabla \cdot (\nabla \times \mathbf{u}) = 0$ 得:

$$\begin{aligned} & \frac{\partial \boldsymbol{\omega}}{\partial t} + \nabla \times (\boldsymbol{\omega} \times \mathbf{u}) - \nabla T \times \nabla s - \nabla \times \mathbf{e} \\ &= \frac{\partial \boldsymbol{\omega}}{\partial t} + (\mathbf{u} \cdot \nabla) \boldsymbol{\omega} + \boldsymbol{\omega}(\nabla \cdot \mathbf{u}) - (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} \\ & \quad - \mathbf{u}(\nabla \cdot \boldsymbol{\omega}) - \nabla T \times \nabla s - \nu \nabla^2 \boldsymbol{\omega} \\ &= \frac{D \boldsymbol{\omega}}{Dt} + \boldsymbol{\omega}(\nabla \cdot \mathbf{u}) - (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} - \nabla T \times \nabla s - \nu \nabla^2 \boldsymbol{\omega} \\ &= 0 \end{aligned} \quad (99)$$

根据连续方程, 有:

$$\frac{\boldsymbol{\omega}}{\rho^2} \left(\frac{D \rho}{Dt} + \rho(\nabla \cdot \mathbf{u}) \right) = \frac{\boldsymbol{\omega}}{\rho^2} \frac{D \rho}{Dt} + \frac{\boldsymbol{\omega}}{\rho} (\nabla \cdot \mathbf{u}) = 0 \quad (100)$$

因此有：

$$\begin{aligned} & \frac{1}{\rho} \frac{D\boldsymbol{\omega}}{Dt} - \left(\frac{\boldsymbol{\omega}}{\rho} \cdot \nabla \right) \mathbf{u} - \frac{1}{\rho} \nabla T \times \nabla s - \frac{\nu}{\rho} \nabla^2 \boldsymbol{\omega} - \frac{\boldsymbol{\omega}}{\rho^2} \frac{D\rho}{Dt} \\ &= \frac{D}{Dt} \left(\frac{\boldsymbol{\omega}}{\rho} \right) - \left(\frac{\boldsymbol{\omega}}{\rho} \cdot \nabla \right) \mathbf{u} - \frac{1}{\rho} \nabla T \times \nabla s - \frac{\nu}{\rho} \nabla^2 \boldsymbol{\omega} \\ &= 0 \end{aligned} \quad (101)$$

对于无粘、等熵流动，有：

$$\frac{1}{\rho} \nabla T \times \nabla s = 0 \quad (102)$$

$$\frac{\nu}{\rho} \nabla^2 \boldsymbol{\omega} = 0 \quad (103)$$

因此有：

$$\frac{D}{Dt} \left(\frac{\boldsymbol{\omega}}{\rho} \right) = \left(\frac{\boldsymbol{\omega}}{\rho} \cdot \nabla \right) \mathbf{u} = \frac{\boldsymbol{\omega}}{\rho} \cdot \nabla \mathbf{u} \quad (104)$$

原式得证。

2. 对无黏正压流体的可压缩运动, 证明浴运动方程的表达形式可写为

$$\frac{D\boldsymbol{\omega}}{Dt} = (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} - \boldsymbol{\omega}(\nabla \cdot \mathbf{u})$$

根据第 1 题中的推导，已知：

$$\frac{D\boldsymbol{\omega}}{Dt} + \boldsymbol{\omega}(\nabla \cdot \mathbf{u}) - (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} - \nabla T \times \nabla s - \nu \nabla^2 \boldsymbol{\omega} = 0 \quad (105)$$

对于无粘流动，有：

$$\frac{\nu}{\rho} \nabla^2 \boldsymbol{\omega} = 0 \quad (106)$$

对于正压流动，有：

$$\nabla T \times \nabla s = 0 \quad (107)$$

因此有：

$$\frac{D\boldsymbol{\omega}}{Dt} + \boldsymbol{\omega}(\nabla \cdot \mathbf{u}) - (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} = 0 \quad (108)$$

$$\frac{D\boldsymbol{\omega}}{Dt} = (\boldsymbol{\omega} \cdot \nabla) \mathbf{u} - \boldsymbol{\omega}(\nabla \cdot \mathbf{u}) \quad (109)$$

