

Design, Modeling, and Control Strategies for Soft Robots

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Design, Modeling, and Control Strategies for Soft Robots

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Abstract

Design, Modeling, and Control Strategies for Soft Robots

In the past two decades, the field of soft robotics has sparked significant interest among many scientific disciplines. Contrary to rigid robots, soft robots explore soft materials that significantly enhance the robot's dexterity, enable a rich family of motion primitives, and enhance environmental robustness regarding contact and impact. Since its inception, soft robotics has exemplified its potential in diverse areas such as safe manipulation, adaptive grasping, exploration under environmental uncertainty, rehabilitation, and the biomimicry of many animals. By exploring the uncharted versatile nature of soft materials, soft robotics paves the way towards achieving biological performance in modern-day robotics. This thesis aims to further the advances in soft robotics by addressing some of the open multidisciplinary challenges within this young field of research.

Although soft materials harbor many advantages akin to biology, which are difficult to achieve for rigid robotics, they also pose many fundamental problems. The first issue is the problem of soft robotic design. Traditional robotic design emphasizes high structural rigidity and weight minimization, a well-established practice in engineering. On the other hand, soft robotic design values minimal structural rigidity for motion, leading to complex, highly nonlinear relationships between the input and output. Additionally, distributed soft actuation, in addition to gravitational and inertial forces acting on the continuous elastic body, introduces joint mobilities that are often uncontrollable nor aligned with the control objective, *e.g.*, precise grasping and manipulation. Since describing the underlying continuum mechanics and applying such mathematical theory to systematic design is challenging, a large number of soft robotic systems are still developed *ad hoc*.

Second, a direct duality of the previous challenge is dealing with the innate infinite-dimensionality from a control perspective – particularly with model-based feedback in mind. The transition from rigid to flexible has introduced a new control paradigm: the trade-off between precision and speed in a numerical setting. Not only is control theory for soft robotics in stages of inception, but deriving accurate and numerically efficient model-based controllers is challenging due to the large nonlinear deformations of the soft robotic body.

In light of these challenges, this thesis proposes a set of systematic tools with theoretical and experimental applications for (*i*) the structural design and fabrication of continuum-deformable soft actuators optimized for user-defined joint motion, (*ii*) the development of efficient dynamic models of soft continuum manip-

ulators, and (*iii*) applying such mathematical models to model-based controllers for a subclass of (pneumatic) soft continuum manipulators and soft grippers.

The first part of the thesis addresses the design problem by proposing a novel automated design algorithm for developing efficient soft actuators. These algorithms account for the underlying continuum mechanics described by a set of partial differential equations, which respect the aforementioned nonlinearities between the input and output motion. Tailoring user-defined cost functions to desired motion and control reachability, an implicit representation of the optimal soft material distribution can be found within a fixed design space. Several generative designs for a diverse subset of soft actuation morphologies are produced including, but not limited to, soft rotational actuators, soft artificial muscles, and soft grippers. In what follows, an optimal design for a soft actuator is synthesized; and through Additive Manufacturing (AM) of printable flexible material, the sim-to-real boundary is passed. The proposed approach not only accelerates design convergence but also builds upon the vast library of soft robot morphologies currently unexplored in literature.

The second part of the thesis addresses the question of modeling for control applicable to a class of soft robotic systems – most notably soft continuum manipulators. The thesis proposes a reduced-order modeling strategy for soft robotics, whose dynamics are derived through differential geometric theory on spatial beams. Besides discussing earlier modeling strategies, the thesis also proposes a new strain-based parametrization approach that ensures the structural information and the underlying continuum mechanics are preserved when synthesizing the reduced-order beam models – a possible solution to the aforementioned control paradigm of precision vs. speed. To enhance numerical performance further, spatio-temporal integration schemes are also proposed that exploit the geometric structure of such soft beam models, resulting in real-time simulation with sufficient numerical precision purposefully tailored for control.

The third part of the thesis addresses the development of model-based controllers that can be employed in various control scenarios similar to control for traditional rigid robotics, *e.g.*, inverse kinematics and motion planning, set-point stabilization, trajectory tracking, and multi-point grasping of objects. The stabilizing controller is rooted in an energy-based formalism, providing robustness even when faced with material uncertainties. The effectiveness of the controller is demonstrated both in simulation and experiments for various soft robotic systems that share a resemblance to biology, *e.g.*, the elephant’s trunk or the tentacle of an octopus.

The main contribution of the thesis is a collection of multidisciplinary tools compressed into one general framework for the design, modeling, and control of a class of soft robots, ranging from the theoretical to the experimental domain.

Keywords:

Soft Robots, Hyper-redundant Robots, Design Optimization, Continuum Mechanics, Reduced-order Modeling, Model-based Control, 3D Printing.

Samenvatting

In de afgelopen twee decennia heeft het veld van de zachte robotica veel interesse opgewekt binnen een breed spectrum van wetenschappelijke disciplines. In tegenstelling tot rigide robots verkennen zachte robots zachte materialen die de behendigheid van de robot aanzienlijk verbeteren, een rijke collectie van bewegingsprimitieven mogelijk maken en de omgevingsbestendigheid ten aanzien van contact en impact vergroten. Sinds de oorspong heeft de zachte robotica het haar potentieel aangetoond in diverse gebieden zoals veilige manipulatie, adaptief grijpen, verkenning onder omgevingsonzekerheid, revalidatie en de biomimetica van vele dieren. Door de veelzijdige aard van zachte materialen te verkennen, legt de zachte robotica de eerste stappen naar het bereiken van biologische prestaties in de moderne robotica. Deze scriptie heeft als doel de vooruitgang in de zachte robotica verder te bevorderen door enkele van de open multidisciplinaire uitdagingen binnen dit jonge onderzoeksgebied aan te pakken.

Hoewel zachte materialen, zoals systemen in de biologie, veel voordelen hebben, die soms moeilijk te bereiken zijn voor rigide robotica, brengt het ook veel fundamentele problemen met zich mee. Het eerste probleem is het ontwerp van zachte robots. Traditioneel robotica-ontwerp legt de nadruk op hoge structurele stijfheid en gewichtsminimalisatie - een goed doordachte discipline in de engineering. Aan de andere kant houdt het ontwerp van zachte robots van minimale structurele stijfheid voor beweging, wat leidt tot complexe, zeer niet-lineaire relaties tussen input en output. Bovendien leiden gedistribueerde zachte activering, toegepast door zwaartekracht- en traagheidskrachten die op het continu elastische lichaam werken, tot gewichtsmobiliteiten die in veel gevallen niet te controleren zijn of niet zijn afgestemd op de controle-doelstelling, zoals nauwkeurig grijpen en manipulatie. Omdat het beschrijven van de onderliggende continue mechanica en het toepassen van dergelijke wiskundige theorie op systematisch ontwerp uitdagend is, worden nog steeds een groot aantal zachte robotsystemen *ad hoc* ontwikkeld.

Ten tweede vormt de directe dualiteit van de vorige uitdaging het omgaan met de intrinsieke oneindige-dimensionaliteit vanuit een controleperspectief - met name met modelgebaseerde feedback in gedachten. De overgang van rigide naar flexibel heeft een nieuw controleparadigma geïntroduceerd: de afweging tussen precisie en snelheid in een numerieke omgeving. Niet alleen bevindt de controleteorie voor zachte robotica zich in de beginfase, maar het afleiden van nauwkeurige en numeriek efficiënte modelgebaseerde controllers is uitdagend vanwege de grote niet-lineaire vervormingen van de zachte roboticacontinuüm.

Gezien deze uitdagingen stelt deze scriptie een reeks systematische tools voor

met theoretische en experimentele toepassingen voor (*i*) het structurele ontwerp en de fabricage van continuüm-deformeerbare zachte actuators geoptimaliseerd voor door de gebruiker gedefinieerde gezamenlijke beweging, (*ii*) de ontwikkeling van efficiënte dynamische modellen voor zachte continuüm manipulatoren, en (*iii*) het toepassen van wiskundige modellen op modelgebaseerde controllers voor een subklasse van (pneumatische) zachte continuüm manipulatoren en zachte grijpers.

Het eerste deel van deze scriptie richt zich op het ontwerpprobleem door het voorstellen van nieuwe computer-geautomatiseerde ontwerpalgoritmen voor de ontwikkeling van efficiënte zachte actuators. Deze algoritmen houden rekening met de onderliggende continue mechanica die wordt beschreven door een set partiële differentiaalvergelijkingen, die de eerder genoemde niet-lineariteiten tussen de input en output beweging respecteren. Door een door de gebruiker gedefinieerd doel aan te passen aan een gewenste beweging en controlebereik, kan een impliciete representatie van de optimale zachte materiaalverdeling worden gevonden binnen een vast ontwerpruimte. Verschillende generatieve ontwerpen voor een diverse subset van zachte actuator-morfologieën worden geproduceerd, waaronder, maar niet beperkt tot, zachte rotatie-actuators, zachte kunstmatige spieren en zachte grijpers. Vervolgens wordt een optimaal ontwerp voor een zachte robotmanipulator met een adaptieve grijper gesynthetiseerd. Door middel van Additive Manufacturing (AM) van printbaar flexibel materiaal wordt de grens tussen simulatie en realiteit overschreden. De voorgestelde aanpak versnelt niet alleen het convergeren van het ontwerp, maar bouwt ook voort op de enorme bibliotheek van zachte robot-morfologieën die momenteel onontdekt zijn in de literatuur.

Het tweede deel van de scriptie richt zich op de modellering voor controle die van toepassing is op een klasse van zachte robotica-systemen - met name zachte continuüm manipulatoren. De scriptie stelt een modelleerstrategie voor met gereduceerde orde voor zachte robotica, waarvan de dynamica worden afgeleid door middel van differentiële geometrische theorie op ruimtelijke balken. Naast het bespreken van eerdere modelleerstrategieën stelt de scriptie ook een nieuwe spanning-gebaseerde parameterisatiebenadering voor die ervoor zorgt dat de structurele informatie en de onderliggende continue mechanica behouden blijven bij het synthetiseren van de gereduceerde balkmodellen - een mogelijke oplossing voor het eerder genoemde controleparadigma van precisie versus snelheid. Om de numerieke prestaties verder te verbeteren, worden ook spatio-temporele integratieschema's voorgesteld die de geometrische structuur van dergelijke zachte balkmodellen benutten, wat resulteert in real-time simulatie met voldoende numerieke precisie die specifiek is afgestemd op controle.

Het derde deel van de scriptie behandelt de ontwikkeling van op modellen gebaseerde controllers die kunnen worden gebruikt in verschillende controle scenario's vergelijkbaar met de controle voor traditionele rigide robotica, bijvoorbeeld inverse kinematica en bewegingsplanning, set-point stabilisatie, traject volgen en multi-point grijpen van objecten. De stabiliserende controller is geworteld in een op energie gebaseerde formulering, die robuustheid biedt, zelfs wanneer er sprake is van materiaalonzekerheden. De effectiviteit van de controller wordt zowel in simu-

latie als in experimenten aangetoond voor verschillende zachte robotica-systeem die een gelijkenis vertonen met de biologie, bijvoorbeeld de slurf van een olifant of de tentakel van een octopus.

De belangrijkste bijdrage van de scriptie is een verzameling multidisciplinaire tools gecomprimeerd in één algemeen framework voor het ontwerp, de modellering en de controle van een klasse van zachte robots, variërend van het theoretische tot het experimentele domein.

Trefwoorden: Zachte robots, hyper-redundante robots, ontwerpopimalisatie, continuümmechanica, model-gebaseerd regelen, 3D-printen.

Societal summary

Soft robotics is an emerging field that focuses on the design, development, and implementation of robots made from soft, flexible materials. Unlike traditional rigid robots, soft robots are able to mimic the movements and behaviors of living organisms, making them well-suited for a wide range of applications in fields such as healthcare, manufacturing, and robotic exploration.

One of the main benefits of soft robotics is their ability to interact with humans and delicate objects in a safe and gentle way. Soft robots can be designed to be compliant and adaptable, allowing them to work in close proximity to people without causing harm. They can also be used in healthcare applications, such as wearable devices and prosthetics, where their flexibility and ability to conform to the human body can provide greater comfort and functionality than traditional rigid devices. Another advantage of soft robotics is their ability to operate in unstructured and unpredictable environments, such as disaster zones or outer space. Soft robots can change shape and adapt to their surroundings, making them more versatile and capable of performing a wide range of tasks. For example, soft robots can be designed to crawl through small spaces, squeeze through tight openings, and manipulate objects with greater precision than rigid robots.

However, there are also challenges associated with the development and implementation of soft robotics. One major challenge is the complexity of designing and controlling soft robots, which often requires sophisticated algorithms and advanced materials. Additionally, there is a need for more research into the long-term durability and reliability of soft robots, particularly in harsh or extreme environments.

Despite these challenges, the potential benefits of soft robotics are significant, and the field continues to grow and evolve. As more researchers and engineers develop new materials, technologies, and applications for soft robots, we can expect to see these versatile and adaptable machines play an increasingly integral role in our lives and society.

Nomenclature

Vector and matrix notations

x	Scalar notation
\boldsymbol{x}	Vector notation
\boldsymbol{X}	Matrix notation
$\boldsymbol{\chi}$	Tensor notation
\mathcal{Q}	Manifold
$T_{\mathcal{Q}}$	Tangent space of \mathcal{Q}

Set notations

\emptyset	Empty set
\mathbb{R}	Set of real numbers
\mathbb{R}^n	n -dimensional Euclidean space
$\mathbb{R}_{>0}$	Strictly positive reals
$\mathbb{R}_{\geq 0}$	Positive reals
\mathbb{N}	Set of natural numbers
\mathbb{T}	Compact time domain
\mathbb{X}	Compact set in \mathbb{R} (<i>i.e.</i> , line segment)
\mathbb{V}	Compact set in \mathbb{R}^2 or \mathbb{R}^3 (<i>i.e.</i> , volume)

Groups

id	Identity group
$\text{SO}(3)$	Lie group of rotations on \mathbb{R}^3 (<i>i.e.</i> , special orthonormal matrices)
$\text{SE}(3)$	Lie group of homogeneous transformations on \mathbb{R}^3
$\text{se}(3)$	Lie algebra of $\text{SO}(3)$
$\text{so}(3)$	Lie algebra of $\text{SE}(3)$

Vector- and matrix operations

$(\cdot)^\top$	Transpose
$(\cdot)'$	First time derivative
$(\cdot)''$	Second time derivative
$(\hat{\cdot}), (\cdot)^\wedge$	Isomorphism from $\mathbb{R}^6 \rightarrow \text{se}(3)$
$(\cdot), (\cdot)^\vee$	Isomorphism from $\text{se}(3) \rightarrow \mathbb{R}^6$
$(\cdot)^\circ$	Reference or rest configuration
$(\cdot)^*$	Optimal solution
$(\cdot)^{-1}$	Square matrix inverse
$(\cdot)^\dagger$	Moore-Penrose pseudo inverse
$(\cdot)^+$	Generalized matrix inverse
$(\cdot)^\perp$	Annihilator

Operators and letter-like symbols

δ	Variation of a field
∂	Boundary of a set
int	Interior of a set
\sup_t	Supremum over continuous time t
\dim	Dimension of vector
trace	Trace of matrix
diag	Diagonal of matrix
blkdiag	Block diagonal of matrices
$\text{Ad}(\cdot)$	Adjoint action on Lie group
$\text{ad}(\cdot)$	Adjoint action on Lie algebra
\exp_G	Exponential map on the Lie group G
\log_G	Logarithmic map on the Lie group G
T_G	Tangent map on the Lie group G
$\ \cdot\ $	Euclidean norm
$\ \cdot\ _X$	Matrix norm
$\ \cdot\ _{\text{rms}}$	Root-mean-square norm
$\lfloor \cdot \rfloor_i$	Floor operator upto i
$\lceil \cdot \rceil_i$	Ceiling operator from i

Acronyms

CoM	Center of mass
DoF	Degree of freedom
FEM	Finite element method (or model)
MDE	Matrix differential equation
ODE	Ordinary differential equation
PDE	Partial differential equation
PMDE	Partial matrix differential equation
PneuNet	Pneumatic network (actuator)
SRM	Soft robotic manipulator
Sorotoki	Soft robotics toolkit
TopoOpt	Topology Optimization

Contents

Abstract	v
Samenvatting	vii
Societal summary	xi
Nomenclature	xiii
1 Soft robotics – a new perspective	1
1.1 Soft robots: what are they?	1
1.2 Soft robotics from a biometric perspective	3
1.3 State-of-the-art solutions in soft robotics	7
1.3.1 Soft fluidic actuators inspired by muscular hydrostats	7
1.3.2 Human-driven design versus design optimization	8
1.3.3 Model-based control for soft robots	10
1.4 Research objective	12
1.5 Research questions and contributions	13
1.6 Outline of the thesis	17
2 A brief historical overview on the progress of soft robotics	19
2.1 Early soft robotic technology	21
2.2 Recognition of soft robotics' potential	23
2.3 Modern soft robotics boom in academia	28
2.4 Tailoring design of fluidic soft actuation	29
2.4.1 Engineering principles in soft fluidic actuators	29
2.4.2 Exploring optimization and evolutionary algorithms	30
2.5 Gaining performance using feedback control	31
2.5.1 Control-oriented models for soft robots	32
2.5.2 Soft robot simulation and programming environments	34
2.5.3 Closing the loop in soft robotics	34
2.6 Summary	35

3 Gradient-based optimization for soft robots	37
3.1 Introduction	38
3.2 Nonlinear finite element method	39
3.2.1 Strain theory in continuum mechanics	40
3.2.2 Isotropic hyperelasticity materials	41
3.2.3 Variational principle of energy minimization	42
3.2.4 Solving the energy balance via polygonal elements	43
3.3 Nonlinear topology optimization	46
3.3.1 Solid Isotropic Material With Penalization (SIMP)	46
3.3.2 Artificial fluidic loads by elemental dilation	47
3.3.3 Optimization problem	48
3.3.4 Solver and sensitivity analysis	49
3.3.5 Gradient filters and interpolation	51
3.4 Numerical examples: generating soft robotic topologies	52
3.4.1 Linear translational soft actuators	52
3.4.2 Pinching soft grippers	53
3.4.3 Bending soft actuator – PneuNet inspired	55
3.4.4 Solutions for varying material parameters	56
3.5 Conclusion	58
4 Dynamic modeling of soft robots – PCC case	59
4.1 Introduction	60
4.2 Pneumatic soft continuum manipulator	63
4.3 Generalized models for soft manipulators	64
4.3.1 Piecewise curve kinematics	66
4.3.2 Piecewise curve dynamics using Euler-Lagrange	72
4.3.3 Overall dynamic model	74
4.4 Extension to multi-link systems	75
4.5 Accelerated computation of PDE-like systems	76
4.6 Parameter identification	78
4.6.1 Finite element method and hyper-elasticity	78
4.6.2 Hyperelasticity in joint space	81
4.6.3 Viscoelastic creep	84
4.7 Passivity-based adaptive control	85
4.8 Overview of experimental platform	87
4.9 Numerical and experimental implementation	88
4.10 Conclusion	102
5 Port-Hamiltonian Cosserat models – beyond the PCC	105
5.1 Introduction	106
5.2 Generalized models for soft manipulators	107
5.2.1 Preliminaries on geometric Cosserat theory	107
5.2.2 Local strain and velocity	109
5.2.3 Finite-dimensional projection	112

5.2.4	Reduced-order kinematics	114
5.2.5	Reduced-order dynamics using Newton-Euler	115
5.2.6	Tendon and fluidic actuation	119
5.2.7	Port-Hamiltonian formulation	119
5.3	Energy-based controller for tasks on SE(3)	120
5.4	Simulation studies of bio-inspired soft robots	121
5.4.1	Soft robot manipulator inspired by octopus' tentacle	122
5.4.2	Multi-link soft robot inspired by the elephant's trunk	125
5.5	Achieving bio-inspired motion through energy-based control	128
5.6	On modal truncation: applying reduced-order model-based controllers to high-dimensional models of continuum soft robots	132
5.7	Conclusion	136
6	Sorotoki: a MATLAB toolkit for soft robots	139
6.1	Introduction	140
6.1.1	Problem formulation	140
6.1.2	Contribution of Sorotoki software	143
6.2	Related works	144
6.3	Getting started with Sorotoki	148
6.4	Open-source soft robots of Sorotoki	148
6.5	Software architecture	151
6.5.1	Signed Distance Function (Sdf)	151
6.5.2	Mesh generation for finite element analysis (Mesh)	154
6.5.3	Finite element modeling (Fem)	156
6.5.4	Reduced-order soft beam models (Shapes)	165
6.5.5	Model composer (Model)	174
6.5.6	Fluidic control hardware (Control)	180
6.5.7	Computer vision (Vision)	180
6.6	Soft robotics study cases	182
6.6.1	Multi-legged soft passive walker	182
6.6.2	Computational design of bending PneuNet actuator	186
6.6.3	Dynamic manipulation of high dexterity soft gripper	190
6.6.4	Environmental impedance control of soft manipulator	195
6.6.5	Contact robust shape sensing of elastomer soft actuator	199
6.7	Conclusion and future work	202
7	Conclusions, recommendations, and future outlook	203
7.1	Conclusions	203
7.2	Recommendations	206
I	Appendices	211
A	List of definitions	213

B Appendices to Chapter 3	215
B.1 Wachspress shape functions for polygons	215
B.2 Element formulation for the Lagrangian strain	217
B.3 Piolla stress tensor and stress-strain tangent for the nearly incompressible Yeoh model	219
C Appendices to Chapter 4	221
C.1 Adjoint actions on SE(3) and se(3)	221
C.2 Passivity properties of the inertia matrix	221
C.3 Implicit trapezoidal time integration	222
D Appendices to Chapter 5	225
D.1 Preliminaries on Lie group theory	225
D.1.1 Basic definition(s)	225
D.1.2 Exponential and logarithmic map	226
D.2 Time-differentiation of the geometric Jacobian for continuum deformable robots	227
D.3 Derivation of the generalized linear stiffness and damping matrix for continuum robots	228
E Appendices to Chapter 6	231
E.1 Newmark- β solver	231
Bibliography	233
List of publications	253
About the author	255

1

Soft robotics – a new perspective on biomimicry

1.1 Soft robots: what are they?

Biological systems have long been a source of inspiration for roboticists seeking to create machines with astonishing resilience and capabilities. While humans can effortlessly interact with a wide variety of objects, conventional rigid robots require precise knowledge of an object's weight, shape, and orientation to safely and reliably interact with it. The field of soft robotics has emerged as a new discipline that incorporates methodologies commonly found in nature. Soft robots are constructed from highly compliant materials, and the term "*soft*" is used in contrast to rigid robots, but also refers to the flexible, compressible, and environmentally robust properties associated with soft materials. To achieve bio-like performance in modern machines, researchers believe that the general lack of material diversity in robotics may be the missing piece of the puzzle.

In engineering, a common way to convey a measure of elasticity is Young's modulus. While limited to homogeneous materials subject to small deformations, it can still be applied to classify rigidity in robotics. To assist the reader, we have included a spectrum of different materials in Figure 1.1. A careful observation of this spectrum reveals that biological organisms are primarily composed of low-modulus materials (ranging from 10^4 to 10^7 Pa), such as muscle and skin tissue, with rigid materials (such as bone) being much less prevalent. In contrast, conventional robotics predominantly rely on hard materials such as metals and hard plastics. Furthermore, it is worth noting that materials which undergo repeated deformation during motion possess correspondingly low elastic moduli, as opposed to rigid materials in classical robotics. The concept of exploring low-

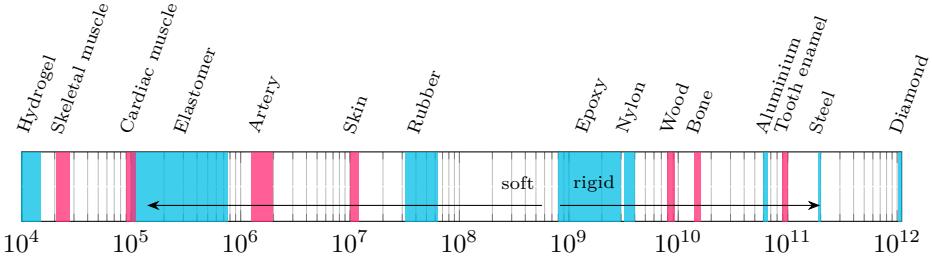


Figure 1.1. Young's modulus spectrum in (Pa) of rigid and soft materials, where (—) are the organic (*i.e.*, biological) materials and (—) inorganic materials. Modulus scale is adopted from the work of Rus et al. [230].

elasticity materials, collectively referred to as "*soft materials*," has fostered a new philosophy in robotics aimed at unifying robots and biology. Although there exist many definitions of soft materials, we propose the following description:

Soft materials are homogeneous materials with a Young's modulus, often referred to as the elasticity modulus, that is typically less than or equal to 10^9 Pa. The term **softness** or **soft** refers to the collective mechanical properties that are commonly associated with materials inside this spectrum¹.

Now, despite the fact that the words "*soft*" and "*robotics*" have clear definitions independently, the collocation of the two has sparked many new ideas and perspectives within the robotics community for the past two decades, especially those aimed at harmonizing robotics and nature. Figure 1.2 exemplifies a range of soft robots that have been specifically developed to mimic biological organisms. Throughout its young academic life, several definitions have been coined. Initially, soft robotics referred to robots with variable joint stiffness [4] or artificial compliance achieved through control [3]. The term was also used to underline the shift from rigid-linked robots to "*bio-inspired continuum robots are inherently compliant and that exhibit large strains in normal operations*" [289]. Paraphrasing the work of Robison et al. [224]: "*soft robotic manipulators are continuum robots made of soft materials that undergo continuous elastic deformation and produce motion through the generation of a smooth backbone curve*". Alternatively, a broader definition was coined in a review by Kim et al. [147] simply referring to soft-bodied robots as "*an analogy to soft-bodied animals*". A concise definition was proposed by Laschi et al. [155], as soft robots being "*any robot built by soft materials*". Rus et al. [230] defined soft robots in terms of their structural elasticity: "*Systems that are capable of autonomous behavior, and that are primarily composed of materials with moduli in the range of that of soft biological materials*".

¹It is important to note that the terms "*soft*" and "*flexible*" do not hold identical meanings as per the aforementioned definition. For example, slender metal rods are classified as flexible but not soft, as the Young's modulus is not within the pre-specified material range.

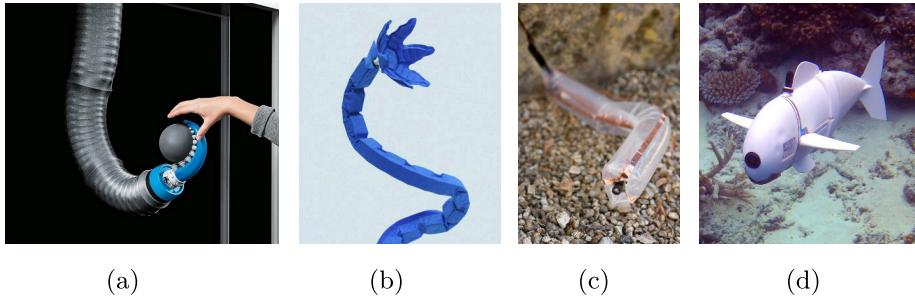


Figure 1.2. Examples of soft robotic systems that draw inspiration from nature: (a) Festo’s Bionic arm, inspired by the elephant’s trunk but with an octopus-inspired gripper [103]. (b) Vacuum-driven origami-inspired artificial muscles by Li et al. [162]. (c) Vine-inspired inspection soft robot by Hawkes et al. [106]. (d) Soft robotic fish by Katszschmann et al. [134], composed of fluid-driven soft actuators by [175].

The ongoing debate regarding the precise terminology for soft robotics may never reach a definitive conclusion. It is of utmost importance to establish a uniform vocabulary, not just for the sake of this thesis, but also to ensure effective communication across a wider scientific community. Previous definitions have placed great emphasis on the natural motion that arises from soft materials with high similarities to nature. In this thesis, we propose our definition of "*soft robots*" based on the historical development of soft robotics and current scientific trends in literature (discussed in Chapter 2), with a particular focus on design and control. Given the interdisciplinary nature of the field, the terms used in this thesis may differ from those used in existing literature. Throughout the thesis, we will refer to the following definition when discussing "*soft robotics*":

Soft robotics is a subclass of robotics with purposefully designed compliant actuators embedded into their soft body that enable control over the robot’s natural ability to perform bio-inspired morphological behavior.

The formulation above, modified from an early definition proposed in [69], emphasizes the significance of soft materials in replicating biological motion, also known as "*biomimicry*" or "*biomimetics*". Soft robotics represents the first stepping stone in the pursuit of harmonizing robotics and biological principles. This newly adopted field of soft robotics delves into the use of soft materials not only from a design perspective but also with regard to their implications for control, with the aim of recovering biological morphologies.

1.2 Soft robotics from a biometric perspective

The octopus is a fascinating subject of study in the field of soft robotics [42, 148, 155, 189, 222, 230, 306]. Unlike animals with rigid skeletons, the octopus has compact arrays of muscle tissue that stiffen and soften when they move. Its eight soft

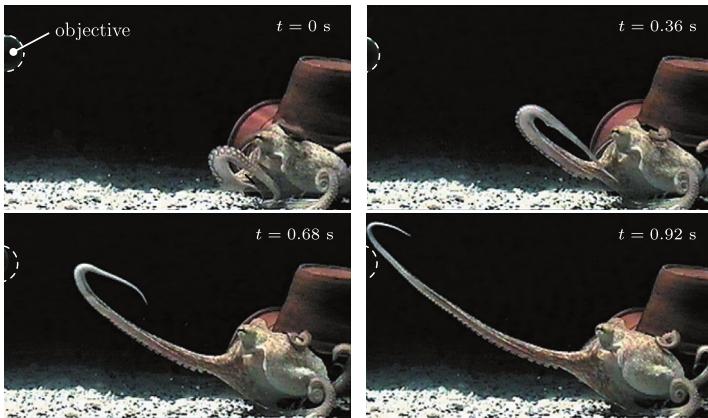


Figure 1.3. Recording of an octopus extending its tentacle towards an object of interest, using coordinated activation of a tightly packed network of muscle fibers. The highly flexible appendage allows for traveling bending wave propagation, while the octopus orients its suckers towards the object to ensure a secure grip [260].

appendages have virtually infinite degrees of freedom (DoF) [138, 142, 260]. The exceptional dexterity of the octopus arms results from their behavior as muscular hydrostats. These arms are composed of densely packed muscle fibers whose orientation can be grouped into transverse, longitudinal, and oblique axes [143]. Each arm can control itself semi-independently from the central brain and is controlled by a decentralized peripheral nervous system that runs axially along each tentacle. Motor control in the octopus arises from approximately 500 million neurons in its body, two-thirds of which are distributed among its limbs, enabling semi-independent control from the central brain. When a tentacle receives a command from the central brain, such as "*find food*," it gathers its own sensory and position data, processes it, and issues its own motor coordination on how to start motion by stiffening or relaxing its muscular network [142, 260]. This remarkable ability to coordinate movement and control each arm independently has inspired soft robotics researchers to develop new approaches to robotic design and control. An example of the amazing behavioral motor abilities of the octopus is shown in Figure 1.3 (obtained from [260]). The figure presents a visual of an octopus attempting to grasp a food particle, which denotes a possible inspiration for many soft robotic systems. Interestingly, the octopus exhibits a remarkable behavior of simultaneous bending and twisting propagation motion to orient the bottom side of its tentacles towards the target.

This exemplifies the remarkable ability of animals to accomplish a hierarchy of tasks, attributed to the hyper-redundancies in their morphological structure. Hyper-redundancy [47, 49, 230] implies that the system possesses many additional DoFs than are strictly necessary to complete a given task. Consequently, free joints can be assigned to sub-tasks that run in parallel. This ability allows many organisms to passively adapt to their environment without affecting the primary motion. These attributes are highly sought after in modern robotic systems [66, 197, 255]

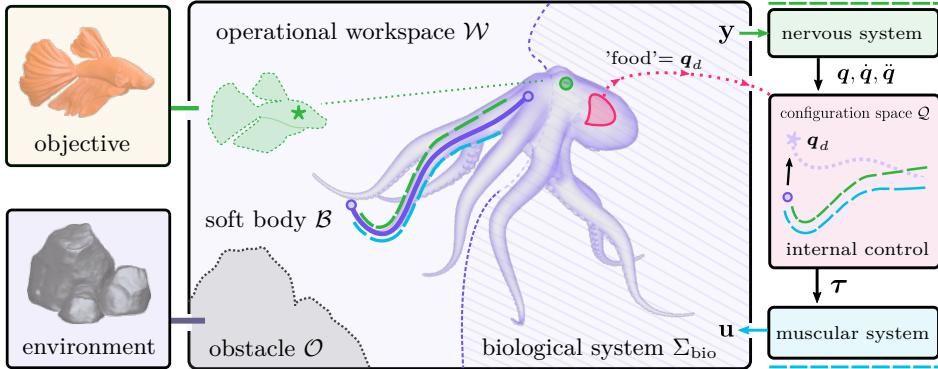


Figure 1.4. A schematic representation of the control architecture of an octopus-inspired soft robot with embodied intelligence. The architecture illustrates the flow of information among significant biological components, including the body (*e.g.*, soft, deformable arm), actuators (*e.g.*, a network of muscle fibers), sensors, and decentralized controller (*i.e.*, peripheral nervous system), and the brain responsible for coordination.

as they enable robustness in unstructured environments and environmental durability, especially regarding impact.

As shown in Figure 1.3, the success of biological systems cannot be attributed to their morphological design alone; rather, it is the interplay between physical structure and coordinated motor control that enables their functionality. To effectively implement embodied intelligence in soft robotics, it is crucial to consider the entire embodiment of the bio-inspired system, which thus encompasses both design and control [106, 230]. Given the multidisciplinary nature of soft robotics, it is important to clarify the distinction between these two aspects:

Design is the process of developing the structure of the soft robot that enables it to perform specific tasks within a predefined workspace. **Control**, on the other hand, refers to the process of finding control laws that steer the robotic system towards a desired static or dynamic behavior.

Recognizing the fact that the body and brain are equal partners in supporting intelligent behavior, we hypothesize a deconstruction of the morphological behavior that underlies the grasping example in Figure 1.3. This is illustrated in Figure 1.4, which presents a schematic representation of a biological system Σ_{bio} . The control objective is to reduce the distance between the prey and one tentacle, denoted by the continuum body $\mathcal{B} \subset \mathbb{R}^3$. Such a soft appendage consists of discrete bundles of muscle fibers for motion and nerve fibers for sensing, which are denoted by the inputs u (*e.g.*, muscle activation) and outputs y (*e.g.*, nerve potentials) as shown in Figure 1.4, respectively. Due to physical design limitations, there is only a finite number of actuators and sensors that can be composed within the body.

This yields a compact region called the "*operational workspace*" \mathcal{W} [197, 203, 255] in which the system can operate. Even though the body has virtually infinite DoF, it can only be controlled via a finite number of inputs \mathbf{u} , and thus soft robots are inherently underactuated [255, 273]. This is further emphasized by possible input saturations, such as the inability for uniaxial extension of the muscle fiber network, which is often resolved using antagonistic design. Part of the soft robot design problem is therefore finding an appropriate composition of the inputs \mathbf{u} such that the system's reachability space \mathcal{W} coincides with the desired task with sufficient kinematic redundancies. A variation where the structural deformations of \mathcal{B} are tuned is called "*optimal shape design*" [19]. This involves altering the shape of \mathcal{B} to achieve the desired deformation but fixing \mathbf{u} in space and time. Given the continuum nature of soft robots, as well as their distributed actuation, sensing, and mechanical saturations, such design problems are not trivially solved [21, 56, 251, 283, 316].

On the other hand, control involves determining a control law for the network of actuators \mathbf{u} that steers the octopus' arm towards its desired goal. Regarding Figure 1.4, two mechanisms of closed-loop control can be observed. The first mechanism employs proprioceptive sensors, which are strain-sensing neurons responsible for controlling muscle contractions and measuring joint position. The second mechanism utilizes visual feedback to inform the soft appendage about the desired setpoint relative to the task. To coordinate motion, the octopus must possess a fundamental understanding of the relationship between the inputs and outputs of its soft arm. From an engineering perspective, the dynamics associated with the motion of the continuum body \mathcal{B} can be modeled via Partial Differential Equations (PDEs) that characterize the deformation in both space and time [12, 70, 230]. This leads to the well-known issue of infinite-dimensionality [72, 115, 187], which infers that such models often lack closed-form solutions. However, this raises a fundamental question: *How do octopi and other invertebrate animals accurately predict their continuous motion without any apparent difficulty?*

A solution might be found in dimensional reduction. Assuming that the motor neurons controlling the movement have limited memory and cognitive capabilities, the octopus likely perceives its soft arm as having only a finite number of DOFs to enable online motion prediction. This may suggest that the continuum joints of the arms, processed by the decentralized controllers, are possibly represented by a reduced state \mathbf{q} belonging to a finite-dimensional configuration space \mathcal{Q} . As such, biological systems may be able to unconsciously identify internal dynamics models based on a reduced representation alone, *e.g.*, $\ddot{\mathbf{q}} = \mathbf{f}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{u})$, that predict how their continuum appendages will evolve over time given the inputs \mathbf{u} and the initial conditions \mathbf{q}_0 and $\dot{\mathbf{q}}_0$. Notably, these dynamic models can serve as a control framework for introducing stabilizing feedback terms to the input \mathbf{u} that ensures convergences towards a desired setpoint. This, however, highlights the main challenge in modeling soft robots; namely (*i*) identifying an appropriate dimensional reduction that preserves both accuracy and computational tractability [70], and (*ii*) finding control structures applicable to such reduced-order models.

In the field of soft robotics, the aforementioned paradigms have attracted a large audience from the robotics control community. Researchers explore various controllers, including model-based approaches [12, 70, 87, 186], data-driven methods [5, 34], and machine learning techniques [144, 236, 281, 282]. The use of dynamical models, whether data-driven or physics-based, in open-loop or closed-loop systems; is essential in enabling effective control strategies that strive for superior performance and robustness. The absence of such models would pose significant challenges in developing efficient control strategies.

1.3 State-of-the-art solutions in soft robotics

Driven by the aspiration for bio-like performance in robotics, there have been significant advances in the development of continuum soft robots since the early 2000s. Besides octopi [42, 181, 222], various researchers draw inspiration from a plethora of biological organisms such as fish [134, 174], elephants' trunks [98, 129, 306], snakes [95, 174, 218], birds [95, 328], and even the human hand [89, 293]. Researchers have discovered several ways to mimic biology by harmonizing soft materials and robotics. This section offers a brief overview of the state-of-the-art solutions concerning design and control.

Remark 1.1 Considering the extensive scope of soft robotics, an additional chapter (Chapter 2) has been included to provide a more comprehensive overview of its origins dating back to the early 1980s, as well as the various research aspects currently associated with this field. Thus, the following section serves as a preliminary introduction, ensuring brevity in the following section while setting the stage for the research problems relevant to the scope of the thesis.

1.3.1 Soft fluidic actuators inspired by muscular hydrostats

Conventional soft robots are characterized by their continuum-bodied motion that arises from a network of compliant actuators embedded throughout its soft body. There exist many options for such embodied actuation, including tendons [223, 228], chemical reactions [18, 119], light-driven liquid crystals [62, 63, 294], and ferromagnetic materials [149, 296], and hydrogels [126, 156]. However, the most common approach is fluidic actuation [71, 78, 134, 174, 206, 293] that mimics muscular hydrostats found in animals. The latter are commonly referred to as "*Soft Fluidic Actuators*" (SFAs), and the majority are designed via human-driven techniques. In this section, we aim to provide a brief explanation of SFA technology and explore the potential benefits of incorporating structural optimization into the design process alongside the common human-driven design techniques.

Soft fluidic actuators are inflatable fluidic channels that are embedded into an elastic soft body. When pressurized fluid is applied, the elastic pressure vessel uniformly distributes the internal stresses along the interior, resulting in motion due to strain relaxation of the surrounding continuum body. Since elasticity is

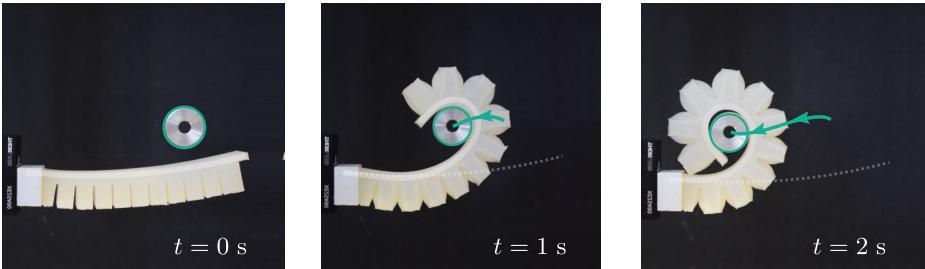


Figure 1.5. An illustrative example of a fluidic PneuNet actuator [195] reaching and grasping a 20 mm aluminum cylinder, which is inspired by the morphological grasping motion of the octopus' soft arm [260] as seen in Figure 1.3. The main body is composed of Dragonskin™ 10A silicone, and 30A for the bottom layer. It is worth noting that despite using open-loop motion control (*i.e.*, linear pressure ramp of 40 kPa), the enveloping properties of soft materials can lead to the emergence of complex "intelligent" behavior.

key, silicone rubbers are commonly employed for their notable material properties. Specifically, silicone rubbers exhibit a low Young's modulus, only display material fatigue at high strains exceeding 100%, and offer many commercial alternatives. By exploring purposefully designed asymmetrical geometries, often created by hand, predictable motion can be guided [120, 230, 316]. The aforementioned principles are analogous to those of (semi-rigid) compliant mechanisms, which flexible structures that facilitate motion or force transmission through elastic deformation of their components, as opposed to conventional rigid-body joints. Through the exploration of structural geometries or deliberate incorporation of stiffer materials, a diverse range of motion primitives can be achieved which may include bending, twisting, and elongation.

1.3.2 Systematic design of soft fluidic actuation: human-driven versus design optimization

A popular example of a soft fluidic actuator (SFA) is the PneuNet actuator, which was proposed by Mosadegh et al. [195]. This actuator has a consistent linear input-output bending behavior and its design is simple, easy to fabricate, and repeatable, making it a standard in the academic field. To illustrate the capabilities, in Figure 1.5, we present an example of it grasping an aluminum cylinder, inspired by the octopus example mentioned earlier [260]. Despite using rudimentary open-loop control, the system can emulate complex behaviors such as reaching, grasping, and pulling objects closer through manipulation, similar to those exhibited by the octopus. As shown in Figure 1.5, an important property is that the inherent mechanical impedance allows for safe and stable interactions with objects of varying rigidity, even without environmental perception. This contrasts rigid robots interacting with unknown environments, where impedance control appears to be a necessary requirement [66, 197].

Given its success in open-loop, common applications for SFA (Soft Fluidic Actuator) technology are therefore soft grippers [10, 91, 113, 120, 244] that are

useful in handling delicate objects. Pushing the technology further, system dexterity has been extended by incorporating many different SFAs into one single body, similar to muscle groups in animals. Consequently, researchers have explored their potential for enabling highly dexterous robots capable of in-hand manipulation [101, 261], as well as autonomous terrestrial and aquatic locomotion [53, 73, 134, 262]. Although SFAs provide a wide range of motion, they require significant amounts of supplied volume inflow, which adversely affects their speed, compactness, and efficiency [206, 230, 316]. A common nonlinear phenomenon called "*ballooning*" occurs when the elastic membrane of the changes deforms significantly, further increasing the channel's volumetric capacitance. This behavior is particularly evident in soft materials that exhibit strain softening nonlinearities, which intensifies this inefficient expansion. In order to address the aforementioned limitations, various researchers have proposed two potential solutions. The first involves the use of hand-designed geometrical features, such as ribs, which increase structural compliance. The second solution involves the utilization of composites made up of different materials. One example of this approach is demonstrated in the work of Polygerinos et al. [212, 213], as well as other similar studies [54, 89, 261]. These studies employ fiber-reinforced SFAs that incorporate fiber weaves to create new soft material composites. The introduction of such weaves results in anisotropic mechanical properties due to the fibers having a low bending-twist modulus but high elongation modulus. Additionally, various weave patterns can be used to steer the deformation characteristics towards a desired kinematic profile [59, 148], or as proprioceptive sensors using magnetic inductance [80, 81] or strain sensors made from EGaIn (Eutectic Gallium Indium) [208, 269]. Recently, multi-material 3D-printing approaches have also been employed, combining actuation with integrated sensing [311, 326]. It is noteworthy that the advent of Additive Manufacturing (AM) technology has significantly contributed to the advancement of soft robotics technology, enabling flexibility in design and materials, surpassing what was previously achievable with subtractive techniques.

Like in nature, there are often no unique design solutions when finding the optimal geometrical shape, material composites, and actuation type, or a combination of the aforementioned. While such design freedom has its benefits, it also poses challenges in establishing effective hand-driven design solutions that are tailored towards functionality. Furthermore, predicting structural deformation *a-priori* is challenging and often requires time-consuming numerical simulations. In response, optimization-based solutions are slowly being considered. Cheney et al. [46] employed a compositional pattern-producing network (CPPN) to determine the most efficient arrangement of soft material voxels and activation patterns, thereby facilitating the synthesis of soft robots capable of terrestrial and aquatic locomotion in simulation. Following that, Kriegman et al. [152] explored auto-generative processes for a variety of candidate creatures in silico, with the aim of achieving specific motor functions like locomotion, object manipulation, and transport.

Although voxel-based [46, 152] and commonly parametric shape optimization [57, 173, 194] approaches have demonstrated success in soft robot design, these

methods are inherently imposed by design restrictions that may perhaps limit the design possibilities in soft robotics, especially given the recent advances in Additive Manufacturing (AM). In contrast, topology optimization [19, 90, 268, 295, 322] (TopOpt) is a versatile technique that enables the design of structures with desired functionality without imposing significant design constraints. Furthermore, TopOpt approaches explore gradient-based optimizers derived from continuum theory that allow accurate descriptions of nonlinear deformations, which are simplified in many schemes for computation speed. Wang et al. [300] and Tian et al. [283] explored TopOpt for soft grippers using tendons and ferromagnets, respectively. Yuhn et al. [320] extended density-based optimization to include time as an additional variable, allowing for simultaneous optimization of structure and movement with gradient-based methods through 4-dimensional TopOpt. However, research on TopOpt applied to fluidic soft actuators is limited, perhaps due to the challenges associated with modeling fluid-structure interaction in adaptive structures.

1.3.3 Model-based control for soft robots

In a previous discussion, we showed that the open-loop approach can accomplish various complex tasks such as locomotion [53, 134, 262], grasping [262], and manipulation [176]. While open-loop control has been successfully demonstrated, it ultimately relies on *a priori* system knowledge that determines the control logic based on numerical surrogate models or experimental regression. This, independent of using open-loop strategies, further establishes the importance of modeling, which is nowadays a crucial ingredient for modern robotics [141, 197, 255]. In the early days of soft robotics, model-based control strategies were deemed unfeasible due to the infinite-dimensional nature of these systems [72]. Over the last two decades, however, a plethora of modeling solutions have surfaced, paving the way for sophisticated model-based controllers, which are expected to push the dexterity of soft robotics systems even beyond what is already achievable in open-loop.

A common modeling approach is the Finite Element Method (FEM), which involves spatially discretizing continuum solids into a group of "*finite elements*," permitting the underlying Partial Differential Equation to be rewritten as an approximate Ordinary Differential Equation (ODE) [115, 146]. These can be solved straightforwardly using standard numerical integration (*e.g.*, `ode45`, `ode23t` in MATLAB[®]). While primarily explored for quasi-static behavior, FEM models have demonstrated their efficacy in handling hyperelasticity, geometric nonlinearities due to large deformation, fluid-structure interactions, and other multi-physical domains [120, 171, 191, 250, 316]. Motivated by the assumption that quasi-static models provide sufficiently accuracy to describe soft robots under slow-varying dynamics, open-loop forward kinematic controllers are used that inversely search the input space for the desired deformation profile [21, 174, 176]. Alternatively, high-fidelity FEM data can be fed into neural networks approximators [79, 325] or Quadratic Programming (QP) algorithms [21] that tackle the inverse kinematic problem directly. Yet, the high-dimensionality of these models, with sometimes millions of DoFs, poses a significant challenge when considering dynamic behavior

[75, 100], thereby limiting their applicability for closed-loop feedback control. Undoubtedly, the significant interest of soft robotics in both academic and industrial sectors arises from its potential applications in dynamic conditions. For example, one of the key advantage is its ability to withstand high-velocity impacts, making it an attractive option for grippers use over rigid options. Another advantage involves converting kinetic energy into potential energy through reversible elastic deformation, which is challenging to achieve with fully rigid robotic systems.

A viable solution for reducing dimensionality of FEM is found in Proper Orthogonal Decomposition (POD). Here, time-series data is collected, and through singular value decomposition, the principal dynamic modes are identified and combined to construct a reduced linear dynamical model. Not only does this approach improve speed, but it also preserves accurate, robust, and efficient models suited for closed-loop controller design [100]. Recent extensions [241] preserve even nonlinear deformations and self-contact. The proposed modeling approach is encapsulated in an open-source software called SOFA [56, 76], which facilitated a wide range of closed-loop controller designs contributed by an active community in past years [76, 100, 154, 161, 312]. Furthermore, it has been successfully implemented in physical systems, and recently Reinforcement Learning (RL) methods have been explored [236]. Alternatively, Koopman system identification tools form a data-driven approach that can be applied directly to experimental data (*e.g.*, measurements from optical markers placed on the exterior of the soft robot), leading to discrete-time dynamical systems. By gathering measured data alone, accurate models of the true system can be identified [34, 151]. These models are often followed by Model-Predictive Control (MPC) approaches [33, 34].

Another common approach for modeling soft robots is based on the Elastica theory, where the volumetric soft body is represented by a smooth backbone which captures its geometric features. The method, often referred to as "*soft beam*" models, are applicable to a specific subclass of soft robots, including soft manipulators [78, 129, 176, 304], fins [135, 175], and soft legs [74, 293]. Elastica is a general mathematical framework developed by Euler in the 1800s to describe the behavior of elastic rods subjected to external forces [11, 157]. Early approaches include the seminal work of Chirikjian et al. [47–49], presenting hyper-redundant continuum robot model represented by a spatial differentiable curve. Using a modal parametrization, their work presented inverse kinematics solutions, path planning, and grasping strategies [48]. Later, Mochiyama et al. [187, 189] extended their work by developing dynamic formulations that led to shape regulation controllers derived from Lyapunov stability theory [140].

A modern approach for soft beams is the "*Piecewise Constant Curvature*" model (PCC) [304]. This generalizable modeling structure discretizes the one-dimensional backbone curve into finite segments of constant curvature. Hence, all strains except curvature are neglected. Following either Lagrangian or Newton-Euler formulations, the approach leads to soft-bodied formulations which are often synonymous with those of rigid robot models. The PCC approximation exhibits modeling structures that closely resemble those of classical rigid serial-link manipulators.

With slight modifications involving compliance, similar to rigid robots with joint compliance [66, 170], it enables the direct implementation of a collection of classic control approaches [72, 85, 87, 97, 98, 129, 134, 137] applied to soft robots.

However, despite the dimensional advantages over FEM, the PCC approach presents some limitations. First, one such limitation is that the model introduces kinematic singularities and discontinuities for the linear velocity components [129, 130]. These artifacts are byproducts of the bending parametrization, which can potentially lead to destabilization in closed-loop when approaching zero-curvature. Some solutions have been proposed by lifting the state parametrization [68], or singularity avoidance by state jumping [78, 271]. Second, although PCC allows for analytic closed-form dynamics, the resulting models are highly nonlinear, complex, and large. A solution is found in augmented rigid body models, which explore PCC kinematics to describe a lumped-mass model of the continuum robot. These mitigate expensive spatial integration required for computation of the inertial forces. Although lumped-mass models are seemingly an oversimplification compared to FEM, such models have proven to be rather effective [72, 86, 87, 135, 137]. For example, Kazemipour et al. [137] propose an adaptive sliding mode control scheme, which is robust against model parameter uncertainties and unknown input disturbances. The last and perhaps largest limitation is that they are only applicable in restrictive settings where constant curvature holds. They are unfit to capture important continuum phenomena, *e.g.*, gravitational deflection, buckling, self-contact, environmental interaction, or wave propagation.

In contrast to PCC surrogate models, Cosserat beam models have demonstrated an ability to capture a broad range of continuum phenomena [30, 95, 222, 223, 284]. Unlike PCC models, they provide truncatable models derived from continuum mechanics. They also provide a precise representation of the hyper-flexible nature of materials under large deformations and even allow for self-collision [95]. Seminal work by Renda et al. [221, 222] and Boyer et al. [29] proposed computational models of Cosserat beams using Geometrically-Exact finite elements on the Lie group SE(3) [242]. While these models have gained popularity in the soft robotics community, literature on model-based control for Cosserat beam models is slowly emerging when compared to PCC, especially those that consider underactuation and hyper-redundancy that are often identified with these systems.

1.4 Research objective

In short, soft robotics is a rapidly emerging subfield within the broader domain of robotics that focuses on the use of soft materials to create systems capable of dexterous bio-inspired morphological behavior akin to animals, capable of locomotion, grasping, and manipulation. Such features are made possible by the unique mechanical properties intrinsic to soft materials and soft fluidic actuation. Although open-loop control strategies have already established bio-like features, soft robotics still lags behind in terms of precision and speed compared to rigid robotics. To address this gap, new design principles for soft fluidic actuation and

accurate, fast control-oriented models are believed to be crucial missing components. Furthermore, in the context of biological systems, it is not solely their morphological design that accounts for their success. Rather, it is the intricate interplay between their physical structure and coordinated motor control that enables their functionality. This leads us to the main objective of this thesis:

Development and analysis of new systematic tools balanced between the design, modeling, and control of soft continuum robots, which strive for similar capabilities as rigid robotics and eventually biological systems.

1.5 Research questions and contributions

In the subsequent section, we shall discuss the challenges linked to the aforementioned objective and list the contributions made by the thesis. To methodically achieve our research objective, we have divided our research approach into three branches: (I) automated design synthesis of soft fluidic actuators, (II) modeling for control of soft robot manipulators, and (III) the development of software aimed to support the soft robotics community. For each research objective, a number of contributions are listed.

I: Automated design synthesis of soft actuators. Our first research focus is on the design aspect of soft robotics. Upon reviewing the existing literature, it can be observed that soft robotic design is typically approached either through hand-driven principles or numerical optimization. Irrespective of the approach, achieving an optimal structural geometry that fully accommodates hyper-redundancies in soft materials remains a challenging task. Unlike their rigid counterparts and many biological systems for that matter, the kinematics are inherently encoded in the topological structure of the soft materials and where actuation is presented in the system. This implies the workspace cannot be characterized analytically in closed form through joint motions stemming from one point, as is commonly done for joints in rigid robotics. It is therefore of paramount importance that the nonlinear behaviors of soft materials, both in hyper-elasticity and nonlinear geometrical deformation, are understood and accounted for during the design process. This brings us to our first research question (R1):

How do we design fluidic-interacting mechanical structures made from soft materials that deform according to a user-defined morphological pattern?

The fundamental principles of compliant mechanical devices can be rigorously described through continuum mechanics. In this thesis, we aim to integrate the underlying theory of continuum mechanics with the automated design of efficient soft actuators that enable user-defined objectives. To achieve this, we utilize optimization algorithms that seek to minimize user-specified objective functions by optimizing the layout of soft materials. This approach is rooted in continuum

mechanics [115, 146] and its subsequent discretization through FEM method. The aforementioned issue is commonly referred to as an "inverse design problem" - determining the shape from final deformation, rather than deducing the deformation from the shape. The field of combining continuum mechanics and free-form optimization in compliant structures is a well-established area known as "*topology optimization*" [19]. However, such techniques are not easily applicable to soft actuation due to the presence of hyper-elasticity and nonlinear geometric deformations in soft materials. Furthermore, fluidic or pneumatic actuation further complicates the optimization process, as these loads become both design and state-dependent. This leads us to our first contribution:

Contribution I. *Development of efficient algorithms, applicable to the general design of fluidic soft actuators, solving the inverse design problem: Given a desired motion and input, what is accordingly the optimal soft material distribution within a design domain to realize such joint motion?*

After applying such automated algorithms, a plethora of soft actuation systems with varying joint mobility can be developed with ease. However, since these designs originate from simulations, concerns arise regarding their transferability to practical applications. Therefore, we will investigate the transfer of simulation-based designs into functional and feasible soft actuators. Recent advancements in Additive Manufacturing have made it possible to fabricate complex 3D geometries with minimal difficulty and effort. Our second contribution therefore reads:

Contribution II. *Testing and validation of optimized soft fluidic actuators by exploring Additive Manufacturing methods of printable soft materials.*

II: Modeling for control of soft manipulators. The second research path focuses on reduced-order modeling (ROM), aiming to balance precision and speed for control. Parallel to design, modeling for control is a crucial aspect of achieving biological performance. Accurate and fast models are required to achieve this goal. However, the infinite-dimensionality inherent in soft continuum robots poses significant challenges. While the PCC approach and its augmented rigid-body variations have been proposed as a solution, such models do not respect fundamental continuum mechanics. As a result, they impose strict operational constraints on any soft system, such as limiting hyper-elastic nonlinearities or slowing down actuation to prevent dynamic mismatching. This leads to the second and third research questions (R2 and R3) on the topics of modeling and control:

How do we derive dynamic models that offer a reasonable trade-off between the accuracy and its applicability for control?

And, can we adopt classical controllers from rigid to soft robotics?

By building upon the original works of Chirikjian et al. [48] and Mochiyama et al. [187] in the 90s, the thesis presents a dynamic modeling formulation for soft manipulators that better preserves their continuum nature. First, to address the issue of infinite-dimensionality, a reduced-order modeling strategy for soft robot manipulators is proposed, whose mathematical framework is based on the differential geometric theory of spatial curves. Such a framework allows for easy transferability to conventional ROM models in soft robotics, like the PCC strain [72, 78, 135]. However, the thesis proposes two improvements that are essential for the development of model-based controllers. Inspired by the success of FEM-based models in soft robotics [75, 100], we bridge the gap between the PCC model and the underlying continuum mechanics by matching the quasi-static behavior to FEM data. Second, to enhance computational efficiency, new reduced-order integration schemes are required that compute the spatio-temporal dynamics in real-time, thus enabling controller design. This brings us to our third contribution:

Contribution III. *Development of computationally fast and accurate dynamic models for soft manipulators composed of hyper-elastic soft materials that are directly applicable to classical control theory akin to rigid robotics.*

As outlined in Section 1.3.3, the PCC method's piecewise continuity imposes limitations on kinematic redundancies, thereby impeding the exploration of the hyper-redundant nature of soft robots, a fundamental characteristic often lacking in rigid robotics. For instance, constant strains alone cannot adequately capture significant nonlinear deflections caused by gravity, nor can they accurately describe environmental interactions. Hence, the research question (R4) that arises is:

Can we effectively explore the intrinsic morphological flexibilities of soft robots, similar to biology, that are meaningful for modeling and control?

Therefore, the third research objective focuses on relaxing the PCC condition to pursue its true infinite-dimensionality more closely. This is achieved by adopting prior modeling strategies of differential curves, where spatially-varying strain fields are considered and approximated through sets of orthogonal shape functions rather than piecewise representations. Building upon prior models presented in the thesis, the underactuated and hyper-redundant soft system is written in a port-Hamiltonian framework [204, 291], which enables energy-shaping techniques by modifying the closed-loop potential energy of the system – a well-known practice in classical robotics [203, 204, 291]. By exploring the hyper-redundancy in soft robotics, more advanced control objectives can be achieved, allowing for multi-modal shape regulation and full-body grasping. However, spatial discretization in these model-based controllers plays a crucial role in their dexterity to achieve various control tasks. Within this context, the fourth contribution reads:

Contribution IV. *A systematic study of spatial discretization in low-order energy-shaping controllers applied to high-order soft robotic models with a focus on closed-loop performance in shape regulation control.*

1

Contributions III and IV provide a stable modeling platform for a variety of possible shape functions tailored to unique joint mobilities in soft robotic systems. Yet, many works in modeling literature choose such functions in *ad-hoc* fashion, *e.g.*, polynomial bases [29, 49, 72]. Within this context, the thesis explores a (geometric) modal decomposition approach. Similar to the eigenmode analysis in structural dynamics, geometric strain modes are extracted from higher-order (volumetric) FEM simulation data and used to construct optimal soft beam models. The approach leads to fast, accurate, and generic low-dimensional models that encode the geometric features and elasticity of the true soft body into a new strain parametrization, we call the "*Data-driven Variable Strain*" (DVS) basis. A merit benefit of the approach can be naturally expanded to identify the hyper-elastic material parameters and the actuation map of the reduced beam model, which is often miss in PCC models. Our fifth contribution therefore reads:

Contribution V. *A novel method for finite-dimensional model reduction in soft manipulators that explores the mechanical interconnection between structural geometry and flexibility modes of the soft manipulator body.*

C: Software development. Our final research branch is centered around interdisciplinary and the transferal of knowledge towards the soft robotics community. Soft robotics is intrinsically multidisciplinary field since it involves the integration of knowledge and techniques from various scientific disciplines, such as materials science, mechanical and electrical engineering, computer science, and biology. Our final research question (R5) therefore reads:

To enable better designs and controllers within the soft robotics community, how can we bridge the interdisciplinary aspects that are intrinsic to the field?

The thesis integrates all the previously mentioned contributions to form a comprehensive software package for soft robotics, which is referred to as **Sorotoki**. The name is an acronym for "SOft RObotics TOOlKit". The primary objective of this software is to bridge the gap between various disciplines of soft robotics, including design, modeling, and control. It provides a minimal programming framework that enables users to solve complex problems using minimal lines of code. The toolkit is closely integrated with Contributions I to V of this thesis and is publicly available at <https://github.com/BJCaasenbrood/SorotokiCode> [36]. Additionally, the software enables real-time hardware control of fluidics, facilitating the evaluation of model-based controllers on physical systems. We also present



Sorotoki

open-hardware soft robots that can be manufactured using commercial printing methods. Thus, the final contribution of this thesis involves the creation of this software package.

Contribution VI. *Developement of a versatile, user-friendly, open-source software called Sorotoki that envelops the presented theory on design, modeling and control of the thesis into one coherent MATLAB® toolkit.*

1.6 Outline of the thesis

This thesis discusses the design, modeling and control of soft robotic systems. Including this introductory materials, the thesis consists of seven chapters.

Chapter 2 presents a historical overview of the field of soft robotics, complementing the earlier introduction. Chapter 3 introduces the design algorithm for soft actuators aiming to address the inverse design problem. The chapter begins with a brief introduction to continuum mechanics applied to three-dimensional deformation of hyperelastic materials, followed by its numerical implementation using finite elements. Subsequently, numerical optimization procedures are introduced to solve the inverse design within the context of fluidic soft actuation. Chapter 4 follows with the second objective of the thesis, which is modeling for control. Instead of volumetric soft robotic models, lower-dimensional soft beam models are introduced, specifically tailored for fast and accurate model-based controllers. The chapter primarily focuses on PCC soft beam models. Chapter 5 addresses the limitations of the PCC model and extends upon it. The chapter formulates a finite-dimensional port-Hamiltonian modeling approach for soft beams, utilizing spatial shape functions to discretize the modal flexibilities of the soft robot. From here, energy-shaping controllers are introduced, enabling shape control for underactuated soft robots. Chapter 6 presents the culmination of all theoretical material presented in the thesis, consolidating it into a concise and user-friendly toolkit called **Sorotoki**. The chapter provides an overview of the included programming tools for the design, modeling, and control of soft robots. It also introduces the Data-driven Variable Strain (DVS) approach, which leads to efficient low-dimensional models. The chapter further showcases a variety of soft robotic systems fabricated using Additive Manufacturing technology, including designs derived from topology optimization techniques. Finally, Chapter 7 concludes the main body of the thesis by summarizing the research deliverables of the previous chapters and providing a list of recommendations that could shape future work.

Note to the reader: Chapters 3-6 are derived from research articles that have been either published or are intended for submission, allowing for autonomous reading. The beginning of each chapter includes a reference to the respective research paper.

2

A brief historical overview on the progress of soft robotics

Abstract - This chapter presents a detailed chronology of the evolution of soft robotics, from its inception in the early 1950s to current research trends. The aim is to provide an insightful introduction to the extensive field of soft robotics. The chapter commences by tracing the origins of soft robotics in pneumatic muscles, including the pioneering work of Joseph McKibben and Victor Scheinman. Subsequently, we explore the emergence of novel concepts and technologies that facilitated the development of increasingly sophisticated soft robots through the utilization of exotic material properties. Throughout the chapter, significant milestones in the development of soft robotics are highlighted, such as the creation of the first soft gripper, the integration of robotics with soft actuators, and the introduction of design and modeling principles for these systems, as well as early control approaches. Additionally, the chapter highlights some of the key challenges that lie ahead for the field, which serve as a basis for standardization of terminology. In short, this chapter offers an insightful and comprehensive perspective on the history of soft robotics and will further aid the reader in solidifying the thesis' objectives introduced in the previous chapter.

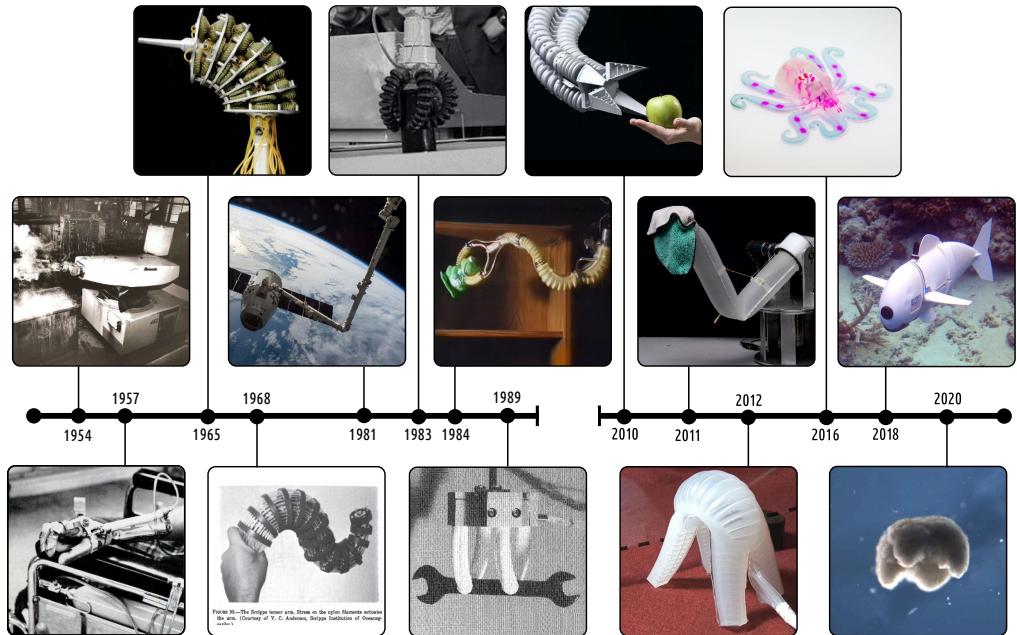


Figure 2.1. A brief timeline of the state-of-the-art of bio-inspired robotics throughout human history. (1954): Unimate, the first industrial robot. (1957): McKibben actuator, an early soft actuator inspired by the human muscle used for rehabilitation purposes [112]. (1965): The Orm, believed to be the first soft robotic system designed by Scheinman and Leifer [93]. (1968): Tensor Scripps arm developed by Anderson [8]. (1981): Canadarm-1, early flexible robotics employed on the International Space Station. (1983): Robot Arm with Pneumatic Gripper by Teleshev [113]. (1984): Bellows robotic arm by Wilson et al. [308]. (1989): The soft robotic gripper developed by Suzumori et al. [261, 262], seen as one of the earliest academic soft robots, developed before the word "*soft robot*" existed. (2010): Festo's Bionic arm inspired by the elephant's trunk [103]. (2011): Soft inflatable robot arm by Sanan and Atkeson [15, 233]. (2012) Multi-gait soft robot capable of terrestrial locomotion [53]. (2016): Octobot, the first autonomous 3D-printed soft robot that explores a stabilizing oscillator chemical network that produces preprogrammed repetitive motion [306]. (2018): Autonomous robotic fish made by Katzschmann [134]. (2020): Xenobot, an organic soft robot composed of skin and muscle cells made by Blackiston and Kriegman [152]. All images sourced from the online historical catalogue by R. Hoggett [114].

2.1 Early soft robotic technology

In this chapter, we will present a brief historical overview of soft robotics, showing that the current trends of biomimicry and elasticity in robotics have roots in a period long before the soft robotic boom in the early 2010s. To guide the reader, in Figure 2.1, we provide a graphical historical overview of soft robotic systems from 1950 to 2023. We will discuss the inception of soft actuation, early soft robotic designs, and modeling and control strategies for these continuum robotics.

To relate the historical progress of soft robots with respect to rigid robots, we begin with early rigid robots. In 1954, George Devol filed a patent describing an autonomous robotic machine that could be preprogrammed to execute step-by-step motions [185]. The machine was designed to reduce the workload on the manufacturing work floor, with a major focus on mimicking repetitive (exhausting) human labor. In 1958, those prototypes led to a robotic system under the name "*Unimate*". An illustration of this early rigid robot is shown in Figure 2.1. The Unimate was used for manipulating metal die-casts and welding them to the main body of automobiles, revolutionizing the car industry shortly after. Victor Scheinman created the Stanford Arm in 1969 [2, 93], which is recognized as the first electronic computer-controlled robotic arm because the Unimate's instructions (*i.e.*, predefined set-points in joint space) were prerecorded on a magnetic drum. Later, in 1972, he developed the well-known PUMA robot (video footage available at [1]), which was the successor to the Unimate. It is important to keep Scheinman in mind as he ultimately ties to early soft robots.

Nearly four years after the development of Unimate, Joseph McKibben created a linearly contractile pneumatic muscle-inspired actuator called the "*McKibben actuator*". The McKibben muscle is a type of Pneumatic Artificial Muscle (PAM) that is still the most frequently used and published artificial muscle in literature. According to [112], he developed the McKibben actuators to help his daughter's polio-paralyzed hand move, grasp, and even write. The McKibben actuator is inspired by the human muscle and consists of an inflatable inner bladder enveloped with a double-helical weave. When pressurized, the fluidic actuator converts radial expansion into uniaxial contraction [64, 65, 237]. The interlacing weave effectively inhibits extensive ballooning, which is the undesirable phenomenon of rapidly accelerating volumetric expansion. Its material composition is often silicone rubber with a nylon-fiber exterior. A schematic representation of a general pneumatic muscle and the effect of ballooning are shown in Figure 2.3. As mentioned earlier, ballooning is an often undesired nonlinear effect where the hyperelastic pressure vessel exhibits strain-softening after a critical point is reached, resulting in further increase of pressure leading to exponential growth in volume, ultimately leading to actuator tearing. At stages of ballooning, mechanical performance significantly drops and even produces adverse effects, like actuation reversal. McKibben solved this problem through a combination of soft and inextensible fiber weaves. These inextensible fibers were placed at the exterior wall of the soft muscle, thereby limiting the radial expansion before ballooning could occur. According to Daerden [64],

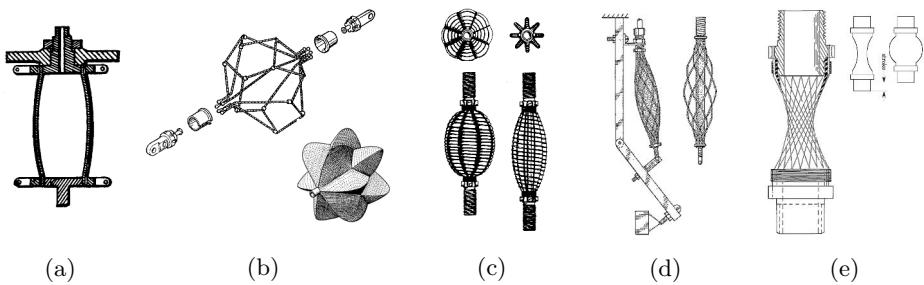


Figure 2.2. Patent diagrams of pneumatic artificial muscles from 1953 to 1988. (a) Morin Muscle [193]; (b) ROMAN muscle [124]; (c) Yarlott muscle [319]; (d) Kukolj muscle [153]; (e) Paynter Hyperboloid [210].

