

MTE321 Formulas

Stresses

Deformation Elongation

$$\delta = \frac{FL}{EA}$$

$$\delta = \frac{\sigma L}{E}$$

Torsional Forumals

Stress

R is the radial distance

$$\tau = \frac{Tr}{J}$$

$$Z_p = \frac{J}{c}$$

$$\tau_{max} = \frac{T}{Z_p}$$

Deformation

θ is the angle of twist across L

For non-circular shafts K is section polar second moment of area and

Q the section polar modulus

$$T = \frac{P}{\omega} \quad T_{lb-in} = 63000 \frac{P}{\omega}$$

$$\theta = \frac{TL}{GJ}$$

$$Non-Circular \tau = \frac{T}{Q}$$

$$Non-Circular \theta = \frac{TL}{GK}$$

Thin-Walled Closed Tubes

A = median area boundary, U is length of median boundary

$$K = \frac{4A^2t}{U}$$

$$Q = 2tA$$

Shear Stress

V section shear force, Q is the first moment area, and t is the section thickness

$$\tau_{(y)} = \frac{VQ}{It}$$

$$Rectangular Beam \tau_{max} = \frac{3V}{2A}$$

$$Solid Round Beam \tau_{max} = \frac{4V}{3A}$$

$$Hollow Round Beam \tau_{max} = \frac{2V}{A}$$

Beam Bending

M is the moment at the section, y is the distance from the neutral axis

$$\sigma_y = -\frac{My}{I}$$

Stress Concentrations

Stress Concentration Factor

K_t is material and loading dependent, values greater than 3 are a waste

$$\sigma_{max} = K_t \sigma_{nom}$$

Curved Beam Bending

$$R = \frac{A}{ASF}$$

r = distance to required stress location

r_c = centroid distance

A = cross-sectional area

$$\sigma_{(r)} = \frac{M(\theta)(R-r)}{Ar(r_c-R)}$$

Thermal Strain

$$\epsilon_x^m = -\alpha \delta T$$

Principle Stresses

$$\tan 2\theta_\sigma = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$Max \sigma_{norm} = \frac{1}{2}(\sigma_x + \sigma_y) + \sqrt{\left[\frac{1}{2}\sigma_x - \sigma_y\right]^2 + \tau_{xy}^2}$$

$$Min \sigma_{norm} = \frac{1}{2}(\sigma_x - \sigma_y) - \sqrt{\left[\frac{1}{2}\sigma_x - \sigma_y\right]^2 + \tau_{xy}^2}$$

Fatigue Testing

$$\tan 2\theta_\sigma = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$Max \sigma_{norm} = \frac{1}{2}(\sigma_x + \sigma_y) + \sqrt{\left[\frac{1}{2}\sigma_x - \sigma_y\right]^2 + \tau_{xy}^2}$$

$$Min \sigma_{norm} = \frac{1}{2}(\sigma_x - \sigma_y) - \sqrt{\left[\frac{1}{2}\sigma_x - \sigma_y\right]^2 + \tau_{xy}^2}$$

Endurance Limit

$$\tan 2\theta_\sigma = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

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$$Min \sigma_{norm} = \frac{1}{2}(\sigma_x - \sigma_y) - \sqrt{\left[\frac{1}{2}\sigma_x - \sigma_y\right]^2 + \tau_{xy}^2}$$

Goodman Method

$$K_t \tan 2\theta_\sigma = \frac{2\tau_{xy}}{\sigma_x - \sigma_y}$$

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$Max \sigma_{norm} = \frac{1}{2}(\sigma_x + \sigma_y) + \sqrt{\left[\frac{1}{2}\sigma_x - \sigma_y\right]^2 + \tau_{xy}^2}$$

$$Min \sigma_{norm} = \frac{1}{2}(\sigma_x - \sigma_y) - \sqrt{\left[\frac{1}{2}\sigma_x - \sigma_y\right]^2 + \tau_{xy}^2}$$

Design: Dynamic Loads

Stress

Periodic

Fluctuating $\sigma_m \neq 0$, R = -1

Pulsating $\sigma_m = 0$, R = 1

Lecture 5

Loading

$$\sigma_m = \text{mean stress} = (\sigma_{max} + \sigma_{min})/2$$

$$\sigma_a = \text{stress amplitude} = (\sigma_{max} - \sigma_{min})/2$$

$$R = \text{stress ratio} = \sigma_{min}/\sigma_{max}$$

$$A = \text{stress ratio} = \sigma_a/\sigma_m$$

$$\text{Loading Cycle : period between peaks}$$

Endurance Limit

s_a =Stress Amplitude Level
N: number of cycles to failure
s_n = fatigue limit
Assume s_n = 0.5s_u if no data

s_n from table appendix 3
C_m material flaws
C_R Reliability Factor

$$s_a = s_n N^b$$
$$s_n = C_m C_{st} C_R C_S s_n$$

C_s = size factor (5-12,5-4 circular),(5-13 for other)

Goodman Method

Gears

Pitch Line Speed

$$V_T = \frac{\pi D \cdot n_p}{12}$$