原式得证。

Section 3.2

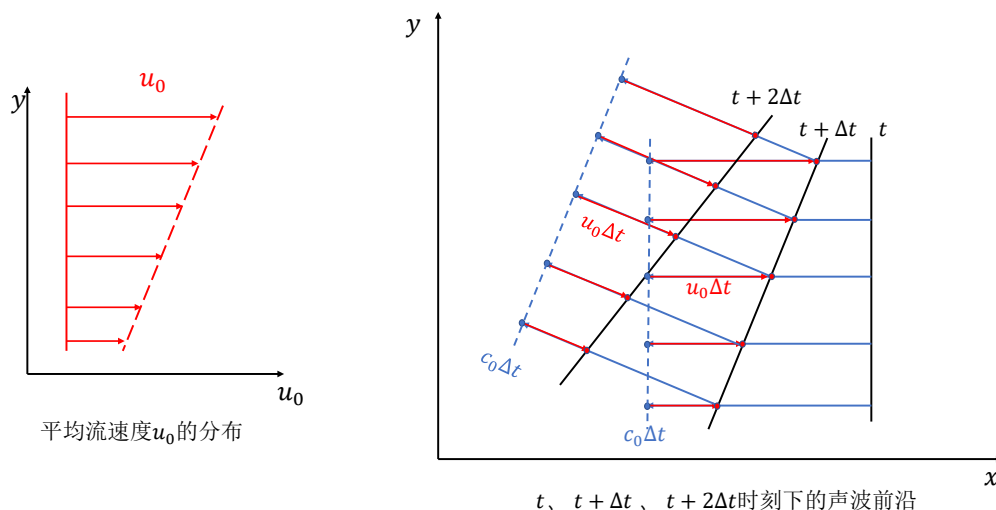
1. 对低马赫数均熵流动绕过静止物体的声辐射问题, 假设声源区域声学紧致, 观察点 \mathbf{x} 位于声学远场。假设近场区域流动信息已知, 且勿略黍性影响, 从涡声方程出发, 证明观察点 \mathbf{x} 的声场可表示为

$$p'(\mathbf{x}, t) = \int_S p'(\mathbf{y}, \tau) \frac{\partial G}{\partial y_i} n_i dS(\mathbf{y}) d\tau - \rho_0 \int (\boldsymbol{\omega} \times \mathbf{u})_i(\mathbf{y}, \tau) \frac{\partial G}{\partial y_i} d^3\mathbf{y} d\tau$$

2. 利用时域三维自由空间格林函数, 消除上题积分方程中的时间积分, 注意考虑不同声源点到 \mathbf{x} 点的延迟时间差异。

Section4.1

1. 考虑平面波在非均匀流中的传播, 假设声速整场均匀, 平均流速度沿水平方向且与纵坐标轴呈线性关系。绘图分析平面波向上游传播时路径的变化趋势。



平面波向上游传播时路径的变化如右图所示。当平均流速度 u_0 分布如左图所示时, 平面波向上游传播会朝着纵坐标轴的正方向偏转, 即向着速度较大的方向偏转。

2. 声衬的消声作用跟边界层厚度与波长的比值有关, 比值越小消声作用越弱, 试分析原因。

由于流体在边界层的速度梯度, 声波在传播时会朝着声衬方向偏转, 当边界层厚度与波长的比值变小时, 边界层对声波的偏转作用变弱, 传播到声衬的声波变少, 消声作用减弱。

Section 4.2

1. 对完全气体, 证明热力学关系式 $\frac{dp}{\rho} = \frac{1}{\gamma} \frac{dp}{p} - \frac{ds}{c_p}$ 成立。

根据热力学第二定律:

$$\begin{aligned} de &= T ds - p d(1/\rho) = C_v dT \\ dh &= T ds + dp/\rho = C_p dT \end{aligned} \quad (110)$$

因此有:

$$\frac{T ds - p d(1/\rho)}{c_v} = \frac{T ds + dp/\rho}{c_p} \quad (111)$$

$$\frac{C_p}{C_v} \frac{p}{\rho^2} d\rho = \frac{dp}{\rho} - \frac{C_p - C_v}{C_p} T ds \quad (112)$$

又因为:

$$\frac{C_p}{C_v} = \gamma \quad (113)$$

$$C_p = C_v + R \quad (114)$$

$$p = \gamma RT \quad (115)$$

因此有:

$$\frac{d\rho}{\rho} = \frac{1}{\gamma} \frac{dp}{p} - \frac{ds}{c_p} \quad (116)$$