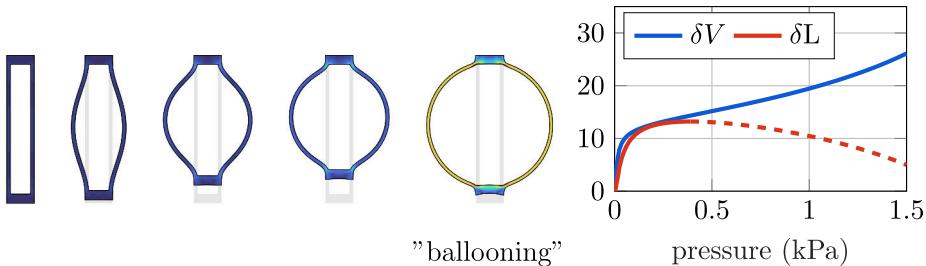


Figure 2.3. Working principle of a basic pneumatic artificial muscle (*i.e.*, Morin muscle [193]) with the internal volume (—) in mL, and the end-effector displacement (—) in mm and (---) is the point at which the undesirable ballooning occurs.

there exist many variations of pneumatic muscles besides braided muscles, such as the netted muscles (*e.g.*, Yarlott [319], ROMAC [124], and Kukolj [153]) and embedded muscles (*e.g.*, Morin [193], Paynter Hyperboloid [209]). Illustrations of their patent schematics are shown in Figure 2.2.

Pneumatic muscles are perhaps one of the first fundamental technologies that enabled soft robotics, and to this day, they remain a framework for many soft robotic systems. Nevertheless, besides the many examples of fluidics [134, 175, 176, 195, 261], there exist many other technologies employed in soft robotic motion, such as thermal [313] or chemical expansion/contraction [18, 285, 306], crystal realignment [62, 166, 212, 294], dielectric elastomers [139], magnetism [31, 150, 182, 226], and naturally the use of tendons paired with electromechanical actuation [21, 56, 145, 222, 299]. Some of these technologies predate the invention of the McKibben actuator. For example, Dielectric Elastomer Actuators (DEA) developed by Röntgen in 1880 [227] are still a popular soft actuation principle applied in soft robotics today. Therefore, given the abundance of soft robotic actuation, it is difficult to pinpoint the exact date of origin of soft actuation technology. Note, however, that these systems are not categorized as soft robots but rather as

soft actuators. Here, we emphasize the difference between soft actuators and soft robots in view of the modeling and control terminology relevant to the thesis:

Soft actuators are controllable flexible actuation units of the constitute soft robot that through external stimuli are responsible for natural motion within the system or for a change in its compliance.

2

Remark 2.1 The above terminology aims to resolve a common ambiguity in soft robotics, where the terms "soft actuator" and "soft robot" are often used interchangeably. Following the terminology applicable to this thesis, a soft robot must consist of one or more soft actuators connected to a single passive deformable body. This soft body serves as a mechanical conduit between the actuators, sensors, and the environment, and the combination of all is referred to as the "robot".

2.2 Recognition of soft robotics' potential

Returning to 1965, nearly a decade after the invention of the McKibben actuator and the Unimate robot, Scheinman and Leifer proposed a novel pneumatic robotic arm named the *Orm* – Norwegian for snake (recall that they also developed the popular PUMA robot [1]). The name was also an abbreviation for Object-Relational Mapping tool [61]. To the author's knowledge, this is believed to be the first instance of soft robotics. Surprisingly, the system predates any rigid snake-like robot, like the Scripps tensor arm by Anderson [8]. Inspired by the anatomy of snakes, the system featured 28 rubber pneumatic artificial muscles (*i.e.*, bellows) distributed along a flexible backbone (*i.e.*, skeletal support). The network of artificial muscles was sandwiched between steel plates to prevent misalignment. It is worth mentioning that the technology is analogous to the pneumatic McKibben muscle, where fiber weaves are used to prevent ballooning. Yet, contrary to a single McKibben actuator, the soft robotic system could undergo three-dimensional movement by inflation or deflation of an embedded pneumatic network. This led to a rich set of movements previously unseen in rigid robotics. As an illustrative example, we provide the mechanics of the *Orm* soft robot in Figure 2.4. The soft robot could achieve bending in any preferred direction by differential pressurization of each channel and elongation through synchronized actuation. Most notably, comparing the volume-strain response of the *Orm* with respect to the McKibben actuator, *i.e.*, comparing Figure 2.3 against 2.4, it is noticeably more linear in nature. Although not documented at the time, the comparison highlights the importance of structural geometry in pneumatic muscles.

According to an interview with Scheinman conducted by Asaro et al. [211] in 2010, the positional accuracy of the *Orm* system was poor, which may have generally led to a loss of academic interest in similar fluidic robotics in the 1960s. However, the concept of continuum robotic arms continued to be explored for many years. Three years later, in 1968, Anderson and Horn proposed and patented

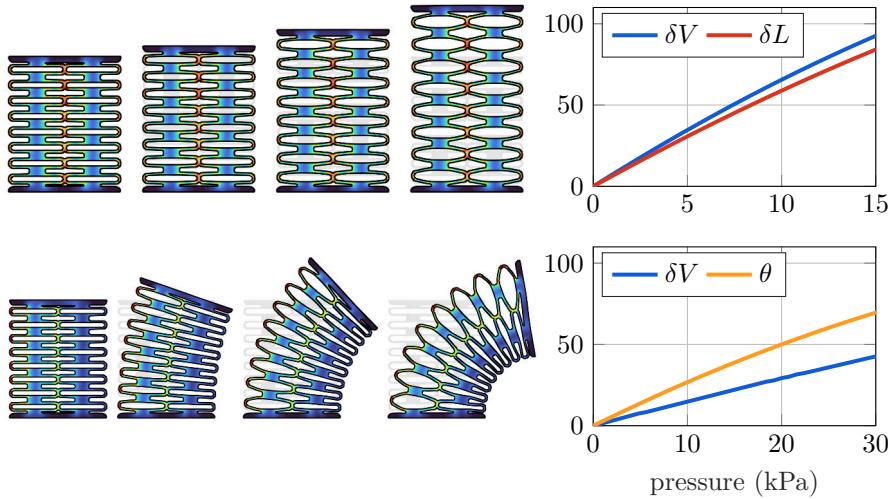


Figure 2.4. Working principle of the Orm robotic manipulator [93] with the internal volume (—) in mL, and the end-effector displacement (—) in mm and bending-angle (—) in deg. By actuation of the pneumatic network, both elongation and bending can be achieved. Observe that the response is significantly more linear than McKibben actuators in Figure 2.3, emphasizing the importance of geometry.

an improved hyper-redundant robot manipulator (see Figure 2.1). Anderson’s design improved upon the Orm, which was deemed slow and had limited positional accuracy. He proposed an array of nylon tendons that were connected to rigid discs distributed along the redundant backbone of the robot. The configurable backbone was comprised of universal spherical joints that allowed for pivoting motion with respect to other discs, totaling 16 Degrees-of-Freedom (DOFs). The entire arm was actuated hydraulically, yet the (soft) actuators were placed outside the robot’s body rather than at each joint, like the Orm. To improve positional accuracy further, Anderson placed sensor tendons parallel to the actuator tendons, which allowed for operator-based positional feedback. Although Anderson’s robot does not classify as a soft robot since it relies mostly on rigid materials, its flexibility arose from thin nylon tendons that were used for both actuation and sensing. Anderson showed that a network of distributed sensors is necessary to control the complex morphological shapes in hyper-redundant robotic systems while also mitigating the sensor’s effect on mobility. Let us introduce the notion of soft sensors – the dual of soft actuators:

(Proprioceptive) soft sensors are flexible measurements units embedded into the soft robotic body that through external stimuli measure the (local) changes of the system. Softness here implies that the sensor minimally alters the global mechanical behavior of the robot.

Remark 2.2 Our definition of soft sensors emphasizes their ability to "minimally alter the global mechanical behavior." It is worth mentioning that these sensors may be comprised of stiff or even rigid components. However, they must be incorporated into or onto the soft body in a way that minimally affects the operational workspace of the soft actuator network in static or dynamic operating conditions. With a slight abuse of definition, exteroceptive sensors such as a camera vision system (e.g., OptiTrack) are inherently soft as they do not affect the compliance.

Soft robotics in the early 80's. Since the seminal works of McKibben and subsequent research by Scheinman and Anderson, the field of soft Pneumatic Artificial Muscles (PAMs) in robotics has experienced rapid growth since the early 1980s. Figure 2.5 shows a few examples of early soft robotic systems. Teleshev [113] developed a soft gripper reminiscent of modern PneuNet actuators [53, 91, 195] - a rectangular bellow-shaped soft actuator. Unlike uniaxial PAMs, which are radially symmetric, these soft grippers explored an asymmetrical design of bellows. The geometry led to a stiffness differential around the circumference, resulting in their iconic bending motion. Still popular today, these pneumatic bending actuators find their origin back in early 1974, as seen in Andorf et al. [9]. A decade later, Takagi et al. [266] developed a soft multi-joint robot manipulator that resembles the human arm with its movements and antagonistic muscle pairs. Although their PAMs, called *Rubbertuator*, had a function and design identical to McKibben's PAMs, their system showed the merits of combining soft and rigid materials. They observed not only a high degree of positional control of the robot arm, but force control was also easily regulated by pressure control, which naturally had safety benefits. The soft robot arm could perform delicate low-force tasks while simultaneously blocking motion when encountering a human. These soft properties were lacking in rigid robotic manipulators at the time but were reminiscent of their biological counterpart – the human arm. Note that, at that time, force and impedance control for rigid robotics had been topics of academic research for years [7, 109, 110, 141], dating back to the early 1970s (e.g., see also [178]). However, achieving similar properties without control was rarely explored at the time.

Shortly after, Wilson [308] developed a soft robot manipulator based on the elephant's trunk at Duke University in Durham. His design effectively combined the works of Teleshev [113] and Takagi et al. [266] into a robot with similar dexterity but minimal use of rigid components. According to Weisburd [307], his idea stemmed from the work of Kier and Smith [142] who studied the biomechanics of muscular hydrostats in animals such as cephalopods (e.g., squids). The work of Kier et al. [142] studied how complex motions are produced in muscular organs, like elongation, shortening, bending, and torsion. Inspired by the muscular hydrostat in the elephant's trunk, Wilson developed a soft arm made from polyurethane tubes that worked as half-bellows, which enabled expansion and bending under positive pressurization [307]. To accommodate three-dimensional movement, each soft pneumatic link was placed at a $\phi = \frac{\pi}{2}$ twist offset relative to the previous link. To illustrate the motion of the soft arm, a few snapshots are provided in Figure

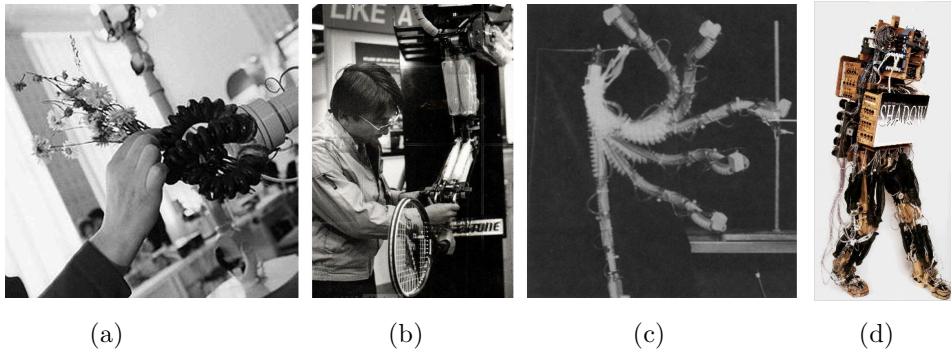


Figure 2.5. Early robotic systems that explored soft PAMs for various tasks. (a) Soft robotic grippers by Teleshev [113]. (b) The soft arm using *Rubbertuator* actuators by Takagi and Sakaguchi [266]. (c) Three-link soft robotic manipulator with gripper reminiscent of the elephant’s trunk, developed by Wilson at Duke University [307, 308]. (d) Shadow bipedal walker by Buckley et al. [111] using McKibben muscle in antagonistic pairs to produce locomotion. All images sourced from the online historical catalogue by R. Hoggett [114].

2.6. Wilson hypothesized that these highly compliant robots would be more mechanically robust and sufficiently dexterous for tight workspaces, contrary to their rigid counterparts. Although the dexterity was novel, the positional accuracy was poor. The main problem stemmed from the soft arm being controlled in open-loop (*i.e.*, remote teleoperation) without proprioceptive sensing or any positional feedback control, an issue akin to the Orm [61].

A few years later, Buckley et al. [111] developed the Shadow Walker – a bipedal rigid robot comprised of antagonistic McKibben muscle pairs. Although not fully soft, their system did explore proprioceptive sensing. The hip, knee, and ankle joints were equipped with resistance-variable potentiometers for position feedback, whereas all the muscles had tension sensors for force feedback. Later on, these resistive sensors were replaced by analog optical sensors to improve robustness [111]. Although the system was top-heavy due to the pneumatic control hardware (*e.g.*, valves and piping), rudimentary locomotion was possible. Interestingly, a similar artificial muscle system is still being explored in humanoid robotics today, such as the Atlas from Boston Dynamics. The success of pairing soft muscles with proprioceptive sensing eventually led to the development of the McKibben Shadow Hand [99, 111], which is comprised of 40 uniquely addressable soft muscles.

Following Suzumori and Saiko [261, 262], they developed a micro flexible soft actuator driven by an electro-hydraulic system (intrinsic length $L \approx 12$ mm). Each end-effector enables three DoFs, including pitch, yaw, and stretch, making it ideal for fingers, arms, and legs. Figure 2.7 shows the level of dexterity in their system. By placing the four PAMs parallel on a gripper mount and assigning a predefined trajectory, they demonstrated that their soft robotic system has sufficient dexterity to mount a hexagon bolt at incredible speed and precision. To achieve such dex-

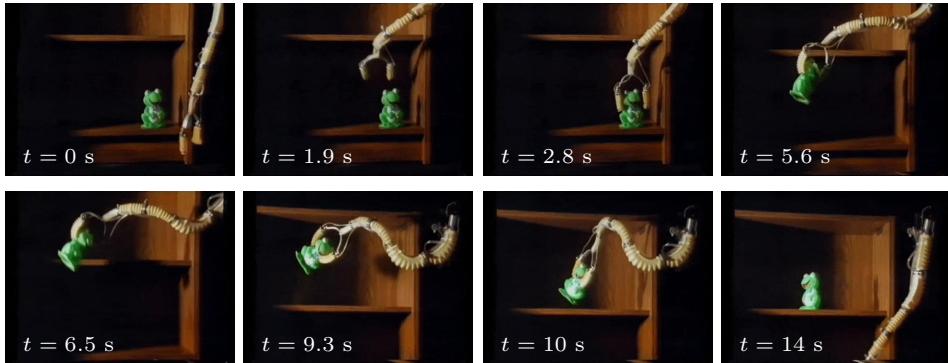


Figure 2.6. Three-link soft robotic manipulator with two-fingered soft gripper by James Wilson from Stanford University [308]. Unlike classic manipulators, where links and joints are separated, Wilson's robot consisted of three pneumatic bending actuators, being both the link and joint simultaneously. Video at Vid. 2.6.

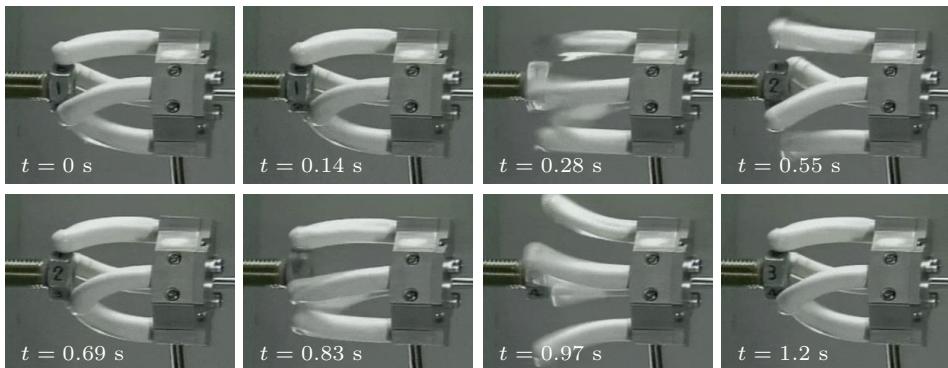


Figure 2.7. Four-fingered soft robotic gripper by Suzumori and Saiko [261, 262]. Each finger possesses three pneumatic chambers that allow for directional bending – analogous to the Orm. Through proper coordination of a set of soft fingers, various gripping complexities can be achieved, such as clockwise turning of a mechanical hex bolt (as shown above). Suzumori et al. showed that these intricate finger motions can be easily achieved by careful modeling of the fingertip dynamics and exploring the adaptability of soft materials. Video at Vid. 2.7.

terity and precision, Suzumori et al. [261] employed various modeling and control strategies to account for the dynamical characteristics under high-frequency, fluid compressibility, and the closing mechanics of pressure valves. Furthermore, the kinematics of each finger were derived using a generalized homogeneous transformation, akin to traditional robotics. Knowing both the compliance characteristics (pressure-deformation relations) and the forward kinematics, a Jacobian-based position controller was employed to regulate the Cartesian coordinates of the fingertip (successfully, one might add, as shown by Figure 2.7).



Vid. 2.6



Vid. 2.7

Early controllers for hyper-redundant (soft) robots. Following the increasing interest in highly-flexible robots in the late 80s, academic research into controlling these *hyper-redundant* robots boomed shortly after. At the time, the term hyper-redundancy – being an extension of redundancy in robotics [183] – was defined as the relative degree of kinematic and/or actuator redundancy that is large or even infinite [48, 52]. The term was first introduced by Chirikjian and Burdick [47]. Others referred to these robots as *highly redundant* [200, 310] or *High Degree-of-Freedom* (HDOF) manipulators [189, 232]. Around that time, Chirikjian and Burdick provided a plethora of mathematical foundations [48–52] focused on the kinematics and motion planning of hyper-redundant manipulators. Their work presented a modal discretization approach to describe the shape of the deformable backbone [51], and from this, geometric approaches were introduced to solve obstacle-avoiding trajectories using generalized *follow-the-leader* strategies [50]. Especially the latter showed the limitations of rigid low-redundancy manipulators. Although Chirikjian laid the foundation for the control of hyper-redundant robots, the basic principles of motion planning in pneumatic hyper-redundant robots were already presented by Wilson et al. [309, 310], yet they were not called hyper-redundant robots or soft robots at that time. Recall also that the work of Wilson et al. has been shown earlier in Figure 2.1 and Figure 2.6. In Brock et al. [32], a similar analysis was used for optimal shape design of thin elastic rods to realize desired robotic compliance. Besides, there exists an abundance of literature prior to [48] on Variable Geometry Truss Manipulators (VGTMs) – a variant of hyper-redundant tensegrity robotics – that dealt with motion planning for such systems [199, 200, 232]. Later, Mochiyama et al. [188, 189], built upon Chirikjian’s work by extending it to a dynamic formulation for elastic rods such that classic controller design is possible. They proposed shape-regulation controllers for HDOF manipulator by projecting them onto time-invariant curves, thereby showing that estimating the desired curve parameters is crucial to solving the problem by Lyapunov design [188]. Although there existed a variety of modeling and control strategies, computational power in relation to modeling complexity was the limiting factor for the simulation-to-reality (Sim2Real) transfer at the time.

2.3 Modern soft robotics boom in academia

The precise date of the emergence of soft robotics as a prominent academic field is uncertain, but it is widely believed to have occurred somewhere in the mid-2000s. From 2008, the term "soft robotics" gained significant traction as a notable keyword in scientific literature [17]. Since then, the field has undergone significant evolution and diversification, with research branching into areas such as active meta-materials, Additive Manufacturing (AM), morphological optimization, model-based control, and learning-based control. In the subsequent sections, we will examine several ongoing research topics in the field of soft robotics. These topics primarily concern the design and control of soft robots. It should be empha-

sized that while these problems may seem distinct, they are often interconnected. For instance, the structural design of a soft robot influences its workspace and consequently affects the feasibility of *a-priori* defined control objectives. This section aims to underscore such scientific interconnections and demonstrate the essential components required to address common paradigms. We will continue this section in Section 2.4, which focuses on design, and in Section 2.5, which focuses on modeling and control.

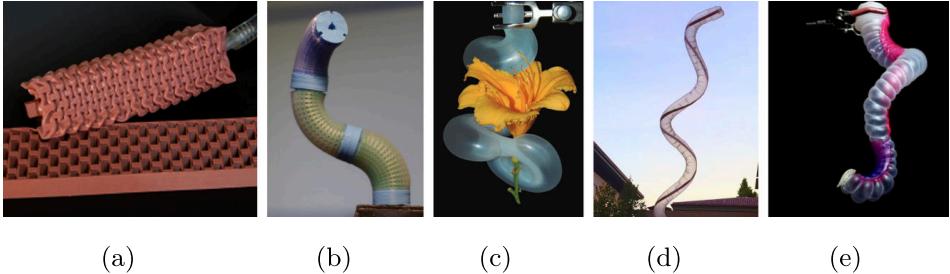
2.4 Tailoring design of fluidic soft actuation

As the name "soft robots" arises from their use of soft materials, it follows that design and fabrication using soft materials play a huge role in their technological development. Contrary to rigid robots, many soft robots explore whole body movement rather than localized regions undergoing motion called "*joints*". In classic robotics, robots are composed of a countable number of rigid links and joints [60, 197, 256], either arranged in series or parallel. Together, they span a workable range of motion called the operational workspace [256] (see Chapter 1). Focusing on rigid manipulators, whose base is often structurally fixated, their workspace can be obtained through a system of kinematics, often derived through a set of geometrical equalities. Rigid manipulators often have a bounded workspace (assuming actuation limits). In robotic locomotion, similar kinematic descriptions can be obtained for the legs and feet, with the exception of an additional free-floating base. In these cases, however, the workspace is of less interest; rather, the different possibilities of "*gait cycles*" that arise from the link-joint configuration and actuator dynamics determine the system's success for locomotion.

Returning to soft robots, the terms such as *joints*, *workspace* and *gait cycles* also apply here. However, the high flexibility of soft robots allows for many non-restricted joint displacements, which makes deriving closed-form mathematical descriptions challenging. The shape of the workspace and locomotion patterns are mainly influenced by the geometry of the soft actuator, its flexibility modes, and how forces are distributed throughout the continuum soft body. Controlling the motion within soft actuation, reducing parasitic mobility and tailoring motion based on structural geometry, is an active topic in soft robotics research for decades.

2.4.1 Engineering principles in soft fluidic actuators

In the past decade, researchers have developed various techniques for exploiting the high elasticity of soft materials for controllable actuation. One key development, with similar working principles to pneumatic muscle groups (see [112, 193] or Figure 2.3), are Soft Pneumatic Actuators (SPAs). A few examples are shown in Figure 2.8. SPAs undergo mechanics similar to McKibben actuators [112] or Morin actuators [193], yet they possess a broader range of motion beyond uniaxial contraction. Examples include axial growth [106], bending [91, 176, 195], con-



2

Figure 2.8. Various examples of continuum-bodied joint motions in modern soft actuation. (a) Soft actuator undergoing contraction by Yang et al. [317]. (b) Set of serial-chain of bending soft actuator (STIFF-FLOP) by Cianchetti et al. [54, 55] (c) Soft tentacle composed of twisting soft actuators. (d) Vine-inspired soft actuators capable of growth by Hawkes et al. [106]. (e) Soft manipulator composed of bending and twisting soft actuators through laminate materials by Kim et al. [148].

traction and elongation [317], helical and twisting, and a hybridization of all the aforementioned motions [148]. An example of soft actuators capable of contraction is the Vacuum-Actuated Muscle-inspired Pneumatic (VAMP) structure by Yang et al. (2016, [317]). Their work proposes a tailored geometrical structure embedded into a soft elastomer medium that is highly sensitive towards buckling. When subjected to a sufficiently large negative differential pressure, the internal structure undergoes a (reversible) mechanically unstable leading to uniaxial contraction, as seen in Figure 2.8. Their work is inspired by a similar buckling behavior of patterned elastomer [25, 196, 239] subjected to axial loads. These muscle-inspired vacuum soft actuators are fast, produce a stable, repeatable motion; and more importantly, explore structural geometry to reduce parasitic motion. An example of soft bending actuators is the STIFF-FLOP system [54]. Similar to the ORM system [93], it has three pressure chambers embedded into a soft cylindrical-shaped elastomer. To prevent ballooning, inextensible rings are placed orthogonal to the deformable backbone. Its design is also reminiscent of [261, 262]. Hawkes et al. [106] developed a soft manipulator inspired by the growing behavior of vines. Kim et al. [148] used laminates that adhere to the volumetrically expanding soft body to govern the motion trajectory through bending and twisting.

2.4.2 Exploring optimization and evolutionary algorithms

Besides designing through engineering principles, optimization in soft robotics has been gaining momentum in recent years. Wang et al. [300] used topology optimization to find the optimal design for a cable-driven soft gripper (Figure 2.9a). Similarly, Tian et al. [283] explored topology optimization for ferromagnetic soft grippers. Besides soft grippers, evolutionary design algorithms are also employed for soft mobile crawlers and swimmers. Joachimczak et al. [127, 128] explored an evolutionary search algorithm with the purpose of automatically designing complex

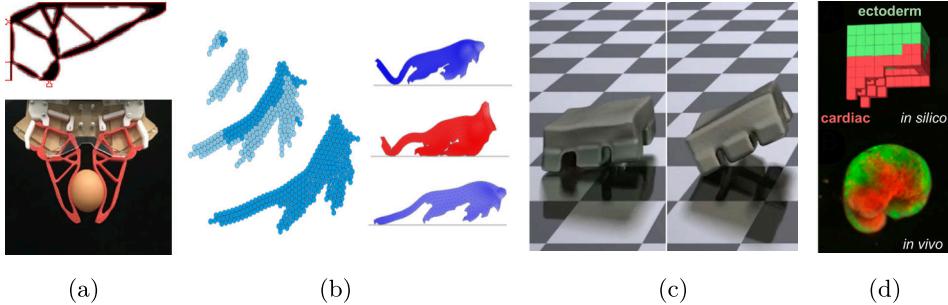
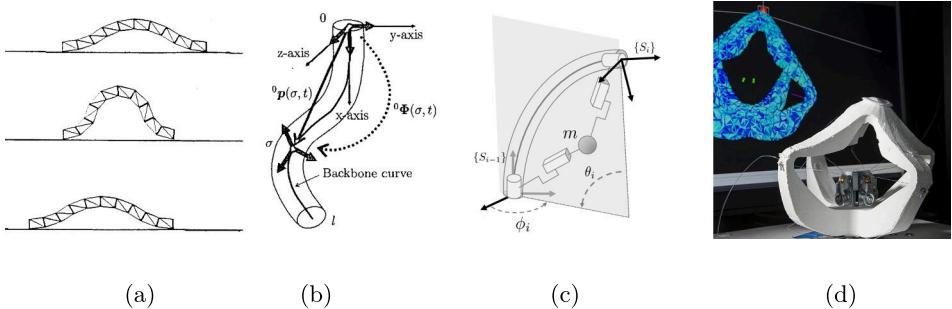


Figure 2.9. Optimization for design and motion of soft robots. (a) Soft gripper by Wang et al. [300]. (b) Evolutionary algorithms for multicellular soft-bodied robots by Joachimczak et al. [127, 128]. (c) **DiffTachi** result for soft crawler by Hu et al. [117]. (d) Voxel-based optimization for Xenobots [152].

morphologies and controllers of multicellular, soft-bodied robots (Figure 2.9c). Hu et al. [117] used a differential physics simulator called **DiffTachi** that efficiently computes gradient information for each simulation timestep. The gradient information can then be fed into neural network controllers to solve, for instance, the appropriate gait cycles required in the locomotion of soft crawlers, see Figure 2.9d.

2.5 Gaining performance using feedback control

As the inherent properties of soft materials bring forth many benefits, such as adaptability, hyper-redundancy, and passivity with respect to the environment, they also hinder progress in model-based controllers. Earlier, we touched upon this subject with the rise of kinematic and dynamic models for hyper-redundant robotics in the late 80s to early 90s. Chirikjian et al. [48] provided a kinematic framework for hyper-redundant manipulators with applications to motion planning (see Figure 2.10a). Here, the elastic backbone is approximated using a modal formulation. Such modeling frameworks are one-to-one transferable to soft continuum manipulators. Mochiyama et al. [188, 190] extended this work to a dynamics formulation, even providing Lyapunov-based control strategies for shape regulation (Figure 2.10b). However, both modeling frameworks were computationally inefficient, lacking transferability to real-time control. The root problem stems from the fact that soft continuum robots, belonging in their exact formulation to the field of continuum mechanics, lead to infinite-dimensional models often expressed as Partial Differential Equations (PDEs). Rigid multi-body systems, like robot manipulators or mobile robots, on the other hand, can be conveniently modeled via Ordinary Differential Equations (ODEs) that stem from Lagrangian or Newtonian mechanical principles. Rigid-body models were (and still are) fast computationally, and their literature on controller design is vast and well-established [60, 197, 256]. The computational issues in early continuum robots may be reflected by the literature gap between the 1990s and mid-2010s.



2

Figure 2.10. Popular modeling strategies for soft robotics. (a) Hyper-redundant modeling description through tensegrity by Chirikjian [48, 52]). (b) Analytic continuum beam description by Mochiyama [189, 190]). (c) Augmented rigid-body model subjected to PCC kinematics by Katzschmann et al. [135]. (d) Diamond-shaped soft robot manipulator controlled using the FEM-based SOFA software by Duriez et al. [75] and related [57, 100].

2.5.1 Control-oriented models for soft robots

In the past decade, significant steps have been made to address the issues of infinite dimensionality [70]. The key is to formulate a finite-dimensional approximation of the soft robot’s dynamics such that they can be written as standard ODEs. Reduced-Order Models (ROMs) have paved the path for model-based controllers for soft robots, whose reduced formulations are both tractable and precise. In the years following its academic boom, many different assumptions and model approximations have emerged to address the issue of control.

Remark 2.3 *The reduced-order formulations for soft robotics are primarily applicable to slender soft robots, leading to a focus on soft robot manipulators in control-oriented studies. This approach is well-motivated given that many soft robots have one dominant physical dimension compared to the other two [70]. As such, this thesis primarily focuses on the modeling and control of soft manipulators rather than a broader scope.*

Focusing on soft robot manipulators, a popular choice of finite-dimensional reduction is the so-called Piecewise Constant Curvature (PCC) soft beam model. The PCC modeling approach is by far the most adopted in the soft robotics community [304]. As the name implies, the soft robot is modeled as an elastically deformable beam with all strains but curvature neglected. Examples of this approximation include [71, 78, 87, 134, 135, 176, 229, 304]. Highlighting a few, Katzschmann et al. [134] proposed to connect the PCC formulation to an augmented rigid robot dynamical model with parallel elastic actuation (see Figure 2.10c). A similar approach was proposed earlier by Falkenhahn et al. [78] and applied to Festo’s bionic arm [103]. Although such lumped models may seem like a major oversimplification, the proposed model allows sufficient speed and accuracy such that model-based feedback is applicable. This formulation was also employed later in an adaptive sliding mode control scheme [137] for the SoPra

soft arm [288]. Following, Renda et al. [222] extended the PCC model to Piecewise Constant Strain (PCS) formulation. This formulation allowed for all strain if and only if considered spatially piece-wise constant (Figure 2.10d). Rooted in SE(3) geometry of the Cosserat approach [242], it provided a closer relation with the rigid body geometry of traditional robotics. The formulation also extends to soft manipulators with fluidic actuation [223, 284]. The PCS model was later employed in feedforward controllers by Thuruthel et al. [282] using model-based policy learning algorithms. To improve efficiency, a recurrent neural network was trained using an offline PCS model. Grazioso et al. [102] explored a similar path of geometric Cosserat beams using helical strain functions. Nevertheless, Constant Strain (CS) models have severe limitations. They often do not originate from continuum mechanics and thus are only applicable in restrictive settings. Although computationally performance might surpass continuous models, due to intrinsic kinematic restrictions, they are unable to capture important continuum phenomena, like buckling, environmental interaction, or wave propagation.

In response to its limitations, many researchers continued their search for efficient and more generalizable alternatives. Della Santina et al. [72] proposed a polynomial description to describe the continuum dynamics, a description analogous to [48]. In their work, they expressed the curvature function of the soft robot in terms of a standard polynomial basis. Not only can an exact infinite-dimensional formulation of the problem be obtained (in theory), but truncation at any level is easily changed. The technique is also widely used for flexible-link robot manipulators to capture small vibrations; see DeLuca et al. [66]. Della Santina et al. also showed that PCC-rooted assumptions as control output produce a minimum-phase system [72] – a fundamental stepping-stone for nonlinear control. Following, Boyer et al. [29] extended upon their prior Cosserat models [221, 222] and presented a tractable and generalizable beam model for slender soft manipulators. A similar approach to [72] was followed, but all strains are discretized using a finite set of strain basis functions. Renda et al. [221] improved computation by introducing a two-stage Gauss quadrature [321] to derive the Magnus expansion [104]. Other examples of the Cosserat beam descriptions, but more focused on the continuum mechanics rather than control, are the work of Gazzola et al. [95]. Their work allowed for efficient Cosserat beam models suitable for self-collision, thus providing various simulations for twirling and coiling under increasing torsional loads.

Another popular alternative, better suited for general soft robotic systems like soft mobile robots, are reduced-order finite element models [56, 57, 75, 100, 136, 278, 279, 287, 312, 324] or neural-network trained using offline FEM simulations [79]. Starting from high-order FEM data (e.g., state dimensions of the order 10k) that capture the whole workspace spanned by the network of soft actuators, Proper Orthogonal Decomposition (POD) techniques are employed to drastically reduce the state dimension of the soft robot model. These techniques can even retain external loads (e.g., contact and friction) with precision as long as they are included in the offline data set [100]. By far, this FEM-driven method has shown the most success in the experimental control regime.

2.5.2 Soft robot simulation and programming environments

The rapid development of soft robotic models in recent years has also increased the demand for (open-access) software packages, especially since many of the aforementioned ROM models require an advanced level of mathematical understanding. In an attempt to help the soft robotics community, many researchers have provided open-source, documented simulators interwoven in their soft robotics research. A popular FEM-based software on soft robotic modeling and control is **SOFA** by Duriez et al. [57, 75]. **DiffTachi** by Hu et al. [116, 117] explores differential simulations to produce soft machines capable of locomotion. Bern et al. [21, 22] developed **SoftIK**, a software for soft deformable plushy robots. Among beam or rod-based models, there exist many options. Examples include **Elastica** or **pyElastica** [275] developed by Gazzola et al. [95, 323], **TMDyn** by Sadati et al. [231], **SimSOFT** by Grazioso et al. [102], and **SoRoSim** by Mathew et al. [180] based on the work of Renda et al. [221] and Boyer et al. [29]. The **Sorotoki** toolkit by Caasenbrood et al. [36], an open-source software package presented as a part of this thesis, explores a combination of FEM models and soft beam models. The toolkit, written in Matlab, aims to bridge the gaps between design, modeling, and control of (hyper-elastic) soft robots.

2.5.3 Closing the loop in soft robotics

Following the many developments in computational efficiency of reduced-order models (and accordingly the advances in soft sensing), academic research in model-based or model-free control for soft robots is significantly growing since early 2019. Note that, feed-forward controllers for soft manipulators have been proposed years prior, *e.g.*, [77, 78, 234, 281].

So far, the PCC model has been more intensively validated experimentally than other models. In Della Santina et al. [71], the augmented rigid-body PCC model was used to design a closed-loop controller for a continuous soft manipulator, presenting two architectures designed for dynamic trajectory tracking and surface following. Prior work is provided in [135]. A similar approach was followed by Milana et al. [186] and applied to an artificial soft cilia. They showed that soft bending actuators could mimic the asymmetric motion of the cilia through model-based control. Cao et al. [41] explored a reduced analytical model [302], which is somewhat equivalent to a linear pendulum model (apart from quadratic terms in the potential force), to develop robust tracking controllers without velocity observers. Their controller was tested experimentally on a soft PneuNet actuator. Wang et al. [303] developed a computed torque controller (see [256]) using the augmented rigid-body PCC model and applied it to a soft Honeycomb Pneumatic Network Arm [125]. Franco et al. [87, 88] used a port-Hamiltonian modeling framework akin to the rigid-body PCC model (*i.e.*, three-link pendulum) and applied such principles to energy-shaping controllers. The performance of their controller was assessed via simulations and experiments on two soft continuum prototypes. On a side note, Franco et al. [85] also developed an energy-shaping

control law together with nonlinear observers for the control of soft growing robots [106] with pneumatic actuation subject to the (ideal) gas laws.

As mentioned previously, the PCC model has significant limitations that raise questions about the usability, dexterity, and robustness of its control derivation. Although primarily focused on simulation, higher-order dynamics have been used for the development of feedback controllers in soft manipulators. Della Santina et al. [67] developed swing-up controllers for a soft pendulum modeled by the affine curvature models (*i.e.*, a polynomial curvature model [72] of order $k = 2$). Their approach mirrors the path of the classic control problem of inverted pendulums in the 90s and early 2000s [203, 240, 254, 255]. Later, Weerakoon et al. [305] extended their work by introducing a revolute base. A common control problem here is under-actuation [197, 256, 274], implying that not all control actions can be realized to steer the configuration space to a desired position. Borja et al. [28] developed a general control framework that can stabilize soft manipulators based on potential energy shaping using the affine curvature model. Their work showed that some linear matrix inequalities can be derived based on the gradient of the potential energy related to the passive and active states, such that local stability can be proven. In layman’s terms, elasticity must dominate the forces resulting from gravity in the underactuated states for (potential) energy-shaping controllers (and mostly others) to work. More recent work by Pustina et al. [216] explores control via input decoupling applied on Lagrangian soft robot models with collocated inputs. In summary, the development of closed-loop control for multi-modal soft robotic deformations is a promising area of research. However, at present, such control mechanisms are limited to simulated environments and have yet to be fully realized in practical applications.

2.6 Summary

In summary, we have provided a comprehensive overview of the evolution of soft robotics, from its inception in the 1950s to current research trends. The chapter traces the origins of soft robotics in pneumatic muscles and explores the emergence of novel concepts and technologies that have facilitated the development of increasingly sophisticated soft robots through the utilization of exotic material properties. We highlight significant milestones in the field, including the creation of the first soft gripper, integration of robotics with soft actuation, and introduction of design, modeling, and control principles for these systems. Additionally, the chapter discusses key challenges facing the field and serves as a basis for standardizing terminology.

3

Optimal design of soft robots – a gradient-based approach

Abstract - In this chapter, we present a novel framework for synthesizing the design of pressure-driven soft robots. Contrary to traditional design methods, a topology optimization scheme is employed to find the optimal soft robotic structure given user-defined motion requirements. To the best of our knowledge, the combination of pressure-driven topology optimization and soft robotics is, as of the date of this thesis, unexplored. Two difficulties are related to this problem. First, pressure-based topology optimization is challenging since the adaptive topology changes the fluidic load at each optimization step. To deal with this issue, we exploit the facial connectivity in polygonal mesh tessellations to efficiently simulate the physics involving fluidic actuation in soft robotics. The second issue is describing the hyper-elastic nature of soft materials. Here, the nonlinear Finite Element Method (FEM) is explored so that large deformations can be accurately described. Numerical investigation shows that the framework can produce meaningful and insightful material layouts with little to no prior knowledge of soft robotic design. We show the existence of new structures, but also familiar soft robotics structures such as the *PneuNet*. Interestingly, when considering a spectrum of soft materials, we demonstrate that parts of the optimal structural topology appear invariant regardless of the choice of materials, while other design aspects are directly related to elasticity, at times even non-monotonically. In short, the proposed framework not only accelerates design convergence but can also extend to the development of new and unexplored soft robot morphologies.

This chapter is based on: B.J. Caasenbrood, A.Y. Pogromsky, and H. Nijmeijer. *A Computational Design Framework for Pressure-driven Soft Robots through Nonlinear Topology Optimization*. IEEE International Conference on Soft Robotics (RoboSoft), 2020. doi: 10.1109/RoboSoft48309.2020.9116010

3.1 Introduction

The field of soft robotics has attracted the interest of many researchers from different backgrounds. Soft robots use compliant and hyper-elastic materials, while minimizing the use of rigid materials. The introduction of soft materials into robotics greatly expands the field of application for robotics. For example, due to their dexterity and environmental robustness, soft robots are often used in medical applications [13, 213, 318], adaptive grasping [91, 120], and locomotion in uncertain environments [73]. Unlike their rigid counterpart, soft robots undergo large continuum-bodied motion that, to some extent, resembles morphologies found in nature. These morphologies arise by virtue of the low compliance in soft materials and, more importantly, the structural layout of the soft robot. As of today, many of the fundamental engineering principles in rigid robotics, such as design, actuation, sensing, and control, are often not applicable to soft robotics systems. Since its inception, most of these engineering problems have remained challenging.

Although the diversity in soft robotics is significant, ranging from adaptive grippers to soft manipulators, most topologies in soft robotics can be associated with nature or engineered geometries for minimal compliance (*e.g.*, bellows shapes). Soft robots often mimic living creatures and their morphologies, such as the tentacle of an octopus [91, 306], or the trunk of an elephant [73]. Hypothetically, the abundance of biomimicry in soft robotics might be associated with the design complexity of developing robots from soft materials. The large number of degrees-of-freedom and exotic mechanical nature of soft robots make designing them significantly challenging, and consequently, the design process can be iterative and time-consuming [306]. Therefore, it is potentially advantageous to use computational tools that assist in or develop appropriate soft robotic topologies given a set of user-defined requirements, like desired motion or force.

In the past, researchers have made efforts to find morphologies through mathematics, particularly through evolutionary algorithms. The concept of automated creature designs was first introduced by Sims [243], who showed that given a set of basic geometries, locomotive organisms could be generated from evolutionary algorithms. These virtual organisms resembled biological morphologies to some extent; however, the complexity of the material layout was limited. More recent work involving the synthesis of virtual soft robots includes Cheney et al. [46], who successfully produced intricate locomotive morphologies using artificial neural networks and multi-material parameter spaces of active and passive soft voxels. Other work involving morphological synthesis includes [21, 194, 292]. Unfortunately, the synthesis of morphologies from previous approaches, though novel, remains only in ideal simulated environments. An accurate representation of the nonlinear material properties in soft robotics can be challenging, and in favor of computational efficiency, little detail is spent on the nonlinear nature governing soft materials. Besides, these evolutionary frameworks typically involve a network of '*activation*' cells or voxels that perform ideal volumetric deformation, biologically resembling muscle functionality while unfortunately lacking resemblance to conventional ac-

tuation in soft robotics (see Section 2.4).

Reviewing previous methods, a more efficient approach to solving the optimal morphology might be founded in topology optimization. Topology optimization is the general formulation of a material distribution problem for mechanical solids, where density-based topologies arise throughout an iterative (non-convex) optimization procedure. The synthesis of compliant mechanisms through topology optimization is investigated thoroughly [19, 90, 169]; however, its application to soft robotics is relatively unexplored [320, 322, 327]. Yet, to obtain meaningful topologies for soft robotics, two problems need to be addressed. Since soft robots undergo large deformations, it becomes necessary to describe the nonlinear geometrical deformations accurately. Inherent to significant deformation of soft materials is the importance of nonlinear material behavior, such as hyperelasticity. Another concern is the design-dependency of the external forces, which in our case are pneumatic loads. This class of structural problems is more challenging than traditional problems since the load is continuously interacting with the adaptive interface during the iterative optimization process [295, 298]. It should be mentioned that the use of compressed air or pressurized fluid is a popular actuation approach in soft robotics.

In this chapter, we present a novel framework for generating topologies of soft robotics. Contrary to biometry or conventional designs, finding the (optimal) material layout of the soft robot is accomplished through a gradient-based nonlinear topology optimization, where the distribution of soft materials is optimized given a user-defined objective. Our main contributions include the description of nonlinear geometrical deformation and pneumatic loading. We exploit the connectivity properties in polygonal meshes such that synchronized volumetric contraction or expansion of a group of polygonal elements can artificially mimic the geometrical loads in pneumatic actuation. The advantages of our framework in comparison to other literature are: (i) a better representation of pneumatic actuation in soft robotics; (ii) improved design convergence in contrast to evolution-based optimization methods. To the best of our knowledge, our approach of pressure-driven nonlinear topology optimization is unexplored for soft robotics, and its application could easily extend to other soft robotic systems.

The chapter is organized as follows. In Section 3.2, we will examine the principles of continuum mechanics applied to hyper-elastic materials. Following, in Section 3.3, we present the optimization method used. In Section 3.4, we present numerical examples that demonstrate the development of a soft robotic structure through optimization, and also analyze the impact of various soft materials.

3.2 Nonlinear finite element method

In this section, we will introduce the preliminaries for the nonlinear topology optimization method by briefly discussing the nonlinear FEM. The approach is similar to FEM but it accounts for various nonlinear aspects in continuum mechanics. It is particularly useful for modeling large geometrical deformations and

hyper-elasticity, which cannot be accurately represented using linear FEM variants. These descriptions are essential in understanding how soft materials deform, and therefore can be beneficial to explore in optimal design solutions.

3.2.1 Strain theory in continuum mechanics

We start by presenting the variational principle of continuum mechanics in a non-linear geometrical context. Consider an undeformed material domain as $\mathcal{B}_0 \subset \mathbb{R}^3$. When external forces act on \mathcal{B}_0 , it undergoes both rigid-body and elastic deformation, resulting in a new body, denoted by $\mathcal{B} \subset \mathbb{R}^3$. Let $\mathbf{X} \in \mathcal{B}_0$ represent an arbitrary material point within the undeformed configuration, whose motion can be described by a continuous path between two position vectors \mathbf{X} and \mathbf{X}' . These vectors correspond to a particular material point in the undeformed and quasi-static deformed configurations (*i.e.*, zero-velocity), respectively. Suppose that the deformation mapping is described by a flow $\varphi^{(t)} : \mathcal{B}_0 \rightarrow \mathcal{B}$ such that $\mathbf{X} \mapsto \varphi^{(T)}(\mathbf{X}) = \mathbf{X}'$ for a time instance $T > 0$ when static equilibrium between elastic deformation and external forces is reached. More conveniently, we can write $\mathbf{X}' = \mathbf{X} + \mathbf{d}(\mathbf{X}, T)$ where $\mathbf{d}(\mathbf{X}, T)$ represents the displacement field at the equilibrium configuration.

In the field of continuum mechanics, the primary objective is to determine an approximation of the displacement field $\mathbf{d}(\mathbf{X}, T)$ that satisfies the boundary conditions imposed on the (undeformed) "reference body" \mathcal{B}_0 . To achieve this goal, it is necessary to establish a relationship between the displacement and strain, as well as a connection between strain and internal stress resulting in material displacement. A fundamental measure of deformation is the deformation gradient tensor, which can be computed as follows: assuming that the mapping φ is sufficiently smooth [115, 146], the second-order deformation gradient tensor is obtained through spatial differentiation:

$$\mathbf{F} := \nabla_0 \varphi = \mathbf{I} + \nabla_0 \mathbf{d} \quad (3.1)$$

where $\nabla_0(\cdot) := \begin{bmatrix} \frac{\partial(\cdot)}{\partial X_1} & \frac{\partial(\cdot)}{\partial X_2} & \frac{\partial(\cdot)}{\partial X_3} \end{bmatrix}$ defines the gradient operator. The deformation gradient tensor, as shown in (3.1), provides valuable information about the local deformation. Specifically, it describes the deformation of an infinitesimal sub-volume of the material domain \mathcal{B}_0 around \mathbf{X} . The volume change of this sub-volume can be calculated using $J := \det(\mathbf{F}) > 0$. Following convention [115, 146], we can derive the Green-Lagrange strain tensor from equation (3.1) as $\boldsymbol{\varepsilon} := \frac{1}{2}(\mathbf{F}^\top \mathbf{F} - \mathbf{I})$. In terms of the displacement gradient $\nabla_0 \mathbf{d}$, the general expression for the Green-Lagrange strain tensor is given by:

$$\boldsymbol{\varepsilon} := \frac{1}{2}(\nabla_0 \mathbf{d} + \nabla_0^\top \mathbf{d} + \nabla_0 \mathbf{d}^\top \nabla_0 \mathbf{d}) \quad (3.2)$$

which is a symmetric second-order tensor. In the context of continuum mechanics, it is crucial to consider the geometric nonlinearities that arise when large

deformations occur. Specifically, the term $\nabla_0 \mathbf{d}^\top \nabla_0 \mathbf{d}$ captures these nonlinearities. However, most structural optimization methods assume small deformations, *i.e.*, $\nabla_0 \mathbf{d}^\top \nabla_0 \mathbf{d} \ll \nabla_0 \mathbf{d}$, and simplify the strain tensor as $\boldsymbol{\varepsilon} = \frac{1}{2}(\nabla_0 \mathbf{d} + \nabla_0^\top \mathbf{d})$, which neglects the last term. Although this is hugely beneficial for numerical performance, this simplification is not always appropriate for soft robotics, where accurate mechanical descriptions require accounting for geometric nonlinearities.

3.2.2 Isotropic hyperelasticity materials

Soft robotics is a field that relies heavily on the use of elastomer materials. These materials possess several desirable properties, such as relatively low Young's moduli, large reversible strains, and mechanical robustness. In material mechanics, these elastic materials are often classified as hyperelastic materials due to their ability to undergo large deformations. As a result of this deformation, rubber-like materials exhibit state-dependent mechanical compliance. Unlike Hookean materials, which have linear elasticity, the constitutive behavior of hyperelastic materials is described by a strain energy density function $\Psi : \mathcal{E} \mapsto \mathbb{R}_{\geq 0}$. This function represents the conservative elastic energy density stored inside the continuum. Therefore, the elastic potential energy is the integration of the energy density over the undeformed domain and can be expressed as:

$$\mathcal{U}_{\text{int}}(\mathcal{E}) := \int_{B_0} \Psi(\mathcal{E}) dV \geq 0. \quad (3.3)$$

In literature, Ψ is often chosen as polynomial regression model which fits empirical data of materials, leaving the choice on Ψ generally free. Nevertheless, there exist popular options that are commonly used for rubber-like engineering materials. Popular constitutive models for hyperelastic behavior include Neo-Hookean [21, 23, 249], Mooney [146], Ogden [316], or Yeoh [220]. In contrast to linear elasticity strain energy, the strain energy for hyperelastic constitutive models is commonly expressed in terms of the strain invariants (I_1, I_2, I_3).

In this work, the nearly incompressible Yeoh constitutive model for hyperelasticity is used to describe the mechanics of soft materials. Let $I_1 = \text{tr}(\mathcal{C})$ be the first strain invariant, with $\mathcal{C} = \mathbf{F}^\top \mathbf{F}$ being the right Cauchy strain tensor. Then, following the work of Renaud et al. [220] and Kim et al. [146], the strain energy function of the nearly incompressible Yeoh model is given by:

$$\Psi = \sum_{i=1}^3 c_i (J_1 - 3)^i + \sum_{j=1}^3 \frac{1}{d_j} (J - 1)^{2j}, \quad (3.4)$$

where $J_1 = J^{-\frac{1}{3}} I_1$ is a modified first strain variant, and $c_1 > 0$ and c_2, c_3 are the material constants related to stiffness (N m^{-2}), and the constants $d_{1,2,3} > 0$ related to material compressibility. For consistency with linear elasticity in the limit of small strains, it is necessary that the shear modulus is $\mu = E_0/2(1 + \nu_0) = 2c_1$ and the bulk modulus is $\kappa = E_0/3(1 - \nu_0) = 2/d_1$ where E_0 the Young's modulus and ν_0 the Poisson's ratio [115, 146].

3.2.3 Variational principle of energy minimization

A common way of finding solutions to the displacements \mathbf{d} of continuum solids, is by the variational principle of energy minimization. The method explores the idea that at the equilibrium configuration, the total potential energy of the system has zero variation, *i.e.*, the slope is zero. To explain the method, we follow the work of Kim et al. [146]. The potential energy of an elastic system is the difference between the internally stored elastic energy \mathcal{U}_{int} and the work done by the external forces \mathcal{U}_{ext} . This work is equivalent by the volume integral of the forces multiplied by their traveled distance, *i.e.*, the displacement field $\mathbf{d}(\mathbf{X}, T)$. Thus, using (3.4), the total potential energy of the elastic system is

$$\begin{aligned}\mathcal{U}(\mathbf{d}) &= \mathcal{U}_{\text{int}}(\mathbf{d}) - \mathcal{U}_{\text{ext}}(\mathbf{d}), \\ &= \int_{\mathcal{B}_0} \Psi(\mathcal{E}(\mathbf{d})) dV - \left[\int_{\mathcal{B}_0} \mathbf{d}^\top \mathbf{f}_b dV + \int_{\partial\mathcal{B}_0} \mathbf{d}^\top \mathbf{f}_t dS \right],\end{aligned}\quad (3.5)$$

where $\partial\mathcal{B}_0$ is the boundary of the undeformed continuum domain \mathcal{B}_0 , and $\mathbf{f}_b(\mathbf{X}, T)$ and $\mathbf{f}_t(\mathbf{X}, T)$ are the body and traction forces evaluated at time T , respectively. The variation of the potential energy can be obtained by taking the first order variation of $\mathcal{U}(\mathbf{d})$ in the direction $\delta\mathbf{d}$, where $\delta\mathbf{d}$ corresponds to the virtual displacements in the principle of virtual work, which must satisfy the homogeneous boundary conditions (*i.e.*, the kinematically admissible displacements). The variation of the potential energy is given by:

$$\begin{aligned}\delta\mathcal{U}(\mathbf{d}, \delta\mathbf{d}) &= \frac{d}{d\varepsilon} \left[\mathcal{U}(\mathbf{d} + \varepsilon\delta\mathbf{d}) \right]_{\varepsilon=0} \\ &= \int_{\mathcal{B}_0} \frac{\partial\Psi}{\partial\mathcal{E}}(\mathcal{E}) : \delta\mathcal{E} dV - \int_{\mathcal{B}_0} \delta\mathbf{d}^\top \mathbf{f}_b dV - \int_{\partial\mathcal{B}_0} \delta\mathbf{d}^\top \mathbf{f}_t dS, \\ &= \int_{\mathcal{B}_0} \mathcal{S}(\mathcal{E}) : \delta\mathcal{E} dV - \delta\mathcal{U}_{\text{ext}}(\delta\mathbf{d}) = 0\end{aligned}\quad (3.6)$$

where $:$ denotes the contraction operator [115, 146], which can be regarded as a double inner product between two tensors, *i.e.*, $\mathbf{a} : \mathbf{b} = a_{ij}b_{ij}$, $\delta\mathcal{E}$ the variation of the Lagrangian strain tensor, and \mathcal{S} the second Piola-Kirchhoff stress tensor. The second Piola-Kirchhoff stress tensor describes the stress state of a deforming solid and is defined as the stress tensor that relates the force per unit undeformed area to the deformation gradient tensor [115]. The variation of the Lagrangian strain, given its definition in (3.2), is then given by

$$\begin{aligned}\delta\mathcal{E}(\mathbf{d}, \delta\mathbf{d}) &= \frac{d}{d\varepsilon} \left[\mathcal{E}(\mathbf{d} + \varepsilon\delta\mathbf{d}) \right]_{\varepsilon=0} \\ &= \frac{1}{2} \left(\nabla_0 \delta\mathbf{d} + \nabla_0 \delta\mathbf{d}^\top + \nabla_0 \delta\mathbf{d}^\top \nabla_0 \mathbf{d} + \nabla_0 \mathbf{d}^\top \nabla_0 \delta\mathbf{d} \right), \\ &= \text{sym} \left(\nabla_0 \delta\mathbf{d}^\top [\mathbf{I} + \nabla_0 \mathbf{d}] \right) = \text{sym} \left(\nabla_0 \delta\mathbf{d}^\top \mathbf{F} \right)\end{aligned}\quad (3.7)$$

where $\text{sym}(\cdot)$ denotes the symmetric part of the tensor. It is important to note that the variation of the Lagrangian strain tensor is a bilinear function of \mathbf{d} and $\delta\mathbf{d}$ [146]. We can explore this property by writing the Lagrangian strain variation in vectorized form:

$$\text{vec}(\delta\mathcal{E}(\mathbf{d}, \delta\mathbf{d})) = \mathbf{B}(\mathbf{d}) \delta\mathbf{d} = (\mathbf{B}_{\text{lin}} + \mathbf{B}_{\text{nl}}(\mathbf{d})) \delta\mathbf{d}, \quad (3.8)$$

where \mathbf{B} is referred to in literature as the strain-displacement matrix. Using the expression above, we can rewrite the contraction between the Piolla stress tensor and the Lagrangian stress tensor in (3.7) as $\mathbf{S} : \delta\mathcal{E} = (\mathbf{B}\delta\mathbf{d})^\top \underline{\mathbf{S}}$ with $\underline{\mathbf{S}}$ a matrix representation of the Piolla stress tensor following Voigt notation. We can use this to simplify the variational energy, as it is now linear in $\delta\mathbf{d}$.

The variational equation in (3.7) cannot be solved as easily as a system of linear equalities, due to the presence of nonlinearities in the displacement-strain relation. To solve this system of nonlinear equalities, a common strategy is to use the Newton-Raphson iterative method, which involves a sequence of linearizations followed by small update steps until the equality is satisfied. If (3.7) is not satisfied, we can introduce a residual scalar which can be defined as follows:

$$r = \int_{\mathcal{B}_0} \delta\mathbf{d}^\top \mathbf{B}^\top \underline{\mathbf{S}} \, dV - \int_{\mathcal{B}_0} \delta\mathbf{d}^\top \mathbf{f}_b \, dV - \int_{\partial\mathcal{B}_0} \delta\mathbf{d}^\top \mathbf{f}_t \, dS. \quad (3.9)$$

It is important to note that the residual above is linear in $\delta\mathbf{d}$ and nonlinear in \mathbf{d} , which stems from the fact that stress and displacements are implicitly related. This allows us to separate the variation from the residual above. Indeed, the residual above forms the weak form of the nonlinear elastic system, which often does not provide a closed-form solution for $r = 0$. Therefore, the following section focuses on spatial discretization.

Remark 3.1 *The current formulation of the continuum problem is versatile in its ability to address both two-dimensional and three-dimensional situations. Nonetheless, in order to facilitate computational feasibility, we will consider \mathcal{B}_0 to be a subset in \mathbb{R}^2 . Thus the emphasis in this chapter is on optimizing 2D designs, where space will be discretized using 2D elements using a polygonal tessellation approach.*

3.2.4 Solving the energy balance via approximations of polygonal finite elements

For two-dimensional finite element problems, the three-node triangular and bilinear four-node quadrilateral elements are widely used, while the use of higher-order polygonal elements is still relatively scarce. Polygonal elements have some attractive features such as facial connectivity, regularity, and adaptability that suit complex material domains. This makes polygonal elements ideal for topology optimization since numerical issues such as checkerboard patterns and single-node connections are inherently alleviated [90, 267].

An efficient method of generating polygonal meshes is constructing a Voronoi tessellation from a set of seeding points, where each point can be associated with

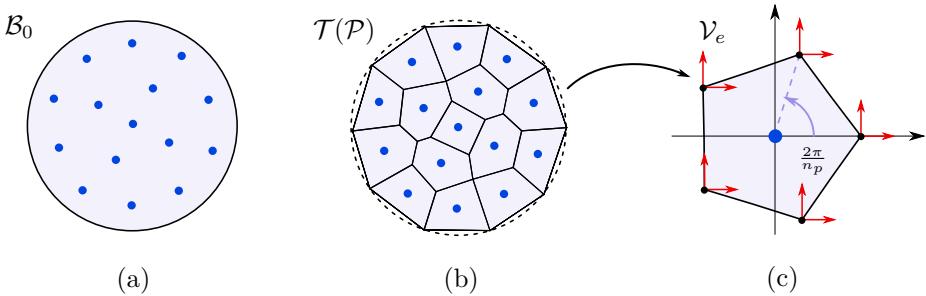


Figure 3.1. Illustration of generating a planar Voronoi tessellation from a circular domain \mathcal{B}_0 . (a) Material domain is sampled with n_e points collected in by point-set \mathcal{P} shown as (●). (b) Using Loyd's algorithm [267], a restricted Voronoi tessellation $\mathcal{T}(\mathcal{P})$ is generated composed of polygonal elements $\{\mathcal{V}_e\}_{e=1}^{n_e}$. (c) An isoparametric element related to the space \mathcal{V}_e , whose shape relates to the nodal displacements.

its respective Voronoi cell. For two-dimensional tessellations, consider a set of n number of unique seeding points $\mathcal{P} = \{\mathbf{p}_i\}_{i=1}^n$ that are uniformly distributed inside $\mathcal{B}_0 \subset \mathbb{R}^2$. Then, the corresponding (restricted) Voronoi tessellation is defined as the set of Voronoi cells that intersect \mathcal{B}_0 , that is,

$$\mathcal{T}(\mathcal{P}) = \left\{ \mathcal{V}(\mathbf{p}, \mathcal{P}) \cap \mathcal{B}_0 : \forall \mathbf{p} \in \mathcal{P} \right\}, \quad (3.10)$$

where \mathcal{V} is the Voronoi cell from the point \mathbf{p}_i . Mathematically, the definition of a Voronoi cell for a point $\mathbf{p}_i \in \mathcal{P}$ is given by

$$\mathcal{V} = \left\{ \mathbf{x} \in \mathbb{R}^2 : \Delta(\mathbf{x}, \mathbf{p}_i) \leq \Delta(\mathbf{x}, \mathbf{y}), \forall \mathbf{y} \in \mathcal{P} \setminus \{\mathbf{p}_i\} \right\}, \quad (3.11)$$

where $\Delta(\mathbf{x}, \mathbf{y}) = \|\mathbf{x} - \mathbf{y}\|_2$ denotes the Euclidean distance between two points $\mathbf{x}, \mathbf{y} \in \mathbb{R}^2$. Clearly, the choice of the point set \mathcal{P} is of paramount importance in generating the Voronoi tessellation. To obtain a uniformly distributed set, Lloyd's algorithm can be used to iteratively update a set of points that are initially chosen randomly. For more detail on the generation of polygonal meshes, we refer the reader to the work of Talischi et al. [267]. As an example, we show the mesh generation of a circular domain in Figure 3.1. The Voronoi cells $\mathcal{V}_e \in \mathcal{T}(\mathcal{P})$ in (3.11) are inherently convex polygons due to the Euclidean distance function's convexity. The convex nature of these shapes implies that all lines connecting any two points within the shapes lie entirely within the shape. In other words, the elements lack indentations or concave portions. The interior of the elements can be described using a finite set of nodes called the "*nodal coordinates*" given by $\mathbf{X}^e \in S$ with $S \in \text{convhull}\{\mathcal{V}_e\}$ the convex hull of the element \mathcal{V}_e .

Building on the finite element approach, a state vector $\mathbf{x}_i^e = (x_{i,1}^e, x_{i,2}^e)^\top$ is attributed to each coordinate. The index e serves to distinguish individual elements, while $i \in \{1, \dots, k\}$ with k the polygonal degree of the element. Subsequently, the

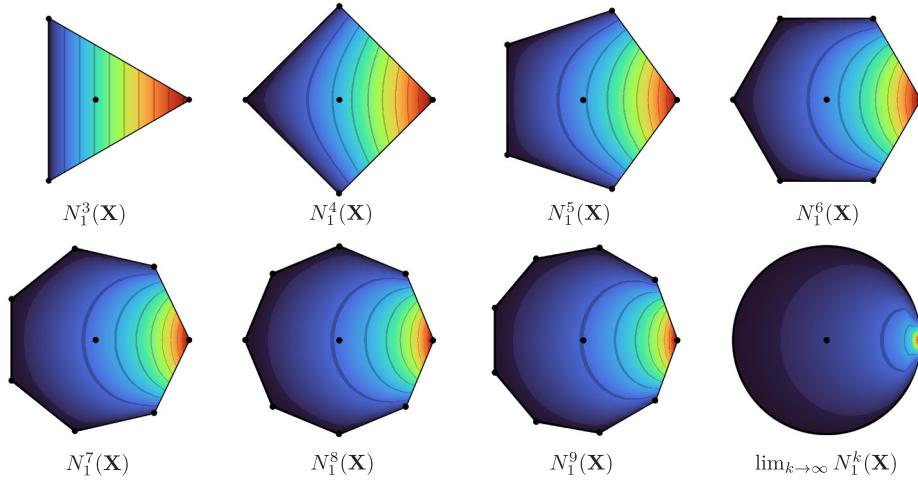


Figure 3.2. Wachspress shape functions related to the first nodal coordinate for an increasing polygonal degree k . The colormap depicts the intensity of the shape function N_1^k with $\textcolor{red}{\square} \in [0, 1]$.

displacement field can be approximated as follows

$$\mathbf{d}(\mathbf{X}, T) \approx \sum_{i=1}^{k(e)} N_i^k(\boldsymbol{\sigma}(\mathbf{X})) \mathbf{x}_i^e =: \mathbf{N}^e \mathbf{x}^e \quad \forall \mathbf{X} \in \mathcal{V}_e, \quad (3.12)$$

where $\boldsymbol{\sigma} : \mathcal{V}_e \rightarrow P_k$ represents the isoparametric mapping from global coordinates to natural coordinates of a regular polygon P_k with polygonal degree $k(e) \geq 3$, N_i^k is the shape interpolation function, and \mathbf{N}^e is the shape interpolation matrix. In this study, we investigate the widely used Wachspress shape functions [83, 259, 267, 268] for isoparametric interpolation of polygons. Figure 3.2 illustrates the Wachspress shape functions related to the first nodal coordinate N_1^k for different polygons of varying degree k . The derivation of N_i^k is available in Appendix B.1, which follows the approach outlined in [83, 268].

Finally, by substitution of the spatial interpolations of the displacement $\mathbf{d} \approx \mathbf{N}^e \mathbf{x}^e$ and virtual displacements $\delta \mathbf{d} \approx \mathbf{N}^e \delta \mathbf{x}^e$, we can reformulate the residual in (3.9) as follows

$$\begin{aligned} r &\approx \sum_{e=1}^n (\delta \mathbf{x}^e)^\top \left(\int_{\mathcal{V}_e} \mathbf{B}_e(\mathbf{x}^e)^\top \mathbf{S}_e(\mathbf{x}^e) dV - \int_{\mathcal{V}_e} \mathbf{N}^e \mathbf{f}_b dV - \int_{\partial \mathcal{V}_e} \mathbf{N}^e \mathbf{f}_t dS \right), \\ &= \delta \mathbf{x}^\top (\mathbf{f}_{\text{int}}(\mathbf{x}) - \mathbf{f}_{\text{ext}}), \end{aligned} \quad (3.13)$$

where \mathbf{x} and $\delta \mathbf{x}$ are the global nodal displacement and the global nodal virtual displacement vectors, and \mathbf{B}_e and \mathbf{S}_e the elemental strain-displacement matrix and Piolla stress tensor, respectively. The derivation of these elemental matrices is found Appendix B.2 which follows the work of Kim et al. [146]. Since the

entries of the displacement variation $\delta\mathbf{x}$ are zero at nodes where displacement is prescribed (*i.e.*, fixed DoFs), we may consider an alternative form, the residual force vector, in which the virtual displacements are omitted by only regarding the free DoFs:

$$\mathbf{r}(\mathbf{x}) = \mathbf{f}_{\text{int}}(\mathbf{x}) - \mathbf{f}_{\text{ext}}, \quad (3.14)$$

The static equilibrium of the structure can be determined by setting $\mathbf{r}(\mathbf{x})$, as given in (3.14), equal to the zero vector. To obtain this equilibrium state, the Newton-Raphson method can be utilized through iterative calculation of a linear system [90, 115, 146]:

$$\mathbf{x}^{(i+1)} = \mathbf{x}^{(i)} - \alpha \left(\mathbf{K}_T^{(i)} \right)^{-1} \mathbf{r}^{(i)}, \quad (3.15)$$

where $\alpha > 0$ an update coefficient, and the subscript (i) denotes the iteration steps, while $\mathbf{x}^{(i)}$, $\mathbf{r}^{(i)} := \mathbf{r}(\mathbf{x}^{(i)})$, and $\mathbf{K}_T^{(i)} := \left[\frac{\partial \mathbf{r}}{\partial \mathbf{x}_1} \dots \frac{\partial \mathbf{r}}{\partial \mathbf{x}_n} \right]_{\mathbf{x}=\mathbf{x}^{(i)}}$ represent the updated displacement vector, the residual force vector, and the evaluated tangent stiffness matrix, respectively. For further details on the derivation of the tangent stiffness based on the Yeoh elasticity model in (3.4), we refer [220], whose approach is outlined in Appendix B.3.

3.3 Nonlinear topology optimization

The present study focuses on the solution scheme for nonlinear deformations in hyper-elastic continuum solids. To enhance this approach, we introduce a modification to the Finite Element Method (FEM) model, known as the Solid Isotropic Material With Penalization (SIMP) method. This method is a widely used material interpolation scheme in topology optimization [19, 90, 268, 295]. Subsequently, we elaborate on how the optimization problem can be formulated to generate topologies driven by soft fluidic actuation.

3.3.1 Solid Isotropic Material With Penalization (SIMP)

In the SIMP approach, each finite element $e \in \{1, 2, \dots, n\}$ is assigned with a scalar density variable $\rho_e \in [0, 1]$ to indicate if an elemental volume is solid ($\rho_e = 1$) or void ($\rho_e = 0$). This leads to a real-valued density field representing the material distribution within a discretized domain \mathcal{B}_0 , where the global material distribution is represented by the density vector $\boldsymbol{\rho} = (\rho_1, \rho_2, \dots, \rho_n)^\top$. The density vector $\boldsymbol{\rho}$ then form the design variables of the optimization problem. To relate these artificial densities to elasticity, the strain energy density of the constitutive material model Ψ is then parameterized using $\boldsymbol{\rho}$. To improve numerical robustness, a modified SIMP approach is used in which the strain-energy function is artificially modified as follows:

$$\Psi_e = [\varepsilon + (1 - \varepsilon) \rho_e^p] \Psi, \quad (3.16)$$

where $p \geq 1$ is the penalty factor for penalizing intermediate densities during the optimization process, and $0 < \varepsilon \ll 1$ is a lower-bound on the material densities. In this work, we choose $p = 4$ and $\varepsilon = 10^{-3}$. Given the artificial elasticity model above, it shall be clear that residual vector in (3.14) now depends on the nodal displacements and the densities of the adaptive topology, \boldsymbol{x} and $\boldsymbol{\rho}$, respectively.

3.3.2 Artificial fluidic loads by elemental dilation

The most general principle of actuation in soft robotics involves fluidic or pneumatic networks embedded into the elastic body. However, within the context of topology optimization, describing the internal pressure loads can be challenging. Unlike conventional optimization problems with static loads, in a pressure-based problem, the location, direction, and magnitude of the load change concerning the material distribution at every optimization step. This inherently yields design-dependency in the global force vector. To resolve this difficulty, we exploit the connectivity properties of polygonal tessellations to describe the physics involving pneumatics efficiently. Specifically, isolated regions of void polygonal elements will artificially mimic the geometrical loads in pneumatic actuation by dilation.

To identify void regions in the topology, we introduce the notion of a so-called "*virus*" element whose purpose is to infect neighboring elements with a low elemental density (voids). These virus elements are chosen *a-priori* and remain invariant, similar to the input of a pneumatic network. If the elements adjacent to an infected element have a density lower than a specified threshold γ , that is, $\rho_e < \gamma$, they become infected, and its infection rule will spread to its adjacent neighborhood. Afterwards, each infected element will be influenced by the same pneumatic load. Clearly, as the topological layout of the discretized domain \mathcal{B}_0 changes during the optimization procedure, the influence of the pneumatic load will vary accordingly. To better reflect the physics involving pneumatics, facial connectivity must be qualified for infection, where two elements must share a common edge to be adjacent, *i.e.*, edge connection rather than node connection.

A flood-fill algorithm is used [44] to find the affected region of a virus element efficiently. In case of irregular tessellations, like the Voronoi tessellation, the flood-fill algorithm requires an adjacency matrix $\boldsymbol{\Gamma}$, which contains information about the mesh connectivity. The adjacency matrix can be directly computed from the element-node-incidence matrix. Here, the incidence matrix $\mathbf{A} \in \mathbb{Z}^{n \times m}$ is a sparse unit-matrix with n columns for each element and m rows for each node, where $\mathbf{A}_{ij} = 1$ iff node i is incident upon element j , and otherwise zero. Given the incidence matrix, the adjacency matrix $\boldsymbol{\Gamma} \in \mathbb{Z}^{n \times n}$ can be computed by

$$\boldsymbol{\Gamma} = \mathbf{A}\mathbf{A}^\top - \text{diag}(\mathbf{A}\mathbf{A}^\top), \quad (3.17)$$

where the matrix has non-zero entries $\boldsymbol{\Gamma}_{ij} = 1, 2$ iff elements i and j share a common node or edge, respectively. As mentioned earlier, the adjacency will be modified such that edge connectivity is required for adjacency. Secondly, all the rows and columns corresponding to elements that satisfy $\rho_e \geq \gamma$, given a predefined

Algorithm 3.1: Find elements subjected to volumetric deformation

Input : Tessellation \mathcal{T} , set of virus elements \mathcal{V} , threshold γ , material density vector ρ

Output: Set of elemental indices \mathcal{E}

```

1 construct  $\mathbf{\Gamma} \leftarrow \text{BuildAdjacencyMatrix}(\mathcal{T})$ ;
2 modify  $\mathbf{\Gamma} \leftarrow \text{EdgeConnectivity}(\mathbf{\Gamma})$ ;
3 find thresholds  $\mathcal{X} = \{ i \in [1, n_e] \mid \rho_i \geq \gamma \}$ ;
4 set zeros  $\mathbf{\Gamma}_i = (\mathbf{\Gamma}^\top)_i = 0$  for all  $i \in \mathcal{X}$ ;
5 initialize empty set  $\mathcal{E} \leftarrow \emptyset$ ;
6 for  $i = 1 : \text{numVirus}$  do
7    $\mathcal{I} \leftarrow \text{doFloodFill}(\mathbf{\Gamma}, \mathcal{V}_i)$ ;
8    $\mathcal{E} \leftarrow \mathcal{E} \cup \mathcal{I}$ ;
9 end

```

3

threshold γ , will be set to zero to ensure those elements are unaffected by the flood-fill. The pseudo-code for the identification of the pneumatic region is provided in Algorithm 3.1.

From a mathematical perspective, let us consider Algorithm 3.1, which can be represented by a mapping $\phi : \mathbb{R}^n \rightarrow \mathbb{Z}$. Here, the mapping $\phi(\rho)$ returns a set of elemental indices of infected elements denoted by $\mathcal{E} \subseteq \{1, 2, \dots, n\}$ that undergo volumetric compression or expansion based on boundary conditions. Using this mapping, we can assemble the global force matrix \mathbf{f} in Equation (3.14) from the elemental force vectors of the affected region of the virus element \mathcal{E} :

$$\mathbf{f}_{\text{ext}}(\mathbf{x}, \rho) = \sum_{e \in \mathcal{E}} \tilde{p}_e \mathbf{W}_e \mathbf{t}_e, \quad (3.18)$$

where \tilde{p}_e is a dimensionless parameter that represents the magnitude and direction of artificial pneumatic loading. \mathbf{W}_e is a diagonal weighting matrix of densities at nodal level, and $\mathbf{t}_e = \int_{\mathcal{V}_e} \mathbf{B}_e^\top \mathbf{D}_e \mathbf{n}_v \, dV$ is the elemental force vector. The volumetric strain is represented by $\mathbf{n}_v = (1, 1, 0)^\top$, and $\mathbf{D}_e := \partial \mathbf{S}_e / \partial \mathcal{E}$ is the fourth-order constitutive stress-strain stiffness tensor in matrix notation [220]. The derivation of \mathbf{D}_e is found in Appendix B.3. It is important to note that the global force vector in (3.18) represents an artificial pneumatic load. This method assumes that pressure loads can be emulated by anisotropic volumetric change of the polygonal elements. By varying the dimensionless parameter \tilde{p}_e , the magnitude and direction of this artificial pneumatic load can be controlled.

3.3.3 Optimization problem

Given the concept of morphology in soft robotics, which is similar to compliant mechanisms, the primary goal is to maximize the output displacement \mathbf{x}_{out} on a virtual workpiece modeled by an artificial stiffness $k_{\text{out}} > 0$ [19, 90]. The objective function or the desired output displacement can be expressed as $\Phi = \mathbf{L}^\top \mathbf{x}(\rho)$,

where $\mathbf{L} \in \mathbb{R}^{2n}$ is a sparse vector composed of non-zero entries for the degrees-of-freedom corresponding to the desired morphology of the soft robot. Given this description of directional output displacement, the topology optimization problem for soft robots can be formulated as:

$$\begin{aligned} \max_{\boldsymbol{\rho}} \quad & \Phi = \mathbf{L}^\top \mathbf{x}(\boldsymbol{\rho}), \\ \text{s.t.} \quad & c := \mathbf{r}(\mathbf{x}, \boldsymbol{\rho}) = 0, \\ & g := \mathbf{v}^\top \boldsymbol{\rho} \leq V^*, \\ & \boldsymbol{\rho} \in \mathcal{P}, \end{aligned} \tag{3.19}$$

where $\mathbf{r} \in \mathbb{R}^{2n}$ the global residual force vector in its equilibrium state, $\mathbf{v} \in \mathbb{R}^{n_e}$ a constant vector of relative elemental volumes, $0 < V^* < 1$ the desired material infill, and $\mathcal{P} = \{\boldsymbol{\rho} \in \mathbb{R}^{n_e} \mid 0 \leq \rho_e \leq 1 \forall e \in [1, n_e]\}$ a set of feasible material densities that ensure numerical robustness.

3.3.4 Solver and sensitivity analysis

In this section, we discuss the use of a gradient-based optimization solver for synthesizing the soft robot. Here, we use the Method of Moving Asymptotes (MMA) proposed by Svanberg [264]. The MMA is similar to other nonlinear programming approaches, such as Optimality Criteria (OC) and Sequential Quadratic Programming (SQP), in that it finds an optimal solution to a nonlinear non-convex optimization problem with inequality constraints. The MMA solves a sequence of sub-problems, *i.e.*, convex approximations of the true problem, which are constructed from gradient-based information of the objective function Φ and their constraints c and g . Svanberg [264] has provided open numerical implementations for his MMA algorithm represented as MATLAB function called `mmasub`, which is subroutine of the MMA algorithm that updates the design parameters $\boldsymbol{\rho}^{(k)} \rightarrow \boldsymbol{\rho}^{(k+1)}$ given the design sensitivities of the objective Φ and the equality and inequality constraints c and g , respectively. By recursively calling `mmasub`, the optimization problem in (3.19) can be solved numerically.

The sensitivity of the inequality constraint in (3.19) is $\partial g / \partial \boldsymbol{\rho} = \mathbf{v}$ since we assume that the elemental volume \mathbf{v} is constant. The sensitivity of the objective function is less trivial due to its dependency on the nodal displacements $\mathbf{x}(\boldsymbol{\rho})$. Since it is computationally expensive to obtain the displacements \mathbf{x} through the Newton-Raphson method, it becomes beneficial to avoid the computation of their sensitivities. Thus, the sensitivities are computed through the adjoint method in which the objective function is augmented to include the equality constraint c . This leads to

$$\Phi(\mathbf{x}, \boldsymbol{\rho}) = \mathbf{L}^\top \mathbf{x}(\boldsymbol{\rho}) - \boldsymbol{\lambda}^\top \mathbf{r}(\mathbf{x}, \boldsymbol{\rho}), \tag{3.20}$$

where $\boldsymbol{\lambda} \in \mathbb{R}^{2n}$ is a constant vector referred to as the adjoint vector. Note that, in case of equilibrium (*i.e.*, $\mathbf{r} = \mathbf{0}_n$), the global residual forces are equivalent to zero;

Algorithm 3.2: Computational design algorithm for pneumatic soft robots.

Input : Domain \mathcal{B}_0 , material Ψ , initial $\rho^{(0)}$, infill V^* , virus \mathcal{V} , output \mathbf{L} , artificial pressure \tilde{p}_e

Output: Optimal soft robot topology ρ^*

- 1 construct tessellation $\mathcal{T} \leftarrow \text{VoronoiMesher}(\mathcal{B}_0)$;
- 2 **while** $\text{convergence} \neq 1$ **do**
- 3 update artificial material Ψ_e using (3.16) ;
- 4 find infected set \mathcal{E} using **Algorithm 1** ;
- 5 build residual forces \mathbf{r} using (3.14) and (3.18);
- 6 solve displacements $\mathbf{x} \leftarrow \text{NewtonRaphson}(\mathbf{r})$;
- 7 evaluate $g_{,\rho} \leftarrow \partial g / \partial \rho_e$;
- 8 evaluate $\Phi_{,\rho} \leftarrow \partial \Phi / \partial \rho_e$ using (3.22) ;
- 9 update $\rho \leftarrow \text{MMA}(\Phi_{,\rho}, g_{,\rho}, \rho)$;
- 10 **end**

therefore, the adjoint vector can be chosen freely without violating the original optimization problem. Differentiations of the objective function with respect to the elemental densities ρ_e for each finite element $e \in \{1, 2, \dots, n_e\}$ yields

$$\begin{aligned} \frac{\partial \Phi}{\partial \rho_e} &= \mathbf{L}^\top \frac{\partial \mathbf{x}}{\partial \rho_e} - \boldsymbol{\lambda}^\top \left(\left[\frac{\partial \mathbf{r}}{\partial x_1} \dots \frac{\partial \mathbf{r}}{\partial x_n} \right] \frac{\partial \mathbf{x}}{\partial \rho_e} + \frac{\partial \mathbf{r}}{\partial \rho_e} \right), \\ &= \left(\mathbf{L}^\top - \boldsymbol{\lambda}^\top \mathbf{K}_T \right) \frac{\partial \mathbf{x}}{\partial \rho_e} - \boldsymbol{\lambda}^\top \frac{\partial \mathbf{r}}{\partial \rho_e}, \end{aligned} \quad (3.21)$$

where the Jacobian of the residual force vector is substituted by the tangent stiffness matrix \mathbf{K}_T , see Appendix B.3 for the derivation. By choosing the adjoint vector $\boldsymbol{\lambda} = (\mathbf{K}_T)^{-\top} \mathbf{L}$, the terms involving $\partial \mathbf{x} / \partial \rho_e$ can be eliminated and thus computation of the gradient becomes feasible. Following this, the gradient of the objective function can be written compactly as:

$$\frac{\partial \Phi}{\partial \rho_e} \stackrel{(3.14)}{=} -\mathbf{L}^\top (\mathbf{K}_T)^{-1} \left(\sum_{e=1}^{n_e} \int_{\mathcal{V}_e} \mathbf{B}_e^\top \frac{\partial \mathcal{S}_e}{\partial \rho_e} dV - \frac{\partial \mathbf{f}_{\text{ext}}}{\partial \rho_e} \right). \quad (3.22)$$

However, it should be noted that deriving the loading sensitivity $\partial \mathbf{f}_{\text{ext}} / \partial \rho_e$ is not straightforward since the global force vector is constructed from nested functions of logic operations such as flood-fill. Therefore, we derive the loading sensitivity numerically using the forward difference method. To reduce computation time, we propose computing the sensitivities of only the elements at the boundary of the pressure region since the gradient of the pneumatic region is largest near the boundary of the infected set \mathcal{E} . We provide pseudo-code for the computational design algorithm for synthesizing pressure-driven soft robots in Algorithm 3.2.

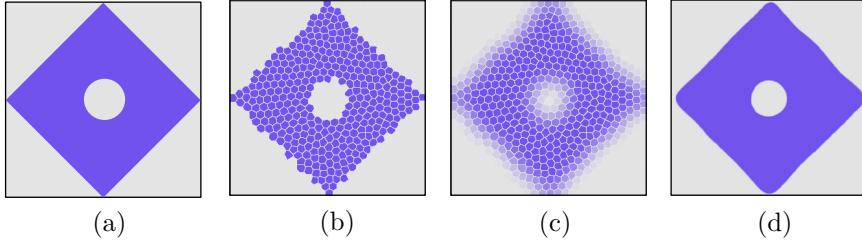


Figure 3.3. An illustration of filter and interpolation schemes developed to minimize mesh artifacts. The areas (■, □) denote the material infill and void regions, respectively. (a) The ground truth. (b) Density field based on the piecewise Voronoi tessellation. Note the jitter around the boundaries of the material infill, which leads to high sharp gradients in $\partial\phi/\partial\rho_e$. (c) To address this issue, filtered densities are obtained using (3.23). (d) The isosurface reconstruction \mathcal{B}^* of the filtered density field of the optimizer.

3.3.5 Gradient filters and interpolation

A well-known filtering technique is used to solve this issue, which has been proposed by Sigmund et al. [19]. The design sensitivities are modified based on a weighted average filtering scheme [19, 90]:

$$\frac{\partial \tilde{\Phi}}{\partial \rho_e} = \frac{1}{\rho_e \sum_{i=1}^n H_{e,i}} \sum_{i=1}^n H_{e,i} \rho_i \frac{\partial \Phi}{\partial \rho_i}, \quad (3.23)$$

where $H_{e,i} := \max \{0, R_{\min} - \Delta(\mathbf{p}_e, \mathbf{p}_i)\}$ is the filter weight, R_{\min} is the filter radius, and $\Delta(\mathbf{p}_e, \mathbf{p}_i)$ is the Euclidean distance between the centers of the elements i and e . The radial filtering is solely applied to the design sensitivities, and therefore, the polygonal mesh discretization heavily influences the final topology design. In order to improve the quality of optimization output, we implement Radial Basis Functions (RBF) interpolation that is weighted with filter densities. This is followed by an isosurface extraction process that aids in achieving a distinct separation between void and filled regions. Mathematically, the filter topology of the optimization routine is given by

$$\mathcal{B}^* = \left\{ \mathbf{X} \in \mathcal{B}_0 \mid \sum_{e=1}^n \psi_{\text{RBF}}(\mathbf{X} - \mathbf{p}_e; \rho_e) \geq \epsilon_{\text{iso}} \right\} \quad (3.24)$$

where we explore a radial interpolation function $\psi_{\text{RBF}}(\mathbf{r}; \rho) = \exp(-\alpha\rho\|\mathbf{r}\|^2)$ with $\alpha > 0$ a tuning parameter, and ϵ_{iso} is the isosurface value. The parameter α enables users to regulate the thickness (or radial dilation) of the optimized soft topology. For our specific investigation, we opt to use $\alpha = R_{\min}$ as a means of aligning with the filter radius specified in (3.23). In Figure 3.3, we show this multi-step filtering scheme which is employed to reduce the tessellation artifacts on the topology optimization solutions.

3.4 Numerical examples: generating soft robotic topologies via optimization

The proposed computational algorithm enables the synthesis of various topologies of soft robots exhibiting diverse motions. The choice of output vector \mathbf{L} is arbitrary, allowing for the generation of motion patterns that are useful in soft robotic locomotion or grasping by customizing the objective function. Our analysis focuses on three cases: (i) linear elongation or contraction, (ii) distributed bending, and (iii) grasping. All simulations are conducted using MATLAB[®] on a modern machine (Ryzen 7-5800H, 3.2GHz). Unless stated otherwise, all simulation examples employ the same material model, specifically, the Yeoh parameters $c_1 = 35$ kPa, $c_2 = 0.25$ kPa, and $c_3 = 0.023$ kPa, which are based on the silicone elastomer Dragontex 10ATM [316].

3

3.4.1 Linear translational soft actuators

One of the simplest forms of motion in soft robotics is linear translation. Such motion can be achieved through the use of various topologies, such as the McKibben actuator or a serial chain for bellow-type actuators. Both of these soft actuation principles operate similar: pressurized fluid is applied to an enclosed interior, and due to low-axial compliance compared to the radial compliance imposed by geometrical shape (*e.g.*, bellow shape) or material composites (*e.g.*, McKibben [209, 210]), linear motion is produced. Given their linear motion, these system are often associated with bio-inspired muscle, due them acting similar to hydrostatic muscular system found in nature [142].

In the first optimization benchmark we aim to find the optimal topology for a soft fluidic muscle. Exploring spatial symmetry, we consider a rectangular material domain \mathcal{B}_0 of dimension 20×10 mm, which forms the upper-left quadrant of the pneumatic soft muscle. This makes the cross-sectional size of the bellow 40 mm in width and 20 mm in height. The bottom of upper-left quadrant is structurally fixed, the left wall can move only vertically (symmetric boundary condition), and the other boundaries can move freely. The objective of the optimization is to maximize the displacement of the top-left corner in positive vertical direction. The top corner is equipped with an artificial spring $k_{out} = 1.0$ N mm⁻¹. The material infill is set to $V^* = 0.25$ (*i.e.*, a material infill of 25%). As for the initial conditions, we consider small circular hole of 3 mm, which also resides the virus element subjected to an artificial pressure parameter $\tilde{p}_e = 0.01$. In our analysis, we consider $n = 10k$ elements.

The evolution of the optimization solver is presented in Figure 3.4. Interestingly, it reveals a bellow-shaped soft actuator structure, bearing resemblance to those commonly utilized in engineering applications. Additionally, the optimizer generates a non-convex bellow with slightly curvature inward. This shape is intended to decrease the axial stiffness of the soft actuators, thereby reducing ballooning during significant elongation. Similar concave bellow designs have

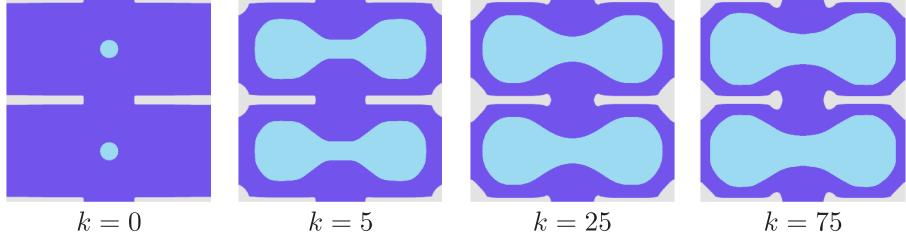


Figure 3.4. Evolution of topology optimization solver for the linear soft actuator, where $V^* = 0.25$. The areas (purple, grey, light blue) denote the material infill, void, and fluidic region, respectively. It can be observed that after a few iterations, a shape appears that is reminiscent of the conventional bellow. It is noteworthy that the shape is non-convex, with a slight curvature inwards, which enhances elongation without introducing excessive ballooning.

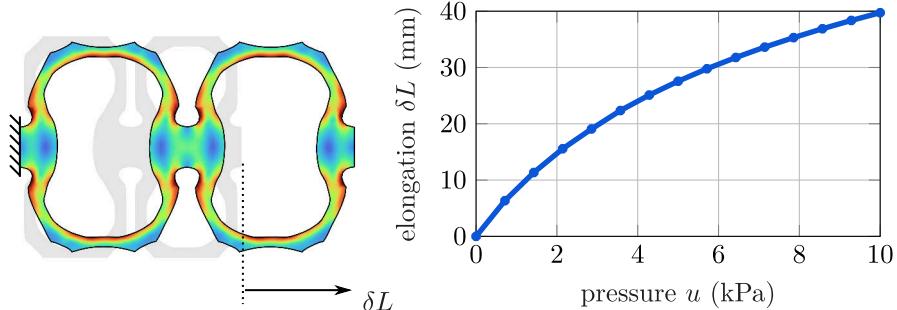


Figure 3.5. (left) Numerical validation of the optimized linear soft actuator, where the Von Mises stress is shown using the colormap $\in [0, 12]$ MPa. (right) Input-displacement characteristic of the optimized soft actuator.

been seen in Festo’s Bionic Arm [104]. The numerical validation of the structure is shown in Figure 3.5, which indicate that the soft topology can achieve 100% extension at 10 kPa. It is important to note, however, that the slope of the input-output trend is positive decreasing, which suggests that further increase in pressure may eventually lead to ballooning.

3.4.2 Pinching soft grippers

The second optimization benchmark involves the study of compliant mechanisms that are capable of transforming linear forces into grasping or pinching motions. In this analysis, we aim to investigate similar motions through fluidic actuation. It is a well-known issue in optimization for gripping mechanics that solvers frequently generate thin hinge-like structures that are susceptible to high stress concentration [19, 169]. We hypothesize that our soft material setting can naturally mitigate this problem, due to low material compliance and enabling large deformation.

The soft fluidic gripper’s design domain is assumed to be symmetrical. Therefore, only the top half of the mechanism, with dimensions of 45×15 mm, is con-

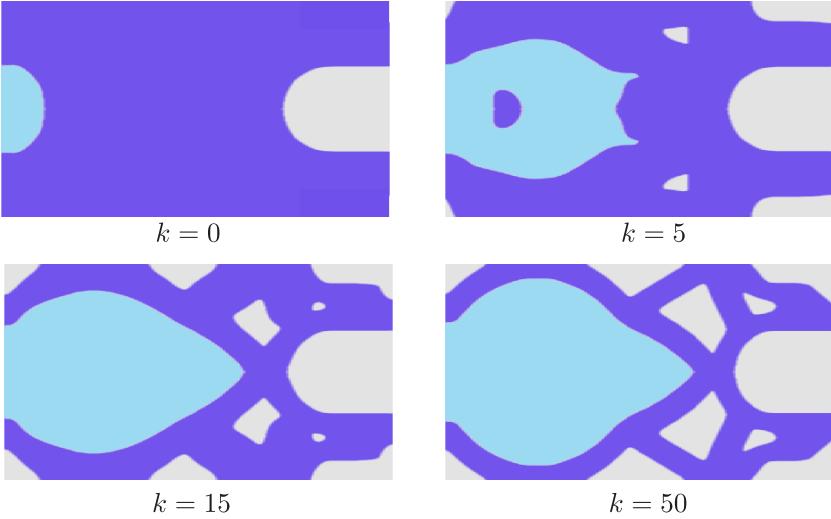


Figure 3.6. Evolution of topology optimization solver for the soft fluidic gripper, where the material infill is $V^* = 0.30$. The areas (purple, grey, cyan) denote the material infill, void, and fluidic region, respectively. The optimizer proposes a topology with a large tear-shaped pressure vessel, whose walls are connected to small struts that transfer the gripping motion.

sidered. The left side is fixed structurally, while the bottom can move horizontally due to the symmetry condition. On the right side, a cut-out is introduced, which serves as the gripper region. The objective of the optimization is to maximize the displacement of the gripper corner in negative vertical direction. This top corner is equipped with an artificial spring $k_{out} = 1.0 \text{ N/mm}$, and the material infill is set to $V^* = 0.30$ (*i.e.*, a material infill of 30%). As for the initial conditions, we consider circular hole of radius 6 mm at the left side. Concerning the pneumatic actuation, the adaptive topology is subjected to an artificial pressure parameter $\tilde{p}_e = 0.01$, where the virus element is also located at the left side. In our analysis, we consider $n = 20k$ elements.

The evolution of the optimization solver is presented in Figure 3.6. The proposed solution consists of a tear-shaped pressure vessel, whose walls are connected to a compliant mechanism through struts that transfer volumetric deformation to pinch-grasping motions. This gripper mechanism is similar to those found in literature [19, 90], which involve a central revolute compliant joint, resembling scissors. To validate the proposed structure, we converted the final 2D topology result shown in Figure 3.6 into a nonlinear FEM model and subjected it to an input pressure of $u = 10 \text{ kPa}$. The numerical validation results are presented in Figure 3.7, which also shows the relationship between pressure and gripper distance. Our numerical results demonstrate that gripping morphologies arise when the structure is subjected to positive pressure, where a closed grasp is achieved at an activation pressure of $u \geq 10 \text{ kPa}$.

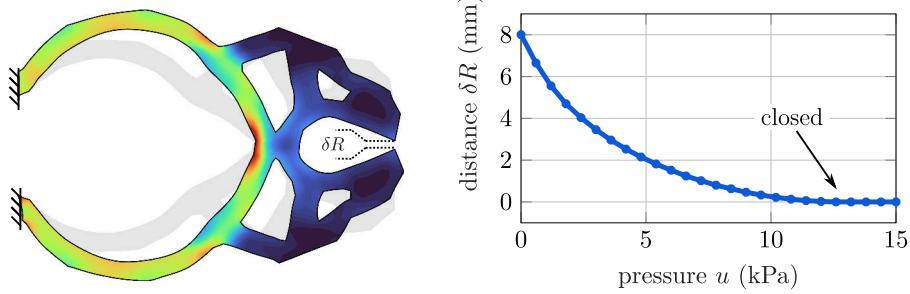


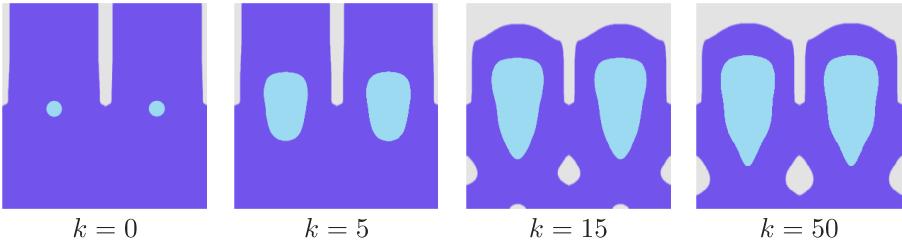
Figure 3.7. (left) Numerical validation of the optimized linear soft actuator, where the Von Mises stress is shown using the colormap $\in [0, 25]$ MPa. (right) Input-displacement characteristic of the optimized soft actuator. Notice that at $u \geq 10$ kPa, no further deformations occur at the end-effector level as the gripper tips are in contact.

3.4.3 Bending soft actuator – PneuNet inspired

Next, we focus on soft actuator that produce distributed bending. Such morphology is often associated with the popular class of soft actuators named "PneuNet" actuators [91, 120, 174, 212, 213]. PneuNet actuators consist of a set of rectangular pneumatic chambers inside an elastomer medium. When pressurized, these chambers inflate, and due a structural stiffness gradient, the elastomer body undergoes bending. Typically, inextensible composite materials are used at the bottom of the structure to further such stiffness gradient and therefore enhance bending. The goal of this numerical study case is to synthesize a soft robot topology that undergoes bending motion similar to the PneuNet actuator.

In our example, the following settings are chosen. We consider a rectangular design domain B_0 with dimensions 20×40 mm (as shown in Fig. 3.8). The maximum material infill is $V^* = 0.3$ (*i.e.*, a material infill of 30%). The bottom left corner is fixed, and the right bottom corner is equipped with an artificial spring $k_{out} = 1.0$ N/mm. The objective of the optimization is to maximize the vertical displacement of the left bottom corner in the negative vertical direction. Concerning the pneumatic actuation, the adaptive topology is subjected to an artificial pressure parameter $\tilde{p}_e = 0.01$, where the virus element is located at the center.

Using the method described in Algorithm 3.2, an optimized topology is obtained (as shown in Fig. 3.8). As can be seen, the computational algorithm provides a new and interesting variation on the well-familiar PneuNet actuator. Contrary to its rectangular predecessor, the optimal structure has a significant resemblance to a bellow-shaped actuator to accommodate bending mobility further. Here, however, these bellows are tear-shaped whose narrow side is oriented downwards. To validate our synthesized topology, a three-dimensional finite element analysis is conducted. First, we use Gaussian radial basis functions (RBFs) to reconstruct a smooth manifold surface from the discretized optimization mesh. Due to spatial symmetry, the spatial reconstruction can be horizontally repeated to construct a full 'PneuNet' actuator, see Figure 3.8. The two-dimensional optimization



3

Figure 3.8. Evolution of topology optimization solver for the bending soft actuator, where $V^* = 0.30$. The areas (purple, grey, light blue) denote the material infill, void, and fluidic region, respectively. The optimization process results in a topology that bears resemblance to that of conventional PneuNets, with the exception that the pressure chambers take on a tear-shaped form. Additionally, the optimizer generates an in-extensibility layer by depositing more material at the bottom.

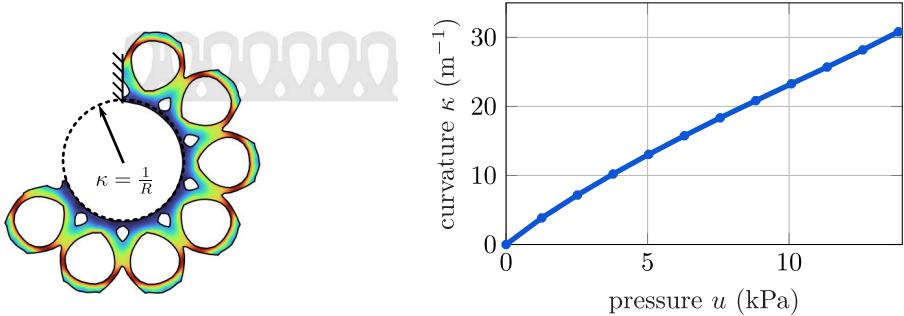


Figure 3.9. (left) Numerical validation of the optimized linear soft actuator, where the Von Mises stress is shown using the colormap $\in [0, 25]$ MPa. (right) Input-curvature characteristic of the optimized soft bending actuator. Notice that the input-output relation is closely linear, which traditionally is accomplished using composite materials by introducing inextensible layers [212, 213].

is then transformed into an nonlinear FEM model. The pneumatic chambers are subjected to a positive differential pressure of $u = 15$ kPa. As can be illustrated by Figure 3.9, the finite element analysis verifies that the synthesized soft robot topology accomplishes the desired bending morphology when pressurized.

3.4.4 Solutions for varying material parameters

A important aspect of topology optimization is that, in addition to selecting an objective function, the numerical solutions can be influenced by the choice of material. Particularly within the realm of soft robotics, which encompasses a wide range of soft material options, it is therefore paramount to explore various material parameters beyond the previously utilized Dragonskin 10 material with $c_1 = 36$ kPa. In the analysis, we investigate four alternative materials commonly exam-

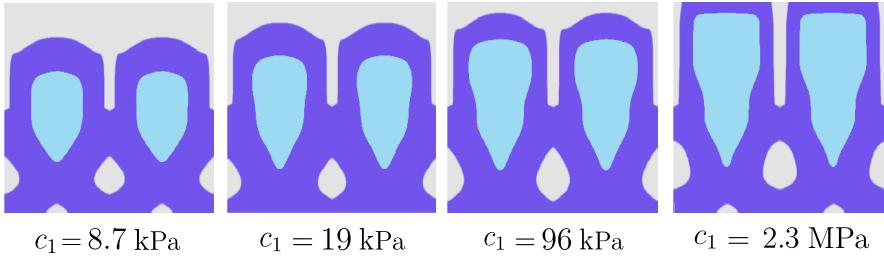


Figure 3.10. Design solutions found using optimization for different material models, arranged from left to right: Ecoflex 00–10, Ecoflex 00–50, Dragonskin 30, and NinjaFlex 85A, with a progressive increase in material stiffness. The areas (█, █, █) denote the material infill, void, and fluidic region, respectively. It is worth noting that all of the optimization solutions exhibit a tear-drop-shaped bellows, which might suggest the existence of material-invariant (sub)-solutions to the inverse design problem of bending soft actuators composed of soft materials.

ined in the field: Ecoflex 00-30TM, Ecoflex 00-50TM, Dragonskin 30TM, and NinjaFlex 85ATM. It is important to note that all materials, except for NinjaFlex 85ATM, are two-component castable silicone rubber materials, with NinjaFlex being a 3D-printable TPU material used for Fused Filament Decomposition (FDM) printing. By adopting material parameters derived from literature, we obtain the following material parameters: Ecoflex 00-10 with $c_1 = 8.7 \text{ kPa}$ [177]; Ecoflex 00-50 with $c_1 = 19 \text{ kPa}$ [315, 316]; Dragonskin 30 with $c_1 = 96 \text{ kPa}$ [177, 315]; and NinjaFlex 85A with $c_1 = 2.3 \text{ MPa}$ [315]. The compressibility parameters are chosen identical to previous simulations. In this investigation, we repeat the inverse design problem of the bending PneuNet actuator as in Section 3.4.3.

Figure 3.10 shows the optimization solutions for various material choices. An interesting observation to note is that all topologies demonstrate a tear-drop-shaped bellows, as also observed in Section 3.4.3 (and Section 3.4.2). This observation might suggest the existence of generalized design solutions, or at the very least partial solutions, that seem invariant with respect to the material choice. The differences between solutions lie in (i) the height, roundness, and volumetric capacity of the bellows, (ii) the wall thickness, and (iii) the topology of the "inextensible" layer at the bottom. Softer materials typically exhibit shorter and rounder bellows, while stiffer materials tend to favor rectangular geometries. With a stiffness value of $c_1 = 2.8 \text{ MPa}$ (*i.e.*, the NinjaFlex 85A), this rectangular geometry is most pronounced, even pushing against the bounded design domain. This might suggest that the design domain is chosen too constrictively. Moreover, the volumetric capacity of the fluidic chamber is reduced, while the wall thickness is increased for softer materials. This can perhaps be attributed to the increased effort required to deform stiffer materials and the tendency for softer materials to experience ballooning earlier.

Although [315] presents the material model in the generalized Rivlin model, the material parameters for the Yeoh model can be found under consistency with linear elastic materials as $c_1 = 0.5(C_{01} + C_{10})$ with C_{01}, C_{10} the Rivlin parameters.

Another intriguing observation is the appearance, disappearance, and re-appearance of optimal topological structures when traversing the elasticity spectrum of soft materials. In Figure 3.10, we see that for $c_1 = 8.7$ kPa (softest) and $c_1 = 2.8$ MPa (stiffest), both solutions favor a hinge-like structure. Yet, for intermediate values of c_1 , the optimizer proposes an inextensible layer at the bottom. This finding is quite unexpected, as optimality in structural optimization may not exhibit a monotonic relationship with increasing material elasticity, whereas others, *e.g.*, fluidic capacity and bellows height, appear to be monotonically correlated with c_1 . We hypothesize that using an inextensible layer is too ineffective for softer material values (*i.e.*, $c_1 < 8.7$ kPa) as their low elasticity cannot be used to constrain motion; thus a hinge-like structure is likely the more effective option for generating bending. Conversely, it is well-established that stiff materials tend to favor hinge-like structures for bending, as demonstrated in various studies on topology optimization for compliant mechanisms [19, 169, 322]. For a lack of better terminology, we refer to this phenomenon as a *transcritical bifurcation* in the optimization solution space, wherein there is an exchange of stability (*i.e.*, the convergence/divergence of the optimization solutions) between two fixed points depending on the material parameter c_1 . In light of this observation, exploring a broader material spectrum during a topology optimization analysis might emphasize different solutions that can otherwise not be observed when fixing material models *a-priori* in a design procedure.

Remark 3.2 (On fabrication) *In Chapter 6, Section 6.6.2, we validate the aforementioned soft bending actuator optimization using Additive Manufacturing. Using the material properties of the printable material (*i.e.*, FormLabs resin 80A [316]), the optimization suggestions are used as a guideline for design and showing the potential for the approach to applied to real structures.*

3.5 Conclusion

In this chapter, we present a novel framework for synthesizing soft robot topologies from hyperelastic soft materials. The design synthesis of classic soft robots is challenging due to material nonlinearities and the numerical implementation of pressure-driven loads in a topology optimization framework. We proposed a nonlinear finite element method for polygonal elements to solve these problems. Compared to previous research, our numerical approach presents a better representation of the physical nature of soft robotics, in particular, the hyperelasticity and the pneumatic actuation. Numerical investigation shows that our framework can produce meaningful and insight-full material layouts when developing a pressure-driven soft robot from soft materials. We further establish that the exploration of a range of materials can potentially yield diverse design solutions, including those that are independent of the specific material used. Theoretically, the proposed framework can be adapted to also express other actuation principles in soft robotics, such as dielectric polymers or thermal expansion; however, minor changes are required.

4

Dynamic modeling of soft robots – the constant strain approach

Abstract - In this chapter, we derive continuum dynamic models for pneumatic soft robot manipulators through the differential geometry of spatial curves. These models are then related to the Finite Element Method (FEM) to capture the intrinsic geometric and material nonlinearities. To accelerate numerical simulation, a reduced-order integration scheme is introduced to compute the dynamic Lagrangian matrices efficiently. This, in turn, allows for high-speed and (multi-link) dynamic models for soft manipulators with a minimal sacrifice in numerical precision. By exploring passivity ideas and a linear parametrization of hyper-elastic material coefficients, we also propose a passivity-based adaptive controller that enhances robustness towards material uncertainty and unmodelled dynamics – slowly improving their estimates online. As a study case, a fully 3D-printed soft robot manipulator is developed, which shows good correspondence with the dynamic model under various conditions, *e.g.*, natural oscillations, forced inputs, and subjected to external disturbances like tip-loads. The solidity of the approach is demonstrated through extensive simulations, numerical benchmarks, and experimental validations.

This chapter is based on: B.J. Caasenbrood, A.Y. Pogromsky, and H. Nijmeijer. *Control-oriented Models for Hyper-elastic Soft Robots through Differential Geometry of Curves*. Soft Robotics, 2022. doi: 10.1089/soro.2021.0035.

4.1 Introduction

Traditional robots are made from rigid and dense materials that ensure accurate and repeatable motions. While rigid robotics excel at fast and precise motion, their structural rigidity lacks the compliance and mechanical robustness needed for safe and passive interaction in an unknown environment. Soft robotics, on the other hand, aim to improve the motion complexity and environmental robustness that is generally lacking its rigid counterpart. To further promote these topics in robotics, researchers aim to mimic living creatures by developing bio-inspired robots with similar morphologies and mechanical properties [78, 97, 98, 152, 175, 261]. The hyper-flexible and continuum-bodied structure in soft robots provides them with a rich family of motion primitives. Besides bio-mimicry, soft robotics has proven to be a prominent alternative for rigid robotics with a variety of applications, *e.g.*, manipulation and adaptive grasping [91], untethered locomotion and exploration through uncertain environments [53, 62, 175], rehabilitation [213], and even minimal-invasive surgery [55, 163]. Although the popularity of the field has increased exponentially in recent years, one of the first soft robots dates back already to the early 1990s, *e.g.*, the work of Suzumori et al. [261]. Yet, despite years of soft robotics research, their intrinsic hyper-flexible nature still possesses numerous challenges on modeling and control.

One major challenge in modeling is that the soft robot's elastic body undergoes large, continuous deformation. Since its inception, numerous works have addressed the kinematics for soft continuum robots [129, 189, 190]; yet, its original framework stems from hyper-redundant robotics nearly a decade earlier [52]. Similar to soft robots, hyper-redundant robots exploit their high joint redundancy to achieve a broader range of tasks (*e.g.*, shape control and collision avoidance) besides end-effector manipulation. To some extent, soft robotics can be seen as the successor to hyper-redundant robotics in which rigid mechanical joints or links are substituted with hyper-flexible soft elements. As such, the resulting dynamics involves one continuous deformable inertial body rather than a set of interconnected rigid bodies. As such, conventional modeling approaches cannot be applied directly to these continuously deformable robots, stressing the importance of novel modeling strategies. In this respect, the dynamics of a continuously deformable soft robot are of infinite-dimensional nature. This paradigm shift has further emphasized the challenges in control-oriented modeling of soft robots, as their physical description are often more suited for a Partial-Differential Equations (PDEs) rather than Ordinary Differential Equations (ODEs).

Recently, some significant steps have been made toward formulating reduced-order ODE models for elastic continuum soft robots, paving a path toward model-based controllers. Perhaps one of the most popular techniques of spatial reduction is the so-called "*Piece-wise Constant Curvature*" model – PCC for short. The PCC model assumes that a soft robot's reachability can be described using a number of spatially-constant curves, which are parameterized using a minimal set of generalized coordinates. Although PCC models can be seen as a significant over-

simplification of true continuum mechanics at hand, and is only applicable within some conservative conditions on soft robots (*e.g.*, elasticity dominates gravity), these models have proven to be remarkably viable for various control applications. Besides its use in inverse kinematic control [129, 175, 176], PCC models have also shown to be suitable for feedforward controllers as demonstrated by Falkenhahn et al. [78]; and more recently, closed-loop feedback controllers by Della Santina et al. [72, 135]. Although the aforementioned works utilize the lumped-mass description, others have employed PCC models with uniform mass distribution [97, 98, 222, 270, 271] and current models even extend beyond the constant curvature [52, 72, 190]. However, in the face of significant external loading or (distributed) contact with the environment, the PCC assumption is relatively conservative and leads to undesired kinematic constraints on the continuum deformation. Besides, these models often need additional identification to model compliance as they do not originate from a continuum mechanical framework.

On the other hand, Finite-Element Method (FEM) models do originate from continuum mechanics and, due to their PDE description, provide a more accurate representation of deformations; and are particularly suited to deal with geometric and material nonlinearities. Duriez et al. [75] and related works [57, 100, 154] showed that reduced-order FEM models could play an important role in closed-loop control – allowing accurate volumetric deformation and hyper-elastic behavior. Although such real-time simulations for FEM-based models are possible, a significant state-reduction is required to ensure sufficient computational speed. In the process, FEM-based models often lose desirable control properties, *e.g.*, passivity preservation, which might play an important role in control. An alternative modeling strategy is the recently emerging geometrically-exact Cosserat-beam model. Similar to the PCC models, the Cosserat models benefit from their Lagrangian model structure – the basis for robotics control theory. Rooted in a geometric method for describing the continuum mechanics using Lie theory proposed by Simo et al. [242], Boyer et al. [29, 30] proposed a geometrically-exact modeling framework for Cosserat beams using nonlinear parametrization of the strain field. Other examples include the work of Renda et al. [221, 222], providing various options for Piecewise-Constant Strain (PCS) and Variable Strain modeling approaches. Although recent variants of the Cosserat models offer good computational performance [102, 284], its use in model-based control is slowly upcoming.

In this respect, the topic of reduced-order modeling of soft robots is an active area of research. Yet, a challenge that is frequently overlooked in control-oriented research is the anisotropic material behavior, mechanical saturation, and more importantly, the nonlinear and possibly time-varying nature of the highly hyper-elastic soft materials [78, 190, 271, 284]. This is further amplified by the fact that soft robots are known for their diversity in elastic materials and corresponding morphologies. Mustaza et al. [198] proposed a modified nonlinear Kelvin-Voigt material model to embody the complex material behavior of silicone-composite manipulators (so-called STIFF-FLOP actuators). A similar silicone composite actuator

was experimentally validated by Sadati et al.[231] who proposed a novel modeling approach with an appendage-dependent Hookean model and viscous power-law to describe nonlinear and time-dependent material effects, respectively. Both nonlinear material models show good correspondence with physical soft robots under various dynamic conditions, yet they lack general transferability to the soft robots with different geometries – intrinsically captured by FEM-driven models. As of today, there are few control-oriented models that both offer geometry and material versatility similar to FEM models and the control convenience similar to spatial curve models.

Ultimately, the strong nonlinearities paired with its continuous nature encourage the use of model-based controllers. Nevertheless, regarding the aforementioned model-based control approaches [72, 78, 135], the stability and performance of the closed-loop system could be undermined by uncertainties in physical parameters or unmodelled dynamics. Particularly for state-feedback linearization (e.g., inverse dynamic), as the inversion of inaccurately estimated systems could lead to poor performance and even instability. Adaptive control [192, 247] or energy-based controllers [203] might offer the needed robustness towards material uncertainties and unmodelled dynamics. Unfortunately, up till now, the applicability of adaptive and energy-based control techniques on soft robotics is scarcely explored. Franco et al. [87] used an adaptive energy-based controller that compensates for external disturbances on the end-effector, yet this controller can be extended to include various slowly-varying material uncertainties, e.g., hyper-elasticity and viscosity.

The contributions here are two-fold. First, to derive a finite-dimensional approximate of a soft continuum manipulator, where we briefly recapitulate existing modeling techniques for soft robot manipulators. To address the issue of infinite-dimensionality, we explore the PCC condition that allows for a low-dimensional description of the continuum dynamics. Although such modeling approaches have been thoroughly developed, we will address two issues that will aid the development of model-based controllers. We aim to bridge the gap between the PCC model and the underlying continuum mechanics by matching the quasi-static behavior to a Finite-Element-driven model (FEM), and we propose a reduced-order integration scheme using Matrix-Differential Equations (MDEs) to compute the spatio-temporal dynamics in real-time. Preliminary results were shown in Caasenbrood et al. [37, 38].

Second, in regards to the FEM-based hyper-elastic modeling and the possible presence of unmodelled dynamics (e.g., material uncertainties or external loads on the end-effector), a passivity-based adaptive controller is proposed that enhances robustness towards material uncertainties and unmodelled dynamics in closed-loop, slowly improving their estimates online.

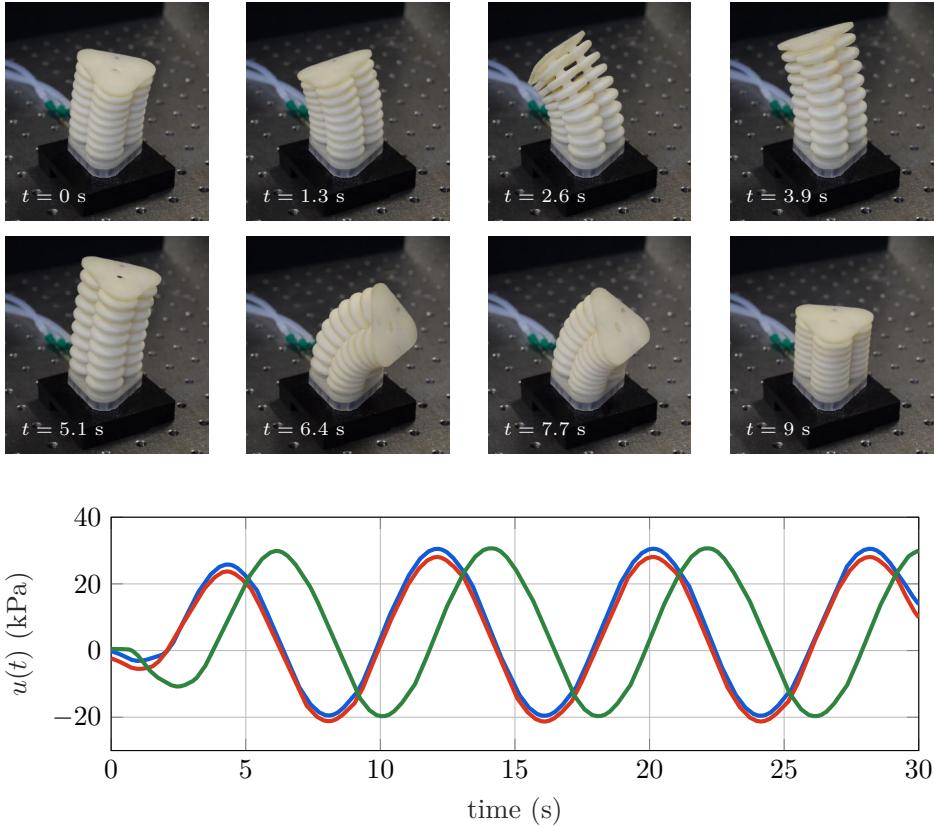


Figure 4.1. (top) Soft robot manipulator with three parallel embedded pneumatic bellows. This manipulator changes its posture by inflation and deflation of an embedded pneumatic network, $\max(|\mathbf{u}|) < 0.1 \text{ MPa}$. (bottom) Differential pressure signals applied on the internal bellows structures given by the input vector $\mathbf{u} = (u_1 \ u_2, \ u_3)^\top$, shown by the trajectories (—, —, —), respectively.

4.2 Pneumatic soft continuum manipulator

By using additive manufacturing, we developed a soft and flexible robot manipulator that is suitable for pick-and-place applications. The 3-DOF soft manipulator can be seen in Figure 4.1. The soft manipulators's design is reminiscent of the Orm robot developed by Scheinman [93], the composition of the network of soft actuators is loosely inspired by the elephant's trunk consisting mainly of parallel muscles without skeletal support. The anatomy of the elephant's trunk provides an excellent study case, as it naturally exhibit continuum-body bending and moderate elongation [78, 129, 271]. The design is also similar to other soft robotic systems [73, 78, 261] that all undergo three-dimensional movement by inflation or deflation of an embedded pneumatic bellow network. The pneumatic network has three in-

dependent inputs, which are labeled $\mathbf{u} = (u_1, u_2, u_3)^\top$. By varying these input, the soft manipulator can achieve bending in any preferred direction by differential pressurization of each channel (<0.1 MPa), *e.g.*, $u_1 > u_2 = u_3 > 0$. Whereas, simultaneous pressurization accomplishes moderate elongation, *i.e.*, $u_1 = u_2 = u_3$. As a demonstration, we provided the following pressure inputs to the system:

$$u_i(t) = \begin{cases} \operatorname{erf}(t) \cdot [P_0 - P_a \sin(\pi t + \delta)] & \text{for } i = 1, 2 \\ \operatorname{erf}(t) \cdot [P_0 - P_a \sin(\pi t)] & \text{for } i = 3 \end{cases} \quad (4.1)$$

where $P_0 = 5$ kPa, $P_a = 25$ kPa, $\delta = \frac{\pi}{2}$, and $\operatorname{erf}(t) := \frac{2}{\pi} \int_0^t \exp(-\tau^2) d\tau$ the error function to ensure a smooth transient. The demonstration is shown in Figure 4.1.

Remark 4.1 (Additive manufacturing) *The soft manipulator is exclusively composed of a printable, flexible thermoplastic elastomer (Young's modulus ≤ 80 MPa), which intrinsically promotes softness and dexterity. The elastomer material is developed explicitly for Selective Laser Sintering (SLS), a 3-Dimensional (3D) printing method that uses a laser to solidify powdered material. The main advantage of SLS printing over other techniques is that the printed parts are fully self-supported, which allows for highly complex and high-detail structures. It should be mentioned, though, that the layer-by-layer material deposition will introduce undesired anisotropic mechanical effects. To mitigate anisotropy, the bellows are printed orthogonal to the printing plane, thereby ensuring mechanical symmetry. For the majority of this work, the 3D-printed soft robot in Figure 4.1 will form the basis of the dynamical model. The 3D model is made publicly available at the Sorotoki software repository at github.com/BJCaasenbrood/SorotokiCode [37].*

4.3 Generalized models for soft manipulators

As mentioned previously, soft robots are composed of elastic bodies that can be modeled as a dynamically deformable continuum with of infinite-dimensional nature. In this section, we aim to derive a compact and computationally efficient model that envelopes the continuous dynamics of the soft manipulator in Figure 4.1 (and soft robotic systems of similar topology, *e.g.*, [78, 93, 134]) through a small set of generalized coordinates. We denote these coordinates by $\mathbf{q} \in \mathcal{Q}$. Their respective velocities are denoted by $\dot{\mathbf{q}} \in T_{\mathbf{q}}\mathcal{Q}$ which belong to the tangent space of the configuration manifold $\mathcal{Q} \subseteq \mathbb{R}^n$. Let it be clear that the choice on \mathbf{q} is free. However, finding a choice that minimizes $n = \dim(\mathcal{Q})$ and that accurately reflects the continuum nature can be challenging. A state representation that satisfies both will help to keep computational cost low which is the current bottleneck for model-based control of soft robots.

We base our modeling framework on the work of Mochiyama et al. [190], who outlined a theoretical foundation for continuum manipulators. Their work is extended upon by including extensibility, serial-chaining of multiple soft links,

pneumatic actuation, and the introduction of nonlinear and time-dependent material behavior. Earlier modeling strategies addressing similar issues can be found in from Godage et al. [97, 98], Della Santina et al [70–72], Renda et al. [222], and Boyer et al. [29]. Leveraging from the aforementioned works, a finite-dimensional approximation of the true soft robot dynamics with can be written in the familiar Lagrangian form:

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{J}^\top(\mathbf{q})\boldsymbol{\lambda} + \boldsymbol{\tau}(\mathbf{q}, \mathbf{u}), \quad (4.2)$$

$$\boldsymbol{\tau} = \mathbf{G}^\top(\mathbf{q})\mathbf{u}, \quad (4.3)$$

where $\mathbf{M}(\mathbf{q}) \in \mathbb{R}^{n \times n}$ denotes the generalized inertia matrix, $\mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) \in \mathbb{R}^n$ a vector of nonlinear state-dependent force contributions. The nonlinear state-dependent contributions possess a structures as follows: $\mathbf{h}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{f}(\mathbf{q}, \dot{\mathbf{q}})$ given by the Coriolis forces and visco-elastic terms, respectively.

Assumption 4.1 (Finiteness generalized inertia) The generalized inertia matrix is a positive definite symmetric matrix that is bounded from both sides $\lambda^- \preceq \mathbf{M}(\mathbf{q}) \preceq \lambda^+$ for all configurations \mathbf{q} , where λ^-, λ^+ are positive scalars.

Assumption 4.2 (Passivity) For any velocity $\dot{\mathbf{q}}$, it holds that $\dot{\mathbf{q}}^\top (\dot{\mathbf{M}} - 2\mathbf{C}) \dot{\mathbf{q}} = 0$ – the so-called passivity condition for Lagrangian systems. If the condition holds, it can easily be shown that map $\mathbf{u} \mapsto \dot{\mathbf{q}}$ is passive, which implies that there exist a constant $\beta \geq 0$, such that the energy produced by the system E^u is bounded from below [203]:

$$E^u := \int_0^T \dot{\mathbf{q}}^\top(\tau) \mathbf{u}(\tau) d\tau > -\beta \quad \forall T > 0. \quad (4.4)$$

Assumption 4.3 (Under-actuation) In many cases, a soft robot that falls under the category hyper-redundant is also intrinsically under-actuated. Mathematically, under-actuation is defined as follows [273]. A second-order system $\ddot{\mathbf{q}} = \mathbf{f}(\mathbf{q}, \dot{\mathbf{q}}, \mathbf{u}, t)$ is fully-actuated if, for any time t and state $(\mathbf{q}, \dot{\mathbf{q}})$, the flow map \mathbf{f} is surjective. In laymen's terms, for any acceleration $\ddot{\mathbf{q}}$ there is exists a unique input \mathbf{u} that produces such response. Otherwise, the system is under-actuated. Given the control affine structure in (4.3), the system is under-actuated if configurations $\mathbf{q} \in \mathcal{Q}$ exist such that $\text{rank}(\mathbf{G}(\mathbf{q})) < \dim(\mathbf{q})$. Let it be clear that fully-actuated systems are dramatically easier to control than under-actuated systems. However, for the sake of simplicity at this stage, we assume the actuation matrix to be full rank and time-invariant, *i.e.*, $\mathbf{G}(\mathbf{q}) \simeq \mathbf{G}$. Under-actuation will be treated further in Chapter 4 and is not considered here in Chapter 3 .

In this chapter, a similar modeling framework is adopted to [190]; however, we propose an extension to incorporate FEM-driven data to more accurately reflect the underlying continuum mechanics – in particular, hyper-elasticity and visco-elastic creep. We also propose a numerical scheme that significantly accelerates the computation of the continuous dynamics.

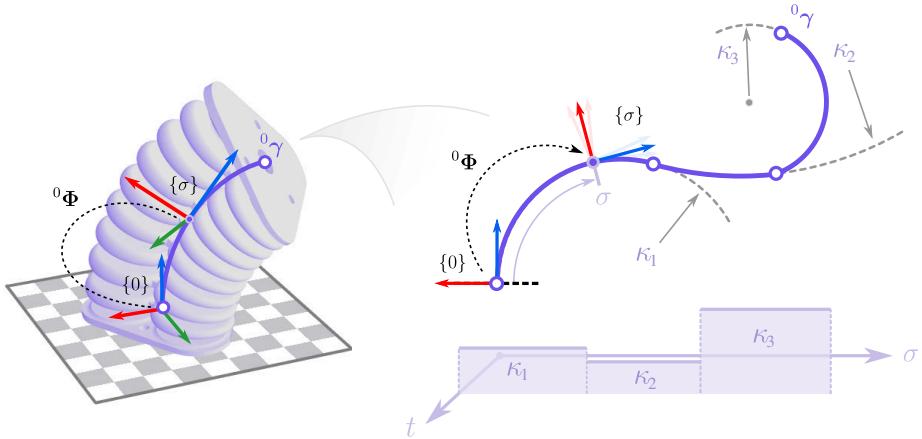


Figure 4.2. Schematic representation of the Piece-wise Constant Curvature (PCC) description for general soft manipulator systems, given by a parameterized curve ${}^0\gamma : \mathbb{X} \times \mathcal{Q} \rightarrow \mathbb{R}^3$ and orientation matrix ${}^0\Phi : \mathbb{X} \times \mathcal{Q} \rightarrow \text{SO}(3)$. The frame $\{\sigma\}$ is an inertial coordinate frame that evolves over the backbone ${}^0\gamma$ such that variations in σ give insight into its differential geometry.

4.3.1 Piecewise curve kinematics

To represent the hyper-flexible configuration of the soft robot, consider a smooth spatial curve that passes through the geometric center of the continuously deformable body, as shown in Figure 4.2. In literature, this curve is called the *backbone curve* as it simplifies the three-dimensional deformation imposed by distributed forces acting on the elastic body. The arc-length of the backbone corresponds to the extensible length of the soft robot denoted by the variable $l(t)$ which we assume bounded $l_- \leq l \leq l_+$, and let L be a constant denoting the total unstressed length of the soft robot. Next, let us introduce a spatial variable $\sigma \in \mathbb{X}$ that belongs to the one-dimensional material domain of the backbone curve, *i.e.*, $\mathbb{X} = [0, L]$. Let it be clear that the spatial variable σ represents the arc-length of a material coordinate along with the unstressed material domain of the soft robot manipulator.

Given each material coordinate, we wish to find a suitable low-dimensional coordinate representation \mathbf{q} such that the position vector ${}^0\gamma(\sigma, \mathbf{q})$ anywhere on the continuous backbone can be written as a mapping from generalized coordinates and space into Euclidean space \mathbb{R}^3 :

$${}^0\gamma : \mathbb{X} \times \mathcal{Q} \rightarrow \mathbb{R}^3; \quad (4.5)$$

and similarly the rotation matrix ${}^0\Phi(\sigma, \mathbf{q})$ by a mapping from the generalized coordinates and space into $\text{SO}(3)$:

$${}^0\Phi : \mathbb{X} \times \mathcal{Q} \rightarrow \text{SO}(3), \quad (4.6)$$

where $\text{SO}(3)$ denotes the special orthogonal group for rotations about the origin of \mathbb{R}^3 . Under this notion, the position vectors ${}^0\gamma(0, \mathbf{q})$ and ${}^0\gamma(L, \mathbf{q})$ relate to the base and the end-effector of the soft manipulator, respectively. Note that left-sided superscripts are used to indicate the frame of reference. The set of all points on the backbone $\mathcal{C} = \{ {}^0\gamma(\sigma, \mathbf{q}) \in \mathbb{R}^3 \mid \sigma \in \mathbb{X}\}$ draws a possible spatial configuration of the soft robot given a time instance $t \in \mathbb{T}$ on a finite horizon $T = [0, T]$. For sake of brevity, the remainder of the chapter will drop the superscripts that indicate the frame of reference, *i.e.*, ${}^0\Phi = \Phi$ and ${}^0\gamma = \gamma$.

Assumption 4.4 (Piece-wise Constant Curvature) Despite the inherent flexibility in soft robotics, it is sometimes sufficient to express the kinematics according to the *Piecewise Constant Curvature* (PCC) condition. This properties often originates from the "*proper*" structural design of the soft robot, where parasitic motion is reduced by structural compliance. Mathematically, it implies that the curvature of the continuous body satisfies $\kappa(\sigma_1, \mathbf{q}) = \kappa(\sigma_2, \mathbf{q})$ for spatial coordinates on a local region on the soft manipulator $\sigma_1, \sigma_2 \subseteq \mathbb{X}$. As a result, this condition allows us to describe the full forward kinematics with a significantly reduced set of generalized coordinates, mitigating kinematic complexity in the model. Numerous works employ PCC models [71, 78, 97, 135, 176, 271], and depending on the elasticity and structural geometry of the soft robot, the PCC condition has been proven to be consistent for various soft robotic systems.

Following this Constant Curvature (CC) approach, we assign a coordinate frame that twists minimally along the backbone – formally called the "*Bishop frame*" (see [27]) – parametrized by the following generalized coordinate vector:

$$\mathbf{q} := (\varepsilon \quad \kappa_x \quad \kappa_y)^\top \in \mathcal{Q}, \quad (4.7)$$

where $\varepsilon_- \leq \varepsilon \leq \varepsilon_+$ is the elongation strain, and $\kappa_x, \kappa_y \in \mathbb{R}$ are the curvatures or angular strains in x - z and y - z plane, respectively; and $\mathcal{Q} \subset \mathbb{R}^3$ is an admissible space on which \mathbf{q} evolves. We will also introduce the following geometric variables $\kappa = \langle \kappa_x, \kappa_y \rangle$ and the curvature angle $\phi = \text{atan}2(\kappa_y, \kappa_x)$. It is worth mentioning that the joint description above is somewhat related to Renda. et al. [222] who proposed a *Piece-wise Constant Strain* (PCS) parametrization with the exception of including the twist along the tangent.

By exploring the differential geometry of the smooth backbone curve similar to Mochiyama et al. [190], we can write the position vector $\gamma(\sigma, \mathbf{q})$ and the orientation matrix $\Phi(\sigma, \mathbf{q})$ for each material point σ along the smooth backbone as a differential equation:

$$\frac{\partial \Phi}{\partial \sigma}(\sigma, \mathbf{q}) = \Phi(\sigma, \mathbf{q}) \Gamma^\times(\sigma, \mathbf{q}), \quad (4.8)$$

$$\frac{\partial \gamma}{\partial \sigma}(\sigma, \mathbf{q}) = \Phi(\sigma, \mathbf{q}) \mathbf{U}(\sigma, \mathbf{q}), \quad (4.9)$$

where $\Gamma^\times \in \text{so}(3)$ is a skew-symmetric matrix composed of the entries of the vector $\Gamma \in \mathbb{R}^3$, and $\mathbf{U} \in \mathbb{R}^3$ a vector representing the tangent along the extensible

backbone. The skew-symmetric operator $(\cdot)^\times$ denotes the isomorphism between the Lie algebra $\text{so}(3)$ and \mathbb{R}^3 . The vectors $\boldsymbol{\Gamma}$ and \boldsymbol{U} are vectors that define the differential geometry of the backbone [190] which are unique entries that live in the tangent space of the rigid-body transformation group (*i.e.*, $T_{\text{SE}(3)}$). Given the Bishop parametrization shown in (4.7) and assuming the Piecewise Constant-Strain (PCC) condition, these geometric entities yield

$$\boldsymbol{\Gamma}^\times(\sigma, t) \simeq \boldsymbol{\Gamma}^\times(\sigma, \boldsymbol{q}(t)) \xrightarrow{\text{PCC}} \boldsymbol{\Gamma}^\times = \begin{pmatrix} 0 & 0 & \kappa_y \\ 0 & 0 & \kappa_x \\ -\kappa_y & -\kappa_x & 0 \end{pmatrix}, \quad (4.10)$$

$$\boldsymbol{U}(\sigma, t) \simeq \boldsymbol{U}(\sigma, \boldsymbol{q}(t)) \xrightarrow{\text{PCC}} \boldsymbol{U} = \begin{pmatrix} 0 \\ 0 \\ \varepsilon + 1 \end{pmatrix}. \quad (4.11)$$

4

Now, given an initial configuration of backbone's base, *i.e.*, $\boldsymbol{\Phi}(0, \boldsymbol{q}) = \boldsymbol{\Phi}_0$ and $\boldsymbol{\gamma}(0, \boldsymbol{q}) = \mathbf{0}_3$, we can now solve for the position and orientation for each material coordinate σ along the backbone:

$$\boldsymbol{\Phi}(\sigma, \boldsymbol{q}) = \boldsymbol{\Phi}_0 \exp_{\text{SO}(3)}(\sigma \boldsymbol{\Gamma}^\times(\boldsymbol{q})), \quad (4.12)$$

$$\boldsymbol{\gamma}(\sigma, \boldsymbol{q}) = \int_0^\sigma {}^0\boldsymbol{\Phi}(s, \boldsymbol{q}) \boldsymbol{U}(\boldsymbol{q}) ds, \quad (4.13)$$

where $\exp_{\text{SO}(3)} : \text{so}(3) \rightarrow \text{SO}(3)$ is the exponential map. Luckily, there exists a compact expression for the exponential mapping related to the orthogonal group of rotation matrices $\text{SO}(3)$ called the "*Rodriguez formulas*". The rotation angle along a constant-strain soft body can be computed by $\theta(\sigma, \boldsymbol{q}) := \int_0^\sigma \kappa(s, \boldsymbol{q}) ds = \kappa(\boldsymbol{q})$. Notice that the rotation angle θ linearly depends on σ , which is a property that follows from Assumption 4.4. Then, given the expression for the angle of rotation, we can compactly rewrite the rotation matrix (4.12) in terms of $\cos(\theta)$ and $\sin(\theta)$ using these formulas as follows [170]:

$$\boldsymbol{\Phi}(\theta) = \boldsymbol{\Phi}_0 \left(\mathbf{I}_3 + \left[\frac{\sin(\theta)}{\theta} \right] \boldsymbol{\Gamma}^\times + \left[\frac{1 - \cos(\theta)}{\theta^2} \right] \boldsymbol{\Gamma}^\times \boldsymbol{\Gamma}^\times \right). \quad (4.14)$$

Note that the closed-form solutions (4.12) and (4.13) represent the forward configuration kinematics of the backbone curve. To express the forward velocity kinematic, let $\boldsymbol{\eta}(\sigma, \boldsymbol{q}, \dot{\boldsymbol{q}}) = (\boldsymbol{\omega}^\top, \boldsymbol{v}^\top)^\top \in \mathbb{R}^6 \cong \text{se}(3)$ be the aggregate of the angular velocity and linear velocity components relative to an inertial frame at σ , where the space $\text{se}(3)$ denotes the Lie algebra of $\text{SE}(3)$. The velocity twist is computed by the following integration procedure:

$$\begin{aligned} \boldsymbol{\eta}(\sigma, \boldsymbol{q}, \dot{\boldsymbol{q}}) &= \mathbf{Ad}_{\boldsymbol{g}(\sigma, \cdot)}^{-1} \int_0^\sigma \mathbf{Ad}_{\boldsymbol{g}(s, \cdot)} \boldsymbol{J}^* \dot{\boldsymbol{q}} ds, \\ &=: \boldsymbol{J}(\boldsymbol{q}, \sigma) \dot{\boldsymbol{q}}, \end{aligned} \quad (4.15)$$

where $\mathbf{Ad}_g : \text{SE}(3) \rightarrow \mathbb{R}^{6 \times 6}$ denotes the adjoint transformation matrix regarding the rigid body transformation $g \in \text{SE}(3)$ that maps local velocities (i.e., twist) to a frame located at σ , and $\mathbf{J}^* : \mathcal{Q} \rightarrow T_q \mathcal{Q}$ the joint-axis matrix that relates the DOFs to the generalized coordinate description. Let it be clear that the joint-axis matrix is naturally constant for a soft segment modeled with the Constant-Strain (CS) assumption. We will later relax this assumption in Chapter 4. Nevertheless here, the joint-axis matrix for an extensible and bendable CS segment parametrized by the Bishop parameters is given by

$$\mathbf{J}^* := \begin{pmatrix} \partial \Gamma^\top & \partial \mathbf{U}^\top \\ \partial \mathbf{q} & \partial \mathbf{q} \end{pmatrix}^\top = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ -1 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}^\top. \quad (4.16)$$

Although we based the forward kinematics on Mochiyama et al. [190], the derived expression for the velocity twist in (4.15) is analogous to the work of Renda et al. [221, 222], and Boyer et al. [29, 30]. Please also note that (4.15) gives rise to the geometric Jacobian $\mathbf{J}(\sigma, \mathbf{q})$ that defines the mapping from joint velocities to the velocity twist anywhere on the body.

Given the explicit expression for the velocity twist in (4.15), we can derive the acceleration twist [29, 190, 222] which is obtained through differentiation of (4.15):

$$\begin{aligned} \dot{\eta}(\sigma, \mathbf{q}, \dot{\mathbf{q}}, \ddot{\mathbf{q}}) &= \mathbf{J}\ddot{\mathbf{q}} + \mathbf{Ad}_{g(\cdot, \sigma)}^{-1} \int_0^\sigma \mathbf{Ad}_{g(s, \cdot)} \mathbf{ad}_{\eta(s, \cdot)} \mathbf{J}^* \dot{\mathbf{q}} \, ds \\ &:= \mathbf{J}(\sigma, \mathbf{q}) \ddot{\mathbf{q}} + \dot{\mathbf{J}}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) \dot{\mathbf{q}}, \end{aligned} \quad (4.17)$$

where $\mathbf{ad}_\eta : \mathbb{R}^6 \rightarrow \mathbb{R}^{6 \times 6}$ denotes the adjoint transformation regarding the velocity twist $\eta^\wedge \in \text{se}(3)$. The reader is referred to Appendix C.1 for more detailed expressions on the adjoint transformations.

Remark 4.2 (Numerical instability near zero-curvature) *For many of the PCC modeling frameworks [78], there are mentions of a singularity point or discontinuity of the kinematic formulations at zero-curvature $\kappa = 0$. It is often reported that trajectories that pass through the origin lead to unbounded linear velocities $\mathbf{v} := [\boldsymbol{\eta}]_3$, which may result in critical problems in practice. Although it is believed the problem is simply a by-product of the PCC hypothesis, this is however a common misconception, and it stems from a numerical origin. To illustrate this, consider the inextensible planar case: $\varepsilon = \kappa_y = 0$ and $\kappa = \kappa_x$. For simplicity, we assume $L = 1$. Hence, by solving the forward kinematics for the position vector $\boldsymbol{\gamma}(\sigma, \kappa)$, and approaching zero-curvature from the positive domain $\kappa^+ \rightarrow 0$, we see that*

$$\lim_{\kappa \rightarrow 0^+} \boldsymbol{\gamma}(\sigma, \kappa) = \left(\frac{1 - \cos(\sigma\kappa)}{\kappa}, \quad 0, \quad \frac{\sin(\sigma\kappa)}{\kappa} \right)^\top = (0 \quad 0 \quad \sigma)^\top, \quad (4.18)$$

so its limit clearly exists. Since the position vector $\boldsymbol{\gamma}$ is continuously differentiable when approaching the origin from both sides $\kappa \rightarrow 0^+$ and $\kappa \rightarrow 0^-$, it follows that

$\dot{\gamma}$ must be bounded for all $\kappa \in \mathcal{Q}$. We can simply check this by investigating the behavior of the linear-velocity components of the geometric Jacobian near zero-curvature, which yield

$$\begin{aligned} \lim_{\kappa \rightarrow 0^+} [\mathbf{J}]_3(\sigma, \kappa) &= \left(\frac{\sigma \kappa \sin(\sigma \kappa) + 1 - \cos(\sigma \kappa)}{\kappa^2}, \quad 0, \quad \frac{\sigma \kappa \cos(\sigma \kappa) - \sin(\sigma \kappa)}{\kappa^2} \right)^\top \\ &= (\sigma^2 \quad 0 \quad 0)^\top. \end{aligned} \quad (4.19)$$

Again, its limit exists. Since both limits exist, we define $\gamma(\sigma, 0) := \lim_{\kappa \rightarrow 0} \gamma(\sigma, \kappa)$ and $\mathbf{J}(\sigma, 0) := \lim_{\kappa \rightarrow 0} \mathbf{J}(\sigma, \kappa)$. Consequently, the magnitude of the linear velocity of the end-effector reads simply $\|\dot{\gamma}(L, \dot{\kappa})\| = L^2 \dot{\kappa} = L \omega_1$ with ω_1 the angular velocity at the tip. Moreover, it is bounded for all $\kappa \in \mathcal{Q}$. This naturally poses an ambiguity on the origin of the kinematic singularity so often reported literature. The problem is believed to be of numerical origin when considering the zero-division. To make matters worse, deriving analytical expressions for accelerations will contain similar expressions that are hard to stabilize numerically. To resolve this issue, we opt for a numerical approximation of the forward kinematics – namely, we employ an explicit forward integration scheme (i.e., trapezoidal integration) to solve (4.8) and (4.9).