原式得证。

2. 对等熵过程, 利用上述热力学关系式, 进一步证明

$$\frac{1}{\rho} \frac{D\rho}{Dt} = \frac{1}{\gamma} \frac{D}{Dt} \ln \left(\frac{p}{p_0} \right) - \frac{1}{c_p} \frac{Ds}{Dt}$$

其中, p_0 为常数。

由第 1 题的结论, 已知:

$$\frac{d\rho}{\rho} = \frac{1}{\gamma} \frac{dp}{p} - \frac{ds}{c_p} \quad (117)$$

因此有:

$$\frac{1}{\rho} \frac{D\rho}{Dt} = \frac{1}{\gamma} \frac{1}{p} \frac{Dp}{Dt} - \frac{1}{c_p} \frac{Ds}{Dt} \quad (118)$$

又因为：

$$\frac{1}{p} \frac{Dp}{Dt} = \frac{p_0}{p} \frac{D}{Dt} \left(\frac{p}{p_0} \right) = \frac{D}{Dt} \ln \left(\frac{p}{p_0} \right) \quad (119)$$

因此有：

$$\frac{1}{\rho} \frac{D\rho}{Dt} = \frac{1}{\gamma} \frac{D}{Dt} \ln \left(\frac{p}{p_0} \right) - \frac{1}{c_p} \frac{Ds}{Dt} \quad (120)$$

原式得证。

Section4.3

1. 将当地密度 ρ 、速度 \mathbf{u} 和压力 p 分解为时均值和脉动值两部分，即

$$\begin{aligned}\rho(\mathbf{x}, t) &= \rho_0(\mathbf{x}) + \rho'(\mathbf{x}, t) \\ \mathbf{u}(\mathbf{x}, t) &= \mathbf{u}_0(\mathbf{x}) + \mathbf{u}'(\mathbf{x}, t) \\ p(\mathbf{x}, t) &= p_0(\mathbf{x}) + p'(\mathbf{x}, t)\end{aligned}$$

对线性小振幅扰动，以 $(\rho', \rho_0 \mathbf{u}', p')$ 为声学变量，建立线化欧拉方程组。

对于连续方程：

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \mathbf{u}) = 0 \quad (121)$$

代入声学变量，得：

$$\frac{\partial \rho'}{\partial t} + \nabla \cdot (\rho_0 \mathbf{u}_0 + \rho' \mathbf{u}_0 + \rho_0 \mathbf{u}' + \rho' \mathbf{u}') = 0 \quad (122)$$

又因为：

$$\nabla \cdot (\rho_0 \mathbf{u}_0) = -\frac{\partial \rho_0}{\partial t} = 0 \quad (123)$$

得到线化连续方程：

$$\begin{aligned}& \frac{\partial \rho'}{\partial t} + \nabla \cdot (\rho' \mathbf{u}_0 + \rho_0 \mathbf{u}' + \rho' \mathbf{u}') \\ &= \frac{\partial \rho'}{\partial t} + \mathbf{u}_0 \cdot \nabla \rho' + \rho' \nabla \cdot \mathbf{u}_0 + \rho_0 \nabla \cdot \mathbf{u}' + \mathbf{u}' \cdot \nabla \rho_0 \\ &= -\nabla \cdot (\rho' \mathbf{u}')\end{aligned} \quad (124)$$

对于动量方程：

$$\rho \frac{\partial \mathbf{u}}{\partial t} + \rho \mathbf{u} \cdot \nabla \mathbf{u} + \nabla p = 0 \quad (125)$$

代入声学变量，得：

$$\begin{aligned}
& (\rho_0 + \rho') \frac{\partial(\mathbf{u}_0 + \mathbf{u}')}{\partial t} + (\rho_0 + \rho')(\mathbf{u}_0 + \mathbf{u}') \cdot \nabla(\mathbf{u}_0 + \mathbf{u}') + \nabla(p_0 + p') \\
& = \rho_0 \left(\frac{\partial \mathbf{u}'}{\partial t} + \mathbf{u}_0 \cdot \nabla \mathbf{u}' \right) + (\rho_0 \mathbf{u}_0 \cdot \nabla \mathbf{u}_0 + \nabla p_0) + (\rho_0 \mathbf{u}' + \rho' \mathbf{u}_0) \cdot \nabla \mathbf{u}_0 + \nabla p' \\
& + \left[\rho' \left(\frac{\partial \mathbf{u}'}{\partial t} + \mathbf{u}_0 \cdot \nabla \mathbf{u}' \right) + \rho \mathbf{u}' \cdot \nabla \mathbf{u}' + \rho' \mathbf{u}' \cdot \nabla \mathbf{u}_0 \right] = 0
\end{aligned} \tag{126}$$