Example 4.1 (Kinematic behavior of PCC segment). As an illustrative example, we perform a numerical simulation of the forward kinematics for a single PCC segment. We select a differentiable reference trajectory $\mathbf{q}(t) \equiv \mathbf{q}_d(t)$, $\dot{\mathbf{q}}(t) \equiv \dot{\mathbf{q}}_d(t)$ and $\ddot{\mathbf{q}}(t) \equiv \ddot{\mathbf{q}}_d(t)$ that passes the zero-curvature point given by:

$$\mathbf{q}_d(t) = \text{erf}(t) \cdot (\varepsilon_0 \sin(\omega t) \quad \kappa_0 \cos(\omega t) \quad \kappa_0 \sin(\frac{3}{2}\omega t - \frac{\pi}{4}))^\top,$$

where $\text{erf}(t) := \frac{2}{\pi} \int_0^t \exp(-\tau^2) d\tau$ is referred to as the error function. Note that these are smooth functions such that reference velocity $\dot{\mathbf{q}}_d$ and reference acceleration $\ddot{\mathbf{q}}_d$ exist and are bounded. The reference signals for the geometric strain of

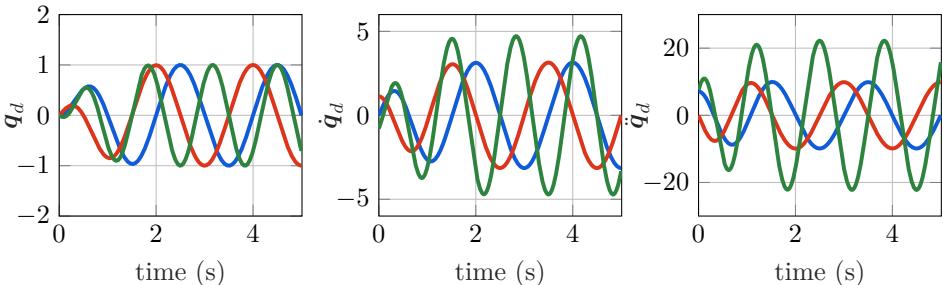


Figure 4.3. The time evolution of the predefined geometric strain parameters of the Piece-wise Constant curvature model $\mathbf{q}_d \rightarrow (\varepsilon, \kappa_x, \kappa_y)^\top$ and their corresponding time-derivatives $\dot{\mathbf{q}}_d$ and $\ddot{\mathbf{q}}_d$, given by the (spatially constant) elongation ε (—), and the (spatially constant) curvatures κ_x (—) and κ_y (—).

the soft robot are shown in Figure 4.3. Please note that the reference \mathbf{q}_d has been carefully selected to ensure it passes the line $\kappa_x = \kappa_y = 0$ on the configuration manifold \mathcal{Q} , *i.e.*, the numerical instability point for (near) zero-curvature.

Then, by injecting the reference into the kinematic relations given by (4.8), (4.9), (4.15), and (4.17), we obtain a (close) approximation of forward kinematics as shown in Figure 4.4. Furthermore, we provided a 3D-rendering of the soft robot subjected to the reference \mathbf{q}_d in Figure 4.5. Now, two key observations can be made. First, although a simple harmonic trajectory is used, the resulting trajectory of the end-effector as shown in Figure 4.4 is rather complex. This perhaps stresses the importance of inverse kinematic solver that can be used for task-space control. Second, although we pass the point of numerical instability for $\kappa \rightarrow 0$, we see that the velocity solutions are smooth and bounded at these instances. This result shows our approach does not suffer from the near-zero curvature instabilities that are notoriously mentioned in [72, 78].

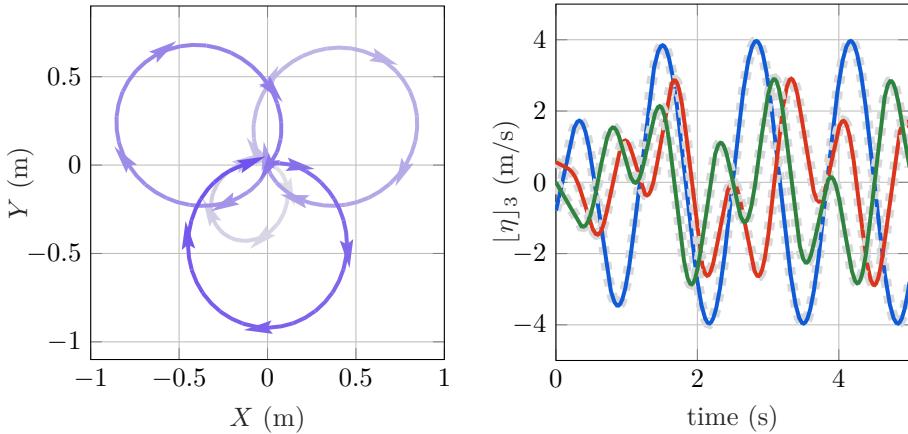


Figure 4.4. (left) The forward kinematics of the end-effector γ related to the prescribed reference $\mathbf{q}_d(t)$. The time evolution is shown by the colormap $\in [0, 5]$ (s). (right) The linear velocities $[\eta]_3 = (v_1, v_2, v_3)^\top$, shown as (—, —, —), respectively. The dashed lines (—) are obtained using numerical time differentiation of γ – and the overlap exactly with the forward kinematic model. A key observation here, is that our numerical approach prevents the common numerical instability for near-zero curvatures, *i.e.*, $\kappa \rightarrow 0$, since the linear velocities are bounded and continuous even for $\kappa(\mathbf{q}) = 0$.

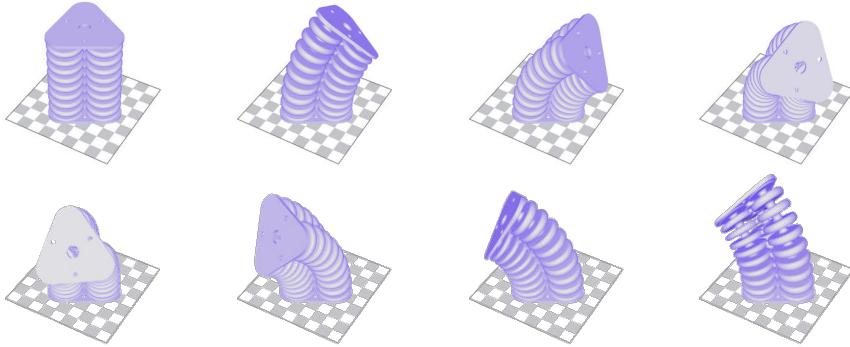


Figure 4.5. Three-dimensional deformation of the three-bellow soft robot manipulator using the PCC model. Based on the prescribed reference \mathbf{q}_d (and its time-derivative $\dot{\mathbf{q}}_d$), the forward kinematic relations for each point σ along the backbone is computed and the volumetric mesh is deformed accordingly to its closest material-point on the backbone curve $\gamma(\sigma)$.

4.3.2 Piecewise curve dynamics using Euler-Lagrange

Given the forward kinematics in (4.12), (4.13), (4.15) and (4.17), we can shift our attention to formulating the finite-dimensional dynamics of the soft robot. Our goal here is to write the spatio-temporal dynamics of the hyper-elastic soft robot as a second-order ODE into the Lagrangian form:

$$\frac{d}{dt} (\nabla_{\dot{\mathbf{q}}} \mathcal{L}) - \nabla_{\mathbf{q}} \mathcal{L} = \mathbf{Q}^{\text{nc}}, \quad (4.20)$$

where $\nabla_{\mathbf{q}} (\cdot) := \left[\frac{\partial(\cdot)}{\partial q_1} \dots \frac{\partial(\cdot)}{\partial q_n} \right]^T$ is defined as the gradient operator, $\mathcal{L}(\mathbf{q}, \dot{\mathbf{q}}) := \mathcal{K}(\mathbf{q}, \dot{\mathbf{q}}) - \mathcal{U}(\mathbf{q})$ the Lagrangian function, $\mathcal{K} \in \mathbb{R}_{\geq 0}$ and $\mathcal{U} \in \mathbb{R}$ the kinetic and potential energy, respectively; and $\mathbf{Q}^{\text{nc}} \in \mathbb{R}^n$ a vector of generalized non-conservative forces. To apply the Lagrangian formalism to a continuum dynamical system, consider an infinitesimal slice of the continuum body for each material coordinate σ along the backbone curve. Given this notion, we assign the infinitesimal slice with an inertia tensor $\mathbf{M} = \text{blkdiag}(\rho_0 \mathbf{I}, \mathcal{J}_0)$ with $\rho_0 = m_0/L$ the line-density and $\mathcal{J}_0 \in \text{so}^*(3) \times \text{so}(3)$ a symmetric tensor related to the second moment of inertia of infinitesimal slice at σ . Note that operator $\text{blkdiag}(\cdot)$ creates a block diagonal matrix by aligning the input matrices.

The kinetic energy can be obtained through spatial integration of its respective kinetic energy densities [30, 190, 271], i.e., $\mathfrak{T} = \frac{1}{2} \boldsymbol{\eta}^\top \mathbf{M} \boldsymbol{\eta}$:

$$\begin{aligned} \mathfrak{T}(\mathbf{q}, \dot{\mathbf{q}}) &= \frac{1}{2} \int_{\mathbb{X}} \boldsymbol{\eta}(\sigma, \mathbf{q}, \dot{\mathbf{q}})^\top \mathbf{M} \boldsymbol{\eta}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) d\sigma, \\ &= \frac{1}{2} \dot{\mathbf{q}}^\top \left[\int_{\mathbb{X}} \mathbf{J}(\sigma, \mathbf{q})^\top \mathbf{M} \mathbf{J}(\sigma, \mathbf{q}) d\sigma \right] \dot{\mathbf{q}} := \frac{1}{2} \dot{\mathbf{q}}^\top \mathbf{M}(\mathbf{q}) \dot{\mathbf{q}}, \end{aligned} \quad (4.21)$$

where we used $\boldsymbol{\eta} = \mathbf{J}\dot{\mathbf{q}}$ as described in (4.15). Also note that expression for the kinetic energy naturally gives rise to the generalized inertia matrix $\mathbf{M}(\mathbf{q})$ of the Lagrangian model. By substitution of the kinetic energy into the Euler-Lagrange equation (4.20), we find $\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}}$ where $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$ denotes the Coriolis matrix. Instead of computing the Coriolis matrix through the conventional Christoffel symbols [197], we a modified computational scheme introduced by Garofalo et al. [94] that is tailored towards long serial-chain manipulators. In their scheme, we replaced the finite summation of N rigid bodies by a spatial integration over the continuum domain \mathbb{X} . This leads to the following computation of the Coriolis matrix:

$$\begin{aligned} \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) &= \int_{\mathbb{X}} \mathbf{J}(\sigma, \mathbf{q})^\top \underbrace{\left[\mathbf{M} \text{ad}_{\boldsymbol{\eta}} - \text{ad}_{\boldsymbol{\eta}}^\top \mathbf{M} \right]}_{\mathcal{C}_{\boldsymbol{\eta}}} \mathbf{J}(\sigma, \mathbf{q}) + \dots \\ &\quad \dots + \mathbf{J}(\sigma, \mathbf{q})^\top \mathbf{M} \dot{\mathbf{J}}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) d\sigma, \end{aligned} \quad (4.22)$$

where $\mathcal{C}_{\boldsymbol{\eta}} = -\mathcal{C}_{\boldsymbol{\eta}}^\top$ a skew-symmetric matrix. The computation above is slight different from existing literature [29, 221] to ensure that the matrix $\tilde{\mathbf{M}} - 2\mathbf{C}$ is skew-symmetric – the so-called "*passivity condition*"(see Assumption 4.4). The importance of this property will become apparent later in the energy-based controller design. Lastly, the potential energy is given by sum of gravitational potential energy and internal elastic potential, *i.e.*, $\mathcal{U}(\mathbf{q}) = \mathcal{U}_g(\mathbf{q}) + \mathcal{U}_e(\mathbf{q})$. Since gravitational potential energy density is given by $\mathfrak{U}_g = -\rho_0 \boldsymbol{\gamma}(\sigma, \mathbf{q}) \mathbf{a}_g$ with $\mathbf{a}_g \in \mathbb{R}^3$ is a vector of body accelerations, the potential energy related to gravity is obtained by spatial integration of their respective energy densities:

$$\mathcal{U}_g(\mathbf{q}) = \int_{\mathbb{X}} \mathfrak{U}_g(\sigma, \mathbf{q}) d\sigma = -\rho_0 \int_{\mathbb{X}} \boldsymbol{\gamma}(\sigma, \mathbf{q})^\top \mathbf{a}_g d\sigma. \quad (4.23)$$

To model the hyper-elastic nature, lets introduce two nonlinear stiffness functions for both stretching and bending, denoted by $k_e : \mathbb{R} \mapsto \mathbb{R}_{>0}$ and $k_b : \mathbb{R} \mapsto \mathbb{R}_{>0}$, respectively. These functions allow us to describe a collective elastic behavior imposed by the hyper-elastic materials and the continuum-bodied deformation. It shall be clear that these entities are unique to the soft robot's geometry and soft material choice, and thus finding a suitable candidate model requires further analysis. Later, we will sculpt these nonlinear stiffness functions through Finite Element Methods (FEM). For now, we assume that these analytical nonlinear stiffness functions are known, and thus the (hyper)-elastic potential energy takes the form

$$\mathcal{U}_e(\mathbf{q}) = \int_0^{\varepsilon} k_e(s) s ds + \int_0^{\beta(\mathbf{q})} k_b(s) s ds, \quad (4.24)$$

where ε is the elongation strain, and $\beta(\mathbf{q}) := \kappa L(\varepsilon + 1)$ is the bending angle with the total curvature of the segment $\kappa(\mathbf{q}) = ||\kappa_x, \kappa_y||_2$ (see Figure 4.2).

4.3.3 Overall dynamic model

Finally, by combining (4.20), (4.21), (4.22), (4.23), and (4.24), the continuum dynamics of the soft robot can be casted into the familiar closed form [29, 72, 222] similar to aforementioned model (1):

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{f}_e(\mathbf{q}, \dot{\mathbf{q}}) + \mathbf{f}_g(\mathbf{q}) = \boldsymbol{\tau}(\mathbf{u}, \boldsymbol{\delta}), \quad (4.25)$$

where $\mathbf{f}_e = \nabla_{\mathbf{q}} \mathcal{U}_e + \mathbf{R}\dot{\mathbf{q}}$ is a vector of generalized forces imposed by the deformation of the soft materials with $\mathbf{R} \succ 0$ the Rayleigh damping matrix, $\mathbf{f}_g = \nabla_{\mathbf{q}} \mathcal{U}_g$ a vector of generalized gravitational forces, and $\mathbf{u}(t)$ the control input with the index m the number of pressure inputs. The generalized input vector is chosen of the form: $\boldsymbol{\tau}(\mathbf{u}, \boldsymbol{\delta}) = \mathbf{G}\mathbf{u} + \boldsymbol{\delta}$ with $\mathbf{G}\mathbf{u} : \mathbb{R}^m \rightarrow \mathbb{R}^n$ a mapping from the input space to the joint actuation space, and $\boldsymbol{\delta}(t)$ an external disturbance (*e.g.*, unmodelled material uncertainties).

Remark 4.3 Given the context of pick-and-place applications in robot manipulators, a possible disturbance $\boldsymbol{\delta}(t)$ could be an external mass applied to the tip of the soft robot. Given the kinematic relations in (4.15) and (4.17), one can describe the disturbance (modeled here as a point-mass located at L) as an external wrench acting on the point $\sigma = L$. The disturbance has two part related to acceleration: (i) the gravitational acceleration expressed in the body-frame $\mathbf{Ad}_{\mathbf{g}(\cdot, L)}^{-1}\mathbf{a}_g$ and (ii) the acceleration due to the tip motion $\dot{\mathbf{q}}(\cdot, L)$. Together they form a state-dependent vector as follows:

$$\boldsymbol{\delta}_m = m_\delta [\mathbf{J}(\cdot, L)]_3^\top \left(\mathbf{Ad}_{\mathbf{g}(\cdot, L)}^{-1}\mathbf{a}_g + [\dot{\mathbf{q}}(\cdot, L)]_3 \right), \quad (4.26)$$

where $m_\delta > 0$ the applied mass to the end-effector, $[\cdot]_3$ extracts the last three rows of a matrix or vector. Recall that the acceleration twist can be computed through the geometric Jacobian and its time derivative, i.e., $\dot{\mathbf{q}} = \mathbf{J}\ddot{\mathbf{q}} + \mathbf{J}\dot{\mathbf{q}}$. Indeed, the PCC condition for a soft body can only accurately describe the true dynamics if external forces produced by mass m_δ do not excessively exceed the intrinsic elastic balancing forces $\mathbf{f}_e(\mathbf{q})$. Alternatively, a soft body can be modeled using multiple PCC curves of smaller size, similar to standard Finite Element discretization.

Assumption 4.5 (Input mapping of bellows) Uptil now, we have not specific the input map \mathbf{G} . In general, the input map is difficult to properly estimate as the system's inputs are distributed over the soft continuum body. Therefore, it involves integrating the actuation wrench along the backbone curve, while accounting for the spatial dependency of the geometric manipulator Jacobian $\mathbf{J}(\mathbf{q}, \sigma)$. However, we considering the soft robotic system in Figure 4.1, we can introduce some approximations for the actuation mapping \mathbf{G} based on the geometry, placement, and orientation of the (pneumatic) soft actuators. Since the pneumatic chambers are aligned parallel to the backbone curve and are equally spaced along the circumference, we propose the following ansatz:

$$\mathbf{G} \simeq \begin{pmatrix} \alpha_\varepsilon & \dots & \alpha_\varepsilon \\ -\alpha_\kappa \cos(\phi_1) & \dots & -\alpha_\kappa \cos(\phi_m) \\ \alpha_\kappa \sin(\phi_1) & \dots & \alpha_\kappa \sin(\phi_m) \end{pmatrix}, \quad (4.27)$$

where $\alpha_\varepsilon, \alpha_\kappa > 0$ are system parameters representing the effective transferal of differential pressure to joint forces, and $\phi_i = (i - 1) \cdot \frac{2\pi}{m}$ the angular inter-distance between the m -number of pneumatic bellows. Please note that the parameters α_ε and α_κ are dependent on the bellow area and radius from the bellow to the backbone curve.

4.4 Extension to multi-link systems

We previously expressed the position and velocity kinematics as explicit functions of the generalized coordinates (i.e., Bishop parameters) and their time-derivatives. This explicit dependency stems from the PCC conditions inferring the curvature is non-varying along the spatial domain $[0, L]$, i.e., $\kappa(\sigma, \mathbf{q}) = \kappa(\mathbf{q})$. Although sufficient for some cases, the condition is generally restrictive, and to some extent inconvenient, since the inclusion of multiple links demands piece-wise integration of the kinematics (4.13), (4.14), (4.15), and (4.17). Rather than separation of integration, we can extend this PCC description by using piece-wise continuous spatial function to distinguishes multiple soft-bodied links along the continuous body of the soft robot. The idea of parametrization through shapes functions has been explored earlier by Chirikjian et al. [48, 52], and later by Boyer et al. [29], Della Santina et al. [72]. A similar discontinuous shape function series was used by Berthet-Rayne et al. [24] to pursue multi-body dynamics for growing continuum robots; and proposed by Chirikjian [48] for hyper-redundant robots earlier.

Following the aforementioned works, let us parameterize the geometric strains $\boldsymbol{\Gamma}$ and \mathbf{U} for a multi-link soft robot with N number of links through the product of a basis of orthonormal functions $\{\theta_i\}_{i=1}^N$ and the Bishop parametrization. Contrary to (4.10) and (4.11)

$$\boldsymbol{\Gamma}(\sigma, \mathbf{q}) \simeq \sum_{i=1}^N \theta_i(\sigma) [\mathbf{J}^*]_3 \mathbf{z}_i, \quad (4.28)$$

$$\mathbf{U}(\sigma, \mathbf{q}) \simeq \sum_{i=1}^N \theta_i(\sigma) [\mathbf{J}^*]_3 \mathbf{z}_i + \mathbf{U}^\circ, \quad (4.29)$$

where \mathbf{J}^* is the joint-axis matrix as in (4.16), the mathematical operators $[\cdot]_3$ and $[\cdot]_3$ extract the first or last three rows of a matrix, respectively; \tilde{q}_i the joint variables of the i -th link, and $\theta_i : [0, L] \mapsto \{0, 1\}$ is a piece-wise constant shape function, whose purpose is to be non-zero for a given interval on \mathbb{X} . The new generalized coordinate vector becomes the aggregate of all joint variables of the multi-body soft robotic system $\mathbf{q} = (\mathbf{z}_1^\top, \mathbf{z}_2^\top, \dots, \mathbf{z}_N^\top)^\top$ with the vector $\mathbf{z}_i = (\varepsilon_i, \kappa_{x,i}, \kappa_{y,i})^\top$ relating to the Bishop parametrization of the i -th link.

Given (4.28) and (4.29), we may now rewrite the velocity-twist as

$$\boldsymbol{\eta}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) = \left[\mathbf{Ad}_g^{-1} \int_0^\sigma \mathbf{Ad}_g \mathbf{J}^* \boldsymbol{\Theta}(s) ds \right] \dot{\mathbf{q}} := \mathbf{J}(\sigma, \mathbf{q}) \dot{\mathbf{q}} \quad (4.30)$$

where $\Theta(\sigma) = (\theta_1, \theta_2, \dots, \theta_n) \otimes \mathbf{I}_n$ is an unitary selection matrix derived from the basis of piece-wise continuous shape functions $\{\theta_i\}_{i=1}^n$. Substitution of the discontinuous variation of the geometric Jacobian in (4.30) into (4.21) leads to the dynamic model of a N -link soft robot manipulator in the Lagrangian form similar to (4.25).

Example 4.2 (Piece-wise selection for two-link system). To reduce ambiguity on the selection matrix $\Theta(\sigma)$, lets consider a spatial coordinate $\sigma_2 \in [L_1, L_1 + L_2]$ that lies on the spatial interval of the second link. Consequently, the operation $\Theta(\sigma_2)\mathbf{q} = \mathbf{z}_2$ returns the corresponding joint variable of the second link. This selection of generalized coordinates follows analogously for other links along the serial-chain of the soft manipulator.

4.5 Accelerated computation of PDE-like systems using Matrix Differential Equations (MDEs)

Due to the partial differential nature of soft robots, obtaining a closed-form expression for the projected Lagrangian model in (4.25) can become notoriously long and complex (especially for multi-link systems). The origin of this problem stems from the integrands of inertia matrix $\mathbf{M}(\mathbf{q})$ in (4.21) and Coriolis forces $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$ in (4.22); which become highly nonlinear and therefore difficult to calculate a-priori. As a result, solving the forward dynamics using traditional solvers often deteriorates the real-time performance, and in turn its usability for closed-loop control. Inspired by Boyer et al. [29] and Godage et al. [97], instead of finding an exact solution to the dynamic entries $\mathbf{M}(\mathbf{q})$, $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$ and $\mathbf{f}_g(\mathbf{q})$, let us introduce a similar reduced-order integration scheme that produces an approximate of the dynamic model (4.25). Yet, instead of using an inverse Newton-Euler algorithm (*i.e.*, Featherstone algorithm [256]) in which the Lagrangian entries are built column-wise, we propose an explicit integration scheme that efficiently computes all Lagrangian entities in parallel through a so-called Matrix-Differential Equation (MDE).

The idea here is to replace all necessary spatial integrations required for the Lagrangian entities with an equivalent Matrix-Differential Equation of the form:

$$\frac{\partial \mathbf{Z}}{\partial \sigma} = \mathbf{F}(\mathbf{Z}, \sigma), \quad (4.31)$$

where $\mathbf{Z}(\cdot, \sigma)$ is a matrix-valued function composed of the necessary elements for the forward kinematics and forward dynamics, and $\mathbf{F}(\mathbf{Z}, \sigma)$ a matrix-valued flow function that describes the spatial evolution of \mathbf{Z} . Then, by choosing the appropriate initial condition for $\mathbf{Z}(\cdot, \sigma = 0) =: \mathbf{Z}_0$ and numerically solving (4.31) over a finite horizon \mathbb{X} , we can retrieve an approximate of the Lagrangian model in (4.25) by extracting the necessary elements from the solution $\mathbf{Z}(\cdot, L)$.

Before describing the MDE, let us first introduce two intermediate matrices related to the computation of the manipulator Jacobian and its time-derivative,

namely:

$$\frac{\partial \mathbf{B}_1}{\partial \sigma} = \mathbf{Ad}_{g(\cdot, \sigma)} \mathbf{J}^* \Theta(\sigma) \quad (4.32)$$

$$\frac{\partial \mathbf{B}_2}{\partial \sigma} = \mathbf{Ad}_{g(\cdot, \sigma)} \mathbf{ad}_{\eta(\cdot, \sigma)} \mathbf{J}^* \Theta(\sigma) \quad (4.33)$$

such that they satisfy $\mathbf{J}\dot{\mathbf{q}} = \mathbf{Ad}_g^{-1} \mathbf{B}_1 \dot{\mathbf{q}}$ and $\dot{\mathbf{J}}\dot{\mathbf{q}} = \mathbf{Ad}_g^{-1} \mathbf{B}_2 \dot{\mathbf{q}}$. Given the expressions above, we can now include a partial computation Jacobians into the MDE. By collecting all the differential relation for the forward kinematics (4.8), (4.9), (4.15) and forward dynamics (4.21), (4.22) and (4.23), we can assign a flow function $\mathbf{F} := \text{blkdiag}(\mathbf{F}_{\text{kin}}, \mathbf{F}_{\text{dyn}})$ composed of two matrices:

$$\mathbf{F}_{\text{kin}} = \begin{pmatrix} \Phi \Gamma^\times & \Phi \mathbf{U} \\ \mathbf{0}_{3 \times 3} & \mathbf{0}_3 \end{pmatrix} \left| \begin{array}{c|c} \mathbf{Ad}_g \mathbf{J}^* \mathbf{S} & \mathbf{Ad}_g \mathbf{ad}_\eta \mathbf{J}^* \mathbf{S} \end{array} \right. , \quad (4.34)$$

$$\mathbf{F}_{\text{dyn}} = \begin{pmatrix} \frac{\partial \mathbf{M}}{\partial \sigma} & \frac{\partial \mathbf{C}}{\partial \sigma} & \frac{\partial \mathbf{f}_g}{\partial \sigma} \end{pmatrix}, \quad (4.35)$$

in which the differential form of the dynamic entities $\mathbf{M}(\mathbf{q})$, $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$, and $\mathbf{f}_g(\mathbf{q})$ of the Lagrangian model are given by

$$\frac{\partial \mathbf{M}}{\partial \sigma} = (\mathbf{Ad}_g^{-1} \mathbf{B}_1)^\top \mathcal{M}(\mathbf{Ad}_g^{-1} \mathbf{B}_1), \quad (4.36)$$

$$\frac{\partial \mathbf{C}}{\partial \sigma} = (\mathbf{Ad}_g^{-1} \mathbf{B}_1)^\top [\mathcal{C}_\eta(\mathbf{Ad}_g^{-1} \mathbf{B}_1) + \mathcal{M}(\mathbf{Ad}_g^{-1} \mathbf{B}_2)], \quad (4.37)$$

$$\frac{\partial \mathbf{f}_g}{\partial \sigma} = ([\mathbf{B}_1]_3)^\top \rho_0 \mathbf{a}_g, \quad (4.38)$$

We wish to stress that \mathbf{F}_1 collects all elements related to the forward kinematics, whereas \mathbf{F}_2 contains the dynamic entities related to the Lagrangian model. Following the spatial Matrix-Differential equation in (4.31), its solution will be a matrix $\mathbf{Z} := \text{blkdiag}(\mathbf{Z}_{\text{kin}}, \mathbf{Z}_{\text{dyn}})$ composed of two state matrices \mathbf{Z}_{kin} and \mathbf{Z}_{dyn} :

$$\mathbf{Z}_{\text{kin}}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) := \begin{pmatrix} \Phi & \gamma \\ \mathbf{0}_{3 \times 3} & \mathbf{0}_3 \end{pmatrix} \left| \begin{array}{c|c} \mathbf{B}_1 & \mathbf{B}_2 \end{array} \right. , \quad (4.39)$$

$$\mathbf{Z}_{\text{dyn}}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) := (\mathbf{M} \quad \mathbf{C} \quad \mathbf{f}_g), \quad (4.40)$$

Such a set of Matrix-Differentials as in (4.31) are not supported natively by standard ODE solvers. Therefore, an explicit second-order Runge-Kutta solver for MDEs is developed such that efficiently computes the evolution of the state matrix \mathbf{Z} along $\mathbb{X} = [0, L]$. The numerical solver is written in *MATLAB 2021a* and it can be found in the public repository of *Sorotoki*, see [36] for implementation.

As for state trajectories along the temporal regime $\mathbb{T} = [0, T]$, an implicit trapezoidal integration scheme is proposed to solve the approximated continuum

dynamics, which are generally less conservative on discretization to preserve numerical stability. Here implicit schemes are favored over the explicit scheme since a coarser time integration can significantly increase real-time performance. In addition, to further boost the performance of the temporal integration, a cost-effective approximation of the Hessian is introduced. For more detail on the temporal integration scheme of the solver can be found in Appendix C.3

4.6 Parameter identification

In this section, the nonlinear stiffness function for elongation and bending, $k_e : \mathbb{R} \rightarrow \mathbb{R}_{>0}$ and $k_b : \mathbb{R} \rightarrow \mathbb{R}_{>0}$, respectively, are solidified such that the elastic deformation aligns with the physical system seen in Figure 4.1. Numerous studies consider these stiffnesses to be linear, however, the presence of exotic materials and complicated structures would justify the modeling of nonlinear elastic behavior. Here, we extend these conservative material models and explore the nonlinear and time-varying regime.

4.6.1 Finite element method and hyper-elasticity

Generally, soft robots are operated by (differential) pressure to air channels embedded in the elastic body. If the applied pressure is sufficiently larger than the ambient pressure, the elastic body deforms to counteract the external forces – the critical point at which the external force overcome the internal elastic forces is proportional to the Young's modulus of the material. To enable efficient mobility, soft robots often explore of materials (or material composites) with a low Young's moduli, e.g., silicone elastomers. Unfortunately, large deformations of these rubber-like materials inherently lead to state-dependency in the mechanical compliance, and thus Hookean elasticity is no longer accurate – rendering them hyper-elastic. These hyper-elastic materials branch a whole new subfield in continuum mechanics. Although analytic descriptions exist, hyper-elasticity is generally treated numerically through Finite Element techniques [57, 75, 154] paired with a (nonlinear) continuum mechanics framework.

Many variations of constitutive models for hyper-elastic materials are available, including Saint Venant-Kirchhoff, Neo-Hookean, Mooney-Rivlin, Ogden, and Yeoh which are detailed in various work [146, 184, 220]. In Mustaza et al. [198], a Yeoh constitutive model is explored to describe hyper-elastic material characteristics of a silicone-composite actuator. Duriez et al. [75] and related works [57, 154] employ Neo-Hookean material models to enrich the nonlinear deformations in FEM-driven models. There are many different constitutive models available, each better suited to describe specific nonlinear elastic behavior. Constitutive material models are mathematical functions used to express the (nonlinear) relationship between stress and strain in terms of deformation. Let the spatial domain of robot's soft continuum body be given by \mathbb{V} which is a compact subset of \mathbb{R}^3 . This continuum body can be regarded as a collection of continuum particles called "material

"points" represented by a spatial coordinate $\mathbf{X} = [X_1, X_2, X_3]^\top \subseteq \mathcal{B}_0$. Now, assume there exists a mapping $\varphi^{(t)} : \mathcal{B}_0 \rightarrow \mathcal{B}$ that maps these material points \mathbf{x} into their deformed configuration \mathcal{B} . Then, given the deformation map $\varphi^{(t)}$, the local geometrical deformations of the continuum solid relative to an undeformed configuration are described by the deformation gradient tensor given as follows [115, 146]:

$$\mathbf{F} = \nabla_{\mathbf{X}} \varphi^{(T)}(\mathbf{X}). \quad (4.41)$$

For hyper-elastic materials, it is postulated that there exists a potential energy function $\mathbf{F} \mapsto \Psi(\mathbf{F})$ that is a function of the strain tensors. This potential function $\Psi(\mathbf{F})$ is also referred to as strain-energy density function, which depends exclusively on the material deformation.

In this work, we regard the Saint Venant-Kirchhoff constitutive model for hyper-elasticity [115, 146]. The Saint Venant-Kirchhoff model is in many ways similar to linear elastic materials (*i.e.*, Hooke's law), however, it is an extension from linear deformations into the nonlinear regime. The strain-energy density function for the Saint Venant-Kirchhoff model is defined as

$$\Psi^{\text{SV}} := \frac{\lambda}{2} \text{trace}(\mathcal{E})^2 + \mu \text{trace}(\mathcal{E}^2), \quad (4.42)$$

where $\mathcal{E} = \frac{1}{2}(\mathbf{F}^\top \mathbf{F} - \mathbf{I})$ the Green-Lagrange strain tensor, $\text{trace}(\cdot)$ denotes the trace of a tensor, and $\lambda > 0$ and $\mu > 0$ are the Lamé parameters which arise from the strain-stress relationships of the elastic material. The relations for the Lamé parameters are given by

$$\lambda = \frac{\nu E_0}{(1 + \nu_0)(1 - 2\nu_0)} \text{ MPa}, \quad \mu = \frac{E_0}{2(1 + \nu_0)} \text{ MPa}; \quad (4.43)$$

where E_0 is the Young's modulus or elasticity modulus and ν_0 is a dimensionless constant denoting the Poisson ratio. It is worth mentioning that the Yeoh or Ogden model is more suitable for silicone elastomer materials that are conventional material models for soft robotics.

In order to invoke the constitutive material law (4.42) for three-dimensional solids, we explore the finite element method. We generated a finite element mesh of the soft robot manipulator in Figure 4.1. The finite element analysis has been carried out in Abaqus/CEA with variable time increments. Given preliminary uniaxial tension tests, the 3D-printed elastomer material is estimated to be linear isotropic described by the following Lamé parameters: $E_0 = 80$ MPa, $\nu_0 = 0.4$ (-). The Lamé parameters can be computed according to (4.43). Furthermore, tangential (frictionless) contact interaction is included in the numerical simulation to prevent self-intersection of the elastic body.

Two finite element simulations are performed to independently characterize the elongation and bending stiffness of the soft robot. Due to simplicity, we start with the elongation stiffness. Each embedded bellow is actuated simultaneously up to a



Figure 4.6. High resolution finite element simulations of the soft robot manipulator (—) subjected to various input pressures $-20 \text{ kPa} \leq u_i(t) \leq 80 \text{ kPa}$. These results are produced using Abaqus/CEA numerical solver. To validate the PCC condition, an optimal backbone curve $\gamma(\mathbf{q}^*)$ is shown (—) whose joint coordinates are recovered by solving the optimization problem (4.44).

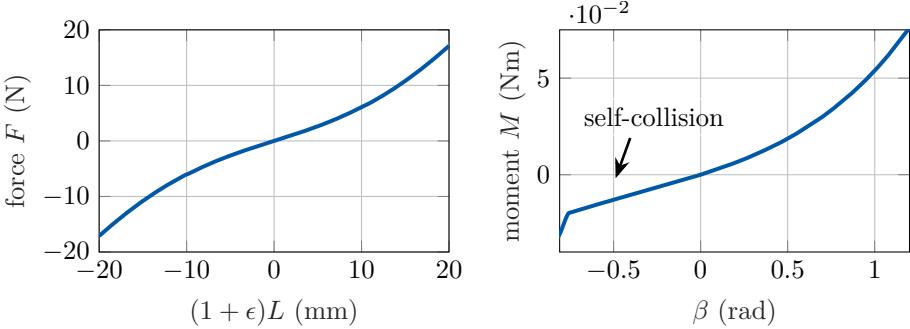


Figure 4.7. Elongation force F (N) and bending moment M (N m) recovered from the finite element data analysis. Note that the curve parametrization using the Bishop variables $\varepsilon = q_1$ and $\kappa = \sqrt{\kappa_x^2 + \kappa_y^2} = \sqrt{q_1^2 + q_2^2}$ are found using the optimization routine in (4.44). Notice also that self-collision occurs between the bellows for negative bending angles.

quasi-static differential pressure $-20 \text{ kPa} \leq u_1(t) = u_2(t) = u_3(t) \leq 30 \text{ kPa}$. Due to the symmetry of soft actuators, the resulting deformation will be exclusively in axial-direction. The corresponding elongation strain of the soft robot can then be found by recovering the maximum vertical displacement of the nodal mesh, *i.e.*, $\varepsilon = L^{-1} \max(U_z)$. Secondly, the analysis of the bending stiffness is conducted by actuating a single bellow up to a quasi-static differential pressure $-30 \text{ kPa} \leq u_1(t) \leq 80 \text{ kPa}$, while $u_2(t) = u_3(t) = 0 \text{ kPa}$. To recover the bending angle of the elastic body, certain spatial coordinates of nodes close to the end effector are tracked. Given their global coordinates, a constraint nonlinear optimization `fmincon.m` is used to recover optimal Bishop parameters κ and ε subjected to the kinematic relation in (4.14) and (4.13).

$$\begin{aligned} \mathbf{q}^* = \underset{\mathbf{q}}{\operatorname{argmin}} \quad & \left\| \log_{\text{SE}(3)} [\mathbf{g}^{-1}(L, \mathbf{q}) \mathbf{g}_L^{\text{FEM}}(\mathbf{u})] \right\|_2, \\ \text{s.t.} \quad & \mathbf{q} \in \mathcal{Q} \end{aligned} \quad (4.44)$$

where $\mathbf{g}_L^{\text{FEM}}$ is simply the corresponding end-effector configuration derived from

the high-resolution finite element simulation given the quasi-static input \mathbf{u} . To some extent, the problem (4.44) can be viewed as an inverse kinematics optimization problem subject to the desired end-effector configuration.

Remark 4.4 It is worth noting that the optimization routine (4.44) for state variable \mathbf{q}^* has a global minimizer. Namely, when both position and orientation are considered in the inverse kinematic optimization, there exist only one solution to \mathbf{q}^* on the configuration manifold \mathcal{Q} (i.e., the length is bounded). This makes the problem well-defined. Uniqueness is desirable as this makes it more easy to relate the reduced beam model to the FEM data. A problem arises, however, when the approach extends to non-constant curvature or multi-link cases. In this cases, the system is hyper-redundant and thus many, perhaps infinite, solutions may exist. To solve this, a regularization term must be added $\mathcal{U}^* = \frac{1}{2}\mathbf{q}^\top \mathbf{K}\mathbf{q}$ with some positive definite matrix $\mathbf{K} \succ 0$. An example for \mathbf{K} is the generalized stiffness matrix linearized around $\mathbf{q} = \mathbf{0}_n$. This ensures the inverse kinematic solutions on \mathcal{Q} will also minimize the elastic potential energy, which is again a global minimum. If gravity dominates elasticity, the optimization routine can be enriched by using the full potential energy and energy applied by the external (pressure) input. However, in this case many solution may exist thus making it difficult to relate the estimates to the FEM data. Furthermore, its solutions also depend on the initialization of the solver.

Following the PCC condition, the bending angle β can be calculated straightforwardly. Given these geometric curve parameters and the effective areas of the bellows, the applied elongation force and bending torque can be computed accordingly. The numerical results are provided in Figure 4.7. In practice, these nonlinear strain relations can also be determined experimentally; however, the numerical methods have the beneficial convenience of several post-processing procedures and gravitation-free deformations. To support our previous claim concerning the consistency of the PCC condition, Figure 4.6 provides a few FEM snapshots results together with the optimal backbone curve from (4.13). It can be seen that the piece-wise constant curvature (PCC) condition, although a clear oversimplification of the true mechanics at hand, is remarkably consistent with the FEM simulations.

4.6.2 Hyperelasticity in joint space

From the finite element results in Figure 4.6, the mathematical description for the nonlinear stiffness can be detailed further. However, a suitable candidate function must be chosen first to properly represent the hyperelastic stress-strain relation. The stiffness function $k_e(\varepsilon)$ and $k_b(\beta)$ have to satisfy the following properties.

Assumption 4.6 (Elastic boundedness) There exists positive constants k^- and k^+ such that $k^- \leq k_e(\xi), k_b(\xi) \leq k^+$ for all possible strains $\xi \in \mathbb{R}$. Given these bounds, it follows that conservative force produced by any deformation, given by $\mathcal{F} = \int_0^\xi k(s)s ds$, must be a monotonically increasing function.

Assumption 4.7 (Deformations reversibility) The stiffness functions k_e and k_b have a global optimum (i.e., either a maximum or minimum) at the origin.

Assumption 4.6 and 4.7 are necessary since they inhibit any buckling-type behavior, *i.e.*, elastic bodies being able to store energy when a large enough forces is applied. Then, consider the following elasticity models for the nonlinear (hyper-elastic) elongation and bending stiffness:

$$k_e(\varepsilon) = \alpha_1 + \alpha_2 (\tanh[\alpha_3 \varepsilon]^2 - 1), \quad (4.45)$$

$$k_b(\mathbf{q}) = \alpha_\phi(\mathbf{q}) \cdot [\alpha_4 + \alpha_5 (\tanh[\alpha_6 \beta(\mathbf{q})]^2 - 1)], \quad (4.46)$$

where $\boldsymbol{\alpha} = (\alpha_1, \alpha_2, \alpha_3, \alpha_4, \alpha_5, \alpha_6)^\top$ is a vector composed of the (possibly time-varying) stiffness parameters, and $\alpha_\phi : \mathcal{Q} \rightarrow [1, \infty)$ a nonlinear correction term for asymmetry along the circumference of the radial-axis. Please note that these nonlinear functions possess a decomposable structure: a linear term and a nonlinear term that mimics strain-hardening or strain-softening. As for the asymmetric stiffness due to the layout of the pneumatic bellows, we propose the following ansatz:

Assumption 4.8 (Stiffness variation under radial offset) Given the radial layout of the pneumatic bellows of the soft robot (see Figure 4.1), we assume that the nonlinear correction term for asymmetric radial stiffness along the circumference can be modeled by:

$$\alpha_\phi(\mathbf{q}) = \frac{1}{2} \beta [\sin(m \phi(\mathbf{q})) + 1] + 1, \quad (4.47)$$

where m is the number of bellows, and $\phi(\mathbf{q}) = \text{atan2}(\kappa_y, \kappa_x)$ the direction angle or heading. This stiffness correction term ensures the nonlinear bending stiffness becomes larger between bellows – as it causes simultaneous deformation of multiple bellows. Please note that $\alpha_\phi(\mathbf{q}) \geq 1$ for all $\mathbf{q} \in \mathcal{Q}$.

To satisfy the aforementioned conditions, it should hold that $\alpha_1 > \alpha_2$, $\alpha_4 > \alpha_5$ and $\alpha_{1,4} > 0$. To find the hyper-elastic parameter vector $\boldsymbol{\alpha}$, we use a weighted least-squares optimization. Recalling the previous profiles for elongation force and bending moment obtained from the FEM data, see Figure ??, we integrate the expressions (4.45) and (4.46) to find an analytic approximation, *i.e.*, $F(\varepsilon; \boldsymbol{\alpha}) := \int_0^\varepsilon k_e(\xi) \xi \, d\xi$ and $M(\beta; \boldsymbol{\alpha}) := \int_0^\beta k_b(\xi) \xi \, d\xi$, respectively. The weighted regression is biased towards positive strains, to better represent the deformation characteristics under positive pressurization. Again, we use `fmincon.m` optimizer in *Matlab*. The hyper-elastic material parameters $\boldsymbol{\alpha}$ that minimize the residual between the FEM data and the analytic model are given in Table 4.1, and the comparison between the FEM force profiles and our solution is given in Figure 4.8. Notice that self-collision is not capture by the stiffness model. Theoretically, the self-contact interactions (as seen in Figure 4.8) can also be parameterized using a different set of polynomials, which are non-zero for the compression regions and zero otherwise. In other words, the regression can be enriched with polynomials that are asymmetric with respect

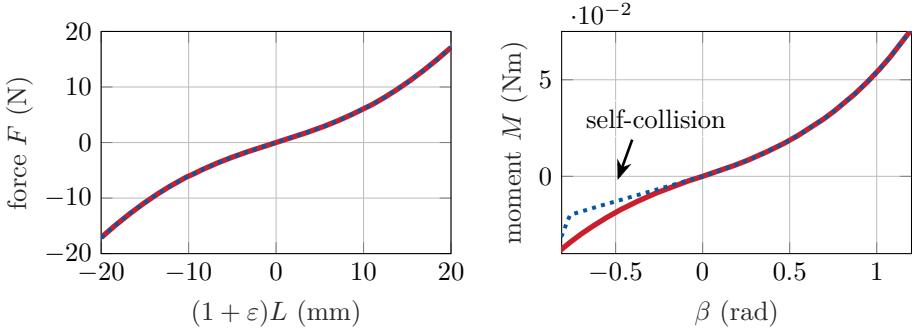


Figure 4.8. Comparison of the (nonlinear) mechanical compliance between the proposed hyper-elastic model (—) and the finite element simulations (—). Notice the proposed stiffness model (4.46) does not capture the self-collision.

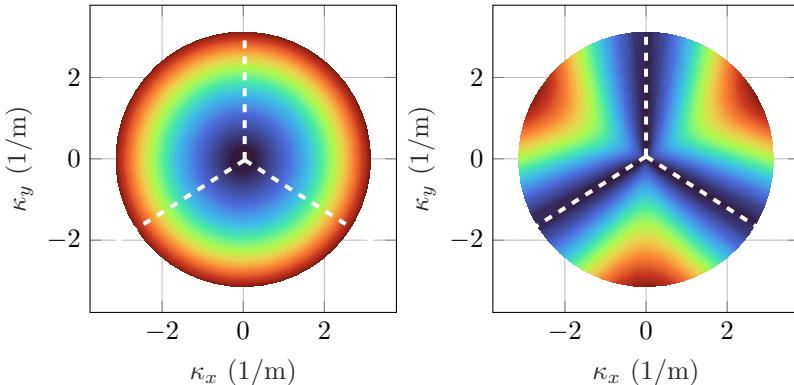


Figure 4.9. Amplitude of the nonlinear stiffness components for elongation and bending. Both stiffness functions are evaluated for a radially distributed sampling of the curvature joint space $(\kappa_x, \kappa_y) \in [-\pi, \pi]$ (left) Elongation stiffness, the stiffness values is shown by the colormap $\in [0.8, 1.2] \text{ Nm}^{-1}$. (right) Elongation stiffness, the stiffness values is shown by the colormap $\in [10, 100] \text{ mN m}$. Note that the bending stiffness has a discrete symmetry in the circumferential direction with periodicity $\phi = k \frac{\pi}{3}$.

Table 4.1. Estimated hyper-elastic and viscoelastic material parameters for the study case soft robot

	$i = 1$	$i = 2$	$i = 3$	$i = 4$	$i = 5$	$i = 6$
α	$2.23 \cdot 10^{+3}$	$1.74 \cdot 10^{+3}$	$-4.55 \cdot 10^{+2}$	$1.31 \cdot 10^{-3}$	$1.23 \cdot 10^{-2}$	$-2.29 \cdot 10^{-1}$
α_λ	$3.21 \cdot 10^{+2}$	$5.22 \cdot 10^{-1}$	$26.4 \cdot 10^{+1}$	$1.82 \cdot 10^{-4}$	$26.4 \cdot 10^{+1}$	$1.82 \cdot 10^{-4}$

to the origin. We also provided Figure 4.9 to show the change in stiffness when the soft robot deforms, where we can clearly see a discrete radial symmetry arise due to the radial composition of the three bellow network.

4.6.3 Viscoelastic creep

In material mechanics, the tendency of mechanical solids to move slowly under stress is called creep. Unlike ideal elastic materials, when polymeric materials are subjected to abrupt change in stress, the constitutive network of polymer chains reconfigure until the stress is evenly distributed. Therefore, we introduce a new state vector $\boldsymbol{\lambda}(t) \in \mathbb{R}^n$, which contains the creep state variables. According to Meyer et al. (2009, [184]), the Kelvin-Voigt model for creep is given by a first-order ordinary differential equation of the form

$$\frac{d}{dt} \begin{pmatrix} \lambda_1 \\ \vdots \\ \lambda_n \end{pmatrix} = \begin{pmatrix} -\alpha_{\lambda,1} & \dots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \dots & -\alpha_{\lambda,2n-1} \end{pmatrix} \begin{pmatrix} \lambda_1 \\ \vdots \\ \lambda_n \end{pmatrix} - \begin{pmatrix} \alpha_{\lambda,2} \\ \vdots \\ \alpha_{\lambda,2n} \end{pmatrix} \dot{\boldsymbol{q}} \quad (4.48)$$

where the vector $\boldsymbol{\alpha}_\lambda = (\alpha_{\lambda,1}, \alpha_{\lambda,2}, \dots, \alpha_{\lambda,2n})^\top$ contains positive parameters that describe the viscoelastic material dynamics, and the state variables $\lambda_i(t)$ with $i \in \{1, 2, \dots, n\}$, i.e., the creep strains. Note that the state dimension of the creep strains is equivalent to the state dimension $\dim(\boldsymbol{q})$. Now, the dynamics of the viscoelastic creep can be easily included into (4.25) as an external disturbance $\boldsymbol{\delta}(t)$. Hence, consider the viscoelastic creep forces of the Kelvin-Voigt model to be characterized by

$$\boldsymbol{\delta}_c(\boldsymbol{\lambda}) = \mathbf{K}_\lambda^\top \boldsymbol{\lambda}, \quad (4.49)$$

where $\mathbf{K}_\lambda \succ 0$ denotes the creep compliance matrix, which is a linear mapping from creep strains to creep forces. Since creeping strains are difficult, if not impossible, to distinguish from the elastic strains alone, we must include dynamic experiments to properly identify the creep coefficients. Using a regression approach similar to Section 4.6.2, the creeping parameters $\boldsymbol{\alpha}_\lambda$ and the creep compliance \mathbf{K}_λ are empirically estimated from experimental data (e.g., unforced oscillations). In this regression, the full dynamics are simulated and the parameter $\boldsymbol{\alpha}_\lambda$ are optimized to minimize the dynamic residual in tip position of the soft robot. The estimated viscoelastic parameters are also provided in Table 4.1. The linear damping parameters from the Rayleigh damping matrix \mathbf{R} and the initial conditions for $\boldsymbol{\lambda}(t_0)$ are identified similarly.

Example 4.3 (Kelvin-Voigt creep dynamics). To highlight the dynamics of elastomer materials exhibiting creep, let us consider an rudimentary illustrative example of a 1-DOF mass-spring-damper system with a Kelvin-Voigt creep element. Let $\boldsymbol{x} = (x_1, x_2, x_3)^\top = (\varepsilon, \dot{\varepsilon}, \lambda)^\top$ be the state vector composed of the elongation strain, elongation rate, and the creep strain, respectively. Then, the dynamics can be written in the familiar state space form as follows:

$$\dot{x}_1 = x_1, \quad (4.50)$$

$$\dot{x}_2 = \frac{1}{m} [-kx_1 - cx_2 + k_\lambda x_3 + u], \quad (4.51)$$

$$\dot{x}_3 = -\alpha_{\lambda,1}x_3 - \alpha_{\lambda,2}x_2 \quad (4.52)$$

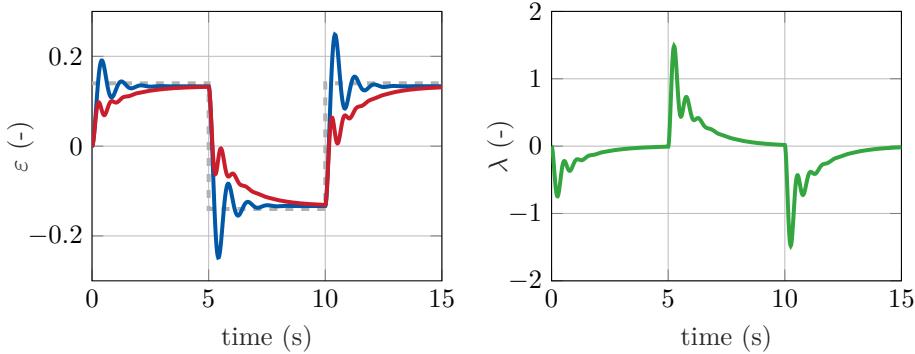


Figure 4.10. Simulation study of introducing viscoelastic Kelvin-Voigt dynamics to a mass-spring-damper system, where we show the evolution of the elongation ε subjected to a smooth block signal $u(t) = 0.15 \cdot \text{sign}[\sin(0.2\pi t)]$ in (—) compared between the original Hookean model (—) and viscoelastic Kelvin-Voigt model (—). Also, the evolution of the viscoelastic creeping strain λ is shown in (—).

where $m, k, c > 0$ the mass, spring, damper coefficients; respectively, $k_\lambda > 0$ the creep stiffness, $\alpha_\lambda > 0$ the creep parameters, and $u : \mathbb{T} \rightarrow \mathbb{R}$ an auxiliary input (*i.e.*, prescribed force). The following parameters are consider for this illustrative example: $m = 0.1$ kg, $k = 10$ Nm $^{-1}$, $c = 0.1$ Nsm $^{-1}$, $k_\lambda = \alpha_{\lambda,1} = 2$, and $\alpha_{\lambda,2} = 5$. To highlight the effects of viscoelastic creep, we choose a reference signal with fast-changing dynamics: $u(t) = 0.15 \cdot \text{sign}[\sin(0.2\pi t)]$. Given the input, the simulation results are shown in Figure 4.10. Note that the simulation result presents an unmodified Hookean model (—) in which $k_\lambda = 0$, and the Kelvin-Voigt variant (—). Clearly, we see a difference between the two trajectories. The original Hookean model oscillates around the quasi-static equilibrium, whereas the Kelvin-Voigt variant slowly converges to the setpoint. Note that this is clearly different than the traditional overdamped response, as the Kelvin-Voigt model does allow for oscillations during the smooth transient.

4.7 Passivity-based adaptive control

As briefly discussed in the introduction, the dynamics model will be used as a control-oriented framework for model-based controllers applicable to soft robotics. In retrospect to previous model-based controllers, Della Santina et al. [72] proposed a combination of feedforward and model-based feedback; yet, satisfying the passivity condition, more robustness approach could be acquired through energy-based controller (especially in the face of material uncertainties). Franco et al. [87] proposed an adaptive energy-based controller but the underlying model (multi-link pendulum) is not rooted in a continuum description. Here, we wish to provide a mix of the control methodologies – an energy-based control approach for the continuous PCC model with an adaptive material law.

The continuous dynamics of the soft robotic manipulator are described by (4.25), where the Lagrangian system matrices depend on physical parameters, e.g., mass, moments of inertia, stiffness, and viscosity. Within the context of robust control, these parameters often deviate from their true value. So merely an estimate of the system matrices $\tilde{\mathbf{M}}(\mathbf{q})$, $\tilde{\mathbf{C}}(\mathbf{q}, \dot{\mathbf{q}})$, $\tilde{\mathbf{f}}_g(\mathbf{q})$ and $\tilde{\mathbf{f}}_e(\mathbf{q}, \dot{\mathbf{q}})$ can be acquired, where we denote $\Delta(\cdot) = (\tilde{\cdot}) - (\cdot)$ as the difference between the true value and its estimate. The difference (or uncertainty) between true and estimated values is of particular relevance in soft robotics, where material properties play a significant role on both the statics and dynamics. Poor estimates of the material parameters could lead to instability in some model-based controllers if not considered carefully. Exploiting the passivity in Lagrangian models, we can derive a passivity-based adaptive controller similar to the works of Slotine et al. [247] and Ortega et al. [203]. The benefit of passivity-based control techniques is its robustness regarding parameter uncertainties and unmodelled dynamics. Passivity-based control is rooted in energy-shaping and damping injection techniques, leading to simple implementation yet effective means of stabilization.

Let $\mathbf{q}_d \in \mathcal{Q}$ be the desired trajectory of the soft robot together with its time-derivative $\dot{\mathbf{q}}_d, \ddot{\mathbf{q}}_d \in \mathbb{R}^n$. Next, let $\boldsymbol{\pi} \in \mathbb{R}^p$ be a vector containing all unknown values from a set of physical parameters, and the parametrization error $\mathbf{e}_p := \tilde{\boldsymbol{\pi}} - \boldsymbol{\pi}$ in which the the vector $\tilde{\boldsymbol{\pi}} \in \mathbb{R}^p$ denotes the parameter estimates. An important note is that the model must be linear in $\boldsymbol{\pi}$, which holds true for the line-density ρ_0 , the linear elasticity parameters in (4.46) and (4.45), damping, creep coefficients in (4.48) and (4.49), and also for an unknown mass applied at the tip of the soft robot (4.26). Unfortunately, we cannot included the material parameters α_3 and α_6 due to their nonlinear dependence. The control objective is given by finding an appropriate control input and update law such that $\lim_{t \rightarrow \infty} \mathbf{q}(t) = \mathbf{q}_d(t)$ is achieved with good transient behavior. Assuming linearity in the parameters the linear parametrizability matrix of the soft robot's dynamics is given as follows

$$\mathbf{Y}(\cdot, \boldsymbol{\pi}) \mathbf{e}_p = \Delta \mathbf{M} \ddot{\mathbf{q}}_r + \Delta \mathbf{C} \dot{\mathbf{q}}_r + \Delta \mathbf{f}_g + \Delta \mathbf{f}_e + \Delta \boldsymbol{\delta}, \quad (4.53)$$

where $\dot{\mathbf{q}}_r = \dot{\mathbf{q}}_d - \boldsymbol{\Lambda} \mathbf{e}$ is called the reference velocity vector, $\boldsymbol{\Lambda} \in \mathbb{R}^{n \times n}$ a positive diagonal matrix, and $\mathbf{Y}(\mathbf{q}, \dot{\mathbf{q}}, \ddot{\mathbf{q}}_r, \dot{\mathbf{q}}_r, \boldsymbol{\pi}) \in \mathbb{R}^{m \times n}$ is called the regressor matrix. Following the work of Slotine and Li [247], the control law and adaptation law are given by

$$\boldsymbol{\tau} = \tilde{\mathbf{M}} \ddot{\mathbf{q}}_r + \tilde{\mathbf{C}} \dot{\mathbf{q}}_r + \tilde{\mathbf{f}}_g + \tilde{\mathbf{f}}_e - \tilde{\boldsymbol{\delta}} - \mathbf{K}_p \mathbf{e} - \mathbf{K}_d \mathbf{e}_r, \quad (4.54)$$

$$\dot{\tilde{\boldsymbol{\pi}}} = -\mathbf{K}_{\boldsymbol{\pi}} \mathbf{Y}^{\top} \mathbf{e}_r, \quad (4.55)$$

where $\mathbf{e}_r := \dot{\mathbf{q}} - \dot{\mathbf{q}}_r = \dot{\mathbf{e}} + \boldsymbol{\Lambda} \mathbf{e}$, $\mathbf{K}_p, \mathbf{K}_d \in \mathbb{R}^{n \times n}$ are controller gains, and $\mathbf{K}_{\boldsymbol{\pi}} \in \mathbb{R}^{p \times p}$ is a positive definite matrix called the adaptation rate. Since $\boldsymbol{\tau}$ define the desired generalized forces acting on the system (4.25), the desired pressures are computed as $\mathbf{u} = \mathbf{G}^+ \boldsymbol{\tau}$ with \mathbf{G}^+ the generalized inverse of \mathbf{G} . A schematic diagram of the passivity-based controller is provided in Figure 4.11. It should be mentioned that the magnitude of adaptation rate does not affect the global stability of the system

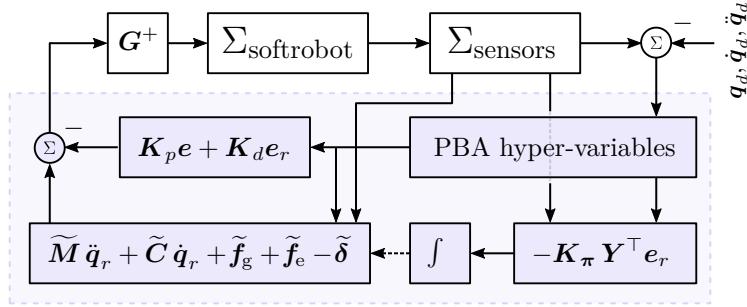


Figure 4.11. Schematic diagram of the passivity-based adaptive controller (PBAC), where $\Sigma_{\text{softrobot}}$ denotes the dynamical system (4.25) and Σ_{sensor} a system of sensors suitable of measuring \mathbf{q} and $\dot{\mathbf{q}}$.

(if unmodelled dynamics are not excited); however, it sets the rate of adaptation, and accordingly the performance of the system.

Remark 4.5 (Persistence of excitation) *It is important to note that the convergence of the tracking error $e \rightarrow 0$ does not imply convergence of the estimated parameter to their true values. According to [246–248], asymptotic convergence can be shown if the matrix $\mathbf{Y}(\mathbf{q}, \dot{\mathbf{q}}, \ddot{\mathbf{q}}_r, \dot{\mathbf{q}}_r, \boldsymbol{\pi})$ is persistently excited and it is uniformly continuous. To elaborate, under the condition of persistent excitation, that is, for any instances t_1, t_2 with $t_1 \leq t_2$ there exists a positive constant α such that $\int_{t_1}^{t_2} \mathbf{Y}^\top \mathbf{Y} dt \preceq \alpha \mathbf{I}$, it can be proven that the parameter estimates converge asymptotically to their true values. The authors in [247] state that the proof for convergence here applied to nonlinear robot dynamics is similar to those of linear dynamics [192] although the proof is fairly involved.*

4.8 Overview of experimental platform

Before invest, we detail the experimental setup and control platform of the soft robotic system. Since sensing is a challenging issue in soft robotics, due to large distributed deformations, a combination of sensors were used to recover an estimate of the states $\mathbf{q} \in \mathcal{Q}$. A full overview of the setup is given in Figure 4.12. First of all, we employed a 6-DOF inertial measurement unit (MPU-6050, InvSense) that measures the angular displacement of the soft robot's end-effector (*i.e.*, $\sigma = L$). Through on-board sensor fusion, the bending angle of the soft robot can be recovered, *i.e.*, $\beta = \kappa l$. Since the bending angle alone is not sufficient to decouple the curvature and elongation, additional sensing is required. Consequently, we use a stereo-vision depth camera (RealSense D435, Intel) with an infrared dot projector and RGB camera module. A spherical optical marker is attached to the end-effector of the soft robot, whose relative position can be recovered using a combination of depth-sensing and image post-processing with a Hough-space

circle transformation. To retrieve a global reference frame of the vision system, four 30×30 mm Aruco marker are uniformly distributed whose location and orientation can be found using the `opencv-python` library. We show the implementation of the optical vision system and its post-processing in Figure 4.13. Through trigonometry and the measured bending angle β , an filter measurement of the position vector $y = \tilde{\gamma}_L$ can be recovered. Given the analytic expressions for the orientation and position in (4.12) and (4.13), an inverse Jacobian kinematic solver is employed to recover an estimate of the state vector, *i.e.*, $\tilde{\mathbf{q}}_{\text{dyn}} = \text{argmin}_{\mathbf{q}} \|\tilde{\gamma}_L - \gamma(L, \mathbf{q})\|_2$. During each experimental trail, it was made sure the soft robotic body does not occlude the optical marker.

As for the pneumatic actuation, an array of proportional-pressure regulators (VEAB-B-D16, Festo) was used with an active pressure range of $-0.1 \text{ MPa} < u(t) \leq 0.1 \text{ MPa}$, which simultaneously allow for pressure measurements. These measurements are fed into the (quasi-static) model to also recover a quasi-static estimate of the states $\tilde{\mathbf{q}}_{\text{qs}}$. Then, the dynamic estimates $\tilde{\mathbf{q}}_{\text{dyn}}$ and the quasi-static pressure-based estimates $\tilde{\mathbf{q}}_{\text{qs}}$ are fused using an ordinary complementary filter. The control and data acquisition are done using a Raspberry Pi 4 (2GB).

4.9 Numerical and experimental implementation

In this section, we will discuss the simulation results of the dynamic model (4.25), the passivity-based controller (4.54), and the adaptive law (4.55). To illustrate effectiveness and performance of the approach, we segregate our analysis into several study-cases of various complexity. First, focusing on the physical one-link soft robot in Figure 4.1 ($N = 1$), we investigate the unforced system’s equilibria and their corresponding stability. In continuation, we compare the simulated trajectories of the dynamical model with experimental data for natural oscillations, forced pneumatic inputs, and external loading conditions; where we also highlight contribution of the hyper-elastic FEM-driven material model. Second, to illustrate the flexibility and computational efficiency of the numerical framework, we extend the one-link model to a multi-link model with $N = 6$ soft-bodied links.

The numerical solutions to the ordinary differential equations in (4.25) together with (4.54) and (4.55) are computed using the aforementioned MDE integration scheme which is developed in *MATLAB*, and the underlying code can be found at Caasenbrood et al. [39]. The software architecture is compactly written as Object-Oriented class labeled under `./src/Model.m` that enables a minimal programming interface to set-up various soft robotic simulation models easily. The simulation results provided in this section can be reproduced using the open-source *Sorotoki* package found at [36].

Natural dynamics – One-link soft robot: The following physical parameters are chosen for the soft robot: the mass $m_0 = 17.3$ g, the relaxation length $L = 64.4$ mm. The material parameters for hyper-elasticity and visco-elasticity models are chosen identical to Table 4.1. For the additional viscous material be-

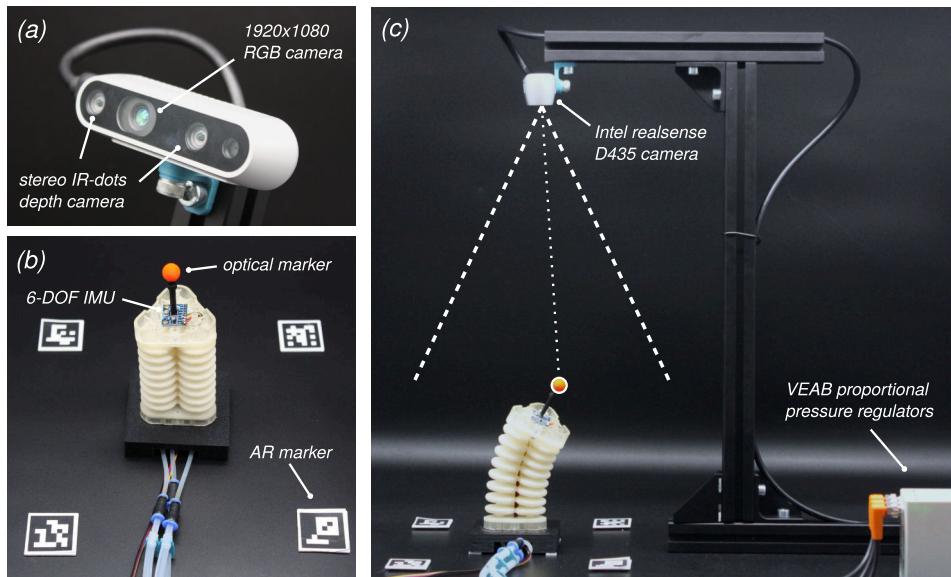


Figure 4.12. General overview of the experimental platform for the testing and development of the 3-DOF soft manipulator. (a) Close-up of the RealSense D435 stereo-vision depth camera. (b) Soft continuum manipulator with pressure inputs $\mathbf{u} = (u_1, u_2, u_3)^\top$, a MPU-6050 Inertial Measurement Unit (IMU) to measure the end-effector angle β , and a color-coded optical marker to recover γ_L , and four Aruco markers to recover Φ_0 and γ_0 . (c) Overview of full setup with the array of three VEAB-B-D16 pressure regulators.

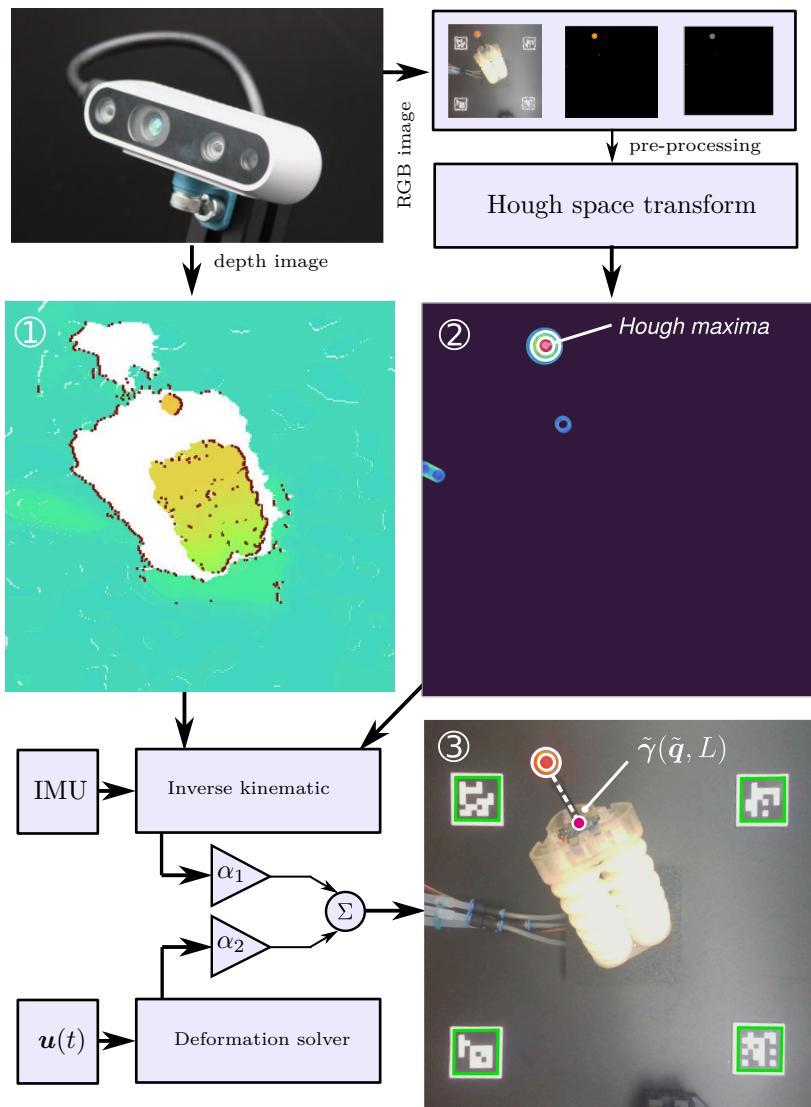


Figure 4.13. General overview of the optical vision system used to estimate the state variables \mathbf{q} . ① First, an RGB image is processed using a Circular Hough transformation filtering for circles with a radius 32 pix, it has a global maxima at the optical marker. ② Then, a sample of the depth camera is generated. ③ Finally, all sensor data is combined using a sensor fusion algorithm of depth, RGB camera, input pressures and IMU data, resulting in an accurate estimate of soft manipulator's end-effector $\tilde{\gamma}(L, \tilde{\mathbf{q}})$.

havior, the Rayleigh damping matrix and the creep compliance matrix are chosen a follow:

$$\mathbf{R} = \begin{pmatrix} 0.01 & 0 & 0 \\ 0 & 1.05 \cdot 10^{-5} & 0 \\ 0 & 0 & 1.05 \cdot 10^{-5} \end{pmatrix};$$

$$\mathbf{K}_\lambda = \begin{pmatrix} 502.3 & 0 & 0 \\ 0 & 1.53 \cdot 10^{-2} & 0 \\ 0 & 0 & 1.53 \cdot 10^{-2} \end{pmatrix}.$$

We stress that the values for the Rayleigh damping and creep compliance shown above are identified empirically through open-loop measurements, similar to the creep coefficient provided in Table 4.1. We will explain how these coefficients are derived later in this chapter.

First, we investigate the existence and the stability of the equilibria of the unforced system. If the system is at rest (i.e., $\dot{\mathbf{q}} = 0$, $\ddot{\mathbf{q}} = 0$), then by definition there are no conservative forces acting on the system. Thus, for any equilibrium point \mathbf{q}_0 it holds that $\nabla \mathcal{U}(\mathbf{q}^*) \equiv \mathbf{0}$. If $\mathcal{U}(\mathbf{q}^*) \equiv E_0$ is a local minimum, then the equilibrium is deemed stable. Any small disturbance will result in a new energy-state E_1 and will consequently bring the system in motion. However, regarding E_0 is a local minimum, the system will remain in a neighborhood of \mathbf{q}^* and eventually converge towards its nearest low-state energy E_0 . If $\mathcal{U}(\mathbf{q}^*) \equiv E_0$ is a local maximum, the equilibrium is deemed to be unstable, since there exist a configuration close to \mathbf{q}^* with a lower energy-state, *i.e.*, $\mathcal{U}(\mathbf{q}^* + \delta\mathbf{q}) < E_1$. By analysis of the gradient of the potential energy function $\nabla \mathcal{U}(\mathbf{q})$, two unique equilibria can be found numerically. The potential function has a local maximum for $\mathbf{q}_{\text{unstab}}^* = \left(-\frac{m_0 g}{L(\alpha_1 - \alpha_2)}, 0, 0\right)^\top$ which is unstable. To some extent, it is analogous to the unstable equilibrium position of the inverted pendulum system.

For the stable equilibria, the bisection method was used to find the zero-crossing of $\nabla \mathcal{U}(\mathbf{q})$, where it was found that all stable solutions of the unforced system will tend to the following set:

$$\Omega_{\text{stab}} = \left\{ \mathbf{q} \in \mathcal{Q} : \varepsilon = -\varepsilon_*, \kappa(\mathbf{q}) = \frac{\kappa_*}{\alpha_\phi(\mathbf{q})} \right\},$$

where ε_* and κ_* are nonzero constants. Notice that the set Ω_{stab} is topologically equivalent to a ring. This set corresponds to the hanging position of the soft robot. Given the physical parameters of the robot in Figure 4.1, the following constants are found: $\varepsilon_* = 0.0021$ and $\kappa_* = 0.0174$. It is important to note that the stable set of equilibria stems from the force balance between the internal elastic potential forces and the external gravitational potential forces, and thus any stiffness will lead to a stable set with a similar topology. By changing the base orientation of the soft manipulator (*i.e.*, by modifying Φ_0), both equilibria vanish and all state trajectories will tend to a global stable equilibrium. For fully reversing the orientation, this trivially leads to the stable equilibrium $\mathbf{q}_{\text{stab}}^* =$

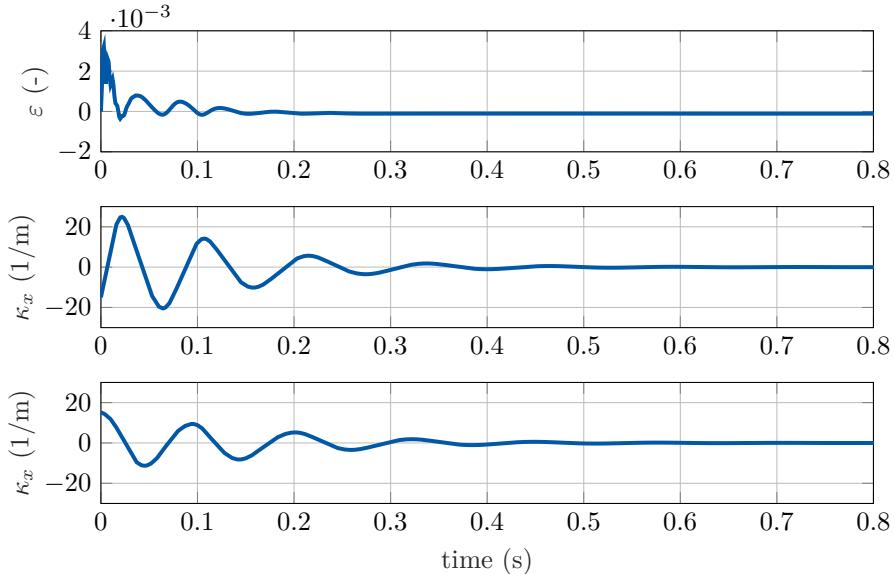


Figure 4.14. State trajectories of one-link soft robot model with initial conditions $\mathbf{q}_0 = (0, -15, 15)^\top$ and $\dot{\mathbf{q}}_0 = (0, 2500, 0)^\top$. The figure shows the elongation strain ε and the curvatures κ_x , κ_y in the xz -plane and yz -plane, respectively. Clearly the one-link soft robot oscillates about the set Ω_{stab} .

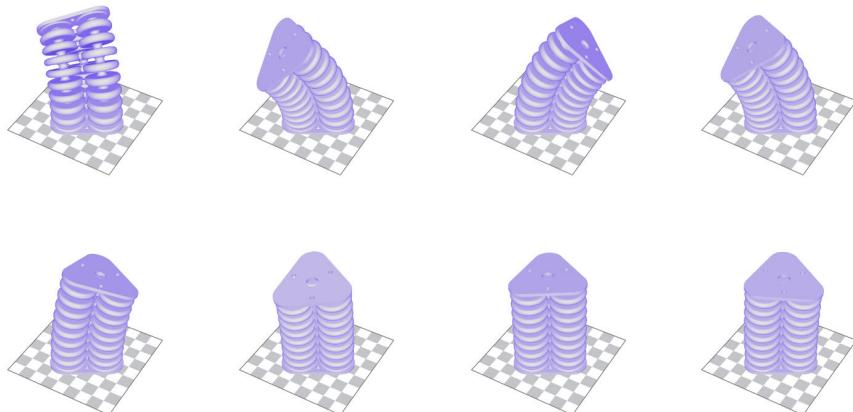


Figure 4.15. Three-dimensional volumetric evolution of the one-link soft robot model with initial conditions $\mathbf{q}_0 = (0, -15, 15)^\top$ and $\dot{\mathbf{q}}_0 = (0, 2500, 0)^\top$. Notice that the states of the one-link soft robot quickly converge to the the set of stable equilibria Ω_{stab} .

$(+\frac{m_0 g}{L(\alpha_1 - \alpha_2)}, 0, 0)$. This phenomenon is referred to as local bifurcation, in which the change of parameter values alters the existence and stability of equilibria. This property might be interesting for soft robot manipulators with multiple soft-bodied links, as they are likely to be subjected to different gravitational loads.

To illustrate the unforced dynamics and the existence of stable equilibria, time-domain simulations of the dynamical model with nonzero initial conditions:

$$\mathbf{q}_0 = (0, -15, 15)^\top,$$

$$\dot{\mathbf{q}}_0 = (0, 2500, 0)^\top.$$

Figure 4.14 shows the state trajectories of the soft robot; whereas Figure 4.15 is provided to better illustrate the underlying dynamics and the trajectory of the end-effector.

Besides the existence of stable solutions, the numerical simulations perfectly illustrate the coupled dynamics between the elongation and bending of the soft robot. Due to the difference in mechanical stiffness for elongation and bending, we observe high-frequency and low-frequency oscillation for the elongation strain $\varepsilon(t)$, and we observe low-frequent oscillations for the curvatures $\kappa_x(t)$ and $\kappa_y(t)$. Interestingly, the low-frequency oscillations are passed from the curvature dynamics to elongation dynamics; conversely, the dynamics of the elongation barely affect the curvatures. After sufficient time passes, the trajectories indeed tend to the set of stable equilibria Ω_{stab} .

Experimental comparison—unforced, forced, and external loads: To validate the dynamic model, the solutions of the model are compared with measurements of the physical system in unforced, forced, and tip-load conditions. As such, the model validation is separated into three parts: *i*) unforced, *ii*) forced conditions, and *iii*) external tip-loads applied on the end-effector.

We start with the unforced scenario, *i.e.*, no input is considered $u_i(t) \equiv 0$. For the unforced analysis, two experimental trials are performed for the unforced validation. First, the soft robot is deformed slightly and then released from rest, which corresponds to the initial conditions $\mathbf{q}_0 = (0.015, 4.75, 0)^\top$ and $\dot{\mathbf{q}}_0 = \mathbf{0}_3$. Since the mechanical deformations are relatively small here, the presence of hyper-elastic and visco-elastic material behavior are less dominant. Secondly, the soft robot is moderately deformed such that the initial configuration (or shortly after) lies within the hyper-elastic and visco-elastic regime. In this scenario, the non-linear and time-dependent material effects may not be neglected. These initial conditions correspond to $\mathbf{q}_0 = (0.046, 11.25, 0)^\top$ and $\dot{\mathbf{q}}_0 = \mathbf{0}_3$. It is worth mentioning that the creep strains $\boldsymbol{\lambda}$ are difficult to distinguish from the true strain, and thus the initial conditions for $\boldsymbol{\lambda}(t_0)$ are determined empirically using a set of dynamic measurements with different initial condition. The comparison between our model and the unforced dynamic measurements are shown in Figure 4.16.

As can be seen, the state trajectories of the end-effector closely match the ground truth trajectories, even for significant nonlinear deformation. For the first test run (inside linear elastic regime), the RMS error and the maximum error

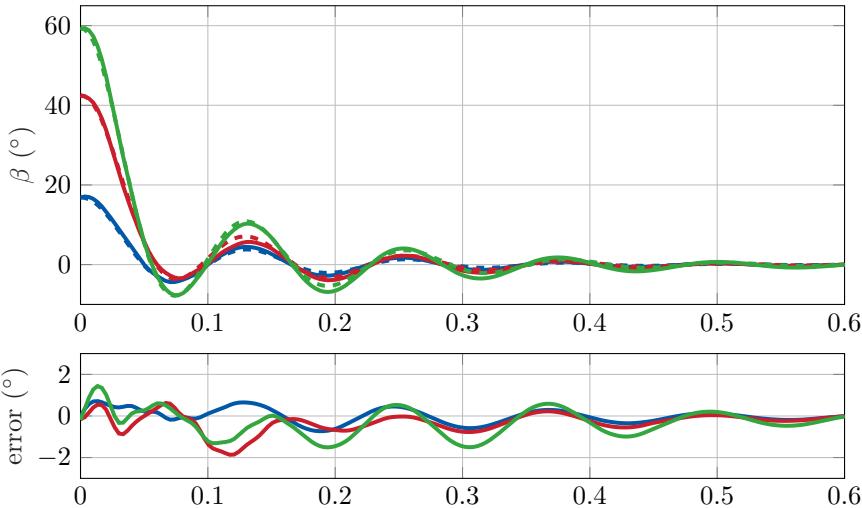


Figure 4.16. Experimental comparison results of the dynamic model in unforced conditions. (top) Bending angles of the soft robot in unforced conditions, where the dashed lines represent the experimental measurements and the solid lines are the simulated trajectories. The dataset (—) are within a nearly linear elastic regime whereas datasets (—, —) are in the nonlinear regime. (bottom) The error between experiments and the optimized numerical model. As can be seen, all trajectories remain within an error bound of $\pm 2^\circ$ degree.

are ± 0.19 and ± 0.50 degrees, respectively. For the second case (outside the linear elastic regime), the RMS error and the maximum error is ± 0.78 and ± 2.33 degrees, respectively.

Second, we consider a forced scenario in which a regulated pressure input is applied to the pneumatic bellows, *i.e.*, $\mathbf{u} \neq \mathbf{0}_3$. Since the pneumatic mapping \mathbf{G} in (4.27) plays an important role here, the actuator coefficients are recomputed to match the experimental data better. To be more specific, by considering a pre-defined set of excitation signals $u(t)$ of various amplitudes and frequencies, a least-squares optimization routine is employed that minimizes the difference between the measured states \hat{q} with the simulated states q by tuning the coefficients α_ε and α_κ . This leads to the following values: $\alpha_\varepsilon = 2.34 \cdot 10^{-7}$ and $\alpha_\kappa = 1.61 \cdot 10^{-8}$. As for the excitation signal, we have chosen the following input:

$$u_i(t) = P_0 + P_A \left(\frac{1}{2} + \frac{1}{2} \sin(t + \phi_i) \right) \cdot \max(0.05t, 1), \quad (4.56)$$

with a static offset $P_0 = 10$ kPa, an amplitude $P_A = 25$ kPa, and a phase offset $\phi_i = (i - 1) \frac{2\pi}{m}$ rad. To highlight the significance of the proposed hyper-elastic modeling approach, we also compare the results using an optimized Hookean material model with $k_e = 50.6$ N/m and $k_b = 5.8 \cdot 10^{-4}$ Nm/rad. The initial conditions are set to zero. The validations results for both the FEM-driven hyper-

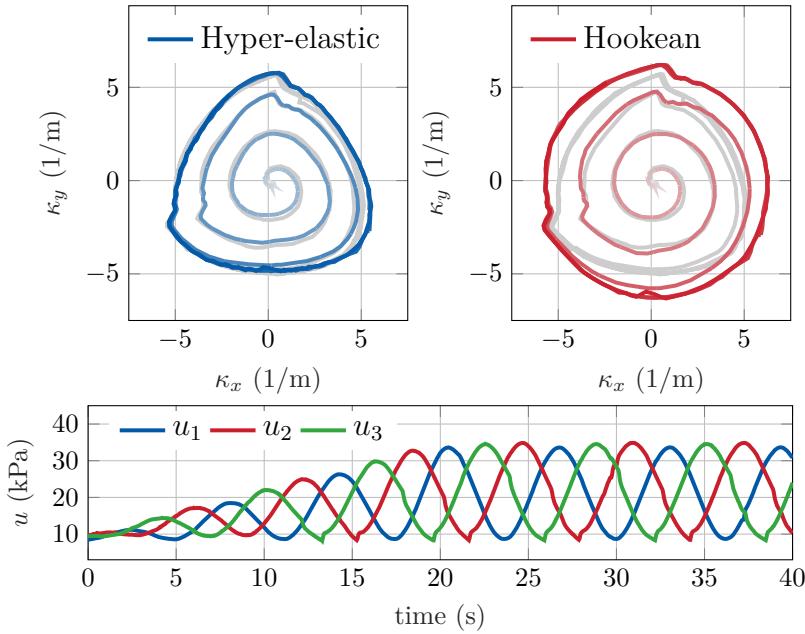


Figure 4.17. Spatial representation of the nonlinear stiffness, *i.e.*, elongation stiffness (left) and bending stiffness (right) for a radially distributed sampling of the curvature joint space $(\kappa_x, \kappa_y) \in [-\pi, \pi]$. The experimental data is shown in (—). Again, note that the bending stiffness has a discrete symmetry in the circumferential direction with periodicity of $\frac{2\pi}{3}$.

elasticity model and linear model in the forced setting are shown in Figure 4.17. The figure also shows the measured outputs from the pneumatic VEAB regulators $u_i(t)$, which are directly fed into both linear and hyper-elastic models.

Given these results, two key observations can be made. First, both the linear Hookean and hyper-elastic models provide reasonable accuracy for small deformations $0 \leq \kappa(t) \leq 3$ with a RMS error of ± 0.13 and ± 0.16 in curvature, respectively. However, as deformations exceed the linear regime, the hyper-elastic model significantly outperforms the Hookean model. Focusing on the hyper-elastic model, both the asymmetric stiffness in radial direction and the strain-hardening are captured well, where the linear models are not sufficiently rich to capture the material effects. The overall RMS errors for the linear and hyper-elastic model are ± 1.79 and ± 0.21 in curvature, respectively. Regarding the end-effector accuracy, the overall RMS errors for the linear and hyper-elastic model are ± 2.58 and ± 0.65 mm, respectively; which translates to an arc-length normalized error of $\pm 4.09\%$ and $\pm 1.03\%$. These numerical comparison results show that introducing nonlinear elastic effects driven by FEM-data can further improve the accuracy for a larger region of the soft robot's workspace.

For the last validation case, we subject the soft robot to an external payload

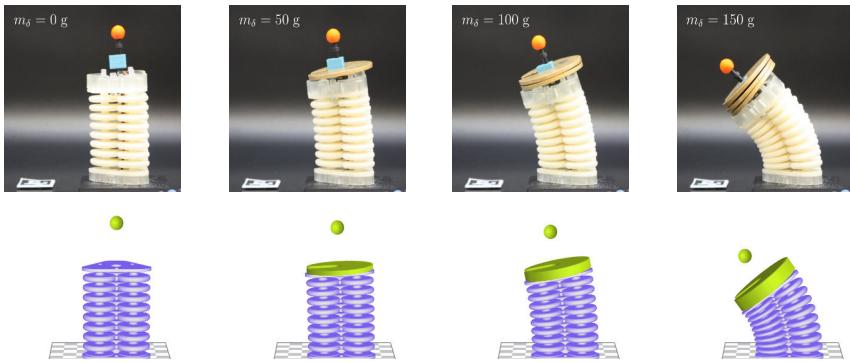


Figure 4.18. Experimental validation of the one-link soft robot subjected to various end-effector payloads of different mass $m_\delta = \{0, 50, 100, 150\}$ g. The deformed 3D-model in (■) corresponds to the estimated joint configuration based on the measurements from the IMU and depth camera, where the optimal marker location is shown in (●).

of mass δ_m located at the end-effector. To model the disturbance, we use the expression for the external payload disturbance model δ_m in (4.26). The goal here is *a)* to demonstrate the accuracy of the proposed payload model and quasi-static behavior of the dynamic model, and *b)* to highlight the limitations of the PCC assumptions under certain conditions. In this analysis, we consider three different payloads $m_\delta = \{0, 50, 100, 150\}$ g. The experimental results of the payloads deformations and the resulting quasi-static deformations of the dynamic model are shown in Figure 4.18.

As can be seen, the quasi-static behavior of the dynamic model matches the experimental results relatively well for smaller payloads. For the mass $m_\delta = 0.05$ kg, the Euclidean error between the model and the measurement are ± 1.31 mm. Increasing the payload to $m_\delta = 0.1$ kg leads to an error of ± 2.15 mm. We can also clearly observe that the estimate of the backbone curve subject to the PCC condition is beginning to deviate from the ground truth yet the overall shape still matches the experimental data. Lastly, by further increase the payload $m_\delta = 0.15$ kg, we clearly observe the limitations of the PCC condition under external loads – with an end-effector error of 3.98 mm. Also, there is a clear discrepancy in the backbone curve of the model and the ground truth, which might imply the PCC condition is no longer valid here as the payload could induce non-constant curvatures along the backbone. A possible solution might be to introduce a different shape parametrization, similar to the works [29, 52, 72, 221].

Model benchmark – Multi-link soft manipulator case: In this section, we benchmark the proposed numerical integration scheme for a dynamic model of a six-link soft robot manipulator ($N = 6$). Here, we want to highlight that sufficient numerical speed can be obtained while preserving sufficient numerical

precision. This is an important criteria for model-based control, as slow numerical models lack transferability from theory to application. As mentioned earlier, the numerical integration of the Lagrangian entities is the computational bottleneck. Although the MDE solver does aid with numerical performance; ultimately, using a balanced spatial and temporal discretization impacts real-time performance the most. Trivially, using larger stepsize – both in space and time – lead to a decrease in numerical precision; and in some cases numerical instability. In this benchmark, we investigate these effects by varying two solver parameters: the spatial stepsize of the explicit MDE solver denoted by $\Delta\sigma$ and the temporal stepsize of the implicit trapezoidal solver denoted by Δt . For convenience, we represent these stepsizes as standardized parameters: the number of finite elements $N_s = L/\Delta\sigma$ and the implicit solver frequency $f_s = \Delta t^{-1}$. For the benchmark, we choose a total length of $L = 0.15$ m and simulation time of $T = 10$ s.

The extension to the multi-link soft robot ($N = 6$) can be described by a following generalized coordinates with the following structure:

$$\mathbf{q} = (\varepsilon_1, \kappa_{x,1}, \kappa_{y,1}, \dots, \varepsilon_6, \kappa_{x,6}, \kappa_{y,6})^\top \in \mathcal{Q} \quad (4.57)$$

To ensure the soft manipulator is self-supporting, we introduce slight variations to the hyper-elastic stiffness, link lengths, and the inertial properties of the dynamical system. Considering homogeneity, all links are chosen identical in length and mass: intrinsic link length $L_i = 0.025$ m and mass $m_i = 0.05$ kg. Next, the bending stiffness is slightly altered where we choose $\alpha_3 = 0.425$ Nm/rad and $\alpha_4 = 0.4$ Nm/rad. Please note that the material domain is now given by $\mathbb{X} = [0, \sum_{i=1}^N L_i]$. To introduce some interesting dynamics for the benchmark, we purely excite the first link of the serial-chain soft robot manipulator with a harmonic input:

$$u_i(t) = \begin{cases} P_a \cos(\pi t) & \text{for } i = 1, \\ 0 & \text{otherwise,} \end{cases} \quad (4.58)$$

where $P_a = 125$ kPa is the pressure amplitude. As for the pneumatic mapping that converts pressure to joint torques, we choose $\boldsymbol{\tau} = (\mathbf{G} \otimes \mathbf{I}_6) \mathbf{u}$ as the corresponding pneumatic map for the six-link soft manipulator. In total 36 benchmark simulations with different solver settings were performed and tested for their precision relative to a high-precision model ($f_s = 500$ Hz and $N_s = 500$). The state trajectories of the high-precision model are shown in Figure 4.19, whereas Figure 4.20 is provided to highlight the underlying dynamics and the trajectory of the end-effector. The results for all benchmark simulations are shown in Table 4.2.

Let us first discuss the dynamics of the six-link soft manipulator subjected to a harmonic input. Given this relatively straightforward harmonic excitation, some interesting (stable) nonlinear dynamics appear. Although we excite the system using one harmonic, the dynamics of the soft robot show a rich collection of harmonic oscillations – highlighting its nonlinear nature.

Remark 4.6 After a short transient time (i.e., $t < 5$), the solutions of the multi-link soft robotic system tend to a so-called periodic solution. Here, a solution is

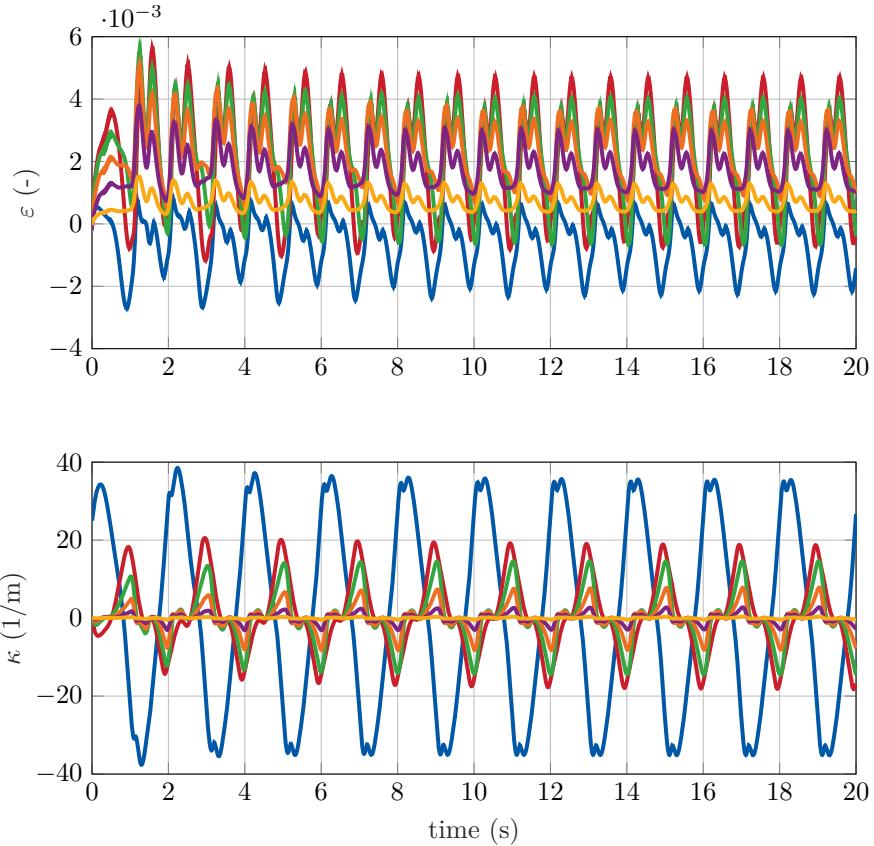


Figure 4.19. State trajectories of six-link soft robot model under dynamic excitation. The figure shows the extensible elongation strains and the total curvature κ (i.e., planar dynamics). The link indexing follows (—, —, —, —, —, —).

called periodic if there exists a period time $T_c > 0$ such that $\mathbf{q}(t) = \mathbf{q}(t + T_c)$ for all time t . Similar observations of the existence of periodic solutions (and control of such oscillations) were reported by Della Santina et al. [70] for articulated soft robots. Given the harmonic excitation in (4.58), the period time here is $T_c = 1$.

Now, we can exploit these periodic solutions for benchmarking the numerical solver in which we compare the solution of a high-resolution model (i.e., ground truth) to the benchmark solution. Let us define the benchmark error as the Euclidean distance between the two periodic solutions:

$$\begin{aligned} e &= \int_0^{T_c} \left\| \tilde{\gamma}(L, \tilde{\mathbf{q}}(t)) - \gamma(L, \mathbf{q}(t)) \right\|_2 dt, \\ &\approx \frac{1}{W} \sum_{i=1}^W \left\| \tilde{\gamma}(L, \tilde{\mathbf{q}}(t_i)) - \gamma(L, \mathbf{q}(t_i)) \right\|_2, \end{aligned} \quad (4.59)$$

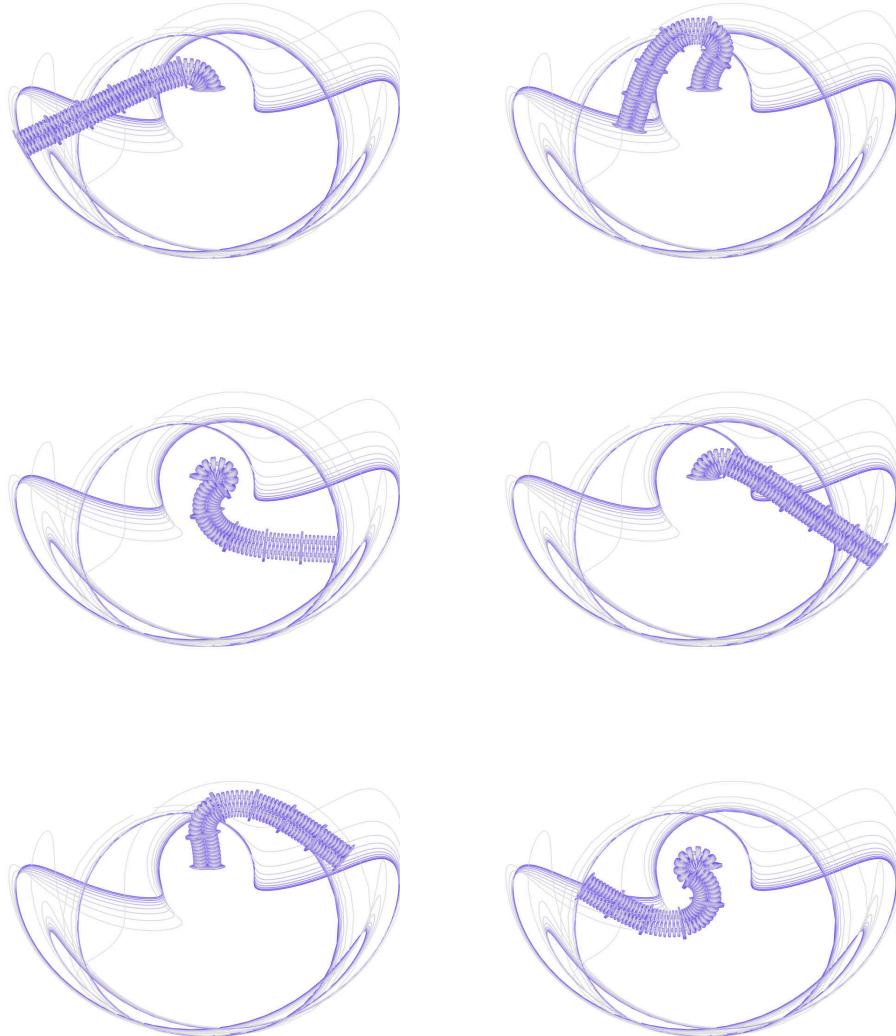


Figure 4.20. The deformed 3D-model of the six-link soft robot according to the input excitation \mathbf{u} . Notice that the dynamics of the six-link robot converge to a periodic solution which is shown in curve (—). Interestingly, the periodic orbit is slightly asymmetric with respect the sagittal plane at the origin, which is caused by the *hanging-down* initialization of the soft arm at the left side.

where W is the number of time samples of the benchmark model inside the time interval of the periodic solution, and $\tilde{\gamma}(\cdot, L)$ and $\gamma(\cdot, L)$ the tip position of the benchmark and the ground truth, respectively. The index W naturally depends on the sampling frequency of the implicit solver. Table 4.2 shows the normalized errors (i.e., the tracking error e normalized with the manipulator length L) together with the effective computation times of the numerical solver.

The benchmark table above gives some useful insight into which settings benefit numerical precision and speed the most. First, regarding the coarser models $N = 24$ (i.e., 4 elements per link), we observe large numerical errors of $> 10\%$ independent of solver frequency. Although one could argue these settings guarantee real-time performance (2s of simulation time for 1s computation at $N_s = 24$, $f_s = 75$ Hz) and might suffice for model-based control in slow settings (i.e., set-point stabilization), they are most likely unsuited for dynamic tracking objectives. Moving towards $N_s = 60$ (i.e., 10 elements per link), we observe a significant improvement in numerical precision $\pm 4\%$ and while still retaining real-time performance (1.6s of simulation time for 1s computation time at $f_s = 50$ Hz). As such, these settings show that both numerical precision and real-time computation can be achieved for more complicated multi-links soft robots. However, regarding the high-accuracy models $N_s > 100$, we see only a slight increase in numerical precision $\pm 3\%$ yet lose real-time capabilities. Consequently, these models might be suited for offline simulations, but lack transferability to online model-based control. However, a possible solution here might be to convert the MATLAB model into a C or C++ equivalent model to further increase numerical speed [102, 231].

Closed-loop – Passivity-based controller under material certainty and mass disturbance: In the last numerical analysis, we demonstrate the results of the proposed passivity-based adaptive scheme. Due to its compactness and computational speed, we again consider the model of the one-link soft robot as seen in previous simulations. To illustrate the robustness of the controller, we purposely introduce some uncertainties. First, we introduce uncertainties in the hyper-elastic material parameters that deviate moderately from their true values in Table 1. Second, we introduce a payload to the end-effector of mass $m_\delta = 0.1$ kg. We again model this external disturbance using the relation in (4.26). Following the linear parametrizability of the uncertainties, the parameter estimation vector yields:

$$\tilde{\pi}(t) = (\tilde{\alpha}_1, \tilde{\alpha}_2, \tilde{\alpha}_4, \tilde{\alpha}_5, \tilde{m}_\delta)^\top, \quad (4.60)$$

with initial conditions $\tilde{\pi}(t_0) = \tilde{\pi}_0 = (0.75\alpha_1, 0.75\alpha_2, 0.45\alpha_4, 0.45\alpha_5, 0.65m_\delta)^\top$. Furthermore, the feedback gains and the adaptation rate are chosen as diagonal matrices as follows:

$$\mathbf{K}_p = \begin{pmatrix} 5 & 0 & 0 \\ 0 & 5 \cdot 10^{-5} & 0 \\ 0 & 0 & 5 \cdot 10^{-5} \end{pmatrix}, \quad \mathbf{K}_d = \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 \cdot 10^{-5} & 0 \\ 0 & 0 & 1 \cdot 10^{-5} \end{pmatrix},$$

Table 4.2. Benchmark results of the six-link soft robot manipulator for various temporal and spatial discretizations ($T = 10$ s). The tables shows the mean tracking error of the end-effector relative to a ground truth ($f_s = 500$ Hz and $N_s = 500$ elements). The RMS errors are normalized with the total length $L = 0.15$ (i.e., the errors are presented in %). The CPU times are also given, where the entries labelled (✓) achieve real-time computation (consistently).

	$T = 10$ s	$N_s = 24$	$N_s = 36$	$N_s = 60$	$N_s = 90$	$N_s = 120$	$N_s = 180$
$f_s = 25$ Hz	19.03% / 1.77s (✓)	9.37% / 2.54s (✓)	5.36% / 4.06s (✓)	4.63% / 5.98s (✓)	4.62% / 7.93s (✓)	4.43% / 11.75s	
$f_s = 50$ Hz	17.51% / 3.50s (✓)	7.04% / 5.04s (✓)	4.33% / 6.73s (✓)	3.69% / 11.60s	3.60% / 15.3s	3.69% / 22.71s	
$f_s = 75$ Hz	13.77% / 5.31s (✓)	5.80% / 7.56s (✓)	4.51% / 12.41s	4.22% / 17.49s	3.68% / 22.35s	3.72% / 33.33s	
$f_s = 100$ Hz	14.73% / 6.48s (✓)	6.12% / 9.10s (✓)	4.42% / 14.54s	3.71% / 21.46s	3.53% / 28.35s	2.89% / 42.03s	
$f_s = 150$ Hz	15.22% / 7.26s (✓)	5.73% / 9.78s (✓)	4.32% / 15.58s	3.46% / 23.07s	3.16% / 30.38s	2.67% / 45.06s	
$f_s = 250$ Hz	14.61% / 11.98s	5.32% / 16.71s	4.14% / 27.11s	3.35% / 40.19s	2.86% / 53.06s	2.21% / 78.61s	

$$\mathbf{K}_\pi = \begin{pmatrix} 5 \cdot 10^3 & 0 & 0 \\ 0 & 2 \cdot 10^{-6} & 0 \\ 0 & 0 & 2 \cdot 10^{-6} \end{pmatrix};$$

and $\mathbf{\Lambda} = \mathbf{I}$. These values were found to yield the best performance while avoiding noticeable oscillations in the closed-loop dynamics. In this controller gain tuning process, we first find suitable values for \mathbf{K}_p and \mathbf{K}_d such that controller stabilizes the closed-loop and the error transients are within acceptable time windows (e.g., converge within < 5 s). During this process, the adaption gain is chosen zero. Once \mathbf{K}_p and \mathbf{K}_d are found, we slowly increase the adaptation gain. Again, we observe the transients of the parameter estimates. During the tuning of the adaptive controller, it was observed that a high-gain \mathbf{K}_π diminishes performance. Better convergence was found for low adaption gains – resulting in slowly-varying parameter estimates. Lastly, the following reference trajectory is considered:

$$\mathbf{q}_d(t) = (0.01 + 0.01 \sin(t), 30 \sin(t), 30 \cos(t))^\top, \quad (4.61)$$

Since the reference trajectory above satisfies persistence of excitation (see Remark 4.5), it should grantee the all convergence of the hyper-elastic material estimation and the unknown mass contribution. Figure 4.21 shows the state trajectories of the soft robot, and Figure 4.22 shows the evolution of the nonlinear stiffnesses estimates, $\tilde{k}_e(\mathbf{q}, \tilde{\boldsymbol{\pi}})$ and $\tilde{k}_b(\mathbf{q}, \tilde{\boldsymbol{\pi}})$, respectively; and the payload estimate \hat{m}_δ .

As can be seen in Figure 4.21 and 4.22, the passivity-based controller offers good performance in the face of material uncertainties and external disturbances. The RMS tracking error in steady-state (*i.e.*, $t \geq 30$ s) between the desired end-effector trajectory and true trajectory is ± 0.77 mm; which translates to an arc-length normalized error of $\pm 1.22\%$. Despite the presence of uncertainties, the passivity-based controller also ensures the states converges to the desired trajectory with a smooth transient. Regarding the results of Figure 9, the (nonlinear) stiffness estimates $k_e(\mathbf{q}, \tilde{\boldsymbol{\pi}})$ and $k_b(\mathbf{q}, \tilde{\boldsymbol{\pi}})$, and the unknown payload mass \hat{m}_δ slowly converge to the their true values. It should be mentioned that increasing the adaption rate leads to undesired (but bounded) oscillations of the estimates rather than faster convergences, therefore negatively affects the controller’s performance.

4.10 Conclusion

In this chapter, we aimed to reduce the gap between modeling and control-oriented research in soft robotics. First, the dynamic models that describe the continuum-bodied motions need to be sufficiently accurate, and second the model must retain real-time performance to be applicable in control. By building upon the existing PCC models, we express the continuum deformation using a minimal set of coordinates related to the differential geometry of spatial curves; and explored FEM-based data to model the hyper-elasticity. To retain numerical efficiency, a reduced-order integration scheme is developed that efficiently computes the entries of the Lagrangian model through a Matrix-Differential equation; resulting in

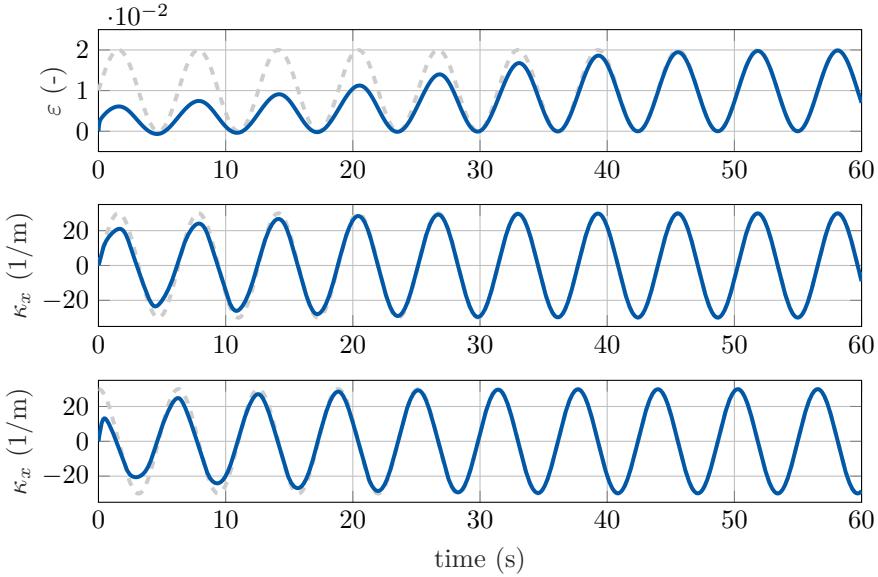


Figure 4.21. State trajectories of soft robot with the passivity-based adaptive controller in (4.54). The figure shows the elongation strain $\varepsilon(t)$ and the curvatures $\kappa_x(t)$, $\kappa_y(t)$ in the xz -plane and yz -plane, respectively; where (—) shows the reference trajectory of the joint configuration \mathbf{q}_d .

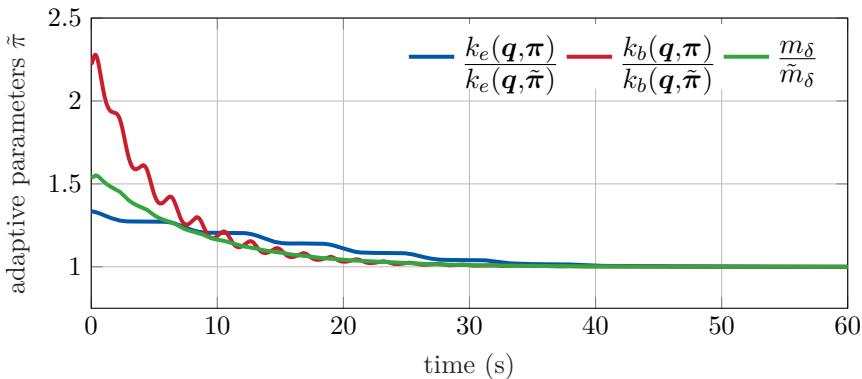


Figure 4.22. The evolution of the elongation stiffness estimate and bending stiffness estimate, $k_e(\mathbf{q}, \tilde{\boldsymbol{\pi}})$ and $k_b(\mathbf{q}, \tilde{\boldsymbol{\pi}})$ respectively; and the estimate of the payload \tilde{m}_δ . For illustration, the estimates are normalized with their true value, where we can see they slowly approach one after sufficient time passes. This implies the adaptive algorithms converges to the true hyper-elastic stiffness values independent of parameter uncertainties.

a continuum dynamical model for soft manipulators with real-time capabilities at minimal lost in numerical precision.

The dynamic model has been extensively analyzed through simulations and experimental results. Not only does the dynamic models allow for real-time simulations with systems with various degrees of motion, it show good correspondence with the true physical soft robot. Furthermore, a passivity-based adaptive controller is proposed that provides good tracking performance even in the face of parameter uncertainties. The adaptive controller enables online estimation of the hyper-elastic stiffness and external loads, which further enhances the robustness toward modeling uncertainty undoubtedly present in soft robotics. In future work, we wish to further explore FEM-driven data for the parametrization of the spatial shape functions – extending beyond constant-curvature, and employ the proposed controller methods to multi-link soft robots.

5

Port-Hamiltonian Cosserat models for soft robots – beyond the constant strain approach

Abstract - This chapter addresses some of the limitations of the previously presented *Piecewise-Constant-Curvature* (PCC) model in Chapter 4, in particular when infinite-dimensionality of the soft robot's deformable body is assumed. The continuous dynamics of the soft robot are modeled through the differential geometry of Cosserat beams. Using a finite-dimensional truncation, the infinite-dimensional system can be written as a reduced-order port-Hamiltonian (pH) model that preserves desirable passivity conditions. Contrary to prior PCC models, a wide variety of spatial discretizations can be explored that better respect the spatial continuity and continuum mechanics present in soft robots. Given the pH model structure, we derive a stabilizing controller rooted in energy-based techniques and exploits the passivity of the soft robotic system. The model-based controller derived from the reduced Cosserat model produces a local minimizer of closed-loop potential energy that steers end-effector towards a desired configuration. Furthermore, we propose an alternative geodesic setpoint description inspired by the octopus' morphology. We show that stereotypical motions, such as bending wave propagation, can also be achieved via our proposed control scheme with a striking resemblance to its biological counterpart. The effectiveness of the controller is demonstrated through extensive simulations of various soft manipulators.

5.1 Introduction

The field of soft robotics is slowly growing as a well-recognized research discipline aimed at developing highly compliant bio-inspired robot. Contrary to rigid robots, soft robots explore ‘*soft materials*’ that significantly enhance the robot’s dexterity, inherent safety, enable a rich family of motion primitives, and provide environmental robustness. By fully exploiting soft materials, soft robotics places the first steps towards achieving performance similar to biology [53, 78, 175]. In this work, we primarily focus on a subclass of soft robots called ‘*soft manipulators*’.

Although significant steps have been taken towards bridging biology and soft robotics, the innate infinite-dimensionality of soft robot models poses substantial challenges on the applicability of model-based control. To be more specific, when considering the soft body’s deformation as a state of the system, soft robots theoretical have infinitely many degrees-of-freedom along their continuously deformable body. For this reason, their models are often better suited for a PDE description [75, 154, 312], for example the mass and momentum balance equations, rather than the conventional ODE that are so common to traditional robotics [197, 256]. Additionally, their actuation often employs distributed loads (e.g., pneumatics [78, 175] and tendons [284, 312]). Consequently, classical descriptions of rigid links and joints paired with local actuation are no longer viable nor physically representative. This paradigm shift calls for novel control-oriented modeling approaches tailored for hyper-flexible and under-actuated robots.

In the last decade, the field of modeling for soft robotic systems has matured sufficiently and currently their applicability in model-based control is slowly feasible [70]. To highlight a few modeling approaches: reduced-order finite element models [75, 312, 324], constant and non-constant curvature approaches [72, 135], Cosserat-beam models [29, 221], and learning-based approaches [34]. Recalling Chapter 4, a popular method of state reduction is the *Piece-wise Constant Strain* (PCS) model that assumes piecewise constant strains along the soft robot’s body. Such assumption has proven to be remarkably reliable in solving the dimensionality issue. *Piece-wise Constant Curvature* (PCC) is a subclass of the PCS assumption. Models following either the PCC or PCS assumption have shown successful implementation in feed-forward controllers [78], and more recently model-based feedback controllers [72, 135]. Nevertheless, the PCC assumption has (severe) limitations. It does not properly reflect the continuum mechanics and thus it is only applicable in restrictive settings. Although computationally performance might surpass continuous models, due to intrinsic kinematic restrictions, these models are unable to capture important continuum phenomena, like buckling, environmental interaction, or wave propagation.

On the contrary, Cosserat beam-models have shown to capture a wide range of continuum deformations. Cosserat models originate from a continuum mechanical PDE description and thus allow a more accurate description of the hyper-flexible nature under large deformations. The computational dynamics of Cosserat beams have been extensively developed by [242] through Geometrically-Exact finite el-

ements on the Lie group $\text{SE}(3)$; and recently, these models are slowly gaining popularity in the soft robotics community [29, 95, 221, 222, 284]. Ultimately, the strong nonlinearities paired with the diligence to achieve biological morphologies in robotics encourages the use of Cosserat models for control. Yet, compared to the abundance of PCC soft robotic models, literature on model-based control is scarce.

In this chapter, we aim to highlight the capabilities of Cosserat models for model-based control, in particular energy-based strategies. To this end, a finite-dimensional modeling approach is proposed such that the continuous dynamics can be cast into a port-Hamiltonian (pH) structure. The Lagrangian modeling framework is adopted from [29] and [221], but modified to suit a pH-structure. The main advantage of pH systems is the common formalism with energy-based control. Through the pH structure, we propose an energy-shaping control law that ensures stabilization of the end-effector of the soft robot. Similar energy-based control strategies can be found in [87, 203, 204, 291] for rigid-body systems. As a study case, we consider a soft robot manipulator inspired by an octopus tentacle. With the ability to deform continuously and its distributed muscular system, it is ideal for illustrating the complex morphological motions present in soft robotics. Again, all code is made publicly available under the `Sorotoki` toolkit on [36], which builds upon previous work Caasenbrood et al. [39] that is presented in Chapter 6 of the thesis.

The chapter is organized as follows. Section 5.2 will detail a modeling approach for a general class of soft robot manipulators, starting with the Cosserat-beam theory. In Section 5.3, we propose an energy-shaping control strategy. Lastly, we show the effectiveness of energy-based controller through numerical simulation in Section 5.4, followed by a brief conclusion in Section 5.7.

5.2 Generalized models for soft manipulators

In this chapter, we will explore Lie group theory applied to deformable robots. We have introduced some of notations earlier in Chapter 4, but for convenience, we briefly recapitulate this here. The Lie group of rigid-body transformation on \mathbb{R}^3 is denoted by $\text{SE}(3)$. The group of homogeneous rotation is denoted by $\text{SO}(3)$. The tangent space at the identity of the group is called its *Lie algebra*, and it can be used to describe the evolution of the Lie group. The Lie algebras of $\text{SE}(3)$ and $\text{SO}(3)$ are denoted by $\text{se}(3)$ and $\text{so}(3)$, respectively. Lastly, the cross operator (*i.e.*, " \times ") and hat operator (*i.e.*, " \wedge ") are used to transform a column vector of \mathbb{R}^3 or \mathbb{R}^6 into an element of the Lie algebra $\text{so}(3)$ or $\text{se}(3)$, respectively. A comprehensive introduction is given in Appendix D.1 based on the work of Murray et al. [197].

5.2.1 Preliminaries on geometric Cosserat theory

In Cosserat theory, slender deformable solids are modeled as elastic strings subjected to geometric finite-strain theory. Drawing the analogy to soft robotics, we

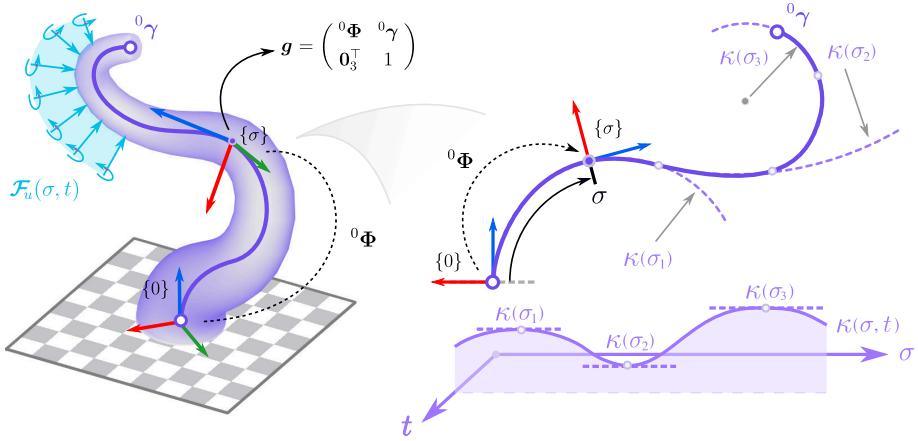


Figure 5.1. Schematic representation of the continuously variable Cosserat beam model for a general class of soft manipulators, given by a backbone curve γ and orientation matrix Φ relative to a base frame at $\{0\}$. Together they form a parameterized curve $\mathbf{g}(\sigma, t) = (\Phi(\sigma, t), \gamma(\sigma, t)) \in \text{SE}(3)$. The representation of the soft robot is inspired by the octopus' tentacle whose the muscle forces are modeled as a distributed input \mathcal{F}_u .

model the soft robot as a one-dimensional spatial curve passing through the geometric center of the soft robot (see Figure 5.1). Given its spatial-temporal nature, we introduce a temporal variable $t \in [0, +\infty)$, and a spatial variable $\sigma \in [0, L]$ with L the undeformed length of the soft robot. For each point on the backbone, we introduce a (mobile) coordinate frame. The homogeneous rotation related to these coordinate frames is given by the rotation matrix $\Phi : [0, L] \times [0, +\infty) \rightarrow \text{SO}(3)$, and their origin by the position vector $\gamma : [0, L] \times [0, +\infty) \rightarrow \mathbb{R}^3$. For convenience and readability, we will denote the temporal and spatial domains as $\mathbb{T} = [0, +\infty)$ and $\mathbb{X} = [0, L]$, respectively.

Following the geometric approach [29, 30, 221, 222, 242], we may equivalently represent each coordinate frames that are rigidly attached to the continuous backbone of the soft robot by a parameterized space curve in $\text{SE}(3)$:

$$\mathbf{g}(\sigma, t) = \begin{pmatrix} \Phi(\sigma, t) & \gamma(\sigma, t) \\ \mathbf{0}_3^\top & 1 \end{pmatrix} \in \text{SE}(3). \quad (5.1)$$

An important notion in Lie group theory applied to robotics is the so-called "*exponential coordinate representation*". Conventionally, for rigid multi-body mechanics, any rigid-body transformation from one coordinate frame into another can characterized by a vector living in \mathbb{R}^6 , called the *twist*, whose six entries are referred to as the exponential coordinates. Three of these exponential coordinates are related to the translation and the other three to orientation. As such, the same principle applies to rigid-body rotations described by matrices in $\text{SO}(3)$ that can be parameterized by three exponential coordinates. For example, we may express a general rotation in terms of its exponential coordinates

$\mathbf{R}(\boldsymbol{\Omega}, t) = \exp(\boldsymbol{\Omega}^\times t)$ where $\boldsymbol{\Omega}^\times \in \text{so}(3)$ is a skew-symmetric matrix with its three unique entries $\boldsymbol{\Omega} = (\omega_1, \omega_2, \omega_3)^\top$ being the unit-time angular velocities. Recall that the superscript denotes the skew-symmetric matrix operator $(\cdot)^\times : \mathbb{R}^3 \rightarrow \text{so}(3)$.

Since soft robot models are expressed in spatial and temporal coordinates, we aim to seek two exponential coordinate descriptions – a spatial (strain) twist $\boldsymbol{\xi}$ called the geometric strain, and a temporal (velocity) twist $\boldsymbol{\eta}$ called the geometric velocity. The expressions for the strain field $\boldsymbol{\xi}$ and velocity field $\boldsymbol{\eta}$ anywhere on the Cosserat beam can be found by exploring the differential geometry of the curve \mathbf{g} . To do so, we must introduce some smoothness conditions.

Assumption 5.1 (Distributed actuation and body loads) In this study, we assume any control input of the continuum robot can be represented by a distributed input force $\mathbf{n}_u : \mathbb{X} \times \mathbb{T} \rightarrow \mathbb{R}^3$ and distributed input moment $\mathbf{m}_u : \mathbb{X} \times \mathbb{T} \rightarrow \mathbb{R}^3$, which act upon the deformable backbone \mathbf{g} . These inputs are conveniently collected into a vector $\mathcal{F}_u = (\mathbf{m}_u^\top, \mathbf{n}_u^\top)^\top$ referred to as the "*control wrench*". It is important to note that the modeling of distributed input wrenches encompasses various forms of soft actuation, such as pneumatics, hydraulics, tendons, and ferro-magnetic and thermo-mechanical actuation. Similarly, we also introduce a distributed body-load force (*e.g.*, due to gravity) given by $\mathcal{F}_b = (\mathbf{0}_3, \mathbf{n}_b^\top)^\top$ where $\mathbf{n}_b = -\rho_0 A_0 \Phi^\top \mathbf{a}_b$ with \mathbf{a}_b a body acceleration, ρ_0 the density, and A_0 the cross-sectional area. Both \mathcal{F}_u and \mathcal{F}_g are wrenches expresses in the body frame whose direction depends on the body configuration \mathbf{g} .

Assumption 5.2 (On differentiability) Any external distributed force acting on the continuum time-variant backbone curve (5.1) is considered to be sufficiently smooth as a function of t and σ such that parametrized backbone $\mathbf{g}(\sigma, t) \in \text{SE}(3)$ is differentiable everywhere on \mathbb{X} and \mathbb{T} .

5.2.2 Local strain and velocity

Following the Cosserat beam modeling approach from Simo et al. [242], Boyer et al. [29], Renda et al. [221, 222], let $\boldsymbol{\Gamma} = (\kappa_1, \kappa_2, \kappa_3)^\top$ and $\mathbf{U} = (\nu_1, \nu_2, \nu_3)^\top$ be the torsion-curvature and elongation-shear strain vector, respectively. First, the spaces $\text{se}(3)$ and \mathbb{R}^6 are isomorphic (*i.e.*, structure preserving) and we denote the mapping between these spaces is called the "*isomorphism*" by $(\hat{\cdot}) : \mathbb{R}^6 \rightarrow \text{se}(3)$ and its inverse $(\check{\cdot}) : \text{se}(3) \rightarrow \mathbb{R}^6$. Then, an expression for strain field $\boldsymbol{\xi}(\sigma, t)$ is obtained through spatial differentiation of \mathbf{g} :

$$\hat{\boldsymbol{\xi}} := \mathbf{g}^{-1} \frac{\partial \mathbf{g}}{\partial \sigma} = \begin{pmatrix} \boldsymbol{\Gamma}^\times & \mathbf{U} \\ \mathbf{0}_3^\top & 0 \end{pmatrix} \xrightarrow{\text{isomorphism}} \boldsymbol{\xi} := \begin{pmatrix} \boldsymbol{\Gamma} \\ \mathbf{U} \end{pmatrix}. \quad (5.2)$$

Note the difference between $\hat{\boldsymbol{\xi}}$ and $\boldsymbol{\xi}$ in (5.2), being a matrix element of $\text{se}(3)$ and column vector of \mathbb{R}^6 , respectively.

Following, the temporal exponential coordinates are given by $\boldsymbol{\Omega} = (\omega_1, \omega_2, \omega_3)^\top$ and $\mathbf{V} = (v_1, v_2, v_3)^\top$ that denote the angular and linear velocity vector, respectively. Then, an expression for velocity field $\boldsymbol{\eta}(\sigma, t)$ is obtained through time

differentiation of \mathbf{g} :

$$\hat{\boldsymbol{\eta}} := \mathbf{g}^{-1} \frac{\partial \mathbf{g}}{\partial t} = \begin{pmatrix} \boldsymbol{\Omega}^\times & \mathbf{V} \\ \mathbf{0}_3^\top & 0 \end{pmatrix} \xrightarrow{\text{isomorphism}} \boldsymbol{\eta} := \begin{pmatrix} \boldsymbol{\Omega} \\ \mathbf{V} \end{pmatrix}. \quad (5.3)$$

Let it be clear that $\boldsymbol{\xi}(\sigma, t)$ and $\boldsymbol{\eta}(\sigma, t)$ are yet unknown vector fields, they simply follow from the differential geometry of SE(3). As such, they live in its tangent space se(3) called its Lie algebra. Now given the geometric structures in (5.2) and (5.3), we can start detailing the forward kinematics of the soft continuum robot by exploring the differential geometry of the spatio-temporal manifold $\mathbf{g}(\sigma, t)$. Their connection is described in detail in [29, 30, 222, 223, 242], but briefly recapitulated here to be self-contained.

Recalling Assumption 5.2, which assumes the configuration space \mathbf{g} to be everywhere differentiable, we can introduce the equality of mixed partials, *i.e.*, $\frac{\partial}{\partial t}(\frac{\partial \mathbf{g}}{\partial \sigma}) = \frac{\partial}{\partial \sigma}(\frac{\partial \mathbf{g}}{\partial t})$. Then, by substitution of $\frac{\partial \mathbf{g}}{\partial t} = \mathbf{g}\hat{\boldsymbol{\eta}}$ and $\frac{\partial \mathbf{g}}{\partial \sigma} = \mathbf{g}\hat{\boldsymbol{\xi}}$, we obtain the so-called *compatibility equation*:

$$\mathbf{g}\hat{\boldsymbol{\eta}}\hat{\boldsymbol{\xi}} + \mathbf{g}\frac{\partial\hat{\boldsymbol{\xi}}}{\partial t} = \mathbf{g}\hat{\boldsymbol{\xi}}\hat{\boldsymbol{\eta}} + \mathbf{g}\frac{\partial\hat{\boldsymbol{\eta}}}{\partial\sigma}, \quad (5.4)$$

The equality above ensures that the partial derivatives with respect to time and space are continuously connected on the manifold \mathbf{g} . Simply put, deformations that are tied to the spatial derivatives need to have continuous velocity profiles (*i.e.*, the temporal derivative) – and vice versa. Pre-multiplication of the expression above with $\mathbf{g}^{-1} \in \text{SE}(3)$ and rearranging the equality, we obtain

$$\frac{\partial\hat{\boldsymbol{\eta}}}{\partial\sigma} = -\left(\hat{\boldsymbol{\xi}}\hat{\boldsymbol{\eta}} - \hat{\boldsymbol{\eta}}\hat{\boldsymbol{\xi}}\right) + \dot{\hat{\boldsymbol{\xi}}}. \quad (5.5)$$

Focusing on the RHS term $(\hat{\boldsymbol{\xi}}\hat{\boldsymbol{\eta}} - \hat{\boldsymbol{\eta}}\hat{\boldsymbol{\xi}})$, we can recognize the Lie bracket or the commutator between the geometric vector fields $\boldsymbol{\xi}$ and $\boldsymbol{\eta}$ (see [197]). Since the Lie bracket $[\hat{\boldsymbol{\xi}}, \hat{\boldsymbol{\eta}}]$ itself also belongs to the Lie algebra se(3), which is isomorphic to \mathbb{R}^6 via the operator $\hat{\boldsymbol{\eta}} \rightarrow \boldsymbol{\eta}$, we can rewrite the expressions as follows

$$\frac{\partial\boldsymbol{\eta}}{\partial\sigma} = -\mathbf{ad}_{\boldsymbol{\xi}}\boldsymbol{\eta} + \dot{\boldsymbol{\xi}}, \quad (5.6)$$

where $\mathbf{ad}_{(.)} : \mathbb{R}^6 \rightarrow \mathbb{R}^{6 \times 6}$ defines the adjoint action on vectors belonging to the Lie algebra se(3). Drawing an analogy to rigid robotics, the expression in (5.6) may be seen as the forward velocity kinematics for a serial chain robot manipulator with infinitely many links. To that end, we can collect the PDEs (5.2), (5.6) and the time derivative of (5.6) (*i.e.*, the acceleration) into one global *Partial Matrix Differential Equation* (PMDE) that describes the full continuum-body kinematics of the soft deformable robotic body. The PMDE curve kinematics takes the form

$$\frac{\partial}{\partial\sigma} \left(\begin{bmatrix} \mathbf{g} \\ \mathbf{0} \end{bmatrix}, \boldsymbol{\eta}, \dot{\boldsymbol{\eta}} \right) = \left(\begin{bmatrix} \mathbf{g}\hat{\boldsymbol{\xi}} \\ \mathbf{0} \end{bmatrix}, -\mathbf{ad}_{\boldsymbol{\xi}}\boldsymbol{\eta} + \dot{\boldsymbol{\xi}}, -\mathbf{ad}_{\boldsymbol{\xi}}\dot{\boldsymbol{\eta}} - \mathbf{ad}_{\boldsymbol{\xi}}\boldsymbol{\eta} + \ddot{\boldsymbol{\xi}} \right) \quad (5.7)$$

which is a square differential matrix. For the general case, the boundary conditions of PDE in (5.7) should satisfy $\mathbf{g}(0, t) = \mathbf{g}_0$, $\boldsymbol{\eta}(0, t) = \boldsymbol{\eta}_0$ and $\dot{\boldsymbol{\eta}}(0, t) = \dot{\boldsymbol{\eta}}_0$. However, in case of a manipulator whose base is spatially fixed, the boundary conditions should satisfy $\mathbf{g}(0, t) = \mathbf{g}_0$, and $\boldsymbol{\eta}(0, t) = \dot{\boldsymbol{\eta}}(0, t) = \mathbf{0}_6$. An importance remark is that if the strain fields $\boldsymbol{\xi}$, $\dot{\boldsymbol{\xi}}$, and $\ddot{\boldsymbol{\xi}}$ are analytic such that we choose an instance $t \in [0, T]$ and keeping σ variable, the PMDE in (5.7) becomes an ordinary Matrix Differential Equation (MDE) which can be solved numerically using the techniques discussed in Chapter 4.

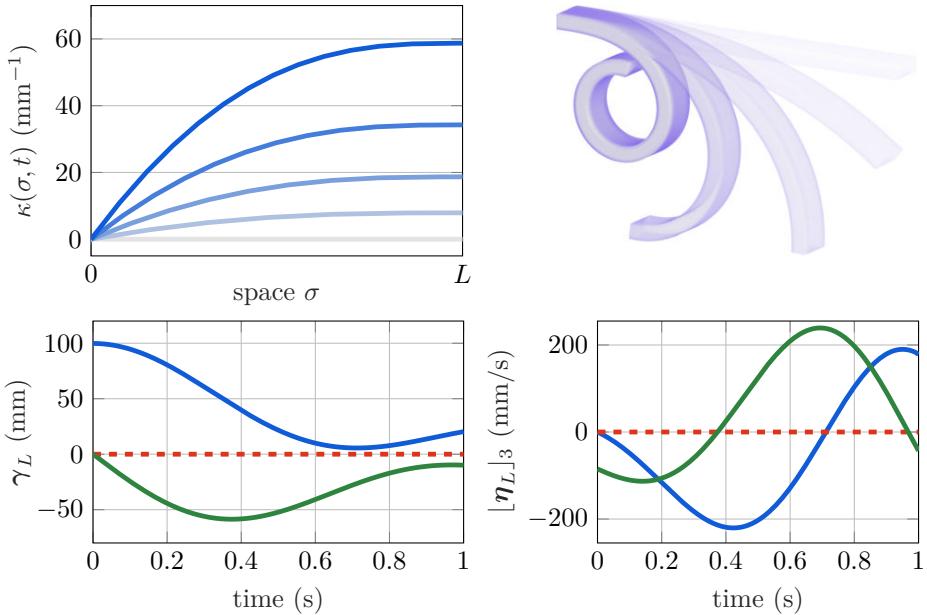
Example 5.1 (Kinematic behavior of variable strain soft segment). Let $\mathbb{X} = [0, L]$ with $L = 100$ mm and $\mathbb{T} = [0, T]$ with $T = 1$ s. Consider in this example a planar bending problem where the geometric strain vector takes the form $\boldsymbol{\xi} = (0, \kappa(\sigma, t), 0, 1, 0, 0)^\top$ with κ is an a priori known non-constant curvature profile. Inspired by the analytic solutions of the Euler-Bernoulli cantilever model [115], we propose an analytic expression for the planar curvature strain:

$$\kappa(\sigma, t) = \kappa_{\max} \theta(\sigma) h(t), \quad (5.8)$$

$$\theta(\sigma) = \sinh(\beta\sigma) + \sin(\beta\sigma) + \frac{\cos(\beta L) + \cosh(\beta L)}{\sin(\beta L) + \sinh(\beta L)} (\cos(\beta\sigma) - \mu \cosh(\beta\sigma)), \quad (5.9)$$

where $\kappa_{\max} = 60 \text{ mm}^{-1}$ is the curvature amplitude, $\theta(\sigma)$ the first strain eigenmode of the cantilever beam model, $h(t) = \frac{(1-k)t}{(1+k)-2k|t|}$ a transient modeled after a sigmoid function with $k = \frac{1}{2}$, and a parameter β which is the smallest positive real that satisfies the nonlinear equality $\cos(\beta L) \cosh(\beta L) = 1$. The physical interpretation β is the inverse wavelength thus it is inversely proportional to the beam length L . A numerical approximation of this value is $\beta \approx 0.597 \pi L^{-1}$. The strain velocity $\dot{\boldsymbol{\xi}}$ and strain acceleration $\ddot{\boldsymbol{\xi}}$ are obtained straightforwardly by differentiation of $\kappa(\sigma, t)$ with respect to time. Hence, we have explicit expressions on the strain, its velocity and acceleration. Therefore, we can evaluate $\mathbf{s}_i(\sigma) := \boldsymbol{\xi}(\sigma, t_i)$, $\mathbf{v}_i(\sigma) := \dot{\boldsymbol{\xi}}(\sigma, t_i)$, and $\mathbf{a}_i(\sigma) := \ddot{\boldsymbol{\xi}}(\sigma, t_i)$ for any time sample $t_i \in \mathbb{T}$.

Then, substitution of \mathbf{s}_i , \mathbf{v}_i and \mathbf{a}_i into (5.7) leads to an ordinary differential equation that depends exclusively on σ . The forward kinematics can then be solved for the spatial horizon $\mathbb{X} = [0, L]$ using an explicit integration routine (fourth order Runge Kutta method), which produces \mathbf{g} , $\boldsymbol{\eta}$ and $\dot{\boldsymbol{\eta}}$. We repeat this process until the full forward kinematics is recovered for all $t \in \mathbb{T}$. The results for the Euler-Bernoulli cantilever beam are shown in Figure 5.2. Figure 5.2 shows for $\kappa(\sigma, t)$ evolves over space and time, and how they relate to the continuum deformations. It also shows the position $\boldsymbol{\gamma}_L$ and the linear velocities $[\boldsymbol{\eta}]_3$ of the end-effector. Note that this approach can easily deal with non-constant curvature situations, in contrast to the approach discussed in Chapter 4. Namely, Chapter 4 subdivided the domain \mathbb{X} into small PCC segments leading to notorious discontinuities at the interfaces (see Figure 5.3).



5

Figure 5.2. Spatio-temporal evolution of the cantilever beam obtained by solving the exact continuum forward kinematics described in (5.7). The figure shows the forward kinematic solutions of the end-effector position $\gamma_L := \gamma(L)$ and its linear velocities $[\eta_L]_3 := [\eta(L)]_3$, where the following color coding is used $\{x, y, z\} = \{\text{blue}, \text{red}, \text{green}\}$.

5.2.3 Finite-dimensional projection

The problem is, however, that the exponential coordinates of the geometric strain vector belong (in theory) to an infinite set of real-valued functions. Similar to many continuum mechanics problems, the state dimension for such multi-variable coordinate representation are of infinite dimensional nature. To solve this, we must project our solution space onto a finite dimensional subset that is countable and therefore computable in this setting. In the finite element method, the solution presents itself by dividing the continuum into a finite set of elements. Here we follow an approach similar to Chirikjian et al. [48, 49] that proposed to express the spatial deformations of slender (semi-rigid) continuum robots by finite set of basis functions called *spatial modes*. This idea also finds application in disturbance rejection for structural vibration of semi-rigid flexible manipulators whose modeling strategies are identical the Euler-Bernoulli assumptions. Here though we introduce a modal approximation to find a suitable finite-dimensional approximation of the strain twist $\xi(\sigma, t)$ for all points along the material domain \mathbb{X} . To do so, we assume the following:

Assumption 5.3 Assuming the strain field has a separable spatio-temporal nature, any entry of the strain vector field $\xi = (\xi_1, \xi_2, \dots, \xi_6)^\top$ can be written as an

infinite expansion of the following form:

$$\xi_i(\sigma, t) = \sum_{n=1}^{\infty} \theta_n(\sigma) q_{i,n}(t) + \xi_i^o(\sigma) \quad i \in \{1, \dots, 6\}, \quad (5.10)$$

where $\{\theta_n\}_{n=1}^{\infty}$ is a set of (orthogonal) basis functions $\theta_n : \mathbb{X} \rightarrow \mathbb{R}$ together with modal coefficients $q_{i,n} : \mathbb{T} \rightarrow \mathbb{R}$, and an intrinsic time-invariant strain $\xi_i^o : \mathbb{X} \rightarrow \mathbb{R}$. The basis functions $\theta_n(\cdot)$ and modal coefficients $q_n(\cdot)$ are both smooth functions.

Assumption 5.4 Given infinite expansion (5.10), the k -th order truncation for any entry of the strain field, defined as

$$[\xi_i]_k(\sigma, t) := \sum_{n=1}^k \theta_n(\sigma) q_{i,n}(t) + \xi_i^o(\sigma) \quad i \in \{1, \dots, 6\}, \quad (5.11)$$

converges uniformly on \mathbb{X} and \mathbb{T} as the index $k \rightarrow \infty$. Moreover, we assume that uniform convergence holds for its partial derivatives $\frac{\partial}{\partial t} [\xi]_k$ and $\frac{\partial}{\partial \sigma} [\xi]_k$.