又因为：

$$\rho_0 \mathbf{u}_0 \cdot \nabla \mathbf{u}_0 + \nabla p_0 = 0 \tag{127}$$

$$\frac{D_0}{Dt} = \frac{\partial}{\partial t} + \mathbf{u}_0 \cdot \nabla \tag{128}$$

得到线化动量方程：

$$\rho_0 \frac{D_0 \mathbf{u}'}{Dt} + (\rho_0 \mathbf{u}' + \rho' \mathbf{u}_0) \cdot \nabla \mathbf{u}_0 + \nabla p' = -\rho' \frac{D_0 \mathbf{u}'}{Dt} - \rho_0 \mathbf{u}' \cdot \nabla \mathbf{u}' - \rho' \mathbf{u}' \cdot \nabla \mathbf{u}_0 \tag{129}$$

对于能量方程：

$$\frac{\partial p}{\partial t} + \mathbf{u} \cdot \nabla p + \gamma p \nabla \cdot \mathbf{u} = 0 \tag{130}$$

代入声学变量，得：

$$\begin{aligned}
& \frac{\partial(p_0 + p')}{\partial t} + (\mathbf{u}_0 + \mathbf{u}') \cdot \nabla(p_0 + p') + \gamma(p_0 + p') \nabla \cdot (\mathbf{u}_0 + \mathbf{u}') \\
& = \left(\frac{\partial p'}{\partial t} + \mathbf{u}_0 \cdot \nabla p' \right) + (\mathbf{u}_0 \cdot \nabla p_0 + \gamma p_0 \nabla \cdot \mathbf{u}_0) + \mathbf{u}' \cdot \nabla p_0 + \mathbf{u}' \cdot \nabla p' \\
& + \gamma p_0 \nabla \cdot \mathbf{u}' + \gamma p' \nabla \cdot \mathbf{u}' + \gamma p' \nabla \cdot \mathbf{u}_0 \\
& = 0
\end{aligned} \tag{131}$$

又因为：

$$\mathbf{u}_0 \cdot \nabla p_0 + \gamma p_0 \nabla \cdot \mathbf{u}_0 = 0 \tag{132}$$

得到线化能量方程：

$$\frac{D_0 p'}{Dt} + \mathbf{u}' \cdot \nabla p_0 + \gamma p_0 \nabla \cdot \mathbf{u}' + \gamma p' \nabla \cdot \mathbf{u}_0 = -\mathbf{u}' \cdot \nabla p' - \gamma p' \nabla \cdot \mathbf{u}' \tag{133}$$

综上，得到线化欧拉方程组

$$\begin{aligned}
& \frac{\partial \rho'}{\partial t} + \mathbf{u}_0 \cdot \nabla \rho' + \rho' \nabla \cdot \mathbf{u}_0 + \rho_0 \nabla \cdot \mathbf{u}' + \mathbf{u}' \cdot \nabla \rho_0 = -\nabla \cdot (\rho' \mathbf{u}') \\
& \rho_0 \frac{D_0 \mathbf{u}'}{Dt} + (\rho_0 \mathbf{u}' + \rho' \mathbf{u}_0) \cdot \nabla \mathbf{u}_0 + \nabla p' = -\rho' \frac{D_0 \mathbf{u}'}{Dt} - \rho_0 \mathbf{u}' \cdot \nabla \mathbf{u}' - \rho' \mathbf{u}' \cdot \nabla \mathbf{u}_0 \\
& \frac{D_0 p'}{Dt} + \mathbf{u}' \cdot \nabla p_0 + \gamma p_0 \nabla \cdot \mathbf{u}' + \gamma p' \nabla \cdot \mathbf{u}_0 = -\mathbf{u}' \cdot \nabla p' - \gamma p' \nabla \cdot \mathbf{u}'
\end{aligned} \tag{134}$$