Accordingly, we can rewrite the k -th order truncation of the complete strain field as a linear matrix operation as follows

$$\begin{aligned} [\xi]_k &= (\mathbf{I}_6 \otimes [\theta_1 \ \dots \ \theta_k]) \mathbf{q} + \xi^o, \\ &= \underbrace{\begin{pmatrix} \theta_1 & \dots & \theta_k & \dots & 0 & \dots & 0 \\ \vdots & \ddots & \vdots & \ddots & \vdots & \vdots & \vdots \\ 0 & \dots & 0 & \dots & \theta_1 & \dots & \theta_k \end{pmatrix}}_{\Theta(\sigma)} \underbrace{\begin{pmatrix} q_{1,1} \\ \vdots \\ q_{6,k} \end{pmatrix}}_{\mathbf{q}(t)} + \xi^o, \end{aligned} \quad (5.12)$$

where $\Theta \in \mathbb{R}^{6 \times 6k}$ is a sparse matrix-valued function whose columns are mutually orthonormal, the operator \otimes denotes the Kronecker product, and the vector $\mathbf{q} \in \mathbb{R}^{6k}$ the collection of all time-varying modal coefficients related to the columns of Θ . Although a wide variety of bases are possible (see for instance [29, 72]), we have chosen a modified Legendre polynomial set:

$$\theta_n(\sigma) = \frac{2}{2^n(n-1)!} \frac{d^{n-1}}{d\sigma^{n-1}} \left[\left(\frac{2\sigma}{L} - 1 \right)^2 - 1 \right]^{n-1} \quad (5.13)$$

with $n \in \mathbb{Z}_{>0}$ the polynomial degree. A comparison between the proposed basis and previous method in Chapter 4 is shown in Figure 5.3. Important to note is that the previous PCC condition discussed introduces discontinuities in space that violate the compatibility equation in (5.4). Also note now that the inner product between elements of the set of modified Legendre functions $\{\theta_n\}_{n=1}^k$ satisfies $\langle \theta_i, \theta_j \rangle_{\mathbb{X}} := \int_{\mathbb{X}} \theta_i \theta_j d\sigma = 0$ for $i \neq j$, and 1 otherwise. An alternative option could be constructing the set of basis functions through the so-called '*snapshot decomposition method*' [14, 75, 154].

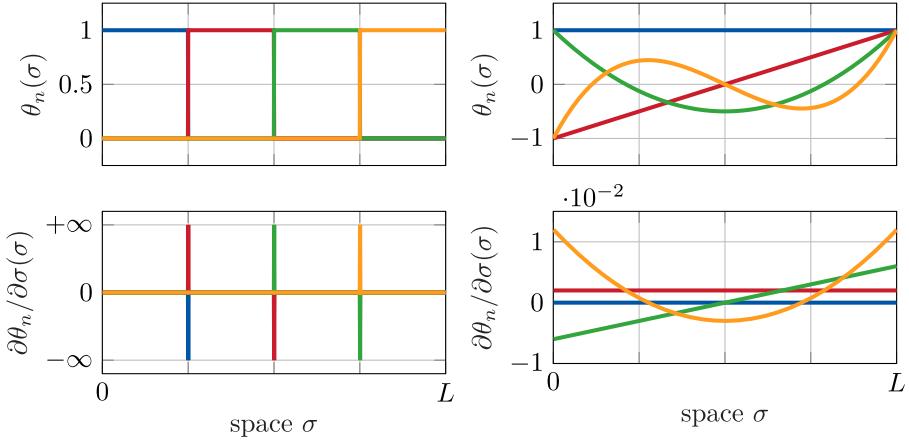


Figure 5.3. Example plot of the Constant-Strain parametrization in Chapter 3 (left), and the new strain parametrization (5.13) using Chebyshev polynomials (right). The ordering of the strain basis is as follows $\{\theta_1, \dots, \theta_4\} = \{\text{blue}, \text{red}, \text{green}, \text{orange}\}$. Notice that the spatial discontinuities in the PCC model induces spikes that directly violate the compatibility equation in (5.4).

5

5.2.4 Reduced-order kinematics

Given the finite-dimensional truncation in (5.12), we can now find an expression for the finite-dimensional forward kinematics in terms of the generalized coordinates \mathbf{q} and its velocities components $\dot{\mathbf{q}}$.

First, let us regard the configuration of the soft robot $\mathbf{g} \in \text{SE}(3)$. Recall that the spatial evolution of the curve is described by $\partial\mathbf{g}/\partial\sigma = \mathbf{g}\boldsymbol{\xi}^\wedge$, see (5.2). Given the initial condition $\mathbf{g}(0, \cdot) = \mathbf{g}_0$, an approximation of the continuously deformable soft robot can be obtained by partial integration over the spatial domain¹:

$$[\mathbf{g}]_k(\sigma, \mathbf{q}) = \mathbf{g}_0 \exp_{\text{SE}(3)} \left(\int_0^\sigma [\hat{\boldsymbol{\xi}}]_k(s, \mathbf{q}) ds \right). \quad (5.14)$$

The computation of the mapping $\exp_{\text{SE}(3)}$ is given in Appendix D.1. Note that the expression above nothing more than the reconstruction of the curve by integration of its tangent space along its spatial parameter σ . Next, we aim to find a solution for the velocity $\boldsymbol{\eta}$ related to non-homogeneous, linear, differential equation [222]:

$$\frac{\partial \boldsymbol{\eta}}{\partial \sigma} = -\mathbf{ad}_{\boldsymbol{\xi}} \boldsymbol{\eta} + \dot{\boldsymbol{\xi}}. \quad (5.15)$$

To solve the above, let us introduce $\boldsymbol{\chi}(a) = \exp(-\mathbf{ad}_{\int_0^a \boldsymbol{\xi}(\chi) d\chi})$ which allows us to conveniently write the "state transition matrix" as $\phi(\sigma, s) = \exp(-\mathbf{ad}_{\int_s^\sigma \boldsymbol{\xi}(\chi) d\chi}) = \boldsymbol{\chi}(\sigma)\boldsymbol{\chi}^{-1}(s)$ [105, 172]. Subsequently, by fixing a time instance t , substituting

¹ The solution to (5.14) follows from the so-called *Magnus Series Expansion* [221]. Namely, (5.2) can be written in the form $\mathbf{Y}' = \mathbf{YA}(\sigma)$, and following [105] (see Theorem 7.1 from Magnus [172]), it can solved explicitly by $\mathbf{Y}(\sigma) = \mathbf{Y}(0) \exp(\boldsymbol{\Omega}(\sigma))$ with $\boldsymbol{\Omega}$ the Magnus expansion of \mathbf{A} .

the modal approximation of the strain rate $[\dot{\xi}]_k = \Phi \dot{q}$, and assuming the initial condition $\boldsymbol{\eta}_0 = \boldsymbol{\eta}(0, t)$, we can derive an analytical solution for equation (5.15) in the following form:

$$\begin{aligned} [\boldsymbol{\eta}]_k(\sigma, \boldsymbol{q}, \dot{\boldsymbol{q}}) &= \phi(\sigma, 0)\boldsymbol{\eta}_0 + \int_0^\sigma \phi(\sigma, s)[\dot{\xi}]_k(s, t) ds, \\ &= \chi(\sigma)\boldsymbol{\eta}_0 + \chi(\sigma) \int_0^\sigma \chi^{-1}(s)\Theta(s)\dot{\boldsymbol{q}} ds. \end{aligned} \quad (5.16)$$

Given the fact that $\exp(-\text{ad}_Y) = \text{Ad}_{\exp(Y)}^{-1}$ for every Y belonging to the set $\text{se}(3)$ (as documented by Taylor [272], page 90), we can utilize the solution discovered in a manner similar to equation (5.14) to rephrase $\chi(\sigma)$ as $\text{Ad}_{g(\sigma)}^{-1}$. Consequently, assuming $\boldsymbol{\eta} = \mathbf{0}_6$, whereby the base of the soft robot is structurally fixed, we can derive a convenient expression for the approximation of the velocity twist:

$$[\boldsymbol{\eta}]_k(\sigma, \boldsymbol{q}, \dot{\boldsymbol{q}}) = \text{Ad}_{[g]_k(\sigma, \boldsymbol{q})}^{-1} \int_0^\sigma \text{Ad}_{[g]_k(s, \boldsymbol{q})}\Theta(s)\dot{\boldsymbol{q}} ds. \quad (5.17)$$

Note from (5.17) that the joint velocity exhibits a linear relationship with the velocity twist. This attribute is typical of rigid robotics, *e.g.*, see [197, 256]. As such, it is possible to extract $\dot{\boldsymbol{q}}$ out of the integrand which naturally gives rise to a linear matrix transformation called the "*geometric manipulator Jacobian*". The geometric Jacobian matrix $[J]_k \in \mathbb{R}^{6 \times 6k}$ is defined by

$$[J]_k := \text{Ad}_{[g]_k(\sigma, \boldsymbol{q})}^{-1} \int_0^\sigma \text{Ad}_{[g]_k(s, \boldsymbol{q})}\Theta(s) ds, \quad (5.18)$$

such that $[\boldsymbol{\eta}]_k = [J]_k \dot{\boldsymbol{q}}$. The geometric Jacobian plays an important role in obtaining the Lagrangian form of the reduced-order dynamic model. Finally, to express the acceleration twist, we take the time-derivative of (5.17) leading to

$$\begin{aligned} [\dot{\boldsymbol{\eta}}]_k &= [J]_k \ddot{\boldsymbol{q}} + [\dot{J}]_k \dot{\boldsymbol{q}}, \\ &= [J]_k \ddot{\boldsymbol{q}} + \text{Ad}_{[g]_k}^{-1} \int_0^\sigma \text{Ad}_{[g]_k(s, \boldsymbol{q})} \text{ad}_{[\boldsymbol{\eta}]_k(s, \boldsymbol{q}, \dot{\boldsymbol{q}})} \Theta(s) ds \dot{\boldsymbol{q}}, \end{aligned} \quad (5.19)$$

which gives rise to the analytic expression of the time-derivative of the geometric Jacobian $[\dot{J}]_k$. Although the expression for the \dot{J} is compact, its derivation is fairly involved. We therefore refer the reader to Appendix D.2 on its derivation.

5.2.5 Reduced-order dynamics using Newton-Euler

Here, we detail the dynamics of the Cosserat beam. A majority of the dynamic framework presented here is adopted from Boyer et al. [29]; yet we introduce some modification to allow a pH-structure. Other works that adopt a similar approach include [94, 221, 222, 284]. First, let us consider an infinitesimal slice of continuum body that is perpendicular to the backbone curve. The kinetic momenta of this infinitesimal slice is then given by $\boldsymbol{\mu}(\sigma, t) := \mathcal{M}\boldsymbol{\eta}(\sigma, t)$ in which $\mathcal{M} \in \text{se}^*(3) \times \text{se}(3) \cong \mathbb{R}^{6 \times 6}$ denotes the symmetric inertia tensor.

Remark 5.1 For some soft robots, the inertia tensor \mathbf{M} may have an explicit dependency on space or time (or both). A common phenomena in soft robotics that innately lead to such dependencies include for instance the ballooning effect of soft pneumatic networks. During actuation, matter expands outwards radially, changing the cross-sectional geometry and thus its inertial properties. That said, the inertial changes due to ballooning is negligibly small. Besides, ballooning is often an undesired phenomena that is reduced by appropriate structural design such as internal ribs, or bellow-like geometries. Nevertheless, examples where inertial changes cannot be neglected include the class of growing or morphing soft robots [106, 127, 128], self-healing soft robots [225, 277], origami soft robot manipulators [125, 158, 314]. Pressure-driven soft robots actuated by near incompressible fluids like water also suffer from these inertial changing effects. But, these robots are scarce and purposefully design for aquatic environments which is outside the scope of this work. For many soft robots, air or gas is preferred over liquids. For sake of simplicity, we limit ourselves to a diagonal invariant inertia tensor:

$$\mathbf{M}(\sigma, t) \simeq \begin{pmatrix} \rho_0 \mathcal{J} & \mathbf{0}_{3 \times 3} \\ \mathbf{0}_{3 \times 3} & \rho_0 A_0 \mathbf{I}_3 \end{pmatrix} \succ 0,$$

in which the (cross-sectional average) density is $\rho_0 > 0$, the cross-sectional area of the soft robot $A_0 > 0$, and the second moment of area $\mathcal{J} \in \text{so}^*(3) \times \text{so}(3) \cong \mathbb{R}^{3 \times 3}$. We emphasize here that considering an invariant cross-sectional inertia tensor is not an overly conservative assumption. It still holds true for a large class of soft manipulators, and it has limited effects on the generality.

Using the expression of the kinetic momenta $\boldsymbol{\mu}(\sigma, t)$ of the infinitesimal rigid body in free-motion, we can write the equation of motion for a particular slice at σ using the Newton-Euler equations [94]:

$$\frac{\partial}{\partial t} (\mathbf{Ad}_g^{-\top} \boldsymbol{\mu}) = \mathbf{Ad}_g^{-\top} \mathcal{F}, \quad (5.20)$$

where again $\mathbf{Ad}_{(\cdot)}$ stands for the adjoint action, and $\mathcal{F} = \mathcal{F}_c + \mathcal{F}_u - \mathcal{F}_b - \mathcal{F}_{\text{mat}}$ the resultant wrench that is composed of the constraint wrench \mathcal{F}_c , the input wrench \mathcal{F}_u , and the potential wrenches due to body accelerations and hyper- and visco-elasticity, \mathcal{F}_b and \mathcal{F}_{mat} , respectively. Further evaluation of (5.20) leads to

$$\mathbf{M}\dot{\boldsymbol{\eta}} - \mathbf{ad}_{\boldsymbol{\eta}}^\top \mathbf{M}\boldsymbol{\eta} = \mathcal{F}, \quad (5.21)$$

where we used the fact that $\frac{\partial}{\partial t} \mathbf{Ad}_g^{-1} = -\mathbf{ad}_{\boldsymbol{\eta}} \mathbf{Ad}_g^{-1}$. Before continuing, we introduce a slight modification to the relation above. Using the fact that $\mathbf{ad}_{\boldsymbol{\eta}} \boldsymbol{\eta} = \mathbf{0}_6$, we can introduce the vector $\mathbf{Mad}_{\boldsymbol{\eta}} \boldsymbol{\eta}$ to (5.21) without affecting the dynamics. The importance of this modification originates from the preservation of passivity in the Lagrangian model, which is an important property in stability theorems for robotics. By substitution of the null vector, the equation of motion becomes

$$\mathbf{M}\dot{\boldsymbol{\eta}} + (\mathbf{Mad}_{\boldsymbol{\eta}} - \mathbf{ad}_{\boldsymbol{\eta}}^\top \mathbf{M}) \boldsymbol{\eta} = \mathcal{F}, \quad (5.22)$$

which is nothing more than the Newton-Euler equation for rigid-body motion on \mathbb{R}^3 . To introduce the (reduced-order) Cosserat kinematics and make the expression symmetric, we substitute (5.17) and (5.19) into (5.22) and pre-multiply by $[\mathbf{J}]_k^\top$:

$$[\mathbf{J}]_k^\top (\mathcal{M}[\mathbf{J}]_k \ddot{\mathbf{q}} + \mathcal{M}[\dot{\mathbf{J}}]_k \dot{\mathbf{q}} + \mathcal{C}_{[\eta]_k} \dot{\mathbf{q}}) = [\mathbf{J}]_k^\top (\mathcal{F}_u - \mathcal{F}_g - \mathcal{F}_{\text{mat}}), \quad (5.23)$$

where $\mathcal{C}_{(\cdot)} = -\mathcal{C}_{(\cdot)}^\top := \mathcal{M}\mathbf{ad}_{(\cdot)} - \mathbf{ad}_{(\cdot)}^\top \mathcal{M}$ is a skew-symmetric matrix. It is important to note that by pre-multiplication of the transpose Jacobian, we have eliminated the constraint wrenches, *i.e.*, $[\mathbf{J}]_k^\top \mathcal{F}_c = \mathbf{0}_n$ [197]. Finally, the finite-dimensional dynamics of the deformable soft robot is found by spatial integration of (5.23) over the material domain \mathbb{X} . The overall dynamics can be written in the familiar Euler-Lagrangian (EL) form as follows

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{f}_g(\mathbf{q}) + \mathbf{f}_{\text{mat}}(\mathbf{q}, \dot{\mathbf{q}}) = \boldsymbol{\tau}(\mathbf{q}, \mathbf{u}) \quad (5.24)$$

with the system matrices:

$$\mathbf{M}(\mathbf{q}) = \int_{\mathbb{X}} [\mathbf{J}]_k^\top \mathcal{M}[\mathbf{J}]_k d\sigma, \quad (5.25)$$

$$\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}}) = \int_{\mathbb{X}} [\mathbf{J}]_k^\top (\mathcal{M}[\dot{\mathbf{J}}]_k + \mathcal{C}_{[\eta]_k} [\mathbf{J}]_k) d\sigma, \quad (5.26)$$

$$\mathbf{f}_g(\mathbf{q}) = \int_{\mathbb{X}} [\mathbf{J}]_k^\top \mathcal{F}_b d\sigma, \quad (5.27)$$

$$\mathbf{f}_{\text{mat}}(\mathbf{q}, \dot{\mathbf{q}}) = \int_{\mathbb{X}} [\mathbf{J}]_k^\top \mathcal{F}_{\text{mat}} d\sigma =: \mathbf{K}\mathbf{q} + \mathbf{D}\dot{\mathbf{q}}, \quad (5.28)$$

$$\boldsymbol{\tau}(\mathbf{q}, \mathbf{u}) = \int_{\mathbb{X}} [\mathbf{J}]_k^\top \mathcal{F}_u d\sigma =: \mathbf{G}(\mathbf{q})\mathbf{u}, \quad (5.29)$$

where \mathbf{M} is the generalized inertia matrix, \mathbf{C} the Centripetal-Coriolis matrix, \mathbf{f}_g a vector of generalized potential forces with $\mathcal{F}_b = -\mathbf{Ad}_{[g]_k}^\top \mathcal{M}\mathbf{a}_b$ the external wrench acting on the body due to body-frame accelerations \mathbf{a}_b (like gravity), and \mathcal{F}_{mat} a vector of visco-elastic material forces imposed by the stiffness matrix $\mathbf{K} \succ 0$ and damping matrix $\mathbf{D} \succ 0$. The derivation for these constant matrices is shown in Appendix D.3, where it is shown that stiffness and damping matrix are computed through spatial integration similar to standard finite element methods:

$$\mathbf{K} = \int_{\mathbb{X}} \Theta^\top \mathcal{K} \Theta d\sigma, \quad (5.30)$$

$$\mathbf{D} = \int_{\mathbb{X}} \Theta^\top \mathcal{D} \Theta d\sigma, \quad (5.31)$$

where $\mathcal{K} \in \text{se}^*(3) \times \text{se}(3)$ and $\mathcal{D} \in \text{se}^*(3) \times \text{se}(3)$ are the stiffness and damping tensor, respectively. The vector \mathbf{Gu} represents the distributed forces $\mathbf{n}_u(\sigma, t)$ and moments $\mathbf{m}_u(\sigma, t)$ generated by various kinds of the internal actuators (*e.g.*, tendons or pneumatics). We will later detail the derivation of $\mathbf{G}(\mathbf{q})$ in this chapter as it depends highly on the geometrical placement of the soft actuators. If

$\text{rank}(\mathbf{G}) < \dim(\mathbf{q})$, the system (5.24) is said to be underactuated. Within the context of soft robotics, whose infinite-dimensional configuration space cannot be matched by a finite number of actuators, these systems are often intrinsically under-actuated.

To compute the Lagrangian matrices (5.25)-(5.31), that all involve a spatial integration over $\mathbb{X} = [0, L]$, we rewrite these integrations into one global matrix differential equation and solve it efficiently using a Matrix-Differential solver proposed in Chapter 4. As such, these system matrices are not computed exactly but approximated with sufficient precision. The numerical precision depends on the stepsize of the discretized spatial domain \mathbb{X} .

Assumption 5.5 The inertia matrix $\mathbf{M}(\mathbf{q})$ is a symmetric, positive definite, symmetric. and is uniformly bounded such that there exists positive constants $\lambda^- \leq \lambda^+$ such that $\lambda^- \mathbf{I}_n \preceq \mathbf{M}(\mathbf{q}) \preceq \lambda^+ \mathbf{I}_n < \infty$.

The uniform boundedness of the inertia matrix $\mathbf{M}(\mathbf{q})$ is a well-known property for rigid manipulators composed of purely rotational joints. According to Spong et al. [256] the inertia matrix in this case is composed solely of $\cos(\cdot)$ and $\sin(\cdot)$ terms, and thus it is bounded for all $\mathbf{q} \in \mathcal{Q}$. The physical interpretation is that the mass and moment of inertia of the robot must be finite and positive for all configurations. This does not always hold true for instance for robots with prismatic joints. Yet, bounds can be imposed on the configuration space $\mathbf{q} \in \mathcal{Q}$ that enable boundedness, see Ghorbel et al. [96]. In Della Santina et al. [72], it was shown that $\mathbf{M}(\mathbf{q}) = \mathbf{M}^\top(\mathbf{q}) \succeq 0$ for soft manipulators restricted to variable planar curvatures expressed via a polynomial basis $\theta_k = \sigma^{k-1}$. The property holds for the infinite dimensional case where $k \rightarrow \infty$.

Lemma 5.1. *Given the inertia matrix $\mathbf{M}(\mathbf{q})$ and the Coriolis matrix $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$ as described by (5.25) and (5.26), respectively, it can be shown that the matrix $\dot{\mathbf{M}} - 2\mathbf{C}$ is skew-symmetric.* ▲

Proof. To show $\dot{\mathbf{M}} - 2\mathbf{C}$ is skew-symmetric, we start by computing the time-derivative of the inertia matrix. For sake of clarity, we abbreviate the Jacobian matrices $[\mathbf{J}]_k = \mathbf{J}$ and $[\dot{\mathbf{J}}]_k = \dot{\mathbf{J}}$. Through chain differentiation, we find

$$\dot{\mathbf{M}} = \int_{\mathbb{X}} (\dot{\mathbf{J}}^\top \mathbf{M} \mathbf{J} + \mathbf{J}^\top \mathbf{M} \dot{\mathbf{J}}) d\sigma, \quad (5.32)$$

Then, calculating $\dot{\mathbf{M}} - 2\mathbf{C}$ leads to

$$\dot{\mathbf{M}} - 2\mathbf{C} = \int_{\mathbb{X}} \dot{\mathbf{J}}^\top (\mathbf{M} \mathbf{J} - \mathbf{J}^\top \mathbf{M} \dot{\mathbf{J}} - 2\mathbf{J}^\top \mathbf{C} \mathbf{J}) d\sigma. \quad (5.33)$$

Since the matrix $\mathbf{J}^\top \mathbf{C} \mathbf{J}$ is skew-symmetric, the remainder of the proof is to show that the matrix $\mathbf{S} = \dot{\mathbf{J}}^\top \mathbf{M} \mathbf{J} - \mathbf{J}^\top \mathbf{M} \dot{\mathbf{J}}$ also satisfies skew-symmetry. Since the inertia tensor is symmetric $\mathbf{M} = \mathbf{M}^\top$, we can easily show this holds true:

$$\mathbf{S} = \dot{\mathbf{J}}^\top \mathbf{M}^\top \mathbf{J} - \mathbf{J}^\top \mathbf{M}^\top \dot{\mathbf{J}} = -(\dot{\mathbf{J}}^\top \mathbf{M}^\top \mathbf{J} - \mathbf{J}^\top \mathbf{M} \dot{\mathbf{J}})^\top = -\mathbf{S}^\top. \quad (5.34)$$

Therefore, the matrix $\dot{\mathbf{M}}(\mathbf{q}) - 2\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$ is skew-symmetric for all $\mathbf{q}, \dot{\mathbf{q}} \in \mathbb{R}^n$ \square

In literature, Lemma 5.1 is often referred to as the passivity condition [197, 203, 256]. It implies that, in the absence of external dissipation, the total energy of the system (*i.e.*, the Hamiltonian) is conserved. It is also worth mentioning that this condition does not necessarily hold true for any representation of the Coriolis matrix only for particular computations of the Coriolis matrix $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$ (*e.g.*, through the Christoffel symbols).

5.2.6 Tendon and fluidic actuation

Up to now, we have not discussed the derivation of the actuation mapping $\mathbf{G}(\mathbf{q})$. The matrix namely depends on (*i*) the type of actuation, and (*ii*) how actuation fields are distributed along the backbone curve of the soft robot manipulator. Earlier, we introduced the notion of a distributed forces \mathbf{n}_u and distributed moments \mathbf{m}_u acting on the curve \mathbf{g} , which are collocated into a control wrench \mathcal{F}_u . Now, assuming that a general soft manipulator system is either actuated using a set of fluidic chambers or a set of tendons, the control wrench related this network of m number of soft actuators can be represented in the form [29, 221]:

$$\mathcal{F}_u(\sigma, \mathbf{u}) = \sum_{i=1}^m \begin{pmatrix} \mathbf{r}_i^\times(\sigma) \mathbf{t}_i(\sigma) \\ \mathbf{t}_i(\sigma) \end{pmatrix} u_i =: \Theta_u(\sigma) \mathbf{u}, \quad (5.35)$$

where $\mathbf{r}_i : \mathbb{X} \rightarrow \mathbb{R}^3$ is the radial distance between the actuator center-line and the backbone curve γ , and $\mathbf{t}_i : \mathbb{X} \times \mathcal{Q} \rightarrow \mathbb{R}^3$ the tangent vector along the actuator center-line expressed that deforms with the continuum body prescribed by $[\mathbf{g}]_k(\sigma, \mathbf{q})$, $\Theta_u \in \mathbb{R}^{6 \times m}$ a shape function matrix related to the spatial distribution of the soft actuators, and $u_i(t)$ a time-varying scalar related to the activation amplitude of the i -th soft actuator. Generally speaking, for tendon actuation $u_i = -\max\{0, \lambda_i\}$ with λ_i the cable tension and for pneumatic actuation we have $u_i = A_i p_i$ with $A_i > 0$ an effective pressure surface and p_i the applied pressure. Following (5.35), the generalized joint torques can then be computed by projecting the distributed control wrench onto the configuration space using the geometric Jacobian matrix. Then, $\mathbf{G}(\mathbf{q})$ is computed by integrating generalized distributed joint forces over \mathbb{X} :

$$\boldsymbol{\tau}(\mathbf{q}, \mathbf{u}) = \int_{\mathbb{X}} \mathbf{J}^\top(\mathbf{q}, \sigma) \Theta_u(\sigma) d\sigma \mathbf{u} =: \mathbf{G}(\mathbf{q}) \mathbf{u}. \quad (5.36)$$

Similar to the other Lagrangian matrices, the actuation mapping is included into the matrix differential solver to allow fast and efficient computation of (5.24).

5.2.7 Port-Hamiltonian formulation

In this section, the Lagrangian model in (5.24) is rewritten in port-Hamiltonian form. To this end, we define the generalized momenta $\mathbf{p} := \mathbf{M}\dot{\mathbf{q}}$. Then, the

(reduced-order) Hamiltonian is given by $\mathcal{H}(\mathbf{q}, \mathbf{p}) := \mathcal{K}(\mathbf{q}, \mathbf{p}) + \mathcal{U}(\mathbf{q})$ with $\mathcal{K} = \frac{1}{2}\mathbf{p}^\top \mathbf{M}^{-1} \mathbf{p}$ and $\mathcal{U}(\mathbf{q})$ the kinetic and potential energy, respectively.

Given the system's Hamiltonian \mathcal{H} , it can be shown that generalized velocities can be written in terms of partial derivatives of the Hamiltonian function

$$\dot{\mathbf{q}} = \nabla_{\mathbf{p}} \mathcal{H} \implies \nabla_{\mathbf{p}} \mathcal{H} := \left(\frac{\partial \mathcal{H}}{\partial \mathbf{p}} \right)^\top = \mathbf{M}^{-1} \mathbf{p}. \quad (5.37)$$

where we denote $\nabla_{\mathbf{x}}(\cdot) := \partial(\cdot)^\top / \partial \mathbf{x}$ as the gradient w.r.t. a vector field \mathbf{x} . Note that \mathbf{M}^{-1} is always exists due to the positive definiteness condition in Lemma 5.5. Similarly, we seek a differential description that relates the time evolution of \mathbf{p} to a state-derivative of the Hamiltonian function. Applying the chain rule of differentiation to the generalized momenta:

$$\begin{aligned} \dot{\mathbf{p}} &= \dot{\mathbf{M}} \dot{\mathbf{q}} + \mathbf{M} \ddot{\mathbf{q}}, \\ &= (\dot{\mathbf{M}} - \mathbf{C} - \mathbf{D}) \mathbf{M}^{-1} \mathbf{p} - \mathbf{K} \mathbf{q} - \mathbf{f}_g + \mathbf{G} \mathbf{u}, \end{aligned} \quad (5.38)$$

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Taking the partial derivative of the Hamiltonian \mathcal{H} w.r.t. the generalized coordinates \mathbf{q} , we find

$$\nabla_{\mathbf{q}} \mathcal{H} = \frac{1}{2} \nabla_{\mathbf{q}} [\dot{\mathbf{q}}^\top \mathbf{M}(\mathbf{q}) \dot{\mathbf{q}}] + \nabla_{\mathbf{q}} \mathcal{U}. \quad (5.39)$$

To relate (5.38) and (5.39), we explores some structural properties in the Lagrangian model. To be more specific, we exploit the skew-symmetry condition as detailed in Lemma 5.1. According to the Spong et al. [256], if the matrix $\mathbf{M} - 2\mathbf{C}$ satisfies the skew-symmetry in Lemma 5.1, it can be shown that

$$(\dot{\mathbf{M}} - 2\mathbf{C}) \dot{\mathbf{q}} = -\nabla_{\mathbf{q}} [\dot{\mathbf{q}}^\top \mathbf{M}(\mathbf{q}) \dot{\mathbf{q}}] - \dot{\mathbf{M}} \dot{\mathbf{q}}. \quad (5.40)$$

Finally, by combining (5.37), (5.38), (5.39), and (5.40), we can show that the Lagrangian model in (5.24) can be equivalently rewritten as a standard port-Hamiltonian (pH) system:

$$\Sigma_{\text{beam}} : \begin{cases} \dot{\mathbf{q}} = \nabla_{\mathbf{p}} \mathcal{H}, \\ \dot{\mathbf{p}} = -\nabla_{\mathbf{q}} \mathcal{H} - \mathbf{D} \nabla_{\mathbf{p}} \mathcal{H} + \mathbf{G} \mathbf{u}. \end{cases} \quad (5.41)$$

The advantage of the port-Hamiltonian system Σ_{beam} over the standard EL structure in (5.24), and as also seen in Chapter 4, is the general applicability to different physical domains and the common formalism with energy-based control, which we will explore further in the next section.

5.3 Energy-based controller for tasks on SE(3)

Given the reduced port-Hamiltonian model in (5.41), our objective here is to find a controller \mathbf{u} that ensures $\lim_{t \rightarrow \infty} \mathbf{g}(L, t) = \mathbf{g}_d$ in which $\mathbf{g}_d \in \text{SE}(3)$ denotes

the desired configuration of the end-effector. To achieve the control objective, the main idea is to reshape the potential energy function of the reduced-order finite-dimensional system using a standard energy-shaping techniques, common to standard port-controlled Hamiltonian models [204, 291].

We adopted an energy-based control strategy akin to the works of Franco et al. [87], Ortega et al. [203, 204] and Schaft [291]. Following the energy-shaping strategy, the model-based nonlinear controller becomes

$$\mathbf{u} = \mathbf{G}^+ (\nabla_{\mathbf{q}} \mathcal{H} - \nabla_{\mathbf{q}} \mathcal{H}_d), \quad (5.42)$$

where $\mathbf{G}^+ = (\mathbf{G}^\top \mathbf{G})^{-1} \mathbf{G}^\top$ is the generalized inverse of the actuation map \mathbf{G} , and the desired Hamiltonian in closed loop $\mathcal{H}_d = \frac{1}{2} \mathbf{p}^\top \mathbf{M}^{-1} \mathbf{p} + \mathcal{U}_d$ that satisfies $\operatorname{argmin}_{\mathbf{g}_L} \mathcal{U}_d = \mathbf{g}_d$ with $\mathbf{g}_L = \mathbf{g}(L, \cdot)$ the pose of the end-effector. Note that we purposefully omitted any damping injection as the system's intrinsic visco-elastic damping is deemed sufficiently large to guarantee stability. Following the concept of a kinematic feedback controller [29, 35] that artificially mimic an elastic element between the end-effector and the desired configuration in $\text{SE}(3)$, we have choose the gradient of the desired potential energy as

$$\nabla_{\mathbf{q}} \mathcal{U}_d = \lambda_1 \mathbf{J}^\top (\mathbf{J} \mathbf{J}^\top + \lambda_2 \mathbf{I})^{-1} \mathcal{F}_u, \quad (5.43)$$

where $\lambda_1 > 0$ is a proportional gain, $\lambda_2 > 0$ a controller gain related to the artificial damping of the pseudo-inverse, $\mathcal{F}_u = \mathbf{k}_p T_{\text{SE}(3)}(\boldsymbol{\varepsilon}) \boldsymbol{\varepsilon}$ an artificial control wrench with positive definite stiffness matrix \mathbf{k}_p , $\hat{\boldsymbol{\varepsilon}} = \log_{\text{SE}(3)}([\mathbf{g}_L]_k^{-1} \mathbf{g}_d)$ the geometric error where $\log_{\text{SE}(3)}(\cdot)$ and $T_{\text{SE}(3)}(\cdot)$ denote the logarithmic map (see Appendix D.1) and the tangent-space map, respectively. We refer the reader to Sonneville et al. [253] for the numerical computations of the tangent map on $\text{SE}(3)$. The vector $\boldsymbol{\varepsilon}$ may be regarded as the geometric error between the homogeneous transformations \mathbf{g}_d and \mathbf{g}_L such that if $\mathbf{g}_d = \mathbf{g}_L$ will simply yield $\|\boldsymbol{\varepsilon}\|_2 = 0$. Furthermore, the controller gains λ_1 and λ_2 can be tuned accordingly to tweak the desired transient behavior of the closed-loop system, similar to a classical PD controller.

5.4 Simulation studies of bio-inspired soft robots

In this section, we detail the numerical simulations of the port-Hamiltonian model in (5.41) together with the energy-shaping controller in (5.42).

Due to the partial differential nature, we have to employ a nested ODE routine to recover the trajectories for \mathbf{q} and \mathbf{p} . First, we employ an implicit trapezoidal solver with a fixed stepsize of $dt = 30$ ms to solve (5.41). At each time increment, we have to evaluate the dynamic matrices (5.25) to (5.29). To efficiently compute these dynamic entities, we solve the spatial integration problem over the material domain \mathbb{X} by using a second-order Runge-Kutta solver. The stepsize for the spatial solver is chosen sufficiently small $\Delta\sigma = 1$ mm. The spatial stepsize is related to the length of the manipulator L , but also the degree of geometric deformations along the backbone. In some cases, high-gain feedback control can excite

Table 5.1. Parameters setting for the solver, the soft robot, and controller.

Parameter description	Symbol	Value	Unit
Intrinsic length	L	120	mm
Cross-sectional radius	r	8.25	mm
Uniform density	ρ_0	1250	kgm^{-3}
Young's modulus	E	0.25	MPa
Shear modulus	μ_1	0.10	MPa
Constraint modulus	μ_2	1.50	GPa
Rayleigh coefficient	ζ	0.40	-

high-order modes thus requiring a smaller stepsize to capture these phenomena accurately. However, by keeping the control gains small paired with the fact that structural damping is dominant in soft elastomers often lead to slow transients (order of seconds). As such, the spatial discretization has been shown to relatively nonrestrictive. All simulation examples and underlying source code are provided publicly on the `sorotoki` toolkit [37]. Here, the numerical integrations of the system matrices (5.25), (5.26), (5.28) and (5.29) are performed using a so-called Matrix-Differential solver (see [38]). The simulations are performed on a modern machine (Ryzen 7-5800H, 3.2GHz).

For the soft robotic simulations, we have chosen a linear isotropic Hookean material with shear constraints. Given these material properties, the inertia tensor and the stiffness tensor become diagonal matrices:

$$\begin{aligned}\mathcal{M} &= \text{blkdiag}\{\rho_0 \mathcal{J}, \rho_0 A \mathbf{I}_3\}, \\ \mathcal{K} &= \text{blkdiag}\{\mu_1 \mathcal{J}, E A_0, \mu_2 A_0, \mu_2 A_0\},\end{aligned}$$

where A_0 is the (average) cross-sectional area, and \mathcal{J} the second moment of area. Note that A_0 and \mathcal{J} depend on the cross-sectional geometry of the soft robot and is therefore unique for each system. The damping tensor chosen as $\mathcal{D} = \zeta \mathcal{K}$ with damping coefficient ζ .

5.4.1 Soft robot manipulator inspired by octopus' tentacle

In the first study-case, we consider a soft robotic arm that is loosely inspired by the tentacles of an octopus. To introduce the under-actuation typically present in soft robotics, we have chosen an actuation matrix $\mathbf{G} = \text{blkdiag}\{\mathbf{I}_5, \mathbf{O}_3\}$ such that only the first five modes are actively controllable. We assume that the soft manipulator has a circular cross-section, thus the cross-sectional area is given by $A_0 = \pi r^2$ with radius r . The system properties are shown in Table 5.1.

Example 5.2 (Solution convergence for increasing modal order). Before investigating the performance of the controller, we study the affects of the truncation order k . Initially, it can be difficult find the optimal value for k that balances

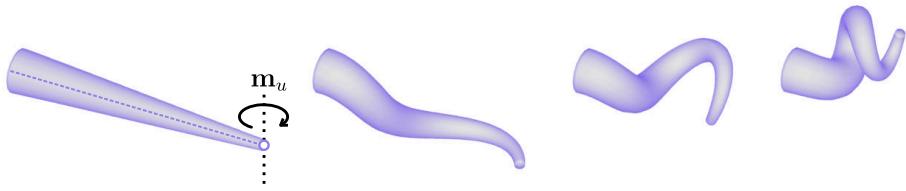


Figure 5.4. Three-dimensional deformation of the soft tentacle due to an external pure-moment wrench of $\|\mathbf{m}_u\| = 75 \text{ N mm}$ acting on its end-effector.

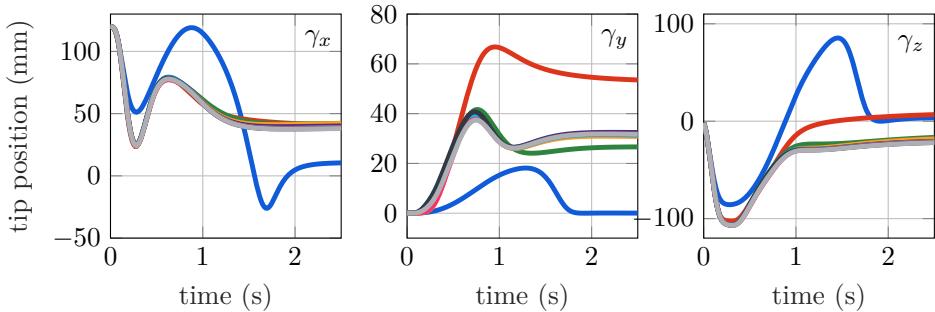


Figure 5.5. Temporal evolutions of the end-effector locations for increasing modal number k , where (left) is the x -position, (middle) the y -position, and (right) the z -position. The modal truncation order is color-coded as follows: $k \in \{-1, -2, -3, -4, -5, -6, -7, -8, -9, -10\}$. Notice that the relative difference in end-effector trajectories γ_L for increasing truncation order k vanishes for $k > 3$.

precision and computational speed. Consider the case where we subject the soft robot by a external tip wrench $\tau_{\text{ext}}(t) = [J]_k^\top (0, 0, \mathbf{m}(t), 0, 0, 0)^\top$ given by a predefined moment $\mathbf{m}(t) = 75 \cdot \text{erf}(t)$ in N mm. The applied moment causes a spiraling deformation of the soft arm, as can be seen in Figure 5.4. Observe that the soft arm undergoes a rather complex nonlinear three-dimensional deformation. Now, we incrementally increase the model truncation parameter $k \in \{1, \dots, 10\}$ and investigate the convergence of the solutions γ_L (*i.e.*, the end-effector location). The numerical results are shown in Figure 5.5.

Furthermore, we compare these simulation runs with a high-order mode of $k = 25$, where investigate the root mean square error, absolute error, and the ratio between actual CPU simulation time T_{sim} and finite horizon T . The benchmark is shown in Figure 5.6. From these results, we observe that the solutions quickly converge to a narrow error band, namely for $k > 3$ the difference in trajectories is near negligible. The RMS error is about 3.25 mm or 2.7% normalized by L . Regarding computation time, we observe a linear decrease for a linear increase in modal order k . Note that for $k > 8$, the simulations are close to losing real-time performance. We therefore choose a modal basis of order $k = 8$.

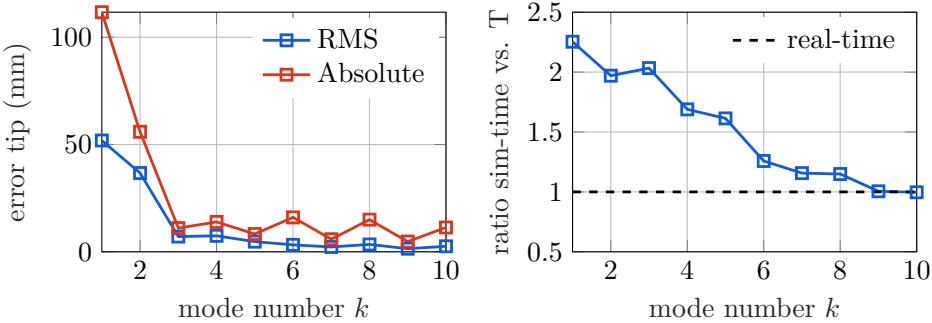


Figure 5.6. The benchmark results of the soft tentacle subjected to a tip-load for increasing model order k . (left) The root mean square error (RMSE) in (—) and absolute error in (—) for increasing k . Notice that the errors converge to an error band of about 3.25 mm. (right) The ratio between CPU simulation time and finite horizon time (*i.e.*, T_{cpu}/T) against the truncation order k , which shows all simulations achieve real-time computation.

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Example 5.3 (Energy-based controller). Following, we now subjected the soft robot to the proposed energy-based controller in (5.42), where the control gains are tuned to produce a smooth transient: $\lambda_1 = 0.01$ and $\lambda_2 = 0.001$. The artificial spring stiffness is chosen as $\mathbf{k}_p = \text{blkdiag}\{0.01 \cdot \mathbf{I}_3, \mathbf{I}_3\}$. Lastly, the desired configuration of the end-effector is chosen as follows:

$$\mathbf{g}_d = \begin{pmatrix} \mathbf{I}_3 & \boldsymbol{\gamma}_d \\ \mathbf{0}_3^\top & 1 \end{pmatrix} \quad \text{with} \quad \boldsymbol{\gamma}_d = \begin{pmatrix} 0.04 \\ 0.00 \\ -0.01 \end{pmatrix}.$$

The numerical results of the closed-loop system are shown in Figure 5.7 and 5.8. It is worth mentioning that these simulation run at ± 120 Hz real-time.¹

Figure 5.7 shows the evolution of the continuous deformation along the soft robotic body, whereas Figure 5.8 shows the modal coefficients $\mathbf{q}(t)$ and generalized momenta $\mathbf{p}(t)$. As can be seen, the end-effector of the soft robot manipulator converges to the desired set-point $\mathbf{g}_d \in \text{SE}(3)$. Although the control gains could be increased to promote a faster transient, it was observed that high gains lead to undesired (propagating) oscillations of the flexible structure. A possible solution might be to introduce negative damping to the controller Hamiltonian \mathcal{H}_d , to overcome the soft robot's structural damping.

For the second simulation run, we modified the control gains to highlight an interesting property of the proposed controller. To be more specific, we increase the controller gains to $\lambda_1 = \lambda_2 = 0.1$. The numerical results for the increased controller gains are shown in Figure 5.9 and Figure 5.10. Although the control

¹Real-time bandwidth is determined by the ratio between finite horizon and CPU's computation time, *i.e.*, $f \approx T/T_{\text{sim}}$, which is affected most by spatial stepsize due to explicit integration.

goal and the initial conditions are chosen identical, the soft robot converges to a different configuration – albeit, a shape with less '*complexity*'. The cause of less complicated bending patterns has two origins. First, increasing the control gains also artificially impacts the structural stiffness of the soft robot, resulting in soft robot with a higher perceived stiffness. Second, by increasing the stabilizing term λ_2 in the damped Jacobian inverse (5.43), more weight is given towards finding a solution that also minimizes the joint angles $\|\mathbf{q}\|_2$. This is to be expected, as intrinsically, it requires more energy to achieve higher-order modes deformations $\{\theta_n\}_{n=1}^k$ of the Legendre basis. Hence, the energy-based controller will thus find a minimizer that accounts for the ordering of the shape basis, penalizing higher-order modes. To some extent, the high intrinsic damping in soft robots acts as a spatial low filter which is beneficial for both modeling as control. This effect is not observed in classical semi-rigid robots. This result indicates that the proposed controller can be effectively tuned alter the structural compliance of the soft robot; and thus could be implemented carefully to preserve '*softness*'.

5.4.2 Multi-link soft robot inspired by the elephant's trunk

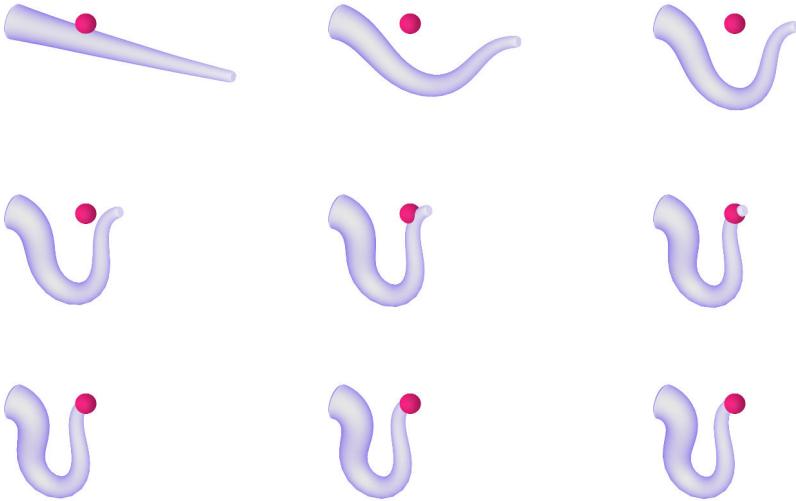
In the second study-case, we consider a two-link soft robot that is inspired by the trunk of an elephant. A similar soft robotic system is considered in [78] (*i.e.*, the elephant-inspired bionic arm by Festo), where mobility of the bio-inspired robotic system is achieved through a pneumatic-network distributed along the continuous body of the robot. Therefore, considering a six-bellow network, the fluidic actuation matrix takes the form:

$$\mathbf{G}(\mathbf{q})\mathbf{u} = \sum_{n=1}^6 \left[\int_{\mathbb{X}} [\mathbf{J}]_k^\top(\sigma, \mathbf{q}) \boldsymbol{\theta}_{u,i}(\sigma) d\sigma \right] u_i,$$

where $\{\boldsymbol{\theta}_{u,i}\}_{n=1}^6$ is a set of piecewise constant wrench functions related to the pneumatic actuation bellows distributed along the soft robotic body, and $\mathbf{u} = (u_1, u_2, u_3, u_4, u_5, u_6)^\top$ a vector of wrench amplitudes. The control input sets $\{u_1, \dots, u_3\}$ relate to the first link and $\{u_4, \dots, u_6\}$ to the second link of the robot. Given this input configuration, it also follows that $\text{rank}(\mathbf{G}(\mathbf{q})) < \dim(\mathbf{q})$ for all $\mathbf{q} \in \mathbb{R}^{6k}$, *i.e.*, underactuated. The system and solver properties are given in Table 5.2. We again consider $k = 8$ spatial modes. To simulate the effect of the gripper, we added an inertial mass at the end-effector modeled by:

$$\boldsymbol{\tau}_{\text{ext}} = \mathcal{M}_{\text{grip}} \mathbf{J}(L, \mathbf{q})^\top \left[\left(\mathbf{0}_3^\top, \mathbf{a}_g^\top \mathbf{Ad}_{[\mathbf{g}]_k(L, \cdot)}^\top \right)^\top + [\dot{\mathbf{q}}]_k(L, \mathbf{q}, \dot{\mathbf{q}}, \ddot{\mathbf{q}}) \right],$$

where $\mathcal{M}_{\text{grip}}$ inertia tensor related to the gripper placed at the end-effector of the robot located at $\sigma = L$. Again we apply the energy-based controller in (5.42) to the system, where the control gains are $\lambda_1 = 5$ and $\lambda_2 = 1$, while the artificial stiffness matrix \mathbf{k}_p is kept identical to previous simulations. Lastly, the desired



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Figure 5.7. Three-dimensional evolution of the soft robot manipulators, converging to the desired set-point $g_d \in \text{SE}(3)$ (indicated by the pink ball). Observe that the morphological motion that arises due to the energy-based controller has a close similarity to those an octopus' tentacle.

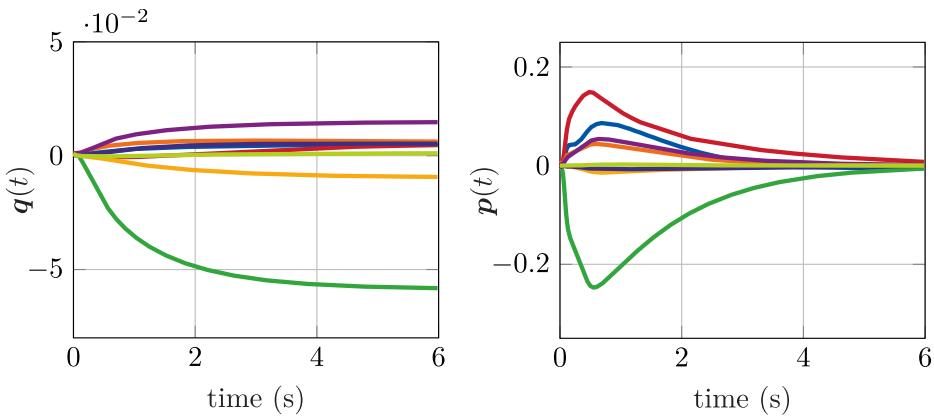


Figure 5.8. The evolution of the modal coefficients and the generalized momenta of the soft robot manipulator. The modal coefficients q are ordered as follows: $k \in \{-1, -2, -3, -4, -5, -6, -7, -8\}$. Observe that mainly mode 3 is dominant.

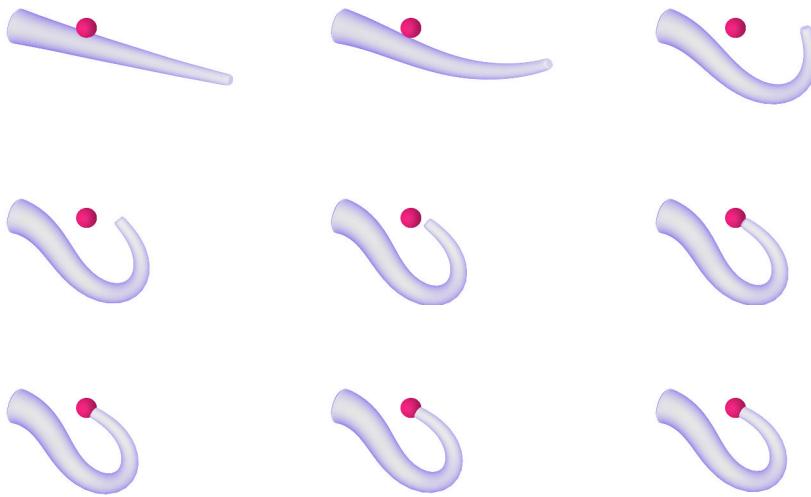


Figure 5.9. Three-dimensional evolution of the soft robot manipulators, converging to the desired set-point $g_d \in \text{SE}(3)$ (indicated by the pink ball). Observe that a different morphology arises due to higher control gains, *i.e.*, $\lambda_1 = \lambda_2 = 0.1$, which is caused by the controller affecting the structural compliance of the soft robot.

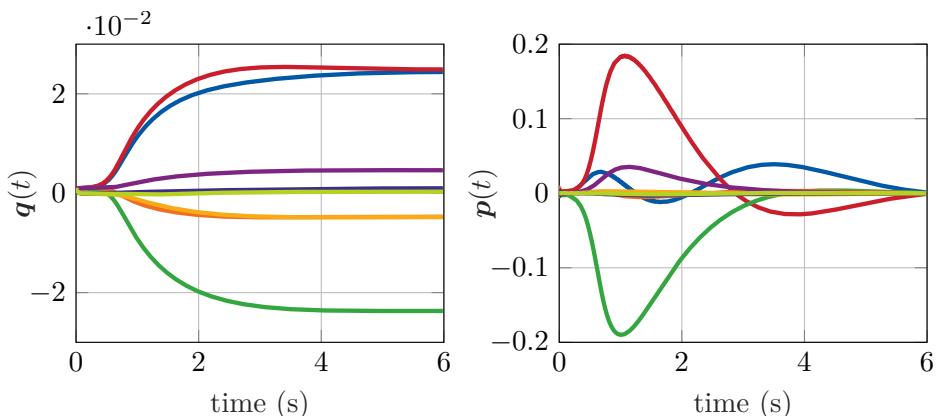


Figure 5.10. The evolution of the modal coefficients (left) and the generalized momenta (right) of the soft robot manipulator with the increased controller gains. The modal coefficients q are ordered as follows: $k \in \{-1, -2, -3, -4, -5, -6, -7, -8\}$. Observe now that modes 1 – 3 are dominant.

Table 5.2. Parameters setting for the numerical solver, the soft manipulator by the elephant’s trunk, and the energy-based controller.

Parameter description	Symbol	Value	Unit
Intrinsic length	L	360	mm
Cross-section radius	r	25	mm
Uniform density	ρ_0	250	kgm^{-3}
Young’s modulus	E	3.50	MPa
Shear modulus	μ_1	2.00	MPa
Rayleigh coefficient	ζ	0.45	-

configuration of the end-effector is chosen as follows:

$$\mathbf{g}_d = \begin{pmatrix} \Phi_d & \gamma_d \\ \mathbf{0}_3^\top & 1 \end{pmatrix} \text{ with } \gamma_d = \begin{pmatrix} 0.125 & 0.100 & 0.175 \end{pmatrix}^\top \text{ and } \Phi_d = \text{Rot}_y\left(\frac{1}{4}\pi\right).$$

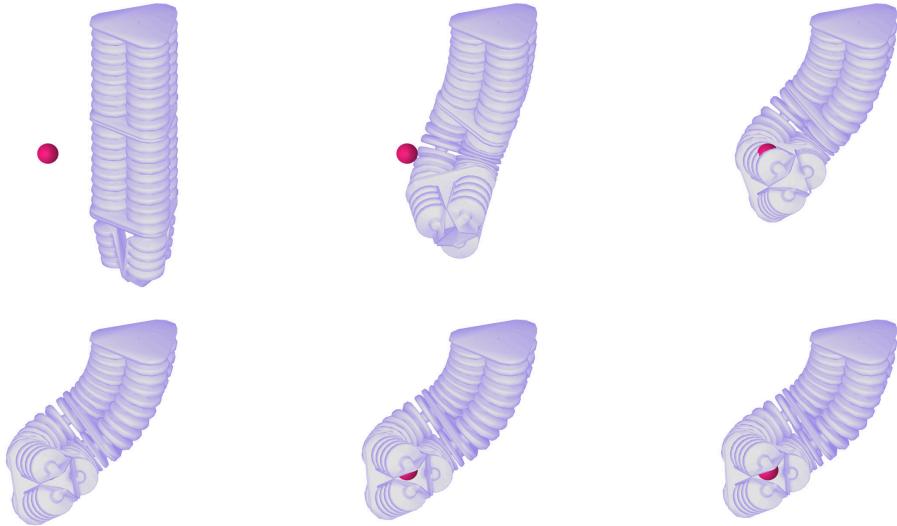
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The numerical results of the closed-loop system are shown in Figure 5.11 and Figure 5.12 which could reach a real-time simulation bandwidth of < 65 Hz. Figure 5.11 shows the continuous deformation along the soft robotic body, while Figure 5.12 shows the trajectories of the modal coefficients $\mathbf{q}(t)$ and the generalized momenta $\mathbf{p}(t)$. As can be seen, the end-effector of the soft robot manipulator slowly converges to the desired set-point $\mathbf{g}_d \in \text{SE}(3)$, even when dealing with piece-wise distributed actuation loads applied to the continuous backbone. To describe the discontinuous actuation profiles, however, higher order modes are required as can be seen in Figure 5.12. This might indicate there exist better tailored compact shape bases for this soft robotic system.

5.5 Achieving bio-inspired motion through energy-based control using relaxed set-points

For in our third study case, we wish to pursue the typical biological motions found in nature via means of model-based control. In particular, we are interested in the experimental recording made by Sumbre et al. [260] of an octopus. Their work studied the goal-directed arm movements of the octopus, produced by the nervous system to generate a sequence of motor commands that bring the arm closer towards the target. Note that the control of the octopus arm is highly complex, as the arm can be moved in any direction with a virtually infinite DoFs. According to [260], the octopus reduces control complexity of this soft arms using highly stereotypical movements that arise from localized motor control embedded in the arm rather than a centralized controller. Figure 5.13 shows such well-known stereotypical motion primitives, namely a bending propagating wave.

Our objective is to qualitatively reproduce these experimental findings, where we aim to seek a model-based control law that, like the octopus [260], explores such stereotypical motion like bending wave propagation likely to preserve energy



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Figure 5.11. Three-dimensional evolution of the soft robot inspired by the elephant’s trunk (whose muscular network is mimicked through six pneumatic bellows), slowly converging to the desired set-point $\mathbf{g}_d \in \text{SE}(3)$ (*i.e.*, the pink ball).

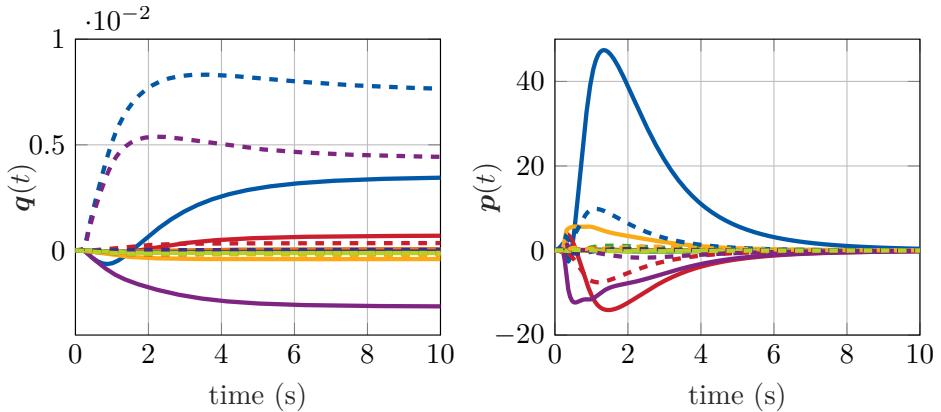
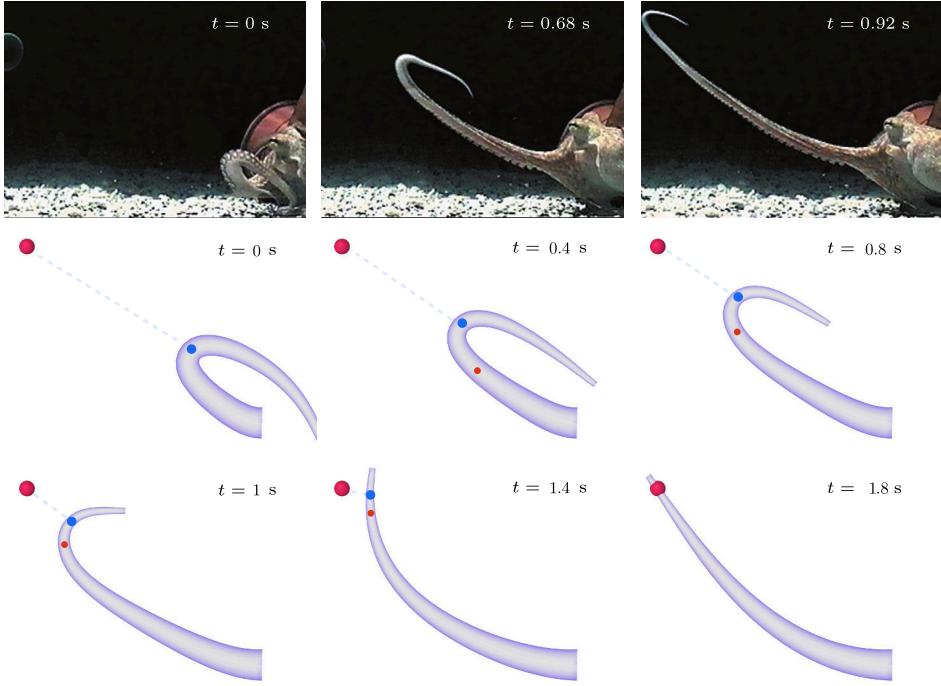


Figure 5.12. The evolution of the modal coefficients (left) and the generalized momenta (right) of the soft robot manipulator inspired by the elephant’s trunk. The modal coefficients q are ordered as follows $k \in \{-1, -2, -3, -4, -5, -6, -7, -8\}$ where the full and dashed lines represent the first and second link, respectively. Observe that mainly modes 1 and 5 are dominant in both links.

expensive. While the Cosserat can describe strain propagation, looking at our previous simulations, we do not observe them. Thus indicative of a mismatch in motion control, we make an ansatz that there are minor ingredients missing in the energy-shaping controller (5.42), but more importantly, the way we define



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Figure 5.13. (top) Recording of an octopus extending its tentacle towards an object of interest using a propagating bending wave motion. (bottom) Three-dimensional evolution of the soft robot inspired by the octopus above using the controller proposed in (5.44). The adaptive location σ_d is shown as (●), and its history (○). Notice it produces a motion highly reminiscent of the true biological counterpart.

the control task. We inspire our modifications on the sensorimotor feedback control proposed by Wang et al. [301] (inspired by [131]). Rather than end-effector setpoint stabilization as in prior examples, they instead minimize the Euclidean distance between the target and anywhere on the backbone curve. Here, we propose several modifications: (i) we explore a energy-shaping technique (5.42) with full system information, (ii) we introduce terms that also minimize the energy spent on elastic structural deformation using null-space projections [197, 256], and (iii) we use geodesics in $\text{SE}(3)$ for the task rather than \mathbb{R}^3 . The controller in (5.42) is modified by choosing a different desired energy gradient $\nabla_{\mathbf{q}} \mathcal{U}_d$:

$$\nabla_{\mathbf{q}} \mathcal{U}_d = \lambda_1 \mathbf{J}_d^\dagger \mathcal{F}_{\mathbf{u}}(\mathcal{E}_d) - \lambda_3 \left(\mathbf{I} - \mathbf{J}_d \mathbf{J}_d^\dagger \right) \nabla_{\mathbf{q}} \mathcal{U}_e, \quad (5.44)$$

where $\mathbf{J}_d := \mathbf{J}(\sigma_d, \mathbf{q})$, its pseudo inverse as $\mathbf{J}_d^\dagger = \mathbf{J}_d^\top (\mathbf{J}_d \mathbf{J}_d^\top + \lambda_2 \mathbf{I})^{-1}$, λ_1, λ_2 and λ_3 the control gains, and $\mathcal{E}_d = \widehat{\log}_{\text{SE}(3)}([\mathbf{g}]_k^{-1}(\sigma_d, \mathbf{q}), \mathbf{g}_d)$ the optimal geodesic error with σ_d an adaptive spatial coordinate that minimizes the geodesic distance between the backbone curve and the desired target setpoint \mathbf{g}_d . To be specific,

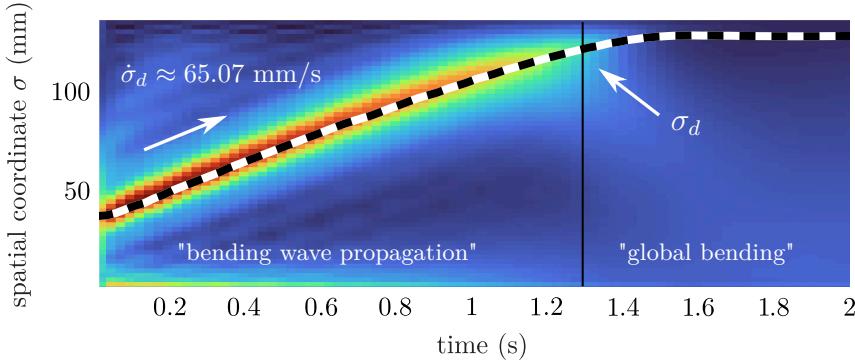


Figure 5.14. The magnitude of the curvature strain field $\kappa := [\xi_2]_k$ as a function of time and space (*i.e.*, $\sigma \in [0, L]$) indicated by the colormap $\in [0, 0.1] \text{ mm}^{-1}$. The adaptive parameter σ_d is shown by the dashed line (—). Note that the duration of the propagating bending wave lasts $T_{\text{wave}} \approx 1.3$ s with a relatively consistent velocity.

this adaptive geodesic minimizer is found using

$$\sigma_d = \underset{\sigma \in (0, L]}{\operatorname{argmin}} \left\| \widehat{\log}_{\text{SE}(3)} \left([\mathbf{g}]_k^{-1}(\sigma_d), \mathbf{g}_d \right) \right\|_2, \quad (5.45)$$

which is found using a line search algorithm. Note that the latter RHS term of (5.44) controls the degree of residual elastic flexibility of the system that, by exploring null-space projections, does not obstruct the primary control objective. Therefore, unlike [301], we do not require gain activation functions parameterized by σ as we are exploring intrinsic structural redundancies.

Inline with the recording from [260] (Figure 5.13), we consider a soft robot model with parameters similar to Table 5.1 albeit with $L = 135$ mm. The control gains are tuned to $\lambda_1 = \lambda_2 = 0.1$ and $\lambda_3 = 0.01$, whereas the desired target is $\Phi_d = \mathbf{I}_3$ and $\gamma_d = (70, 0, 40)^\top$. To simulate the viscous drag caused by the moving fluid, we model an external distributed wrench $\mathcal{F}_{\text{drag}} = -\frac{1}{2}\rho_w \|\mathbf{J}\dot{\mathbf{q}}\| \mathcal{A}_{\text{drag}} \mathbf{J}\dot{\mathbf{q}}$ where $\rho_w = 1000 \text{ kgm}^{-3}$ is the water density, and $\mathcal{A}_{\text{drag}}$ a drag coefficient tensor.

The results of the numerical simulation are depicted in Figure 5.13, illustrating sequential snapshots of the continuous deformations exhibited by the flexible appendage. The location of σ_d is shown as (•). Figure 5.14 shows the temporal and spatial evolution of the curvature strain field $\kappa := [\xi_2]_k$. Notably, we observe that the trajectories of the closed-loop system bear a striking resemblance to those observed in the authentic biological counterpart. Particularly noteworthy is the immediate akinship of the wave-like propagation characteristic of the bending motion commonly associated with octopus' arms. This bending wave starts from $\sigma_d = 41.5$ mm ($t = 0$ s) and at near the end of the wave $\sigma_d = 126.3$ mm ($t = 1.3$ s), the wave-speed along the arm is $\dot{\sigma}_d = 65.07 \text{ mm s}^{-1}$. Although these are naturally related to chosen control gains, these velocity measures are inline with literature. Conclusively, these results demonstrate life-like movements of the soft arm, which emphasizes the importance of model-based control in the field of soft robotics on the premise that these systems should ultimately mimic nature.

5.6 On modal truncation: applying reduced-order model-based controllers to high-dimensional models of continuum soft robots

In the previous section, we made the assumption that the truncation order k of both the dynamic system and the controller is identical. However, in practical scenarios, this is never the case. Soft robots are, in theory, infinite-dimensional systems that can never be precisely matched by a finite state description. This brings forth several issues regarding the selection of an appropriate truncation controller and the potential consequences of an unsuitable truncation choice, such as a deterioration in control performance or even instability.

In light of this, we will examine the impact on performance resulting from varying truncation levels of the model-based controller (5.42) when applied to high-dimensional Cosserat models (*i.e.*, an attempt towards approximating infinite dimensionality). To distinguish between the two, let us introduce k_{sys} (*i.e.*, the truncation of the "true" system) and $k := k_{\text{control}}$ (*i.e.*, the truncation of the controller), with the condition that $k_{\text{sys}} \gg k_{\text{control}}$. In order to maintain computational feasibility, we set $k_{\text{sys}} = 8^2$, *i.e.*, the truncation order at which numerical convergence is observed in Example 5.2. We denote the controller states as \mathbf{q}_c and system states as \mathbf{q} . Despite the difference in dimensions between the soft robot and the controller, *i.e.*, $\dim(\mathbf{q}) \gg \dim(\mathbf{q}_c)$, we can interconnect the two systems by ensuring that the input and output have appropriate dimensions. For simplicity, we choose an actuation map for the controller, denoted as $\mathbf{G}_k = \mathbf{I}_6 \otimes \mathbf{I}_k$, and for the system, denoted as $\mathbf{G} = \mathbf{I}_6 \otimes \text{holdcol}_{1:k}(\mathbf{I}_{k_{\text{sys}}})$, where $\text{holdcol}_{i:j}(\cdot)$ holds all columns from i to j while setting any other columns to zero. Hence it follows that $\dim(\mathbf{u}) = \text{rank}(\mathbf{G}) = \text{rank}(\mathbf{G}_k) = 6k$.

Since we cannot measure \mathbf{q} directly, we propose a controller-observer architecture that estimates the controller states \mathbf{q}_c based on available measurements. Assuming we can measure the end-effector position via sensor system Σ_{sensor} , *i.e.*, $\mathbf{y} = \boldsymbol{\gamma}_L(\mathbf{q})$, we consider a energy-shaping controller plus observer approach Σ_{control} as follows (see Figure 5.15 for the control diagram):

$$\Sigma_{\text{control}} : \begin{cases} \mathbf{u} = \mathbf{G}_k^+ (\nabla_{\mathbf{q}_c} \mathcal{H} - \nabla_{\mathbf{q}_c} \mathcal{H}_d), \\ \dot{\tilde{\mathbf{q}}} = L_1 \mathbf{J}_v^\top \mathbf{e} + L_2 (\mathbf{I} - \mathbf{J}_v^\dagger \mathbf{J}_v) \nabla_{\mathbf{q}_c} \Psi, \end{cases} \quad (5.46)$$

where $\tilde{\mathbf{q}}$ is the controller state estimation, $\mathbf{e} = \mathbf{y} - \tilde{\boldsymbol{\gamma}}_L$ represents the difference between the true end-effector location and its estimate produced by the observer model, \mathbf{J}_v the linear velocity part of the Jacobian matrix, $\mathcal{N} = (\mathbf{I} - \mathbf{J}_v^\dagger \mathbf{J}_v)$ the null space, Ψ a scalar-valued function that represents a sub-task for the observer, and $L_1, L_2 > 0$ are the observer gains. We select a sub-task energy potential Ψ as the difference between the estimated potential energy and the work produced by the control input \mathbf{u} , thus $\nabla_{\mathbf{q}_c} \Psi(\tilde{\mathbf{q}}, \mathbf{u}) = \nabla_{\mathbf{q}_c} \mathcal{H}(\tilde{\mathbf{q}}) - \mathbf{G}_k \mathbf{u}$. Thus, the observer is nothing more than a continuous-time continuum deformation solver.

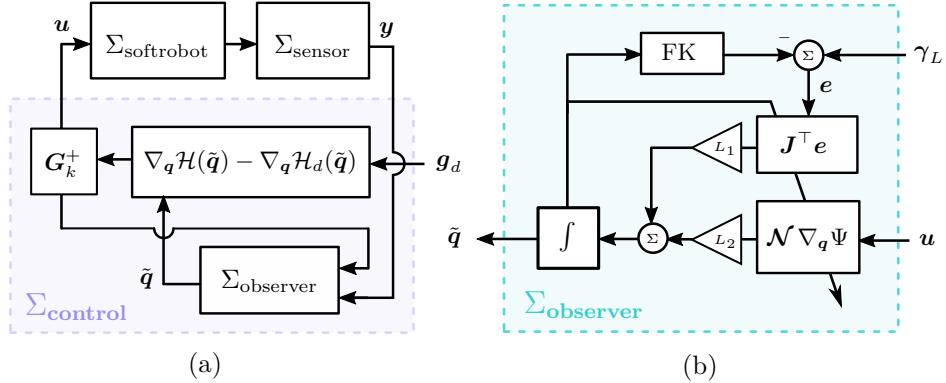


Figure 5.15. Schematic diagram of the low-order energy-based controller and observer applied to the "true" soft robot system depicted as $\Sigma_{\text{softrobot}}$. (a) Control diagram showing the interconnection between the observer, controller, and the soft robot. The block Σ_{sensor} provides online measurements of the end-effector position γ_B . The observer estimates are used to compute the control law (5.42). (b) The observer produces an estimate \tilde{q} based on a measurement error e and the control signals u . Here, FK is the forward kinematic mapping derived using (5.14).

We again consider the soft robot inspired by the octopus arm (see Table 5.1) with the controller-observer gains: $\lambda_1 = \lambda_2 = 0.1$ and $L_1 = L_2 = 1$. The desired end-effector configuration is $\Phi_d = I_3$ and $\gamma_d = (70, 0, 40)^\top$. In this study, we analyze the performance of the reduced-order controller for truncation orders $k \in \{1, 2, \dots, 8\}$. Note that for $k = 1$, the controller explores the "*Piece-wise Constant Strain*" (PCS) assumption similar to Chapter 4, while the true system $\Sigma_{\text{softrobot}}$ is not impeded by such kinematic restrictions.

The numerical simulations conducted for the controller benchmark are presented in Figure 5.16, showcasing snapshots of the closed-loop system in operation. The figure displays the true system as (■) and the low-dimensional shape estimations as (□). Figure 5.17 shows the trajectories of γ_L for various k , while Figure 5.18 shows the RMS error between the backbone of the estimate and the true system. The steady-state values for these metrics are reported in Table 5.3. As anticipated, it is observed that with increasing k , the differences between the

Table 5.3. Error values in the steady-state condition for the energy-based controller are examined as the model truncation k increases. It is noteworthy that as the value of k increases, the accuracy of the backbone estimate improves. However, when it comes to the tip error, a consistent and monotonic trend with increasing k may not be observed.

Truncation	$k = 1$	$k = 2$	$k = 3$	$k = 4$	$k = 5$	$k = 6$	$k = 7$	$k = 8$
Tip error (mm)	14.68	2.36	0.73	0.65	0.46	0.78	0.65	0.54
Curve error	118%	16.1%	14.2%	8.34%	5.31%	4.53%	4.24%	4.01%

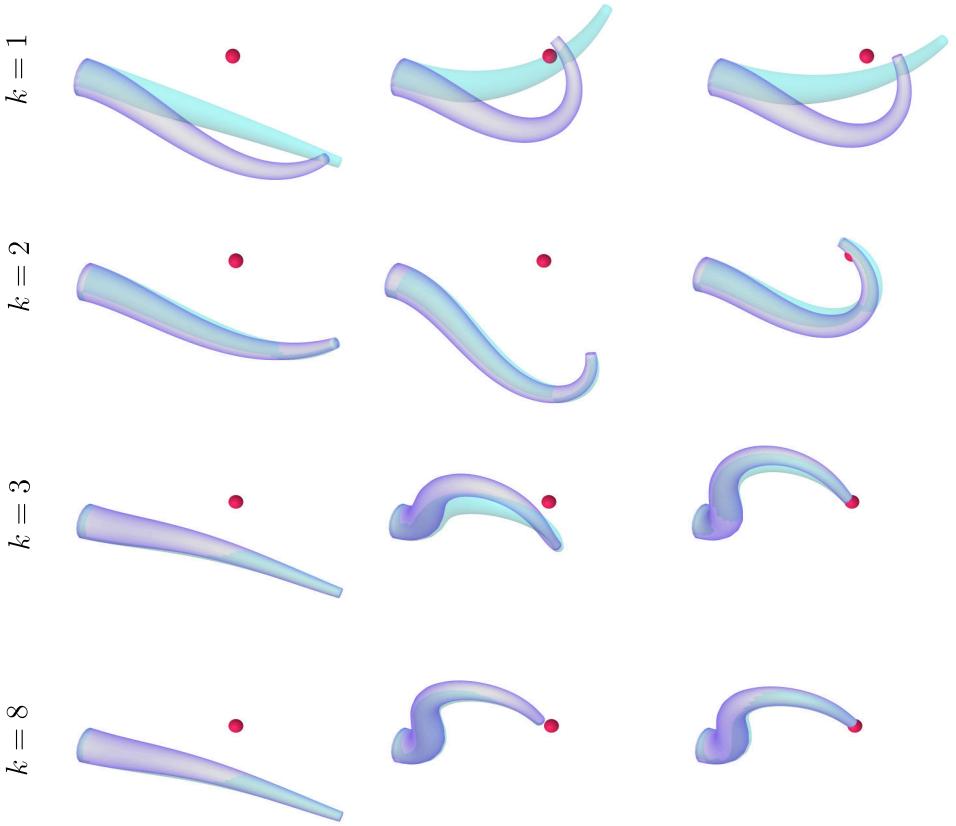


Figure 5.16. Three-dimensional evolution of the high-dimensional soft robotic system subject to a low-dimensional controller. The truncation order is indicated by k . The figure displays the true system as (■) and the low-dimensional shape estimations as (□). Notice that, independent of the truncation order k , all controllers converge to a neighborhood of the setpoint even when the estimates are off.

true system and shape estimates diminish, indicating a monotonically increasing precision. However, a few other remarkable observations can be made.

First, irrespective of the truncation, all controllers guide the end-effector of the soft robot towards a close vicinity of the desired configuration. A particularly intriguing example is seen in the simulation for $k = 1$ (*i.e.*, PCS scenario). In this case, the desired tip configuration \mathbf{g}_d lies outside the workspace of the reduced controller-observer system, *i.e.*, $\mathbf{g}_d \notin \mathcal{W}_c$. Consequently, the PCS (or PCC) shape estimation is, in theory, unable to achieve the assigned control objective. However, since the true system is not constrained by the controller's conservative workspace \mathcal{W}_c , the closed-loop system may lead to a smaller error than any solution confined to \mathcal{W}_c . This discovery may reduce the importance of modal truncation (or the choice of model basis) in the performance of model-based control of soft robots, as soft robots may inherently possess enough redundancy to counteract modeling im-

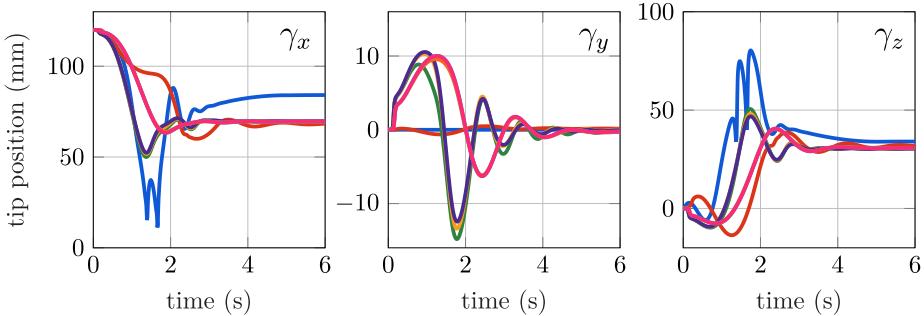


Figure 5.17. Temporal evolutions of the end-effector locations for increasing modal number k , where (left) is the x -position, (middle) the y -position, and (right) the z -position. The modal order is color-coded: $k \in \{-1, -2, -3, -4, -5, -6, -7, -8\}$. Notice all, but the PCS controller ($k = 1$) converges to the desired end-effector position.

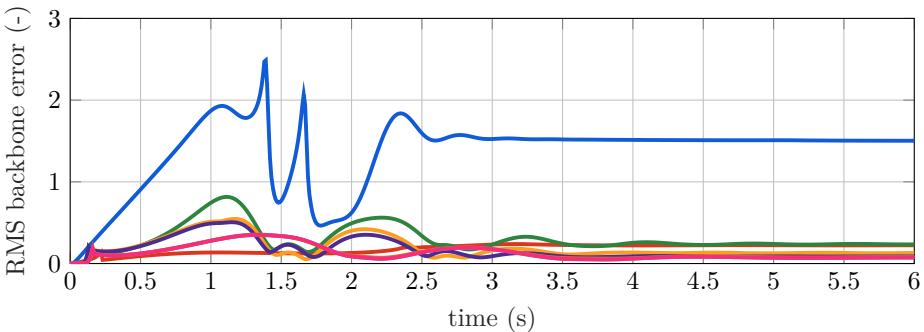


Figure 5.18. Root mean square error of backbone between high-order model and low-order observer. The modal order is color-coded as follows: $k \in \{-1, -2, -3, -4, -5, -6, -7, -8\}$.

perfections. This potentially sheds light on the reason behind the notable efficacy of PCC models in soft robot control, despite their oversimplification. The findings presented in Table 5.3 appear to support this claim, as for $k \geq 3$, the tip error consistently remains within sub-millimeter precision. Achieving sub-millimeter precision for $k = 1$ is perhaps possible by introduce an integral action, or explored adaptive controllers akin to those proposed in Chapter 4.

Second, transitioning from $k = 2 \rightarrow k = 3$, a significant transformation in the stable configurations is observed. Specifically, we observe that the controller drastically switches from an "elbow down" configuration to an "elbow up" configuration (see Figure 5.4). We hypothesize that for low controller orders, *i.e.*, $k \leq 2$, the overall shape estimation error is too large to appropriately compensate gravity, hence an elbow-down solution is preferred. Therefore, in terms of full-body shape control, truncation might play a more important role than tip setpoint regulation.

5.7 Conclusion

Due to their intrinsic compliance of soft robots, they allow for complex morphological motions that mimic animals in nature. Achieving similar performance to biology highlights the need for more accurate dynamic models and control strategies. In this chapter, we provided a modeling framework for Cosserat beams that leads to a finite-dimensional system in a port-Hamiltonian structure. By exploiting the passivity, an energy-shaping controller was proposed that ensures the closed-loop Hamiltonian is minimal at the desired set-point. The numerical model was developed for a several bio-inspired soft robot (octopus' tentacle and elephant's trunk) with distributed control inputs. The key challenges here regarding both the model as the controller are their ability to capture the hyper-flexibility, deal with inherent under-actuation, and exploit its hyper-redundancy to achieve its control task. Given appropriate controller gains, the model-based controller yields smooth convergence of the soft robot's end-effector while accounting for under-actuation. It was shown that by tuning the controller gains, the intrinsic stiffness of the soft body can be adapted. Furthermore, we investigate the possibility of the proposed approach to mimic nature. By introducing an energy-shaping control law that minimizes the geodesic distance at any point on the curve, we obtain closed-loop soft robots that exhibit stereotypical bending propagation closely resembling those found in octopi. This result further highlights the importance of model-based control in the pursuit of developing robotic systems with bio-like features that explore intrinsic structural flexibility to achieve task efficiency with possibly minimal energy expenditure. Finally, we investigate the affects of reduced-order controllers applied to high-dimensional system. We introduce a quasi-static continuum deformation solver that estimates the reduced controller states such that an energy-shaping technique can be applied. We observe that, irrespective of the truncation, all controllers converge towards a close vicinity of the desired configuration – even for extremely low-order models. This finding has the potential to reduce the significance of basis span in the effectiveness of model-based control for soft robots. It suggests that soft robots may possess inherent redundancy that can compensate for modeling imperfections. This sheds light on why PCC models, despite their oversimplification, exhibit good efficacy in controlling soft robots.

There are, however, a few limitations to our approach. The strain parametrization of functional basis does not account for the geometry of the soft robot, meaning some systems require many spatial modes to *accurately* represent the true continuum dynamics. Second, regarding implementation, measuring these spatial modes in an experimental setting is difficult, and future research is required to find a suitable '*soft sensing*' technique that (*i*) has limited impact on the dynamics, and (*ii*) accounts for the continuity of the elastic body. A possible solution might be the optimal placement of a network of distributed localized sensors, *e.g.*, strain gauges or IMUs. Furthermore, the proposed controller is only suited for set-point regulation or slow-varying references. Exploring (fast)-dynamic control objectives will likely require more research. In particular, controllers that suppress natural

resonances of continuum elastic body under fast motion. One could argue that this perhaps fights against the natural dynamics of the soft robot, yet such oscillations might be able to be explored for locomotion or soft manipulators throwing objects rather than traditional pick-and-place strategies.

Given these limitations, future work will focus on (*i*) validating the controller experimentally, and (*ii*) constructing a bases using '*snapshot decomposition method*' of FEM-driven data. In particular, the latter two goals could be interesting to explore. Both advantages in FEM and Cosserat models, being accurate continuum deformations and computational efficiency; leading to a modeling strategy for *optimal* finite-dimensional state projection with insightful structures of the passive and active joints.

6

Sorotoki: a MATLAB toolkit for design, modeling, and control of soft robots

Abstract - In this chapter, we present **Sorotoki**, an open-source toolkit in MATLAB[®] that offers a comprehensive suite of tools for the design, modeling, and control of soft robots. The complexity involved in researching and building soft robots often stems from the interconnectedness of design and control aspects, which are rarely addressed together as a unified problem. To address the complex interdependencies in soft robotics, the **Sorotoki** toolkit provides a comprehensive and modular programming environment composed of seven Object-Oriented classes. These classes are designed to work together to solve a wide range of soft robotic problems, offering versatility and flexibility for its users. We provide a comprehensive overview of the **Sorotoki** software architecture to highlight its usage and capacities. The details and interconnections of each module are thoroughly described, collectively explaining how to gradually introduce modeling complexity for various soft robotic scenarios. The effectiveness of **Sorotoki** is also demonstrated through a range of case studies, including novel problem scenarios and established works widely recognized in the soft robotics community. These case studies cover a broad range of research problems in the field of soft robotics, including: inverse design of soft actuators, passive and active soft locomotion, object manipulation with soft grippers, meta-materials, model reduction, model-based control of soft robots, and shape estimation. Additionally, the toolkit provides access to four open-hardware soft robotic systems that can be fabricated using commercially available 3D printers.

This chapter is based on: B.J. Caasenbrood, A.Y. Pogromsky, and H. Nijmijer. **Sorotoki: a MATLAB toolkit for design, modeling, and control of soft robots** (*in preparation for submission*).

6.1 Introduction

Since the late 1980s, roboticists have been developing fluid-driven robots inspired by biological systems. Examples include the pneumatic three-link soft robot manipulator developed by Wilson et al. [307–309] and the fluidic four-fingered soft gripper presented by Suzumori et al. [261, 262], which both showing high dexterity for advanced object manipulation without the need for advanced (contact-aware) controllers. Although the design and control of these robots were simple, their level of dexterity and adaptability was previously unseen in rigid robotics and strongly resembled biological systems. These benefits were achieved through the use of "*soft materials*" paired with fluidic actuation, where "*soft*" refers to the collective mechanical properties of highly compliant materials such as flexibility, compressibility, and mechanical robustness. Just as nature exhibits diverse evolutionary solutions to environmental locomotion and manipulation, soft materials possess a plethora of beneficial mechanical properties that can be applied to robotics. Today, the philosophy of building robots from soft materials has significantly matured and has become a well-recognized field known as "*soft robotics*".

6

Due to their mechanical composition, soft robots offer several potential advantages compared to traditional rigid robots [230]. First, these robotic systems are less likely to cause injury during collisions, making them a more suitable alternative for tasks involving close human-robot interaction. Secondly, soft robots possess the ability to adapt to unstructured environments and manipulate a diverse array of objects through their ability to change shape and conform adaptively to their surroundings [120, 174]. These features are somewhat analogous to those found in nature, such as the trunk of an elephant grasping tree branches or the tentacles of an octopus squeezing through narrow spaces. Soft materials can be tuned to allow for delicate grasping [91, 244] or high-power densities [162]. Additionally, their high adaptability paired with tunable low compliance make them extremely robust towards abrupt impacts or high compression forces [18], making them suitable for various tasks in harsh environments without breaking [106, 159, 286]. Moreover, soft robots are typically constructed from low-cost materials and fabricated through straightforward manufacturing processes, such as rubber casting, making them more cost-effective compared to traditional rigid robots. With recent advances in soft material Additive Manufacturing (AM), soft robots can even be fully 3D-printed [297, 316]. This not only reduces production time and cost, but also allows for the embedding of printed on-board logic [119, 306]. Additionally, soft robots tend to be lightweight, making them easier to handle and transport, making them ideal for wearable robotics.

6.1.1 Problem formulation

Although significant progress has been made since their inception, generalized solutions for the design and control of soft robots are still lacking in comparison to those available for rigid robots. This can be partially attributed to the in-

herently nonlinear and high-dimensional nature of the mathematical descriptions for deformable robotic bodies composed of soft materials. This presents major challenges in finding suitable models that enable fast simulation, which ultimately hinders efficient structural design and model-based controller design. Despite the numerous challenges in soft robotics, two major research trends can be recognized within the soft robotics community:

A: Design of soft actuators and sensors. A majority of the soft robots are actuated in two ways [230]: (*i*) local actuation through variable length tendons (e.g., cables [222] or shape-memory alloy wires [6]) or (*ii*) distributed actuation through responsive soft materials [294] or surface loads using fluidics [78, 89, 106], commonly implemented as fluidic networks embedded within the soft body. The latter method is often referred to as Fluidic Elastomer Actuators (FEAs) or Soft Fluidic Actuators (SFA). FEAs can be designed through either geometric asymmetries in their structural design or by incorporating a composition of different materials, such as fibers or meshes, that induce the desired deformation when pressurized. While FEA designs date back to the 1980s, there remain significant gaps in understanding and applying established engineering principles to their design. FEAs frequently experience large deformation when actuated, leading to slow actuation due to material relaxation or, in more severe cases, fatigue or tearing caused by ballooning [174] – almost inherent to the elastomeric material effects of FEAs. Furthermore, low-compliance soft elastomer actuators often undergo parasitic deformation when exposed to external forces, like gravitational load. To efficiently solve the design cycle in soft actuators, it is essential to have a comprehensive understanding of the nonlinear deformation characteristics of soft materials under static and dynamic conditions.

On the contrary, proprioceptive soft sensing technology is still in early stages. The high compliance of soft robots often makes it difficult to apply common embedded sensors, such as encoders, capacitive sensors, strain gauges, and inertial sensors. These sensors are well-suited for rigid robots with articulated joints, as they are effective in measuring local joint displacement. However, in soft robots, displacement is often distributed, rendering these sensors less suitable. Furthermore, these sensors must be designed to minimize their impact on mechanical impedance, in order to minimize changes to the structural dynamics and operational workspace. A common approach is to incorporate microfluidic channels filled with a conductive liquids [208, 269, 276], such as Eutectic Gallium-Indium (EGaIn), into the soft body, that are placed antagonistic to the soft actuator. Upon deformation, the resistance changes, allowing for the correlation of specific deformation profiles with the soft robot. Other solutions incorporate integrated Hall sensors to measure changes in the magnetic field of ferromagnets distributed throughout the body [16, 245], or utilize fiber-optic grating bending sensors [92]. Generally speaking, the relationship between sensor output and deformation is non-trivial and often requires the extensive acquisition of *a-priori* measurement data (sometimes synthetic) to be mapped onto a set of motion primitives.

The geometry of soft actuators and sensors plays a crucial role in determining

their functionality and performance. Currently, most soft robotic components are designed using Computer-Aided Design (CAD) software similar to those used for rigid robots. However, as the geometric complexity of soft robots increases, particularly with the increasing trend towards bio-inspired and 3D-printed designs, there is a growing need for software that can handle free-form designs and have predictive capabilities for soft material deformation.

B: Modeling and control of soft robots. With the aim of achieving comparable performance to rigid robots and eventually biological creatures, there is a strong demand for advanced closed-loop control in soft robotic systems. However, the challenges in soft actuation and sensing extend directly to several modeling and control paradigms for soft robots [12, 70]: (i) their high dexterity and adaptability are challenging to incorporate into a modeling framework, and (ii) due to their continuum elastic bodies composed of a finite number of actuators and sensors, soft robots are inherently under-actuated and under-sensed, a problem common to infinite-dimensional systems (*e.g.*, continuum systems). In regard to the closed-loop control of soft robots, the field has introduced two distinct branches that can competently address the relevant issues.

Model-based control uses first-principle mathematical models of the system being controlled to design and implement controllers. The derived models often have conventional structures, *e.g.*, Lagrangian or Port-Hamiltonian, that is (closely) analogous to classic rigid robotics [12, 70, 197, 256]. As such, they extend (with minor modification) to existing control strategies including model-based feedback control [78, 186], impedance control [72], adaptive control [137, 290], iterative learning control [108], and energy-shaping control [28, 43, 86, 87]. Also, model-based approaches provide physical interpretations of the control gains, making controllers more transparent in terms of stability guarantees. Nonetheless, for some scenarios, first-principle modeling approaches (*i.e.*, Euler-Lagrange methods) will not suffice. For example, during environment or self-contact, it can be challenging to select a finite-dimensional state representation of the soft robotic model that balances precision and computational efficiency. Also, *a-priori* unknown system uncertainties, such as unreliability of sensors and actuators, model mismatches, and time-varying parameters, can impede the approach altogether.

Data-driven modeling focuses on utilizing existing data to establish the connection between inputs and outputs, instead of depending on prior knowledge or assumptions to formulate a theoretical model. The training data can be derived from measurements or high-fidelity surrogate models, which empowers the model to adapt as new information becomes available, similar to adaptive control. Despite often being black-box or grey-box approximators, these methods can tailor low-dimensional models which makes highly efficient as simulators. As an alternative, synthetic data generated from digital environments can be used to train learning controllers, *e.g.*, in Reinforcement Learning (RL) [236, 275]. Model-Predictive Control (MPC) can also be applied within a data-driven framework [34, 121]. However, in both cases, it is crucial that the training data be comprehensive enough to encompass the entire dynamic workspace. This requirement limits the general-

izability of the method to unseen scenarios and necessitates retraining for specific control objectives. Additionally, control policies learned through virtual environments may not be effective in the physical system due to differences with reality, known as the Simulation-to-Reality (Sim2Real) barrier [152].

6.1.2 Contribution of Sorotoki software

To address some of these challenges, we introduce **Sorotoki** (short for Soft Robotics Toolkit), an open MATLAB® toolkit for soft robotics that offers a range of tools for design, modeling, and control. **Sorotoki** aims to reduce barriers to entry in the field of soft robotics by providing a comprehensive software package that integrates various layers of modeling and control approaches, including continuum mechanics, dynamic systems and control theory, topology optimization, computer graphics, real-time control, and vision-based sensing. These diverse capabilities provide a highly flexible programming environment that can facilitate the development of innovative soft robotics research. The main feature of the **Sorotoki** are listed below:

1. **Design and fabrication** – Implicit modeling using Signed Distance Functions (SDFs), mesh generation, computational design, STL generation for 3D printing;
2. **Modeling and control** – Finite Element Models (FEM), high-efficiency reduced-order soft beam models (Lagrangian or port-Hamiltonian), programmable interconnections of a network of dynamic systems, e.g., soft robots, pressure reservoirs, and inertial rigid bodies.
3. **Actuation and sensing** – Real-time, high-precision, fluidic control platform using Raspberry Pi, vision-based sensing using RGB-depth camera;
4. **Visualization** – Fast and responsive 3D graphics rendering, mesh deformation modifiers, FK/IK-rigging.
5. **Accessibility** – A minimal programming syntax, characterized by the ability to express complex problems with a minimal number of lines of code.
6. **Open hardware** – Four 3D-printable soft robots (*e.g.*, soft hand, soft manipulator).

We briefly detail the organization of the paper. Section 6.2 reviews existing open-source soft robot software packages. Section 6.3 then assists the reader in getting started with the toolkit and introduces the open-source soft robotic systems. In Section 6.5, we detail the software architecture, the theory underlying the *Sorotoki* functions, and how the theory can be applied through coding examples in *Sorotoki*. Once the reader is familiar with the basic software architecture, Section 6.6 presents advanced study cases based on seminal works in soft robotics research. The paper concludes in Section 6.7 with a summary and outlook for future work.

6.2 Related works

Over the past two decades, significant advancements have been made in the field of soft robotics. To support the growing community, researchers in the field have made efforts to provide open-source software tools alongside their scientific contributions. This section provides a review of related work on open-source software packages for soft robotics, comparing these software packages and discussing how *Sorotoki* addresses any gaps in functionality.

One widely used tool is the **SOFA** (Stand Alone Open Framework for Animation) software [75], which is an open-source framework for real-time physically-based simulations of mechanical systems. Relevant to soft robotics, **SOFA** is commonly used to simulate the behavior of soft robots and to design and test control algorithms on real platforms [57, 75]. **SOFA** employs the Finite Element Method (FEM) to describe the continuum deformations of inertial elastic bodies. FEM is a numerical technique that solves partial differential equations (PDEs) that describe physical systems by dividing the domain of the system into small elements and approximating the PDEs with a set of algebraic equations [115, 146]. FEM models generally provide high-accuracy volumetric deformation simulations of soft materials, but their high state dimension, which can often be in the thousands or millions of degrees of freedom, can render them computationally expensive for state feedback. To enhance efficiency, Goury et al. [100] have explored model reduction using snapshot Proper Orthogonal Decomposition (POD).

Snapshot POD [14, 20] is a method for significantly reducing the dimensionality of a model by collecting snapshots of its state and utilizing Singular Value Decomposition (SVD) to identify the principal components. The projection is achieved by taking a linear combination of the principal components, weighted by their corresponding coefficients (also known as "modes"). The resulting projection is then a reduced-order model of the original system, which can be used for faster simulation. In addition to improving speed, this approach also provides accurate, robust, and efficient models suitable for closed-loop controller design [5, 280, 287, 312]. The numerical FEM model in **SOFA** incorporates both the structural geometry and material properties, facilitating the transfer of control policies to physical systems. This has enabled successful control synthesis using **SOFA** in various experimental settings [136, 312]. **SOFA** also includes tools for real-time visualization and data analysis, making it a valuable platform for testing and debugging control algorithms. Recently, Schegg et al. [236] introduced an interface between **SOFA** and **OpenAI** called **SofaGym**. This wrapper enables the training of reinforcement learning (RL) policies using real-time simulation models, and it incorporates model reduction to further improve the efficiency of RL that otherwise suffer from computationally-intensive simulations.

Another software package that utilizes the nonlinear finite element approach similar to **SOFA** is the **Gibbon** toolbox, developed by Moerman et al. [191]. **Gibbon** is a MATLAB-based pre-processor and post-processor for **FEBio** [171]. The toolkit has recently been used to solve the nonlinear deformation of bending

soft pneumatic actuators using finite shell elements [250], generate designs using a multi-objective heuristic [251], and analyze soft bending actuators composed of an adaptive fiber-elastomer composite [132]. It also features various tools for image segmentation, meshing, and visualization, with a focus on biomedical engineering.

Despite the availability of open-source FEM packages for modeling and controlling soft robots, challenges still exist in using FEM for design-based optimization of these systems, particularly due to the complexity of hyper-elastic materials and fluidic actuation, which are crucial in the field of soft robotics. Currently, there are limited options for frameworks that effectively and efficiently address these issues, although recent developments are promising. Smith et al. [252] recently proposed a versatile free-form design and fabrication workflow called **SoroForge**, which builds upon [250, 251]. Unlike volumetric representation, their approach can design complex soft actuator exteriors using a highly-flexible and fast node-tree interface of implicit function primitives. However, these generative CAD solutions are limited to only addressing quasi-static deformations and do not consider the deformation induced by control.

There are several software packages specifically designed for the dynamic locomotion of soft robots, which take into account the structural design, actuator placement within the soft body, control actions, and even adapt the body's topology accordingly. One such example is **EvoSoro** developed by Kriegman et al. [152], which builds on the work of Hiller et al. [107] and Cheney et al. [46]. This study discretizes a soft continuum body into small voxels, which can be assigned different cell types: soft or hard passive cells, or two different muscle cell types that undergo periodic contraction with an $+ \pi$ phase offset. The dynamic behavior of the system is modeled through a network of mass particles and springs, and a Compositional Pattern-Producing Network (CPPN) is utilized to determine the optimal combination of material type and placement within a specified domain, enabling locomotion. This concurrent optimization of topology and control policy, referred to as "*co-design*", is a subject of active research within the field of soft robotics [316]. Another example of co-design in soft robotics is **EvoGym** [26], which optimizes for a wide range of tasks such as locomotion and object manipulation (e.g., carrying and throwing). More recently, **DiffTachi** (the successor to **QueenChain** [118]) is a differential programming environment that allows users to directly provide gradient-based information into a neural network controller using a least-squares Material Point Method (MPM). Unlike FEM, MPM is a mesh-free approach that describes the continuum using a finite number of hybrid Euler-Lagrangian elements referred to as "material points". In terms of learning control policies, **SoMoGym** by Graule et al. [101] uses reinforcement learning (RL) to teach locomotion and object manipulation in soft robots, and has successfully bridged the gap between simulation and reality (Sim2Real). It is important to note that **QueenChain**, **DiffTachi**, and **SoMoGym** focus purely on learning control and not design. Simultaneous optimization of (free-form) design and control for soft robots remains an open challenge.

Parallel to volumetric-based FEM or MPM soft robotic software, there also

exists a branch of dynamic beam (or rod) models for soft robots. These beam model approaches for soft robots have long been a viable alternative to FEM-based models – examples include the Piecewise-Constant Curvature (PCC) model [38, 78, 258], the augmented PCC rigid-body model [72, 137, 290], and various non-constant curvature descriptions [29, 72, 221, 303]. As the formulations of these models are often synonymous to rigid robot models, they have a rich basis of control-oriented research [28, 38, 82, 215]. TMTDyn by Sadati et al. [231] is a MATLAB toolkit that automates the derivation of dynamic models for hybrid rigid-continuum body soft robots, based on discretized lumped systems and reduced-order models. More recently, **SoroSim** was developed by Mathew et al. [180], which is a MATLAB toolbox with a graphical user interface for modeling, analysis, and control of soft, rigid, and hybrid robots. **SoroSim** is based on the Geometric Variable Strain (GVS) approach applied to the geometric Cosserat beam theory in SE(3), introduced relatively recently by Renda et al. [221] and Boyer et al. [29]. Its Lagrangian formulation also allows for various complex control designs, such as a geometrically-exact inverse kinematic controller that accounts for under-actuation of tendon-based actuation [180]. **SoroSim** has been used for dynamic models of flexible flying rods, hybrid rigid-soft manipulators, design optimization for soft robot swimmers, and inverse dynamic control. The toolbox has also been employed for the simultaneous swimming and grasping dynamics of underwater soft-rigid hybrid robots [179].

Alternatively, **PyElastica** (a wrapper for **Elastica** [201]) by Tekinalp et al. [275] is an open-source software package written in Python that provides the capability to simulate an assembly of Cosserat beams. The software is based on the work of Gazzola et al. [95]. Unlike the Geometric Variable Strain (GVS) approach proposed in [29, 180, 221], **PyElastica** employs a discrete formulation of the Cosserat partial differential equation (PDE) through a finite number of line elements referred to as Discrete Elastic Rods (DERs). Additionally, its c++ architecture enables it to handle problems with higher computational complexity. As demonstrated in [323], **Elastica** has been used to model snake muscular systems, bird wing flapping, and bio-hybrid robots using soft contractile filaments. Furthermore, **PyElastica** has been utilized in energy-based control and even extended to model the full muscular-skeletal system of an octopus' tentacle modeled as an array of Cosserat beams [42], and mimic biological movements accordingly [301]. It also provides wrappers for **OpenAI** to enable reinforcement learning.

To summarize, Table 6.1 provides an overview of the functionalities of the previously discussed software packages for soft robotics. The table highlights the diversity of software options available, each with specialized solution approaches for specific sub-problems in soft robotics. However, there are limited tools that address the combined issues of design and control in an interdependent, holistic manner. For instance, developing a model-based controller for a specific soft robot heavily relies on its structural geometry, material composition, network of soft actuators, and their dynamic interaction with the soft body. On the other hand, finding a suitable soft robot design requires *a-priori* knowledge of the ma-

Table 6.1. Comparison between different open-source software provided by the soft robotics community that are tailored either towards design, modeling, or control of soft robots. *Inverse design here refers to automated algorithms that freely optimize the topology of the soft body. †Sim2Real here implies the software has been used on a real soft robotic platform – either successfully transferring open or closed-loop control policies to reality; or optimized design solution to real soft systems.

Software	Front-end	Model(s)	Hyperelastic	Tendon	Fluidic	Locomotion	Manipulation	Inv.	Design*	Control	Sim2Real†
<i>SOFA</i> [57, 76]	Python	(Reduced) FEM	✓	✓	✓	✓	✓	✗	✓	✓	✓
<i>Gibbon</i> [191]	Matlab	FEM	✓	✓	✓	✗	✗	✓	✗	✗	✗
<i>SoRoForge</i> [232]	Matlab	Shell-FEM	✓	✗	✓	✗	✗	✓	✗	✗	✓
<i>SoftIK</i> [23]	C++	FEM	✓	✓	✗	✓	✓	✗	✗	✓	✓
<i>EvoGym</i> [26]	Python	Mass-spring	✗	✗	✓	✓	✓	✓	✗	✗	✗
<i>EvoSoro</i> [46, 152]	Python	Mass-spring	✗	✗	✓	✓	✓	✓	✗	✗	✓
<i>DiffTachi</i> [118]	C++	MPM	✗	✗	✗	✓	✓	✓	✗	✗	✗
<i>TMTDyn</i> [180]	Matlab	ROM + EBA	✗	✓	✓	✗	✓	✗	✓	✓	✓
<i>SoroSim</i> [180]	Matlab	Cosserat	✗	✓	✓	✓	✓	✓	✓	✓	✗
<i>(Py)Elastica</i> [95]	Python	Cosserat	✗	✓	✗	✓	✓	✓	✗	✓	✗
<i>SoMoGym</i> [101]	Python	Rigid-link	✗	✗	✓	✓	✓	✓	✗	✓	✓
<i>Sorotoki</i> (ours)	Matlab	FEM + Cosserat	✓	✓	✓	✓	✓	✓	✓	✓	✓

terial properties and their deformation under the admissible control inputs. This complex interplay between design, modeling, and control makes studying and developing soft robots a challenging task. **Sorotoki** aims to address these challenges by integrating the scientific disciplines of design and control into a unified toolkit.

6.3 Getting started with Sorotoki

In the following section, we briefly detail a starter’s guide for **Sorotoki**. The software package **Sorotoki** is available via git:

```
$ git clone https://github.com/BJCaasenbrood/SorotokiCode.git
```

To install the toolkit, request the documentation, or preview demonstrations of the toolkit, we call

> sorotoki install	% installation toolkit
> sorotoki doc	% provides documentation
> sorotoki demo	% provides example scripts

in the *Matlab* command prompt, respectively. The online documentation provides information on the features and capabilities, installation instructions, general use, syntaxing and a selection of toy examples. The documentation assists users in comprehending and efficiently navigating the software for their research purpose, and it serves as a complement to the work presented herein.

6

6.4 Open-source soft robots of Sorotoki

Aside from software, we also present a selection of open-source soft robotic systems, see Figure 6.1, as part of the **Sorotoki** toolkit. These systems all feature fluidic actuation and can be fabricated using conventional additive manufacturing techniques such as Selective Laser Sintering (SLS), Stereo-LithogrAphy (SLA), or Direct Light Projection (DLP). FormLabs Elastic 80ATM resin or a flexible TPU with a shore hardness of $\leq 80A$ are suggested for the elastically deformable bodies in SLA/DLP and SLS printing, respectively. Moreover, these soft robots can also be realized using multi-material Fused Deposition Modeling (FDM) with both flexible filaments (e.g., NinjaFlex) and water-soluble filaments. Nevertheless, FDM-fabricated systems may suffer from inferior quality, air-tightness, and anisotropy when compared to those produced by SLS or SLA/DLP. For that reason, we recommend SLS/SLA/DLP over FDM for its simplicity and reliability. For further details concerning the SLS/DLP manufacturing process, consult Proper et al. [214]. The 3D models (in .stl format) are publicly available through Git:

```
$ git clone https://github.com/BJCaasenbrood/SorotokiBots
```

A brief description for each soft robot and their functionality is provided below.



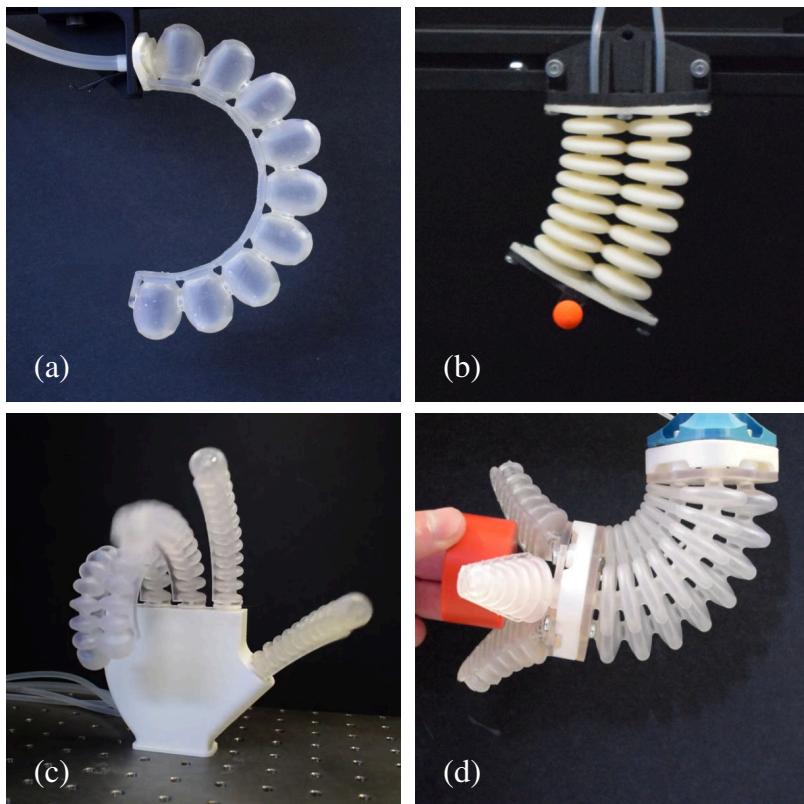


Figure 6.1. Open-source soft robots and soft actuators that are included within the Sorotoki toolkit. All systems are fully 3D-printed using either Selective Laser Sintering (SLS) or Stereolithography (SLA) and their 3D files can be found on the repository. All systems are driven by pneumatics. (a) A two-bellow soft robot suitable for planar motion. (b) An optimized PneuNet bending actuator. (c) A soft robotic hand composed of five soft bending actuators, whose fingers are easily replaceable. (d) A three-bellow soft robot manipulator with a mounted soft gripper at the end-effector. The center axis is hollow, allowing for electronic cables when compact sensors (*e.g.*, IMUs) are mounted on the soft gripper.

6

A: Soft bending actuator. The first system is a soft bending actuator (Figure 6.1a), an alternative to the PneuNet actuator proposed by Mosadegh et al. [195]. Like the PneuNet actuator, our soft actuator consists of an array of bellows placed on a relatively inextensible elastic medium. The stiffness gradient in the actuator allows for pure bending to occur when the network of bellows is pressurized. The geometry of the PneuNet-based soft robot was optimized using Sorotoki’s topology optimizer, which was specifically tailored for use with Form-Labs Elastic 80A resin. The soft actuator is fully 3D-printed using SLA and can accept pressures in the range of $-10 \leq u \leq 100$ kPa at its central pressure input.

B: Planar soft actuator. The second system is a planar soft actuator that comprises two pneumatic bellow networks that are connected in parallel (Figure 6.1b). Similar to the previous soft actuator, bending occurs due to a pressure differential between the two pneumatic networks. However, the system is also capable of pure elongation and contraction if the pressure in both networks is equal. This enhances the motion capabilities of the soft robot, enabling it to move within a planar workspace of approximately 100×100 mm. The system has two pressure range of $-10 \leq u \leq 50$ kPa.

C: Composable soft robotic hand. The third system provided by *Sorotoki* is a soft robotic hand with a higher level of complexity compared to the previous soft robots (Figure 6.1c). This design is inspired by the work of Laake et al. [293] and Fras et al. [89]. The soft robotic hand consists of five independently controlled soft fingers that can be actuated using pneumatics or fluidics. Each finger is fabricated using a SLS technique with Elastic 80A, while the base is fabricated using FDM with PLA. The dimensions and scale of the soft robotic hand are similar to those of a human hand, with approximate dimensions of $190 \times 100 \times 40$ mm. All fingers have a length of 90 mm except for the thumb, which is slightly shorter at 80 mm. The soft robotic hand has five independent inputs that accept pressures in the range of $-10 \leq u \leq 60$ kPa.

D: Full soft manipulator with soft gripper. The final soft robot provided by *Sorotoki* is a soft robotic manipulator that features three independent bellow networks and a three-fingered soft robotic gripper attached to the end effector (Figure 6.1d). With independent actuation of each bellow network, the manipulator has a full 3D workspace of approximately $150 \times 150 \times 150$ mm. The soft elements of the manipulator are fabricated using Elastic 80A resin, while the rigid connector pieces are made using Rigid 10K resin. The gripper has demonstrated the ability to successfully grip objects with a diameter of 40 mm, with a maximum payload of 100 g without significant parasitic deformation. The central axis of the manipulator is designed to be hollow, enabling the pneumatic tubing of the gripper and the cables for state estimation sensors (*e.g.*, IMUs) to be embedded. The manipulator has three inputs that accept pressure values in the range of $-10 \leq u \leq 30$ kPa, and the gripper has one input that accepts values in the range of $-30 \leq u \leq 60$ kPa.

Remark 6.1 High-resolution 3D models are available on the following repository at <https://github.com/BJCaasenbrood/SorotokiBots>. These models can be sliced for 3D printing using popular slicing software such as Cura, PrusaSlicer, or PreForm. Detailed assembly instructions can be found in the documentation on the repository. Additionally, low-resolution 3D models are provided on the repository under `./assets/stl/redux` for real-time visualization of the soft body's deformations.

6.5 Software architecture

In this section, we will present the software architecture of the *Sorotoki* toolkit. The toolkit consists of seven Object-Oriented classes, each designed to address a specific sub-problem within the field of soft robotics. We will introduce each class in the following sequence:

- In Section 6.5.1 we will discuss the class **Sdf**: a Signed Distance Function (SDF) class that are used to build spatial geometries – “*Implicit CAD*”;
- In Section 6.5.2 we will discuss **Mesh** responsible for mesh generation;
- In Section 6.5.3 we discuss the class **Fem**: a Finite Element Model (FEM) solver required for high-detail soft robot simulations;
- In Section 6.5.4, we detail the class **Shapes** responsible for soft beam models required for fast soft robot simulations;
- In Section 6.5.5 we explain **Model** – a model composer to interconnect various dynamic model, and the control synthesis;
- Following, in Section 6.5.6, we highlight **Control** that serves as a control interface for fluidic platform communicating to *Matlab* via TCP/IP;
- Finally, Section 6.5.7 will explain **Vision** – a Vision-based tool for state estimation of soft robots through optical markers.

To assist the reader, we have included a software architectural flowchart in Figure 6.2 that illustrates each class. The flowchart demonstrates how the classes can be interconnected to increase system complexity while maintaining the structured and separable nature of the subproblems. To further clarify their individual functionality, we will provide illustrative examples and corresponding MATLAB executable scripts. The topics covered include design, modeling and analysis, model reduction, and control and vision-based sensing, presented in this chronological order.

6.5.1 Signed Distance Function (**Sdf**)

Signed Distance Fields (SDFs) have been widely applied in various areas of computer graphics, including the representation of implicit surfaces [45, 219], collision detection in robotics [164, 205]. In particular, SDFs have gained attention for their use in implicit modeling [252], a technique for representing 3D shapes as continuous functions, rather than discrete mesh descriptions.

In *Sorotoki*, SDFs are implemented in the class **Sdf.m** and can be used to construct general 2D and 3D geometries. They can also be utilized to model static or dynamic contact environments, generate 3D models of soft actuators that are suitable for 3D printing, and compute inertia tensors for continuum bodies in \mathbb{R}^2 and \mathbb{R}^3 .

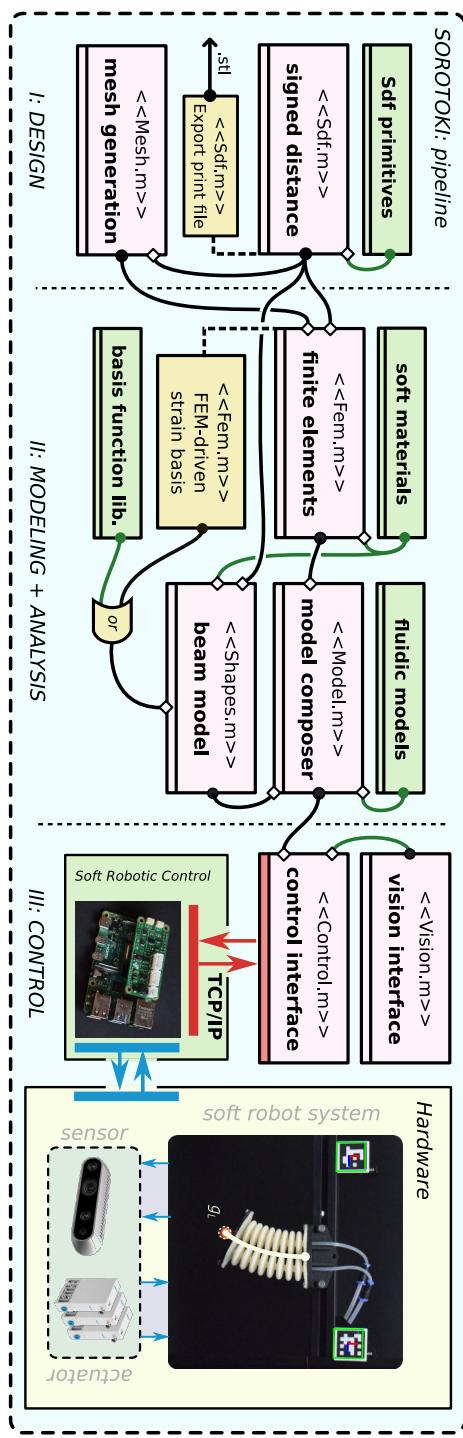


Figure 6.2. The Sorotoki software toolkit is structured according to a problem-solution pipeline, consisting of seven Object-Oriented classes that address common subproblems in the field of soft robotics research. These classes are: **Sdf**, **Mesh**, **Fem**, **Shapes**, **Model**, **Control**, and **Vision**. The software architecture flowchart employs the symbol (\bullet) to represent class outputs and the symbol (\diamond) to denote inputs. It is important to note the interplay between these classes.

A: Implicit modeling using SDFs. In this section, we briefly outline the mathematical foundations underpinning the `Sdf` class. As the name suggests, signed distance functions are a type of function that encodes distance information relative to an object defined implicitly. Adopting the notation used in [219], given a domain $\Omega \subset \mathbb{R}^n$ and its boundary $\partial\Omega$, these functions can be written in the following general form:

$$\text{sdf}(\mathbf{p}) = \begin{cases} -d(\mathbf{p}, \Omega) & \text{if } \mathbf{p} \in \Omega, \\ +d(\mathbf{p}, \Omega) & \text{if } \mathbf{p} \in \mathbb{R}^n \setminus \Omega, \end{cases} \quad (6.1)$$

where $d(\mathbf{p}, \Omega) := \inf_{\mathbf{y} \in \Omega} \|\mathbf{p} - \mathbf{y}\|_2$ is a scalar function that returns the smallest Euclidean distance from a sample point $\mathbf{p} \in \mathbb{R}^n$ to the boundary $\partial\Omega$. SDFs provide a simple and efficient way of determining the location of a set of points relative to a domain Ω defined implicitly. The SDF is a scalar function that encodes the Euclidean distance of a sample point $\mathbf{p} \in \mathbb{R}^n$ to the boundary $\partial\Omega$ of the domain. By evaluating the sign of the SDF, it is possible to classify the set of points as being within or outside the boundary of the domain. This enables set operations such as union, difference, and intersection to be performed.

In our software package, these operations are implemented using Matlab's arithmetic operators between two or more instances of the `Sdf` class, including '+' (union), '-' (difference), '/' (intersection), '*' (scaling), and '.*' (repeating). By utilizing these set operations and a library of basic SDF primitives, it is possible to construct a wide range of complex geometries with relative ease. Subsequently, the SDFs can be transformed into a `.stl` file using the Marching Cube algorithm [167], enabling 3D printing. This functionality is implemented in the command `sdf.export`.

Example 6.1 (Implicit CAD using SDFs). To demonstrate the use of signed distance functions in `Sorotoki`, we present an example of 2D and 3D implicit modeling scheme as shown in Figure 6.3. This example illustrates the utilization of various SDF primitives, which are combined through standard set operations, such as union, difference, and intersection, to generate complex geometries. The accompanying code is provided below:

```

1  %% EXAMPLE: Sdf class
2  % generate 2D sdf
3  c    = sCircle(1);
4  r    = sRectangle(1);
5  sdf = r.rotate(pi/4)-c;
6
7  % generate 3D sdf
8  S1  = sSphere(0,0,0,1,0.5);
9  S2  = sSphere(0,0,0,0.5,1);
10 C   = sCube(0,1,0,1,0,1);
11 sdf = (C - S1)/S2;
```

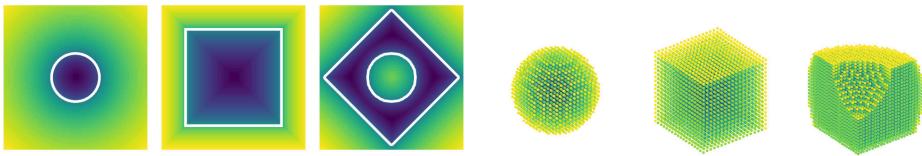


Figure 6.3. Exemplary functionality of the Signed Distance Function (Sdf) operators in *Sorotoki*. The top figures are two-dimensional Sdfs, whereas below are three-dimensional Sdfs. *Sorotoki* allows the user to combine Sdf using Matlab's arithmetics, like '+', '−', and '/', to perform unions, differences, and intersections, respectively. These set operations like union, difference, and intersect lead to new (differentiable) SDFs.

B: SDF differentiability Contrary to mesh-based geometries, signed distance functions (SDFs) possess closed-form differentials. Specifically, if Ω is a subset of \mathbb{R}^n with piecewise smooth boundaries, the SDF is (i) differentiable almost everywhere, and (ii) its gradient satisfies $|\nabla \text{sdf}| = 1$. As a result, the unit-normal vector $\mathbf{n}(\mathbf{p})$ pointing away from the boundary $\partial\Omega$ can be expressed as $\mathbf{n}(\mathbf{p}) := \nabla \text{sdf}(\mathbf{p})$. The gradient can be estimated using a finite-difference scheme:

$$\mathbf{n}_i(\mathbf{p}) \approx \frac{1}{\varepsilon} [\text{sdf}(\mathbf{p} + \varepsilon \boldsymbol{\delta}_i) - \text{sdf}(\mathbf{p})], \quad (6.2)$$

where $\boldsymbol{\delta}_i$ is a vectorized Kronecker delta and ε a small increment.

Such finite difference routine is efficiently implemented such that the normal, tangent, and bi-normal vector computations can be called using `[N,T,B] = Sdf.gradient(p)`. These gradient vector computations are crucial for contact dynamics with the environment whose topology may be arbitrarily complex. The normal vector can also be useful in finding the closest-point projection onto the surface $\partial\Omega$, namely $\text{proj}_{\partial\Omega}(\mathbf{p}) := \mathbf{p} - \text{sdf}(\mathbf{p}) \cdot \nabla \text{sdf}(\mathbf{p})$. The projection operator is implemented as `[P,d] = Sdf.project(p)`, which takes a point cloud \mathbf{p} and returns a point cloud \mathbf{P} that is mapped onto the boundary of the SDF. It also returns the Euclidean distance $d(\mathbf{p}, \partial\Omega)$ from the surface. This can be extremely useful in simulations of soft robotic grippers for grasping, or obstacle avoidance for soft manipulators.

6.5.2 Mesh generation for finite element analysis (Mesh)

In finite elements and computer graphics, mesh tessellation is a common language used to describe the structural geometry through a finite collection of vertices and edges. In *Sorotoki*, meshes and mesh generation features are packaged into the class `Mesh.m`. In general, a mesh defines a discrete representation of a continuum body that is subdivided into smaller convex sub-volumes, referred to as "elements". The nodal and elemental information are stored in data structures that can be accessed using `msh.Node` and `msh.Element`, respectively. For two-dimensional FEM problems, it is common to use linear elements such as `Tri3` and `Quad4` or

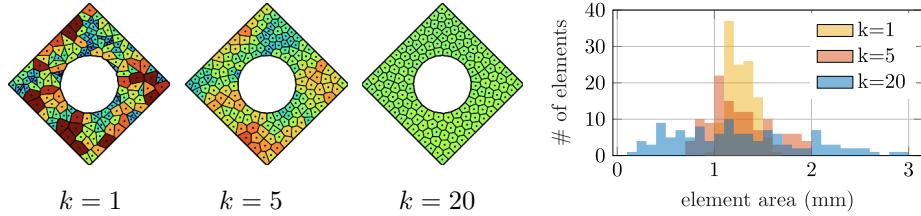


Figure 6.4. Example of mesh generation in **Sorotoki**. The figure shows the evolution of an unstructured polygonal mesh based on Lloyd’s algorithm. The colors relate to the relative element size with respect to the mean element size, given by $\text{color} \in [0, 2] \text{ mm}^2$. Notice that only after a few iterations, the centers of the Voronoi cells become homogeneously distributed within the domain Ω .

quadratic elements like **Tri6** and **Quad8**. For three-dimensional FEM problems, the common practice is to use hexahedron elements (*i.e.*, **Hex8**) or tetrahedral elements (*i.e.*, **Tet4** and **Tet12**). There are also polygonal tessellations, often denoted as **PolyN** finite elements [268]. **Sorotoki** supports all these types.

A: Mesh generation from SDFs. The **Sorotoki** toolkit explores several routines for mesh generation, which are all contained in the class **Mesh.m**. Our primary focus is on using a modified version of the **PolyMesher** software developed by Talischi et al. [268]. Their work provided a stable foundation for generating unstructured meshes of **PolyN** elements. The approach starts by defining a material domain implicitly using SDFs (as discussed in Section 6.5.1). The number of elements is chosen *a priori*, and then repeated random sampling of Equation (6.1) is performed until the number of samples that fall within the specified domain matches the number of elements. A bounded Voronoi diagram is generated using the samples and the centers of the Voronoi cells are updated using Lloyd’s algorithm [165]. To generate a mesh from an **Sdf** class, one can call `msh = Mesh(Sdf)` followed by `msh = msh.generate()`.

Example 6.2 (Meshing of SDFs). We provided a mesh generation example in Figure 6.4 where we used the SDF function from the previous example to generate our tessellation. The code is given below. In Figure 6.4, we see the evolution of the Voronoi cells that produce the **PolyN**-type mesh. Observe that after a few iterations of Lloyd’s algorithm, the centroids are distributed homogeneously over the compact domain Ω (as shown by the color distribution).

```

1  %% EXAMPLE: Mesh class
2  % generate sdf mesh domain
3  c    = sCircle(1);
4  r    = sRectangle(1);
5  sdf = r.rotate(pi/4)-c;
6
7  % sdf conversion to mesh
8  msh = Mesh(sdf,'NElem',150);
9  msh = msh.generate();

```

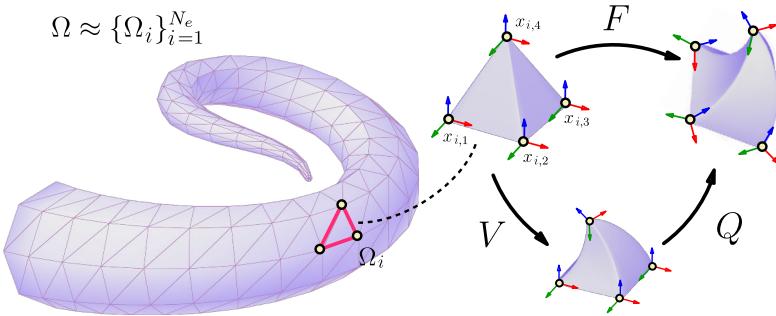


Figure 6.5. Illustration of the Finite Element Method (FEM), where a solid geometry Ω is subdivided into N_e finite elements Ω_e . Each element has $\dim(\mathbf{x}_e)$ DOFs, which allows the computation of the deformation gradient \mathbf{F} . The deformation gradient can be decomposed into $\mathbf{F} = \mathbf{Q}\mathbf{V}$, an isochoric deformation part \mathbf{V} and rigid-body rotation part \mathbf{Q} .

6

B: Mesh from common file formats An alternative option is to use the mesh generation tools provided by the Partial Differential Toolbox in Matlab. Such function is also included in `Mesh.generate`. SDFs can also be used in this process, although an intermediate step is required. For two-dimensional domains, SDFs are first converted into binary images and then the image boundary detection is used to convert them to either a linear mesh (`Tri3`) or a quadratic mesh (`Tri6`). Direct input of black-and-white `.jpg` or `.png` images is also supported. For three-dimensional domains, SDF functions are converted to an `.stl` file using the Marching Cube algorithm [167] and then provided to the Matlab PDE toolbox to generate the tessellation. Importing `.stl` or `.obj` files directly is also possible. Meshes can also be export

6.5.3 Finite element modeling (`Fem`)

Following the mesh generation process, *Sorotoki* offers a nonlinear finite element solver for both quasi-static and fully dynamic simulations. An illustration of the FEM approach is given in Figure 6.5. FEM-based tools are crucial when describing large deformations in soft robots, which also accounts for hyperelastic materials and geometric nonlinearities. The FEM package is provided in a class called `Fem.m` and can be instantiated using `fem = Fem(Mesh)`. This class serves two main purposes: (i) to solve static or dynamic continuum problems with high accuracy, and (ii) to solve gradient-based optimization problems, also known as inverse design problems. It is important to note that, unlike `SOFA`, the focus of *Sorotoki* is on high-detail simulations rather than real-time implementation for control. The presented FEM simulation models are not intended for real-time applications, but rather for system identification and analysis.

A: High-detail finite element model. The nonlinear dynamics of the finite element model in *Sorotoki*, similar to `SOFA` and `Gibbon`, can be described by the

general Newton-Euler equation of motion:

$$\mathbf{M}\ddot{\mathbf{x}} + \mathbf{f}_{\text{mat}}(\mathbf{x}, \dot{\mathbf{x}}) + \mathbf{f}_g = \mathbf{f}_u(\mathbf{x}, \mathbf{u}, t) + \mathbf{f}_{\Omega_{\text{env}}}(\mathbf{x}, \dot{\mathbf{x}}, t), \quad (6.3)$$

where \mathbf{x} , $\dot{\mathbf{x}}$, and $\ddot{\mathbf{x}}$ are the global nodal displacement, velocities and accelerations of the mesh tesselation, respectively; \mathbf{M} the constant generalized mass matrix, \mathbf{f}_{mat} the internal soft material forces, \mathbf{f}_g the constant gravitational forces, \mathbf{f}_u a user-defined input, and $\mathbf{f}_{\Omega_{\text{env}}}$ the normal reaction forces and tangent friction forces imposed by the dynamic contact with a (possibly time-dependent) environment Ω_{env} . The environment Ω_{env} can be described using the SDF functionality (see Section 6.5.1) using the syntax `fem.addContact(sdf)`. A broad collection of generalized external inputs can be added using: `fem.addLoad`, `fem.addDisplace`, `fem.addGravity`, and `fem.addTendon`. Time-varying pressure inputs can be added using the command `fem.addPressure`.

Without loss of generality, the material force can be decomposed into a position-dependent and velocity-dependent part: $\mathbf{f}_{\text{mat}}(\mathbf{x}, \dot{\mathbf{x}}) = \mathbf{f}_e(\mathbf{x}) + \mathbf{f}_d(\dot{\mathbf{x}})$, *i.e.*, an elastic and dissipation contribution, respectively. We assume that the dissipation is given by $\mathbf{f}_d = \zeta \mathbf{M} \dot{\mathbf{x}}$ with damping coefficient $\zeta > 0$. Materials can be assigned using `fem.addMaterial`. Note that the conservative elastic material forces \mathbf{f}_e require more involved computation. Since this computation is not straightforward, we briefly explain the derivation of the nonlinear hyper-elastic material forces in (6.3), which follows standard nonlinear finite element procedures [115, 146, 249].

Intermezzo 6.1 (Deformation gradient). A fundamental measure of deformation in continuum mechanics is the deformation gradient, denoted by \mathbf{F} . The deformation gradient characterizes the local deformation for a neighborhood of the continuum body Ω . Since a subvolume of the continuum body cannot be reduced to a point, it follows that $\det(\mathbf{F}) = J > 0$ and \mathbf{F}^{-1} exists. The term J is called the relative volume change and it is equal to 1 for isochoric deformations, such as rigid body deformations. Given these properties, the deformation gradient can then be factorized into $\mathbf{F} = \mathbf{Q}\mathbf{V}$, where $\mathbf{V} > 0$ is the right-handed stretch tensor and $\mathbf{Q} \in \text{SO}(3)$ is a rotation matrix belonging to the special orthogonal group [115, 146, 249]. For convenience, we summarize the derived quantities of \mathbf{F} in Table 6.2 that will be used throughout this section.

Intermezzo 6.2 (Derivation of hyperelastic forces). Let Ω_i denote the subspace spanned by the i -th element of the finite element mesh, and let \mathbf{x}_i denote its nodal displacement vector. The elasticity of the constitutive soft material can be described by a strain-energy density function $\Psi : \mathbf{F} \rightarrow \mathbb{R}_{\geq 0}$. A comprehensive discussion on common constitutive models for Ψ will be provided later in the subsequent paragraph. The elastic potential energy of the continuum body is given by $\mathcal{U}_e = \int_{\Omega} \Psi(\cdot) dV$, and the conservative hyper-elastic force contribution can be computed as $\mathbf{f}_e := \nabla_{\mathbf{x}} \mathcal{U}_e$. This contribution can be approximated using

Table 6.2. Table of deformations measures relevant for continuum mechanics problem. All measures can be related to the first-order deformation tensor \mathbf{F} , following the works [115, 146, 249].

Deformation measure	Derivation
Relative volume change	$J = \det(\mathbf{F})$
Polar decomposition	$\mathbf{F} = \mathbf{Q}\mathbf{V}$
Right Cauchy-Green tensor	$\mathbf{C} = \mathbf{F}^\top \mathbf{F}$
First strain invariant	$I_1 = \text{trace}(\mathbf{C})$,
Second strain invariant	$I_2 = \frac{1}{2} [\text{trace}(\mathbf{C})^2 - \text{trace}(\mathbf{C}^2)]$
First strain invariant	$I_3 = \det(\mathbf{C})$

piecewise finite element interpolation and integrated using the Gauss quadrature rule [146] as follows:

$$\begin{aligned} \mathbf{f}_e(\mathbf{x}) &= \sum_{i=1}^{N_e} \frac{d}{d\mathbf{x}_i} \left\{ \int_{\Omega_i} \Psi(\mathbf{F}(\mathbf{x}_i, s)) ds \right\}, \\ &\approx \sum_{i=1}^{N_e} \sum_{j=1}^{N_w} w_j \underbrace{\frac{\partial \Psi}{\partial \mathbf{F}}(\mathbf{F}(\mathbf{x}_i, s_j))}_{\text{PK1}} \frac{\partial \mathbf{F}}{\partial \mathbf{x}_i}(\mathbf{x}_i, s_j) \end{aligned} \quad (6.4)$$

where the Gauss weights are denoted by $w_j > 0$, and the number of finite elements and Gauss samples are represented by N_e and N_w , respectively.

The term $\partial\Psi/\partial\mathbf{F}$ is also referred to as the first Piolla-Kirchhoff (PK1) stress tensor, which can be represented in closed-form for many constitutive models. The term $\partial\mathbf{F}/\partial\mathbf{x}_e$ denotes the deformation Jacobian, which can also be given in closed-form but depends on the choice of element type. In addition to the first Piolla stress tensor, we also introduce the Cauchy stress tensor (i.e., true stress) $\boldsymbol{\sigma} := J^{-1} \frac{\partial \Psi}{\partial \mathbf{F}} \mathbf{F}^\top$, which is a symmetric second-order tensor whose components represent the true stress. It should be noted that these tensor calculations are highly nonlinear, making their computation the most time-consuming aspect of the finite element assembly. To enhance computational efficiency, the toolkit employs .mex executable code, generated during installation (**Matlab Coder** is required).

B: Hyperelastic models and soft material presets. An important aspect of soft robotics in general is to accurately describe large nonlinear deformations of inertial continuum bodies in motion. Yet, due to these large deformations, many classical Hookean elasticity models may not be accurate for elastomer materials.

To address this, **Sorotoki** provides a library of hyper-elastic constitutive material models: Neo-Hookean (NH), Mooney-Rivlin (MR), and Yeoh model (YH). The strain energy densities for these models are derived based on the strain invariants I_1 , I_2 , and I_3 provided in Table 6.2 and are shown in Table 6.3. The material models presented in Table 6.3 are implemented in *Sorotoki* under the

Table 6.3. Table of material models included in *Sorotoki*, including the NeoHookean model (NH), Mooney-Rivlin model (MR), and Yeoh (YH) model.

Material model	Parameters	Energy-density potential Ψ
Neo-Hookean (NH)	(μ)	$\Psi_{\text{NH}} := \frac{\mu}{2} (I_1 - 3)$
Mooney-Rivlin (MR)	(c_1, c_2)	$\Psi_{\text{MR}} := \sum_{i=1}^2 c_i (I_i - 3)$
Yeoh (YH)	(c_1, c_2, c_3)	$\Psi_{\text{YH}} := \sum_{i=1}^3 c_i (I_1 - 3)^i$

class `Material`, but have specific constructors tailored towards each material, `NeoHookeanMaterial`, `MooneyMaterial`, and `YeohMaterial`. Regarding their parameters, the work of Marechal et al. [177] provides an open-source database that includes a broad collection of soft materials commonly used in soft robotics, gathered through uniaxial material tests. Based on their dataset and relevant other literature [100, 146, 249, 316], *Sorotoki* offers some preset material models of soft materials commonly used in soft robotics, such as the Ecoflex30/50 series, Dragonskin10/30 series, NinjaFlex, and Formlabs Elastic50A/80A material. These material classes also include the physical data for density, viscosity, and tangential contact friction. Following (6.4), the first Piola-Kirchhoff (PK1) stress tensor is evaluated analytically using the function call `P = Material.PiollaStress(F)`.

C: Finite element solvers and (nonlinear) modal analysis To solve the structural forward dynamics of the system (6.3), the toolkit uses an implicit Newmark- β solver [202], which is briefly outlined in Appendix E.1. Implicit solvers offer improved stability compared to explicit methods, such as the Runge-Kutta solver (`ode45`), particularly when larger time steps are employed. However, the cost of larger time steps is a decreased numerical precision. Alternatively, for quasi-static problems when $\ddot{\mathbf{x}} = \dot{\mathbf{x}} = \mathbf{0}_n$, we aim to seek the solutions to the static force equilibrium $\mathbf{r}(\mathbf{x}) = \mathbf{0}_n$ where $\mathbf{r} := -\mathbf{f}_{\text{mat}} + \mathbf{f}_g + \mathbf{f}_u + \mathbf{f}_{\Omega_{\text{env}}}$ is the force residual vector. The nonlinear equality for nodal displacements \mathbf{x} is solved using an iterative Newton-Raphson solver. To call these solvers, dynamic simulations are executed with `fem.simulate()` and quasi-static simulations with `fem.solve()`. Upon completion of a simulation, all displacements, velocities, forces, and stress information are stored in the `fem.Log` data structure. This log file can be accessed for data analysis or during simulation to facilitate state feedback control.

Alternatively, we can explore nonlinear modal analysis at any quasi-static equilibrium configuration $\mathbf{x}^* \in \mathcal{X}$ of the system (6.3). Let $\mathbf{K}_T := \begin{bmatrix} \frac{\partial \mathbf{f}_e}{\partial x_1} & \dots & \frac{\partial \mathbf{f}_e}{\partial x_2} \end{bmatrix}$ be the Jacobian matrix of the (nonlinear) elastic potential forces, also referred to as the tangent stiffness. Then, the local eigenvalue problem for the linearized FEM model around the point \mathbf{x}^* is given by

$$\left[\mathbf{K}_T(\mathbf{x}^*) - \lambda_i \mathbf{M} \right] \boldsymbol{\theta}_i = \mathbf{0}_n, \quad (6.5)$$

where λ_i is a real scalar eigenvalue and $\boldsymbol{\theta}_i$ is its corresponding eigenmode. The dy-

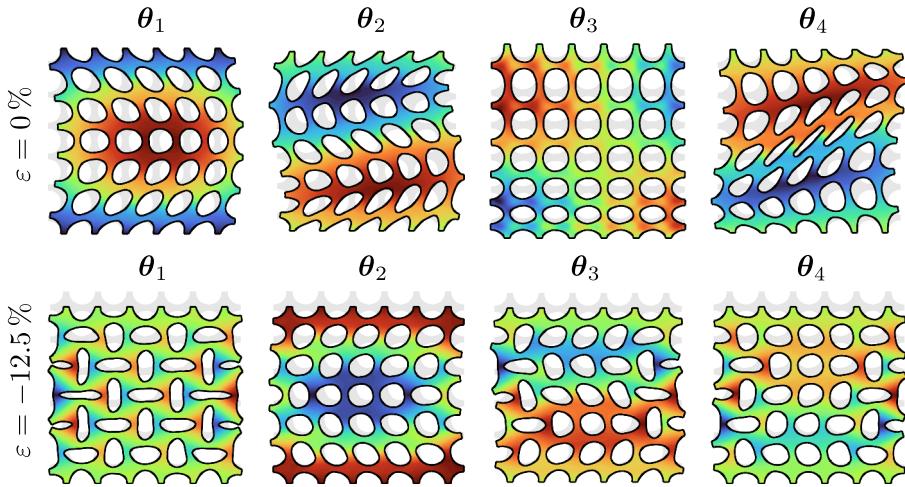


Figure 6.6. Nonlinear buckling mode analysis of periodic circular porous elastic structure inspired by [25, 207]. The horizontal displacements are indicated by $\colorbar \in [-5, 5]$ mm. (top) The first four eigenmodes of the elastomer structure for $\varepsilon = 0\%$ compression, no buckling modes appear. (bottom) The first four eigenmodes for $\varepsilon = -12.5\%$ compression. Notice that the first mode θ_1 is a buckling mode where the collapses holes orient periodically either vertically or horizontally.

6

namic analysis is implemented in Sorotoki using `fem = fem.analysis(x)`, which stores the necessary data in `fem.Log`. It is important to note that, unlike linear finite element models, the set of eigenmodes θ_i obtained from the eigenvalue decomposition in (6.5) is highly dependent on the linearization point x^* and may thus not be unique for all $x^* \in \mathcal{X}$.

Example 6.3 (Nonlinear buckling analysis via decomposition). An excellent case study of the eigenvalue problem in nonlinear elasticity systems is the buckling behavior of patterned elastomer metamaterials, as studied by Bertoldi et al. [25] and later by Overvelde et al. [207]. In their studies, an elastomer specimen with a periodic circular porous structure was subjected to uniaxial compression. The specimen displayed an inward buckling phenomenon at a critical loading point, resulting in the specimen exhibiting a negative Poisson ratio, *i.e.*, auxetic behavior. To be specific, the structure undergoes a so-called "bifurcation" where solutions switch stability or new solutions arise for a critical parameter value. In this case, the bifurcation parameter is the compression ratio ε .

In accordance with [207], a square elastomer specimen with circular holes was modeled using a Neo-Hookean material model, with Young's modulus $E = 19$ (kPa) and Poisson ratio $\nu = 0.45$. As reported in [207], the critical buckling point was observed to occur at approximately $\varepsilon = -12.5\%$ uniaxial compression.

A numerical solution is obtained through quasi-static analysis using the function `fem.solve`. To model compression, a displacement load was added using `fem.addDisplace('Top')`. The resulting equilibrium configuration was then uti-

lized in the eigenvalue problem via the function `fem.analysis(x)`. The eigenmodes for the zero-stress and $\varepsilon = -12.5\%$ compression cases are illustrated in Figure 6.6. It is worth noting that the first three eigenmodes of the elastomer structure at $\varepsilon = 0\%$ compression exhibit no buckling modes. Conversely, the first eigenmode θ_1 at $\varepsilon = -12.5\%$ compression displays a buckling mode, wherein the collapse of the holes is periodically oriented either vertically or horizontally. This buckling mode is in accordance with the experiments from [207] and [25]. The supplementary code is provided below:

```

1  %% EXAMPLE: Fem class
2  load('sdf_porous_square.mat');
3  msh = Mesh(sdf, 'NElem', 5e3);
4  fem = Fem(msh, 'TimeStep', 1/60);
5
6  % assign material
7  fem.Material = NeoHookeanMaterial(1.0, 0.45);
8
9  % add displacement and forces
10 fem = fem.addConstraint('Bottom', [1,1]);
11 fem = fem.addConstraint('Top', [1,0]);
12 fem = fem.addDisplace('Top', [0,-0.125 * W]);
13
14 % quasi-solve and eigen-analysis
15 fem = fem.solve();
16 fem = fem.analysis(fem.Log.x(:,end));

```

Example 6.4 (Locomotion dynamics of soft crawling robot). To demonstrate a dynamic finite element method (FEM) simulation that incorporates contact, we will utilize `Sorotoki` to model the locomotion of a multi-gait soft robot crawler inspired by the work of Shepard [238]. The study by Shepard et al. [238] presents a soft robot system that consists of five pressure chambers - four for each leg and one for the spine. The pressure chambers are actuated in a sequential manner to produce an undulating motion. The work of Shepard et al. [238] demonstrates that complex locomotion can be achieved through the use of open-loop controllers and the dynamic interaction between the soft robot and its environment.

To simplify the model, we assume general plane motion. The geometry of the soft crawler's cross-section is first provided to `Mesh.m` to generate a triangular mesh. Then, a finite element method (FEM) model is generated, with the material model `fem.Material = Ecoflex0030`. To model the environment, the function `fem = fem.addContact(sLine)` is utilized, which simply creates an unbounded horizontal line. In accordance with [238], a harmonic excitation is applied to each chamber, as expressed by the following: $u_i = A \cdot \text{sat}[\sin(\omega t - \phi_i)]$, where the index $i \in \{1, 2, 3\}$ represents the front, middle, and back pressure chambers embedded in the soft body.

```

1  %% EXAMPLE: Fem class
2  msh = Mesh('MultiGait.png', 'MeshSize', 1.0, ...
3             'BdBox', [0, 150, 0, 12]);
4
5  % mesh to fem
6  fem = Fem(msh, 'TimeStep', 1/500);
7  fem.Material = Ecoflex50();
8
9  % add inextensible bottom layer
10 E1 = fem.findElements([0 150 0 2]);
11 fem = fem.addMaterialModifier(E1, 5);
12
13 % add forces and constraints
14 fem = fem.addGravity();
15 fem = fem.addContact(sLine());
16
17 Y = 'BoxSelect';
18 for i = 1:3
19     Ce = fem.findEdges(Y,[50*(i-1), 50*i, 0, 15]);
20     fem = fem.addPressure(Ce, @(x) Pressure(x,i));
21 end
22
23 % solve dynamics
24 fem = fem.simulate();
25
26 % -- open-loop controller
27 function y = Pressure(fem, i)
28     phi = pi / 3 * (i - 1);
29     y = clamp(sin(5*pi*fem.Log.t - phi), 0, Inf);
30 end

```

The excitation signal parameters are set as follows: $A = 45 \text{ kPa}$, $\omega = 5\pi \text{ rad}$, and $\phi_i = \frac{\pi}{3} \cdot (i - 1) \text{ rad}$. The saturation function is defined as $\text{sat}(x) = 0$ for $x < 0$, and $\text{sat}(x) = x$ for $x \geq 0$. Gravitational acceleration is added, and the dynamic simulation solver is invoked using `fem.simulate`. Figure 6.7 presents a comparison between the soft robot described in [238] and the dynamic simulation performed by `Sorotoki`.

The results of the simulation performed using `Sorotoki` show a morphological behavior that is consistent with the experimental recordings. Figure 6.8 depicts the trajectory of the center of mass (CoM) of the soft robot during the undulating locomotion. Note that an identical stair-like evolution of the CoM is also observed in the work of Shepard et al. [238].

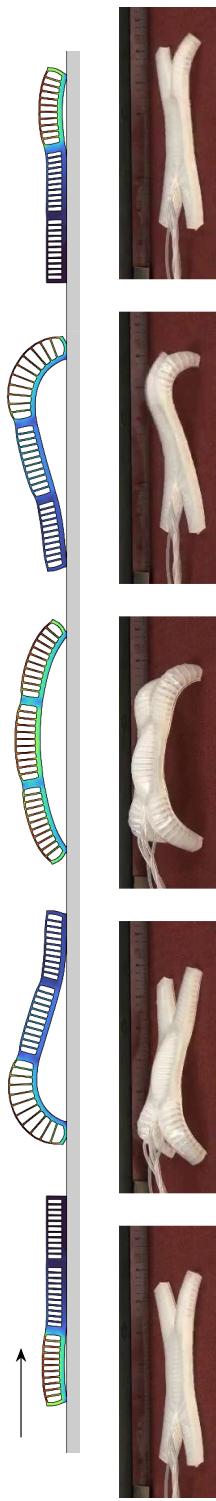


Figure 6.7. (top) Experiment of soft multi-gait crawling soft robot developed by Shepard et al [238] performing an undulating forward motion by periodic pressurization of its internal pressure chambers, back legs \rightarrow middle \rightarrow front legs. The soft robot is made from an elastomer material with strain-inhibit layer at the bottom to enhance bending. The Von Mises stresses are shown as $\in [0, 10]$ MPa. (bottom) Simulation recreation of the experiments performed by Shepard et al [238] using the Finite Element solver in the *Sorotoki* toolkit. Images sourced from public resources, with intellectual property belonging to cited authors, sources, and publishers.

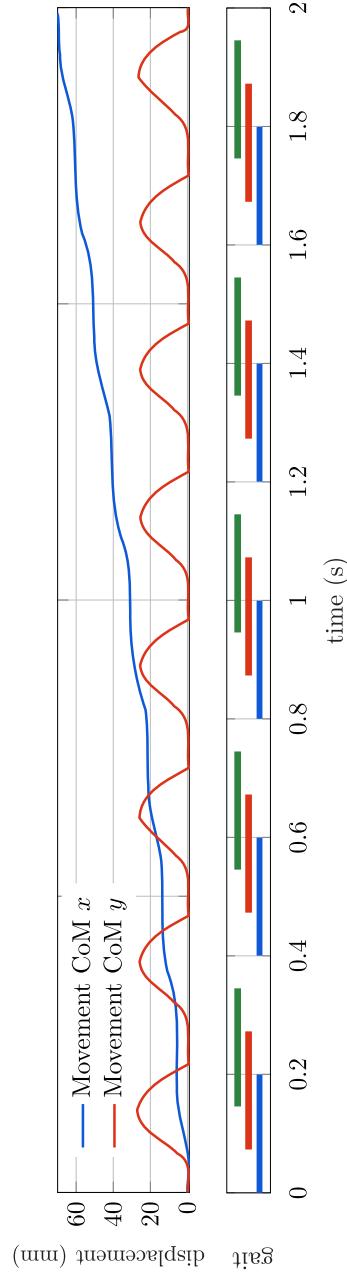


Figure 6.8. (top) Numerical simulation of the center of mass displacement and gait for undulating soft crawler. The horizontal displacement is given by (—), and the vertical displacement as (—). (bottom) The gait cycle of the soft crawler where the sequence {—, —, —} shows the fluidic activation.

Gradient-based computational (inverse) design Besides modeling, the field of computational inverse design can also benefit from the use of FEM models. Building up the `Fem` class, the objective is to find a topological structure of a continuum system based on a desired deformations or compliance. One widely adopted method is the Solid Isotropic Material with Penalization (SIMP) approach, which is a commonly used material interpolation technique in topology optimization [19]. In the SIMP method, each finite element $e \in \{1, 2, \dots, n_e\}$ is assigned a continuous density variable $\rho_e \in (0, 1]$, which serves as an indicator of the material distribution within the mesh. If $\rho_e = 1$, the element is considered solid, while if $\rho_e = 0$, the element is considered void. This assignment of density variables enables the modification of the strain energy density in (6.4):

$$\tilde{\Psi}_e = [\varepsilon + (1 - \varepsilon)\rho_e^p] \Psi, \quad (6.6)$$

where $0 < \varepsilon \ll 1$ a lower bound on the densities, and $p > 1$ a penalty factor for penalizing intermediate densities during the optimization process. By collecting the density values $\boldsymbol{\rho} = \text{col}\{\rho_1, \rho_2, \dots, \rho_{N_e}\}$, the inverse design problem can be formulated in terms of two unknowns: the displacement field \mathbf{x} and the density field $\boldsymbol{\rho}$. Consequently, the computational design problem for general soft material structures can be expressed as a nonlinear topology optimization problem of the following form:

$$\begin{aligned} \underset{\boldsymbol{\rho}}{\text{minimize}} \quad & \Phi = -\beta_1 \mathbf{L}^\top \mathbf{x} + \beta_2 \mathbf{f}_e^\top \mathbf{f}_u \\ \text{subject to} \quad & \tilde{\mathbf{r}}(\mathbf{x}, \boldsymbol{\rho}) = 0, \\ & \mathbf{v}^\top \boldsymbol{\rho} \leq v^*, \\ & \boldsymbol{\rho} \in \mathcal{P}, \end{aligned} \quad (6.7)$$

where \mathbf{L} a sparse unit-vector composed of nonzero entries for the degrees-of-freedom corresponding to the desired morphology of the soft robot, \mathbf{v} the element volumes, v^* the desired volume infill, $\mathcal{P} = \{\boldsymbol{\rho} \in \mathbb{R}^{n_e} \mid 0 < \rho_i \leq 1\}$ admissible set for the design variables, and β_1 and β_2 are positive scalars that can be adjusted to vary the optimization problem, with $\beta_1 \ll \beta_2$ resulting in compliance minimization and $\beta_1 \gg \beta_2$ leading to a compliant mechanism. To solve the optimization problem in (6.7), we utilize the Method of Mixed Asymptotes (MMA) proposed by Svanberg [264, 265]. Earlier work on this computational design approach was presented in Chapter 3, and the chapter is referred to this work for the analytic gradients required for the MMA solver.

The optimization routine in the `Sorotoki` framework is incorporated into the `Fem` class and can be invoked by utilizing the command `fem.optimize('type')`, where '`type`' represents the optimization problem at hand. For minimizing compliance, the cost function is self-adjoint [19], hence objective function and constraints are linear operators. However, when dealing with compliant mechanisms, it is necessary to specify the selection vector \mathbf{L} , which can be defined using the `fem.addOutput(id)` command. The value of `id` represents the nodal indices of interest, which can be identified using the `fem.Mesh.findNode` functionality.

6.5.4 Reduced-order soft beam models (**Shapes**)

While the finite element method (FEM) is known for producing reliable and highly accurate results, its high-dimensional state can make it computationally slow, making direct applications for closed-loop control challenging. To address this issue, the **Sorotoki** toolkit offers reduced-order models based on Cosserat beam theory [12, 30, 242]. In Cosserat beam theory, deformable solids are modeled as elastic strings that are governed by finite strain theory. This formulation can be applied to the dynamic modeling of slender soft robots as one-dimensional spatial curves passing through the geometric center of the deformable soft body. As shown in Figure 6.9, a (slender) soft robot can be described using geometric Cosserat beam models, representing it as a parameterized curve on the group of rigid-body transformations SE(3):

$$\mathbf{g} : [0, L] \times [0, +\infty) \rightarrow \text{SE}(3), \quad (6.8)$$

where SE(3) composed of an orthogonal rotation matrix and a translation vector.

The objective of this approach, similar to the finite element method, is to solve a dynamic system in a continuous manner, often through projecting the problem onto a finite-dimensional subspace. To address the infinite dimensionality of the curve \mathbf{g} and make the continuum kinematics computationally tractable, various methods have been proposed, including elemental discretization [95, 284] (which is analogous to Section 6.5.3). A widely adopted alternative is modal approximation [29, 51]. The concept of modal decomposition for describing the kinematics of continuum robots dates back to the early 1990s [50, 51], and some modal representations (*e.g.*, first-order fourier series) even provide closed-form solutions to the inverse kinematics.

The method for constructing soft beam models in the **Sorotoki** toolkit is expressed using the syntax `shp = Shapes(pod,dof)`. In this expression, `pod` is a modal interpolation matrix that is derived from a modal basis selected by the user, and `dof` is a vector of six unsigned integers (`uint8`) that couples the beam degrees of freedom, including extension, bending, torsion, and shear, to their modal representation. The **Shapes** class serves two primary purposes: (*i*) to enable fast forward dynamic simulation of soft robots and (*ii*) to simplify the design of model-based controllers for both online and offline environments. Compared to the FEM model in (6.3), the soft beam models implemented in **Sorotoki** typically have a significantly lower dimensional representation, resulting in improved computational speed and, in some cases, real-time performance. This enables model-based controllers on real platforms, at the cost of model accuracy.

A: Computationally-efficient soft beam models. Following the geometric Cosserat beam frameworks [29, 39, 221], the reduced nonlinear dynamics of a soft beam model, fixed to a non-inertial base, can be represented using a Lagrangian formulation:

$$\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{f}_{\text{mat}}(\mathbf{q}, \dot{\mathbf{q}}) + \mathbf{f}_g(\mathbf{q}) = \mathbf{f}_{\Omega_{\text{env}}}(\mathbf{q}, \dot{\mathbf{q}}) + \boldsymbol{\tau}(\mathbf{q}, \mathbf{u}), \quad (6.9)$$

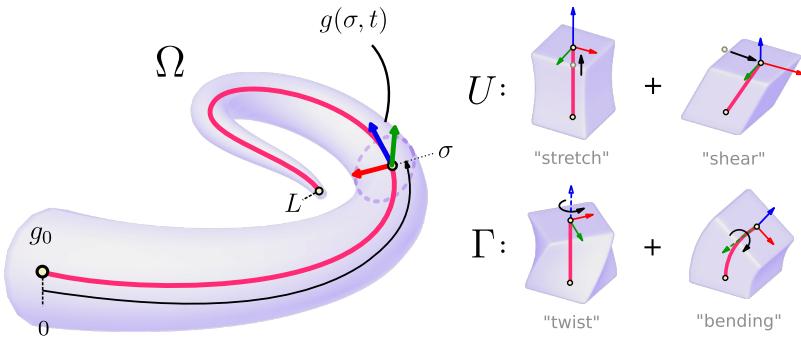


Figure 6.9. Illustration of the soft beam model using geometric Cosserat beam theory, where the backbone curve is $\mathbf{g}(\sigma, t) \in \text{SE}(3)$ shown as (—). The geometric strain vector $\xi := \text{vec}\{\boldsymbol{\Gamma}, \boldsymbol{U}\}$ a vector of size 6 consisting of stretch-shear strains \boldsymbol{U} and twist-bending strains $\boldsymbol{\Gamma}$.

6

where \mathbf{q} , $\dot{\mathbf{q}}$, and $\ddot{\mathbf{q}}$ represent the modal coefficients, velocity, and acceleration, respectively; \mathbf{M} denotes a state-dependent generalized inertia matrix, and \mathbf{C} denotes the Coriolis matrix. The material forces are expressed as $\mathbf{f}_{\text{mat}}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{K}(\mathbf{q})\mathbf{q} + \mathbf{R}\dot{\mathbf{q}}$, where \mathbf{K} is a generalized stiffness matrix and \mathbf{R} is a generalized damping matrix. The environmental forces are represented by the vector $\mathbf{f}_{\Omega_{\text{env}}}$, and the generalized input is given by $\boldsymbol{\tau} = \mathbf{G}\mathbf{u}$, where $\mathbf{G}(\mathbf{q})$ is the input mapping. As in Section 6.5.3, material and contact models can be assigned using comparable syntax, `Shapes.addMaterial` and `Shapes.addContact`, respectively. The intrinsic length of a curve can be altered by utilizing the function `Shapes.setLength`, while its cross-sectional geometry can be modified through the function `Shapes.setGeometry(sdf)`, which accepts a two-dimensional SDF function that may be arbitrarily complex.

Due to the complexity of deriving the forward kinematics and dynamics in the Cosserat model, the following subsections provide a clear summary of the finite-dimensional basis representation and its relationship to reduced kinematics. The system matrices, on the other hand, are notoriously lengthy expressions and thus omitted in this work. The reader is referred to Chapter 5 for a full derivation of model (6.9).

B: Finite dimensional projection. To start, our aim is to obtain a finite-dimensional approximation of the local geometric strain vector, denoted as $\xi := (\mathbf{g}^{-1} \frac{\partial \mathbf{g}}{\partial \sigma})^\wedge := (\boldsymbol{\Gamma}^\top, \boldsymbol{U}^\top)^\top$, where $\sigma \in [0, L]$ is a spatial coordinate and $(\cdot)^\wedge : \text{se}(3) \rightarrow \mathbb{R}^6$ (see [197] or Appendix D.1). Here, $\boldsymbol{\Gamma}_i$ and \boldsymbol{U}_i are the torsion-curvature and elongation-shear curve parameters, respectively. To achieve this, we employ a Ritz-Galerkin modal discretization approach following the work of Boyer et al. [29]. This approach assumes that the strain can be accurately represented through a

finite series of orthonormal basis functions:

$$\begin{aligned} [\xi_i]_{\boldsymbol{\theta}_i}(\sigma, \mathbf{q}_i) &= \sum_{j=1}^{k_i} \theta_{i,j}(\sigma) q_{i,j} + \xi_i^\circ(\sigma), \\ &= \underbrace{[\theta_{i,1}(\sigma) \dots \theta_{i,k_i}(\sigma)]}_{\boldsymbol{\theta}_i^\top(\sigma)} \mathbf{q}_i + \xi_i^\circ(\sigma) \end{aligned} \quad (6.10)$$

where $\boldsymbol{\theta}_i$ is the modal approximation vector related to the i -th strain component, \mathbf{q}_i is its corresponding modal coefficient, and $[\cdot]_{\boldsymbol{\theta}}$ denotes the subspace projection operator. By collecting all terms $q_{i,j}$ and $\theta_{i,j}$, we compactly express the finite-dimensional approximation as an affine operation:

$$[\boldsymbol{\xi}]_{\boldsymbol{\Theta}}(\sigma, \mathbf{q}) = \boldsymbol{\Theta}^\top(\sigma) \mathbf{q} + \boldsymbol{\xi}^\circ(\sigma) \quad (6.11)$$

where $\boldsymbol{\Theta} := \text{blkdiag}\{\boldsymbol{\theta}_1, \dots, \boldsymbol{\theta}_6\}$ is referred to as the "*modal approximation matrix*", and $\mathbf{q} := \text{vec}\{\mathbf{q}_1, \dots, \mathbf{q}_6\}$ is the generalized coordinate vector of the global soft beam model in (6.9). Note that a geometric strain entry may be constrained and therefore not contribute to the overall continuum dynamics, thus $\boldsymbol{\theta}_i, \mathbf{q}_i$ are fixed to zero without loss of generality. The choice of basis plays a crucial role and often relies on *ad-hoc* approaches. It is therefore critical to choose an appropriate basis for optimal performance of the soft robot model.

C: Library of modal strain bases. In Sorotoki, the general constructor for creating a modal basis is defined as `pod = Basis(N,M,'type')`, where N represents the number of samples (i.e., the level of discretization of the spatial curve), M is the degree of the basis, and '`type`' is an input that specifies the basis type.

The literature presents various types of modal bases, with the Piecewise Constant Curvature (PCC) approach being the most commonly used [71, 78]. The Piecewise Constant Curvature approach is suitable for certain conditions, for example, when homogeneous bending moment and homogeneous material properties are considered. However, it lacks the ability to ensure the continuity of the strain field at the boundaries between sections, resulting in jumps in the strain profile. As a result, researchers have been exploring alternative representations that more effectively preserve the continuity conditions of the deformable continua. Examples of alternative representations of bases include piecewise linear [160], affine curvature [67, 257], Fourier cosine/sine series [48, 51], Legendre or Chebyshev [29, 39], and actuation load bases [221]. The Sorotoki package offers access to a library of anonymous functions, facilitating the utilization of a range of basis functions. As an illustration, a collection of basis functions is shown in Figure 6.12.

Remark 6.2 (On the modal order) *Generally, finding a suitable reduction basis and reduction order can be a challenging task. The general assumption is that if the basis belongs to a regular function space (i.e., Sobolev space) and the modal index k_i goes to infinity, the strain approximation converges (uniformly) to the*

exact solution on the interval $[0, L]$. However, as increasing the modal order enhances precision, it also greatly impacts computational performance. Thus, finding a balance between accuracy and computational speed is of utmost importance for the successful implementation of soft robotic models, often mandating an ad-hoc approach.

C: Data-driven strain basis from offline FEM simulations. To address the challenges of improving efficacy in the modal reduction of soft beam models, we propose a novel approach that merges the finite element method and soft beam modeling. This approach involves extracting geometric modal information from FEM simulation data to construct a low-dimensional strain basis, which we refer to as the Data-driven Variable Strain (DVS) basis. The DVS basis is similar in concept to the snapshot method presented by the SOFA toolkit [57, 76, 100], but adapted for use with one-dimensional curves. It takes into account the underlying geometric features of the soft robot and represents them in a minimal subspace representation. This approach leads to a substantial reduction in the number of states while still maintaining high accuracy in deformations, high computational efficiency, and providing a clear structure for passive and active joints. The derivation has two steps:

6

Step 1: Recovery of geometric strain from FEM: The reconstruction of the MIVS basis begins with obtaining geometric strain data from a Finite Element Method (FEM) simulation. Such simulation supports either `Fem.simulate` or `Fem.solve`, and the resultant information is stored in the `fem.Log` data structure. Mathematically, the simulation retrieves the states $\mathbf{x}^{(i)} := \mathbf{x}(t_i)$ at discrete time instances $t_i \in \{0, \dots, T\}$, which in turn provides the nodal position vectors \mathbf{p} and the deformation gradient \mathbf{F} at any point in the mesh. Using the polar decomposition $\mathbf{Q} = \mathbf{F}\mathbf{V}^{-1} \in \text{SO}(3)$, see Table 6.2, we can retrieve the rigid body transformation of the FEM mesh

$$\mathbf{g}_{\text{FEM}}(\mathbf{s}, \mathbf{x}^{(i)}) = \begin{pmatrix} \mathbf{Q}(\mathbf{s}, \mathbf{x}^{(i)}) & \mathbf{p}(\mathbf{s}, \mathbf{x}^{(i)}) \\ \mathbf{0} & 1 \end{pmatrix}, \quad (6.12)$$

where $\mathbf{s} \subseteq \Omega$ is an arbitrary point inside the undeformed mesh. It is important to note that if \mathbf{s} does not correspond to a nodal location of the mesh, interpolation using elemental shape functions is necessary. Now, let $\bar{\gamma} : [0, L] \rightarrow \Omega$ be a unit-speed reference backbone curve that is contained within the mesh domain Ω . Then, we can retrieve $\mathbf{g}_{\text{FEM}}(\bar{\gamma}, \mathbf{x}^{(i)})$. Subsequently, the geometric strain can be approximated as $\boldsymbol{\xi}_{\text{FEM}} \approx (\mathbf{g}_{\text{FEM}})^{-1} \delta \mathbf{g}_{\text{FEM}}$. Here, $\delta \mathbf{g}_{\text{FEM}}$ represents the spatial derivative of the reference curve w.r.t. σ , which is calculated using the central difference method. It is worth noting that the choice of $\bar{\gamma}$ is free, allowing for the estimation of geometric strain for many complex structures. The full procedure is outlined in Algorithm 6.1.

Step 2: POD snapshot basis: Next, we employ the "Snapshot Proper Orthogonal Decomposition" (POD) as described in [76, 100]. This data-driven approach

Algorithm 6.1: Recover geometric strain field ξ_{FEM} from offline FEM

Input: Nodal displacements \mathbf{x} , mesh tessellation \mathcal{T} , reference curve $\bar{\gamma}$, and sample set \mathcal{S}

Output: Geometric strain field ξ_{FEM} at time t_i

```

1  for  $i = \text{each spatial sample } \sigma_i \in \mathcal{S}$  do
2    | get reference position  $\bar{\mathbf{p}} \leftarrow \bar{\gamma}(\sigma_i)$  ;
3    | get element  $\mathcal{E} \leftarrow \text{inElement}(\bar{\mathbf{p}}, \mathcal{T})$  ;
4    | if  $\mathcal{E} == \emptyset$  then
5      |   | get edge  $\mathcal{E} \leftarrow \text{onClosestEdge}(\bar{\mathbf{p}}, \mathcal{T})$ ;
6    | end
7    | initialize  $\Phi^{(0)} \leftarrow \mathbf{I}_3$  ;
8    | initialize  $\delta\gamma^{(0)} \leftarrow \mathbf{0}_3$  ;
9    | for  $j = \text{each vertex spanned by element } \mathcal{E}$  do
10   |   | get nodal displacement  $\mathbf{X} \leftarrow \text{FEM}(\mathbf{x}_j)$  ;
11   |   | get deformation gradient  $\mathbf{Y} \leftarrow \text{FEM}(\mathbf{x}_j)$  ;
12   |   |  $[\mathbf{Q}, \mathbf{V}] \leftarrow \text{PolarDecomposition}(\mathbf{Y})$  ;
13   |   |  $\alpha \leftarrow \text{ElementInterpolation}(\bar{\mathbf{p}})$  ;
14   |   | update  $\Phi^{(j)} \leftarrow \text{AverageSO3}(\Phi^{(j)}, \alpha \mathbf{Q})$  ;
15   |   | update  $\delta\gamma^{(j)} \leftarrow \delta\gamma^{(j)} + \alpha \mathbf{X}$  ;
16   | end
17   |  $\mathbf{g}_{\text{FEM}}^{(i)} \leftarrow \text{SE3}(\Phi^{(j)}, \bar{\mathbf{p}} + \delta\gamma^{(j)})$ ;
18 end
19 for  $i = \text{each spatial sample } \sigma_i \in \mathcal{S}$  do
20   |  $\delta\mathbf{g}_{\text{FEM}}^{(i)} \leftarrow \text{CentralDiff}(\mathbf{g}_{\text{FEM}}^{(i-1)}, \mathbf{g}_{\text{FEM}}^{(i+1)})$  ;
21   | assemble strain  $\xi_{\text{FEM}}^{(i)} \leftarrow (\mathbf{g}_{\text{FEM}}^{(i)})^{-1} \delta\mathbf{g}_{\text{FEM}}^{(i)}$ ;
22 end

```

determines a suitable orthonormal basis from simulated or experimental data [14]. Let $y_i(\sigma, t) := \xi_{\text{FEM}, i}(\sigma, t)$ represent the measurement of the i -th entry of the strain ξ_{FEM} . For each discrete time t_i , the sample is condensed into a column vector $\mathbf{y}_i^{(t)} := \text{col}\{y_i(0, t), \dots, y_i(L, t)\}$ and then stacked into the "snapshot matrix" $\mathbf{S}_i = \text{row}\left\{\mathbf{y}_i^{(0)}, \dots, \mathbf{y}_i^{(T)}\right\}$ where T is the finite horizon time. The correlation matrix $\mathbf{C}_i = \frac{1}{m} \mathbf{S}_i^\top \mathbf{S}_i$ is then computed with $m = \dim(\mathbf{y}_i)$, and the spectral decomposition is performed:

$$\mathbf{C}_i \mathbf{V}_i = \lambda_i \mathbf{V}_i, \quad (6.13)$$

where $\mathbf{V}_i = \text{row}\{\mathbf{v}_{i,1}, \dots, \mathbf{v}_{i,m}\}$ is a eigenvector basis and $\lambda_i = \text{diag}\{\lambda_{i,1}, \dots, \lambda_{i,m}\}$ is a diagonal matrix of sorted eigenvalues. By selecting $k_i \leq m$ such that $\lambda_{i,k_i} \leq \delta$, where δ is a desired threshold, we obtain a truncated orthonormal basis $\{\mathbf{v}_{i,j}\}_{j=1}^{k_i}$. This process is repeated until the modal interpolation matrix Θ , required for (6.11), is fully obtained. Finally, a Gram–Schmidt orthogonalization procedure is

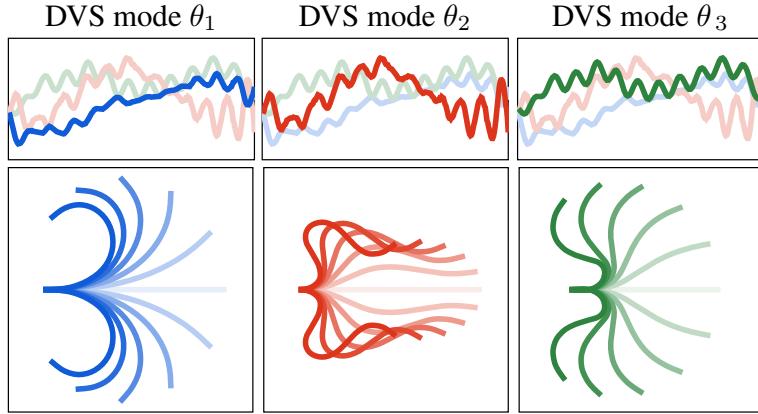


Figure 6.10. Example reconstruction of the Data-driven Variable Strain (DVS) basis for a PneuNet actuator grasping a cylindrical object. (top) The first three modes of the DVS basis related to planar bending, *i.e.*, planar curvature. The ordering is {—, —, —}. (bottom) The positional forward kinematics when regarding the bending modes {—, —, —} individually.

6

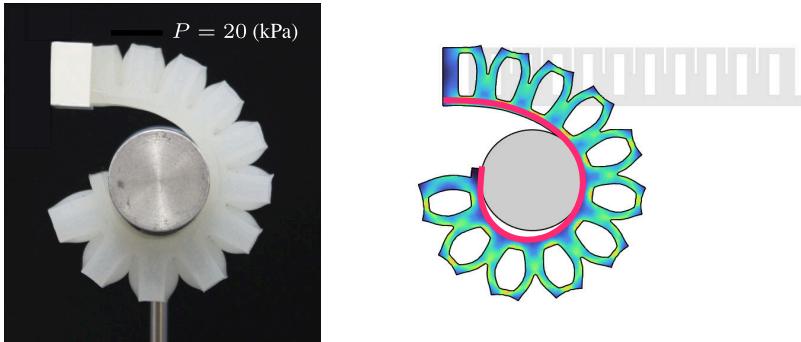


Figure 6.11. Example reconstruction of the Data-driven Variable Strain (DVS) basis for a PneuNet actuator grasping a cylindrical object. A comparison between the true physical system, the FEM model, and the soft beam model shown in (—). The Von Mises stresses are shown as $\in [0, 5]$ MPa.

performed to ensure that its columns are mutually orthogonal.

Example 6.5. Data-driven basis from PneuNet simulation To demonstrate the reconstruction of the DVS basis, we consider a soft bending actuation, also known as the PneuNet actuator. A FEM simulation model is constructed where the soft actuator is subjected to a linearly increasing pressure up to 40 kPa and curls around a cylindrical object when pressurized. Figure 6.10 (top) illustrates the true system and the FEM simulation obtained through `fem.simulate`. The FEM class is then integrated into the `Shapes` class through the syntax `shp = Shapes(fem,dof)`, where `dof = [0,3,0,0,0,0]` indicates the desire to recover the first three curva-

ture bending modes from the `fem` object class. The length and base orientation are specified using `shp.setLength` and `shp.setBase`, respectively. The basis is then reconstructed by calling `shp.reconstruct`. The first three curvature bending modes are displayed in Figure 6.10 (bottom). It can be observed that the geometrical features of the PneuNet actuator are encoded in the basis, with the 12 embedded pressure chambers represented by the DVS strain basis. The associated code is provided below:

```

1  % EXAMPLE: Shapes class (DVS basis)
2  fem = load('femPneuNet.mat');    % load fem model
3
4  dof = [0,3,0,0,0,0];   % pure planar curvature bending
5  shp = Shapes(fem, dof, 'NNode', 200, 'Length', 105);
6
7  % generate DVS basis
8  shp = shp.reference(@(s) [s,0,0].');
9  shp = shp.reconstruct();

```

D: Forward beam kinematics. Once a basis representation Θ has been selected, the forward kinematics of the continuum body can be efficiently solved using exponential maps for the group $SE(3)$. As such, the backbone curve is approximated by

$$[\mathbf{g}]_{\Theta}(\sigma, \mathbf{q}) = \mathbf{g}_0 \exp_{SE(3)} \left[\int_0^{\sigma} [\hat{\boldsymbol{\xi}}]_{\Theta}(s, \mathbf{q}) ds \right] \quad (6.14)$$

On the other hand, the local velocity twist is represented by $\boldsymbol{\eta} := (\mathbf{g}^{-1}\dot{\mathbf{g}})^{\vee}$, which, similarly to rigid robotics, is linear in the joint velocities $\dot{\mathbf{q}}$. Regarding computation, the velocity twist of a point σ on the curve \mathbf{g} can be represented as follows:

$$[\boldsymbol{\eta}]_{\Theta}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) = \left[\text{Ad}_{[\mathbf{g}](\sigma, \mathbf{q})}^{-1} \int_0^{\sigma} \text{Ad}_{[\mathbf{g}](s, \mathbf{q})} \Theta(s) ds \right] \dot{\mathbf{q}} =: \mathbf{J}(\sigma, \mathbf{q}) \dot{\mathbf{q}}, \quad (6.15)$$

where $\mathbf{J}(\sigma, \mathbf{q})$ denotes the geometric Jacobian that maps the joint velocities $\dot{\mathbf{q}}$ to velocity twist. For conciseness, we write $\mathbf{J}_{\sigma} := \mathbf{J}(\sigma, \cdot)$. The Jacobian matrix is of paramount importance, not only for inverse kinematics but also for mapping external wrenches onto the generalized joint torques. For instance, it can be used to calculate the environmental forces as $\mathbf{f}_{\Omega_{\text{env}}} = \int_0^L \mathbf{J}_{\sigma}^{\top} \mathcal{F}_{\text{env}} d\sigma$, where \mathcal{F}_{env} represents a wrench related to the environment Ω_{env} described by SDFs.

Given the expressions in (6.11), (6.14), and (6.15), we can numerically evaluate the forward kinematics. We use a two-step Runge-Kutta integration solver that approximates the spatial integration. The forward kinematics solver is called by `shp = Shapes.string(q,dq)`, which stores all necessary numerical evaluations into a data structure `shp.Log.FK`. To further improve computation speed, `.mex` executable files are utilized.

E: Inverse beam kinematics (shape control). The inverse kinematics problem for soft continuum manipulators involves finding a solution \mathbf{q} such that either (i) the end-effector reaches a specified setpoint, or (ii) shape control of the backbone is achieved. These manipulators often exhibit high levels of redundancy, so called hyper-redundancy [51]; leading to different solution approaches common to rigid robotics. Few modal basis representations possess a closed-form solution to the inverse kinematics, and they are typically solved using an iterative numerical method (e.g., Newton Raphson). In **Sorotoki**, the inverse kinematics solver for soft beam models is implemented as `Shapes.IK`. We briefly detail the theory.

Suppose the desired shape of the soft manipulator is $\mathbf{g}^*(\sigma) \in \mathcal{W}_\sigma$ with

$$\mathcal{W}_\sigma := \{\mathbf{X} \in \text{SE}(3) \mid \mathbf{X} = [\mathbf{g}]_\Theta(\sigma, \mathbf{q}), \mathbf{q} \in \mathcal{Q}\} \quad (6.16)$$

the set of possible configurations of the backbone curve at σ . Note that \mathcal{W}_L spans the workspace of the end-effector, and $\mathcal{W}_\Omega := \{\mathcal{W}_\sigma \mid \sigma \in [0, L]\}$ the workspace of the entire soft body. For sake of readability, we redefine $\mathbf{g}_i(\mathbf{q}) := [\mathbf{g}]_\Theta(\sigma_i, \mathbf{q})$ and $\mathbf{g}_i^* := \mathbf{g}^*(\sigma_i)$. For readability, we also rewrite the geometric Jacobian by $\mathbf{J}_i(\mathbf{q}) := \mathbf{J}(\sigma_i, \mathbf{q})$.

Then, the inverse shape kinematics problem for the discretized soft manipulator can be formulated as an optimization problem of the form:

$$\begin{aligned} & \underset{\mathbf{q}}{\text{minimize}} \quad \Phi = \sum_{i=1}^{N_p} \left\| \mathbf{K}_p \log_{\text{SE}(3)} [\mathbf{g}_i^{-1}(\mathbf{q}) \mathbf{g}_i^*]^\vee \right\|_2 \\ & \text{subject to} \quad \mathbf{g}_i, \mathbf{g}_i^* \in \mathcal{W}_\Omega, \end{aligned} \quad (6.17)$$

where $\log_{\text{SE}(3)}$ denotes the logarithmic mapping from the Lie group to its algebra, see Appendix D.1. Despite the highly nonlinear nature of the optimization problem, its solution procedure is a relatively straightforward two-step procedure:

Given an initial guess $\mathbf{q}^{(0)} \in \mathcal{Q}$, the aim is to compute an incremental update step that brings us closer to a local minimizer of the objective function Φ . For clarity, let $\Xi_i := \mathbf{g}_i^{-1} \mathbf{g}_i^*$ represent the geometric error between the soft robot and the desired shape. The state increment can then be expressed as:

$$\boldsymbol{\lambda}_i^{(k)} = \mathbf{J}_i^\top(\mathbf{q}^{(k)}) \left[\mathbf{K}_p T_{\text{SE}(3)}(\Xi_i) \log_{\text{SE}(3)}(\Xi_i) \right]^\vee, \quad (6.18)$$

$$\mathbf{q}^{(k+1)} = \mathbf{q}^{(k)} + \sum_{i=1}^{N_p} \boldsymbol{\Lambda}_i \left[\boldsymbol{\lambda}^{(k)} - \mathcal{N}_i(\mathbf{q}^{(k)}) \nabla \Psi_{\text{sub}} \right], \quad (6.19)$$

where $T_{\text{SE}(3)}$ denotes the tangent operator map on the group $\text{SE}(3)$, see [35], \mathbf{K}_p an artificial stiffness tensor, $\mathcal{N}_i = (\mathbf{I} - \mathbf{J}_i^\dagger \mathbf{J}_i)$ represents the null-space projection, and $\boldsymbol{\Lambda}_i$ a diagonal activation matrix. The trivial choice is $\boldsymbol{\Lambda}_i = \mathbf{I}_n$. The null space projector can be extremely useful in exploring the high redundancy in soft robots, allowing sub-tasks Ψ_{sub} to be considered parallel to the primary inverse kinematic problem. Classical examples of such subtasks include: minimizing elastic energy

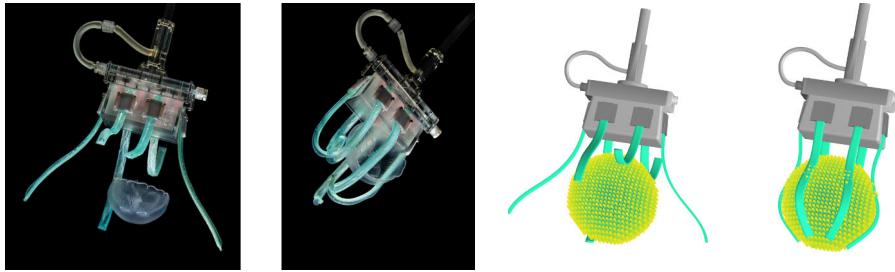


Figure 6.12. (left) A snapshot of the ultra-gentle soft robot gripper developed by Sinatra et al. [244] is shown, demonstrating its ability to grasp a delicate jellyfish. (right) The reconstructed soft gripper using `Sorotoki` is presented, where each tentacle finger is modeled individually using the `Shapes` class. It can be observed that the soft tentacles envelop the SDF object, indicating a balanced solution between task and subtask.

or obstacle avoidance. The iterative solver in (6.18) and (6.19) runs until convergence in $\mathbf{q}^{(k)}$ is achieved.

Example 6.6 (Contact kinematics of ultra-gentle soft gripper). To showcase the forward and inverse kinematic solvers of Sorotoki, we will describe the ultra-gentle underwater soft gripper developed by Sinatra et al. [244]. The soft gripper consists of six soft fingers attached to a rigid palm base, where each soft gripper was designed to apply low contact pressure and minimize harm to common jellyfish species. An illustration of the system is shown in Figure 6.12. The delicate compliance of the soft gripper is achieved through the use of an extremely low durometer silicone matrix (Shore 20A). The actuator has a simple rectangular geometry, with a narrow cross-section of approximately 10×2 mm and an internal off-center rectangular hole. The thinnest part of the soft actuator, called the membrane, is approximately 0.35 mm thick, and length of about 130 mm.

In this study, we aim to reproduce a grasping scenario of a jellyfish modeled as a static SDF object. To achieve this, we first initiate a soft finger by utilizing the `Shapes` class. We employ a third-order Chebyshev basis to approximate the strain field. The geometric properties of the soft finger are specified through the functions `Shapes.setLength` and `Shapes.setGeometry`. Using a for-loop, we generate each soft finger sequentially, defining the spatial location of the fixed base with `Shapes.setBase`. Prior to deployment, each soft finger undergoes predeformation, which is calculated through the application of the forward kinematics solver `Shapes.FK(q)`. The joint configuration, \mathbf{q} , is selected to match the experiments presented in Figure 6.12.

Subsequently, the deformed backbone is projected onto the surface of the SDF jellyfish through the use of the function `sdf.project`. The inverse kinematics solver is then invoked with `Shapes.IK`, resulting in the image depicted in Figure 6.12. Note that the inverse kinematics solver effectively places the soft finger onto the surface of the SDF object without causing penetration. The code for the forward and inverse kinematics is presented below:

```

1  %% EXAMPLE: Shapes class (forwards/inverse kinematics)
2  % jellyfish SDF
3  sdf = sSphere(0,0,-60,40)
4
5  % generate Shapes class
6  N = 200; % discretization
7  M = 3; % number of modes
8  pod = Basis(N,M,'chebyshev');
9
10 shp = Shapes(pod,[0,M,M,0,0,0], 'Length',120);
11 shp = shp.setGeometry(sRectangle(4,1));
12
13 % inverse kinematics on SDF topology
14 for k = 1:6
15     shp = shp.setBase(G{k}); % set base SE(3)
16
17     pos = shp.FK(q0{k}); % forward kinematics
18     prj = sdf.project(pos); % project points
19
20     qd = shp.IK(prj); % inverse kinematics
21     shp.render(qd); % render shape
22 end
23
24 sdf.show(); % render jellyfish

```

6.5.5 Model composer (Model)

In many instances, soft robots comprise multiple dynamic components that are interconnected to form the overall system. For instance, the soft robotic hand depicted in Figure 6.1c comprises five actively controlled soft fingers connected to a rigid palm base, each of which exhibits its own fluid-structure interaction. While each soft finger can be modeled through the `Shape` class, the class itself lacks a composer or solver that addresses the interconnections between a network of dynamic systems.

To address the issue, we propose the `Model.m` class, which concatenates dynamic systems to systematically increase complexity. The class is equipped with an implicit solver that facilitates communication of state information between subsystems. The goal of the `Model.m` class is two-fold: (*i*) to facilitate the composition of multiple dynamic components that form a soft robotic system, and (*ii*) to leverage the dynamic network structure to design controllers through interconnection of subsystems. For example, a soft robot, the fluidic actuation, and the model-based controller can be modeled as three separate entities and be composed into one global closed-loop system. This approach also enables the adaptive controllers that require additional state dynamics for online estimation of parameters. Contact interaction, on the other hand, are embedded functions inside `Fem` and `Shapes` that are called during each state increment of the forward dynamic solver.

A. Interconnected network of dynamical systems. The class `Model.m` allows users to compose an arbitrarily large network of dynamical systems that are presented in the state-space structure $\Sigma_i : \dot{\mathbf{z}}_i = \mathbf{f}_i(\mathbf{z}_i, \mathbf{u}_i, t)$. Then, the network of dynamical systems can be written as

$$\Sigma_{\text{net}} : \dot{\mathbf{z}} = \mathbf{F}_{\text{net}}(\mathbf{z}, \mathbf{u}, t) \quad (6.20)$$

The network system matrices are assembled as: $\mathbf{F}_{\text{net}}(\mathbf{z}) := \text{blkdiag}(\mathbf{f}_1, \mathbf{f}_2, \dots, \mathbf{f}_n)$. The implementation in *Sorotoki* is relatively straightforward. Let `f0 = @(z,u,t) ode(z,u,t)` be an anonymous function that defines a state space model, where `z`, `u`, `t` are the state vector, the input vector, and a time variable, respectively. In contrast to standard ODE solvers in MATLAB® (*e.g.*, `ode45.m`), the input `u` is treated as an additional input to the ODE. This simplifies the design of controllers as it enables the definition of control laws outside of the ODE function caller, as opposed to the standard ODE packages in MATLAB®.

To proceed, we first convert the function to a `sys0 = StateSpace(@f0)` class, which stores information on the state dimension, input dimension, and numerically computes the Hessian. Then, the model class is constructed using `mdl = Model(@f0)`. Other dynamic systems, represented by the `StateSpace` class `sys1`, `sys2`, and `sys3`, are added to the network by `mdl.addSystem(sys1, sys2, sys3)`. The `Model` class is also compatible with other classes, such as the `Fem` and `Shapes` class, allowing for example the interconnection between a FEM model and a soft beam model. To compute the forward dynamics, we call `mdl.simulate([0,T])` which solves the state trajectories on the finite horizon domain $[0, T]$ using an implicit Trapezoidal solver (*i.e.*, similar to `ode23t` solver).

B: Assigning the controller. Once a network of dynamic systems has been composed in the `Model` class, assigning a control is straightforward. Controllers can be defined as auxiliary anonymous functions `@(mdl) Controller(mdl)` and added using `mdl.addController(@Controller)`. At each time instance of the implicit solver, this controller function is called and prompted with the current instance of the `Model`. Once prompted, the solver retrieves the global input vector `u` as in (6.20). All system information of the network can be retrieved within the function by `mdl.getState[I, J]`, where `I` is the system index and `J` the indices of the states of subsystem `J`. Such implementation presents a highly dexterous and efficient controller design platform previously not standard included in MATLAB®.

C. Fluidic reservoir with volume-variance The majority of soft robots are actuated through fluidics. In recognition of this, *Sorotoki* offers a variant of the `StateSpace` class, called `Fluidic`, which incorporates fluid-pressure dynamics of an enclosed pressure reservoir based on the ideal gas law. The dynamics of such fluidic reservoir is determined by the compressibility of the fluid and the capacitance of the reservoir that is related to its volume $V > 0$. As a soft robot deforms, so does its internal volume. As such, consider a scalar variable $J : \mathcal{Q} \rightarrow (0, +\infty]$ such that we can describe the volume by $V(J(\mathbf{q})) = J(\mathbf{q})V_0$ where V_0 is

the intrinsic volume. From a physical point of view, the scalar $J(\mathbf{q})$ can be seen as the relative volumetric change of the reservoir depending on the state of the soft robot. Assuming constant temperature T and polytropic coefficient n_k , the pressure dynamics can be described by

$$\dot{p} = \frac{n_k}{V(J)} \left(RT\dot{m} - \frac{dV}{dJ}(J)\dot{J}p \right) - \mu_{\text{leak}}p \quad (6.21)$$

where the input is \dot{m} the mass flux into the reservoir, R the ideal gas constant, and μ_{leak} a pressure leakage coefficient. For a perfectly enclosed system, the parameter $\mu_{\text{leak}} = 0$. Note however, that the volumetric change \dot{J} might not always be available or it is difficult to derive. As an alternative, we substitute \dot{J} with an "dirty derivative" approximation $\dot{\tilde{J}}$ following the work of Loria et al. [168]:

$$\dot{z} = \alpha_1[z + \alpha_2 J], \quad (6.22)$$

$$\dot{\tilde{J}} = z + \alpha_1 J, \quad (6.23)$$

where $\alpha_1, \alpha_2 > 1$ are filter gains. Hence, the system of equations (6.21), (6.22), and (6.23) leads to the full pressure dynamics. In case of an isochoric compression (*i.e.*, no volume change $\dot{V} = 0$) with $J = 1 \Rightarrow \dot{J} = 0$, we can revert to a single-input-single-output (SISO) system with $u = \dot{m}$ (*i.e.*, the mass flow \dot{m} as the system's input).

Remark 6.3 (On fluidic volume changes derived from FEM) *The Sorotoki toolkit is equipped with functionalities that provide the volume of enclosed regions of the FEM. When `fem.solve()` or `fem.simulate()` is called, the time-series data of these volumes are stored, and thus can be used to identify how the state deformation \mathbf{q} is related to the volume change using, e.g., methods of nonlinear regression*

For many control applications for soft robotics, fluidic reservoirs are internally pressure regulated. Hence, the mass flow $\dot{m}(p, p_d)$ depends on the internal pressure p and a (possibly time-varying) pressure trajectory p_d . The mass flow controller of a proportional pressure-regulated reservoir is modeled here as PI-type controller:

$$\dot{m} = \Psi_v(\nu, p), \quad (6.24)$$

$$\nu = k_p(p - p_d) + k_i \int p(\tau) - p_d(\tau) d\tau, \quad (6.25)$$

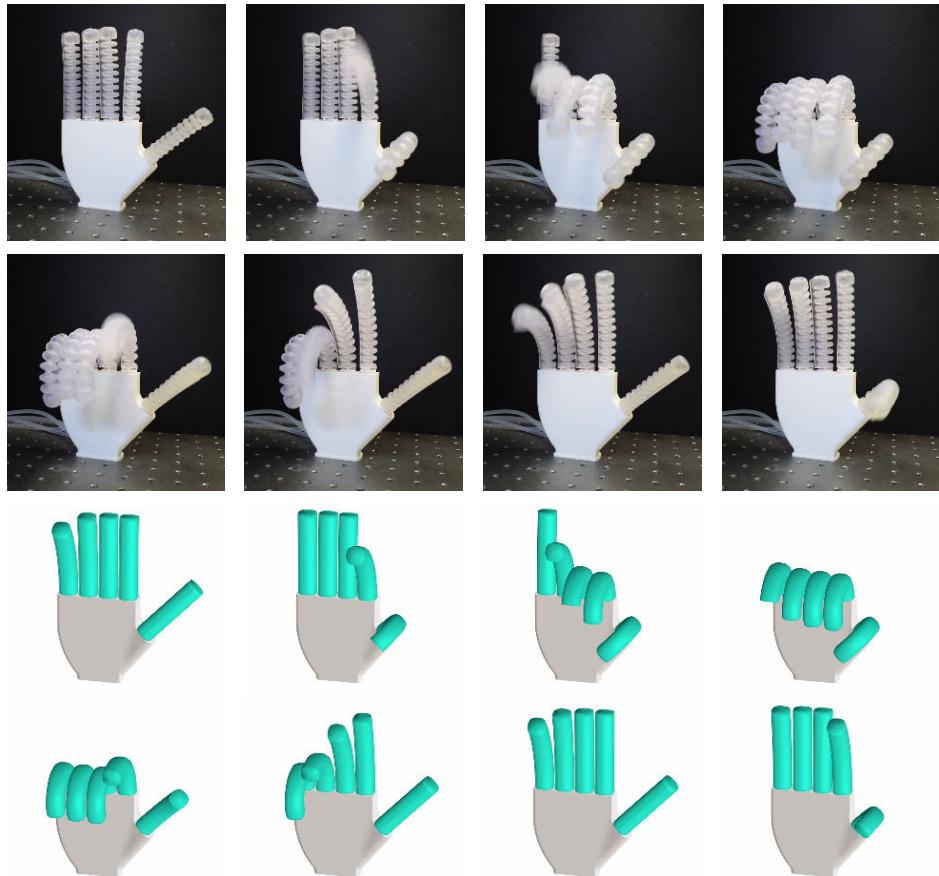
where $\Psi_v(\nu, p)$ is a valve flow function related to mass flow saturation of the pressure valves, and $k_p, k_i > 0$ the proportional and integral control gains, respectively. In Sorotoki, such fluidic system is provided as `Fluidic` class. The volume of the reservoir can be set using `Fluidic.setVolume(@V)` where $V = @(x) \dots$ is an auxiliary anonymous function. The mass flow function can be modified by the user using a similar command `Fluidic.setMassFlow(@M)`. By default, the flow function is $\Psi_v(\nu, p) = \nu$, and the regulation `Fluidic.isRegulated = true`.

Example 6.7. Simulation soft hand with fluidic soft fingers To demonstrate the versatility of the `Model` class and the `Fluidic` class, consider the example of modeling the soft robotic hand previously shown in Figure 6.1. Prior to the simulation model, we conducted an experiment to allow a qualitative comparison with our modeling approach. Here, a predefined harmonic pressure signal is introduced to each of the soft fingers, with each harmonic having a $+\frac{\pi}{6}$ offset relative to its neighboring soft finger. The pressure signal is sinusoidal with an upper and lower bounds of -5 and 80 (kPa), respectively. As depicted in Figure 6.13, an oscillatory motion arises, where the fingers sequentially undergo bending.

The objective is to recreate the experimental oscillatory behavior of the soft hand, incorporating the fluid dynamics and continuum dynamics of the soft fingers. Each soft finger can be modeled separately using the `Shapes` class and its internal fluidic network using the `Fluidic` class. We start by sculpting the model for the soft fingers, assuming a fifth-order Chebyshev polynomial basis and considering planar bending curvature only. We assume that only the first mode can be actively controlled by the fluidic network, thus the input map is manually assigned using `Shapes.setInputMap(@(q) ...)`. The `Shapes` class is duplicated five times using a for-loop routine, with the base frame assigned accordingly at each iteration using `Shapes.setBase`.

For each soft finger, it is assumed that it has its own fluidic network that is equipped with internal pressure regulation. However, as each soft finger deforms, the internal volume of the pressure reservoir also changes. This volumetric change is modeled as $V(\alpha) = V_0(1 + \tanh(\alpha))$, where it is assumed that $\alpha = 0.06q_1$ (i.e., the first joint of the soft beam) and V_0 the initial volume. Then, a for-loop is used to include the both `Shapes` and `Fluidic` systems to the global network of dynamical systems.

Finally, `mdl.addController(@Control)` is used to add the control law. In this auxiliary function, we specify the pressure reference for the fluidic network, and we return the state deformations of the soft fingers to the fluidic network; required for the computation of the volumetric change. The dynamic simulation is solved implicitly using the `mdl.simulate` command. The code for the dynamic simulation of the soft robotic hand is shown in Figure 6.13.



6

Figure 6.13. (top) Experimental snapshots of the open-source soft robotic hand provided by the *Sorotoki* toolkit. The five-fingered robot is subjected to a harmonic oscillator that commands oscillatory pressure to the individual fingers. Since each oscillator has a preset phase difference ($\phi = \pi/6$), the fingers of the soft robot hand undergo a periodic swinging motion. (bottom) Reconstructed soft robotic hand using *Sorotoki*, where each finger is modelled using the `Shapes.m` class and then composed using the `Model.m` class. Following, each oscillator is added using `mdl.addSystem` and then they ouputs are connected to the inputs of each `Shapes.m` class. As can be seen, the dynamics between the numerical model and the experiments are in close agreement.

```

1 %% EXAMPLE: Model class
2 shp = Shapes(pod,dof,'Length',90);
3
4 shp.setInputMap( @(x) [5; 0; 0; 0; 0] );
5 shp.Material = NeoHookeanMaterial(1.5,0.3);
6
7 for ii = 1:5
8     SHP{ii} = shp.setBase( G{ii} );
9 end
10
11 %% building fluidics model
12 V0 = (4*pi/3) * 35^3;
13 V = @(x) V0 * (1 + tanh(x/0.06));
14
15 fld = Fluidic('NInput',3);
16 fld = fld.setVolume(V);
17
18 %% building model
19 mdl = Model([]);
20
21 for ii = 1:10
22     if ii < 5      % add soft finger
23         mdl = mdl.addSystem( SHP{ii} );
24     else            % add fluidic network
25         mdl = mdl.addSystem(fld);
26     end
27 end
28
29 %% assign control and simulate
30 mdl.addController( @(x) Control(x) );
31 mdl = mdl.simulate([0, 5.0]);
32
33 % -- controller function block
34 function u = Control(mdl)
35     phi = @(k) (k-1) * pi/6;
36     Pd = 80 * sign(sin(7.0 * mdl.t + phi(1:5)));
37
38     u = zeros(20,1);
39     u(6:3:end) = Pd;
40     u(7:3:end) = mdl.getState(1:5,[1]);
41     u(1:5)      = mdl.getState(6:10,[1]);
42 end

```

As depicted in Figure 6.13, the dynamics of the numerical model and the experiments are in close qualitative agreement. This serves as a testament to the efficacy of the dynamic model composer `Model` in building dynamic complexity through its modular functionalities. Additionally, the ability to represent the controller as an auxiliary function that can retrieve state information at any given time confers `Sorotoki` with a high degree of flexibility in offline controller design.

6.5.6 Fluidic control hardware (Control)

The implementation of online controllers for physical soft robotic systems is a crucial aspect of *Sorotoki*. Although there are various options available in the research community [316], *Sorotoki* has a specific focus on fast closed-loop control. Drawing from our prior work [40], *Sorotoki* incorporates a TCP communication wrapper (`tcpip`) that enables real-time communication with a host computer, such as a Raspberry Pi (RPI). This host computer is connected to six pressure control boards, each capable of supporting up to two proportional pressure control valves from Festo. As a result, *Sorotoki* offers up to twelve pressure-regulated control ports with a range of -100 to 100 kPa that can be directly controlled using script-based programming in MATLAB®. The entire system, including the software, is open-source and readily reproducible by researchers with diverse technical backgrounds.

By calling `brd = Control('ip','pwd')`, connection with the fluid control platform is established, where '`ip`' is the IP address and password of the RPI. On the RPI, the Python script `ConnectToMatlab.py` must be executed that makes connection with MATLAB and awaits control commands. To initiate the control loop, a while-loop is used whose condition statement is `brd.loop(T)` where `T` is finite horizon time. Within the while-loop, all functionalities of *Sorotoki* are available, thus model-based controller design is possible for instance using the `Shapes` and `Model` classes. Each pressure regulation can be controlled using the command `brd.setPressure(id,P)` or an internal pressure measurement can be retrieved using `P = brd.getPressure(id)`.

Example 6.8 (Pick-and-place control of soft robot manipulator). As an example of the capabilities of the fluid control platform, we used it for a pick-and-place application involving the aforementioned soft robot manipulator with soft gripper. The soft robot has four independent pressure inputs: three for the bellows network embedded into the soft body and one for the soft gripper. The *Sorotoki* toolkit communicates a desired pressure profile to a Raspberry Pi board computer, which is interfaced with an expandable array of proportional pressure regulators. As shown in Figure 6.14, the system successfully manipulates a 40 mm cylinder of 45 (g) into its container. The system has also been successfully simulated using the `Shapes` and `Model` class, shown in Figure 6.15, where the cylinder is modeled as a Newton-Euler rigid body system.

6.5.7 Computer vision (Vision)

The final Object-oriented class addresses the challenge of soft sensing through vision. The class, named `Vision`, can be instantiated using `cam = Vision(Id)`, where `Id` is a user-specified index obtained from the list of available webcams using `webcamlist`. Alternatively, the `Vision` class is capable of reading sensor data from the RealSense D400 series RGB-Depth camera from Intel. The class is equipped with a suite of vision techniques that make use of the `OpenCV` Python

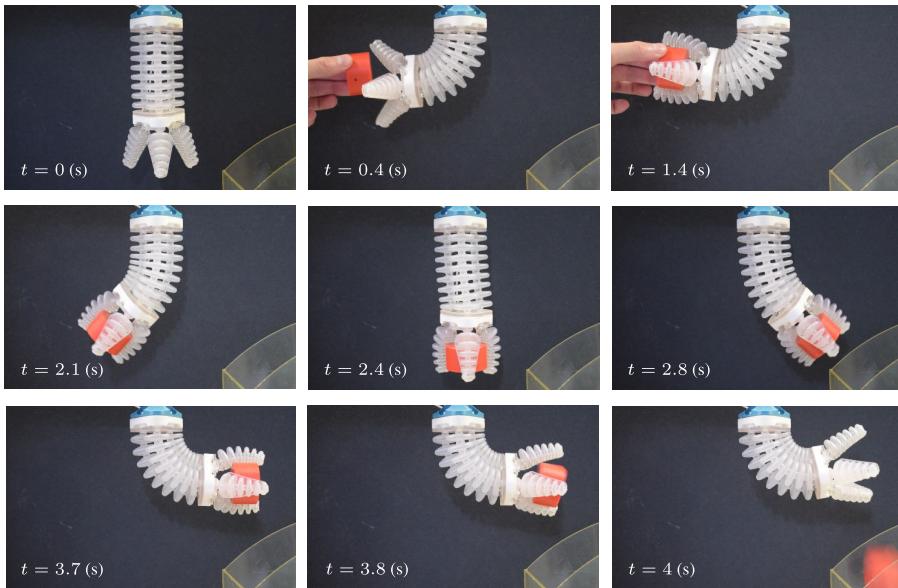


Figure 6.14. Implementation of open-loop control of a 3D-printed soft robot manipulator with a soft gripper using the **Sorotoki** toolkit. The soft robot has four independent pressure inputs: three for the bellows network embedded in the soft body and one for the soft gripper. The **Sorotoki** toolkit communicates a desired pressure profile to a Raspberry Pi board computer, which is interfaced with an expandable array of proportional pressure regulators. A straightforward pick-and-place task can then be easily programmed using the **Control** interface, using auxiliary MATLAB functions.

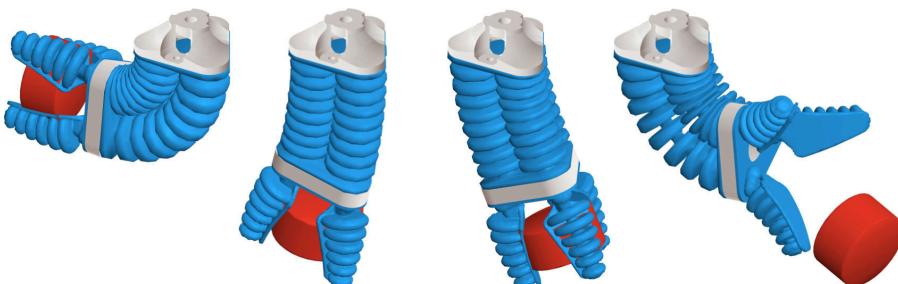


Figure 6.15. Simulation of the soft robot manipulator with gripper using the **Shapes** and **Model** class. The rigid-body is modeled by the Newton-Euler equation of motions implemented via **StateSpace**.

implementation. It features three key functions: (*i*) extraction of optical markers from an image using RGB and depth data, (*ii*) calibration of the world coordinate frame using Aruco markers, and (*iii*) monitoring of a soft robot in real-time using camera feedback. The detection of color markers utilizes a circular Hough transform [123], which provides the pixel location of a circle within the specified search conditions. These tools provide a broad range of options for state estimation of a soft robot, which can be easily incorporated into closed-loop control schemes.

6.6 Soft robotics study cases

In the subsequent section, we will delve into the capabilities of the toolkit, **Sorotoki**. To provide a comprehensive overview of the toolkit, various problem scenarios will be considered, each with specific problem settings aimed at the design, modeling, or control of soft robots. We will also focus on widely cited papers in the field of soft robotics and demonstrate these, mostly experimental, works using the **Sorotoki**.

Remark 6.4 *It is noteworthy that the full code can be accessed in the repository under the folder `./scripts/paper/`, enabling users of the toolkit to reproduce all presented simulation results in the following section.*

6.6.1 Multi-legged soft passive walker

In the first case study, the **Sorotoki** toolkit will be used to examine the dynamics of a multi-legged soft passive walker. The work of Suzumori and Saito [263] served as a key source of inspiration for this modeling problem. They proposed using a specialized soft structure that consists of an array of V-shaped soft legs, which exhibit stable intrinsic locomotion when placed on an inclined surface. This behavior was observed in experiments, as shown in Figure 6.16. The natural locomotion is driven by the elastic deformations of the V-shaped legs and their interaction with the environment, and is propelled forward by gravity. To increase the amplitude of these harmonics, small weights are placed at intermediate locations on the connecting soft body between pairs of V-shaped legs. Each pair of soft legs is tuned to a natural resonance frequency, and when coupled in parallel through a central deformable elastic body, synchronization occurs between the legs during locomotion. In other words, after a transient period, each leg pair will converge to a similar limit cycle, but with a unique phase offset relative to its neighbors.

The objective of this study is to reproduce the dynamics of the soft passive walker described in Suzumori et al. [263] using **Sorotoki**. In the work of Suzumori et al. [263], the material parameters of the soft passive walker were given as: Young's modulus $E_0 = 1.2 \text{ MPa}$, Poisson ratio $\nu_0 = 0.49$, and density $\rho_0 = 3600 \cdot 10^{-12} \text{ kg mm}^{-3}$. Since the material model is not exactly specified in [263], a Neo-Hookean model was utilized with Rayleigh damping $\zeta = 1.5$.

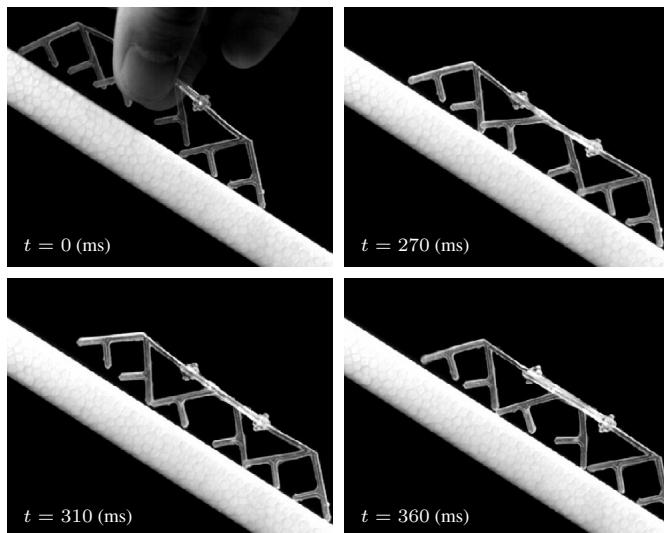


Figure 6.16. Snapshots of the multi-legged passive walker from Suzumori and Saito [263] can be observed. The soft walker is placed on an inclined surface with a slope of $\varphi = -30^\circ$ and initiates locomotion from an offset in the gravitational potential. These video frames were captured using a high-speed camera.

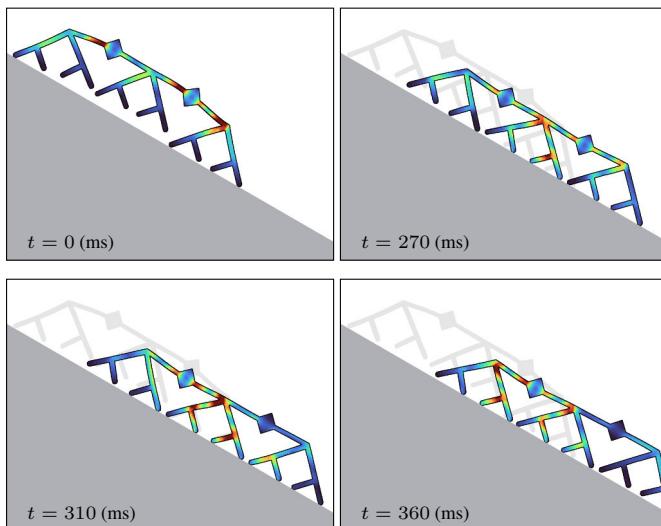


Figure 6.17. Snapshots of the multi-legged passive walker from Sorotoki. The experimental setup is similar to that described in [263]. By comparing the gaits in Fig. 6.16, a resemblance can be seen between the results obtained in Sorotoki and those reported in [263]. The Von Mises stresses are shown as $\in [0, 100] \text{ MPa}$.

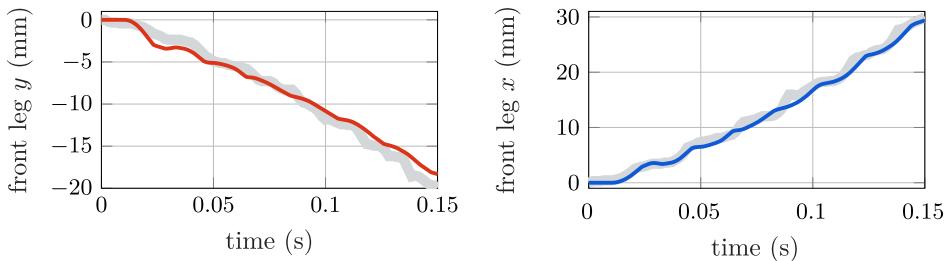


Figure 6.18. Comparison of the front leg rectilinear displacement between the experimental data obtained from Suzumori et al. [263] and the numerical data produced by Sorotoki shows that, although there are discrepancies, the step-like behavior and the traveled distance in the horizontal and vertical directions appear to be truthfully captured in comparison to the original experimental data.

To design the geometry of the V-shaped soft legs, the `sStrut(V1,V2,W)` function was utilized. This function generates an element of the `Sdf` class, requiring two nodal positions `V1,V2` and the strut's width `W` as input. The function was used to assemble a pair of legs iteratively, using the union operator implemented as MATLAB's '+' arithmetic. The legs were then horizontally repeated three times with a uniform spacing of 25 mm. A coupling soft body was added, along with two weights at intermediate locations. The resulting SDF is first converted to an `.png` template and the imported in the `msh = Mesh('SDF.png','ElementSize',1.0)` to generate the finite element mesh.

The mesh is then utilized to construct the finite element model, *i.e.*, `fem = Fem(msh)`. The timestep for the implicit solver is set at $\Delta t = 0.33$ ms, which is set using `fem.setTimeStep(dt)`. Instead of modeling the inclined surface, which would also require rotating the mesh, the direction of the gravitational acceleration vector is modified as follows: $g := \text{Rot}_y(\varphi)a_g$ with $\varphi = -\frac{\pi}{6}$ (rad). The gravitational acceleration is then added using the class function `fem.addGravity`. The inclined surface is modeled as a horizontal line SDF, which is used as a contact environment for the FEM model through the function `fem.addContact`. It should be noted that in Figure 6.16, the soft walker is held in place by two fingers, which results in initial deformations of the soft body and nonzero initial conditions for the dynamic locomotion. To account for this, the mesh is pinned at the grasp locations, and the initial quasi-static deformations are solved for using `fem.solve`. Finally, the forward dynamics are solved implicitly using a Newmark- β solver by calling the routine `fem.simulate`.

Figure 6.17 shows snapshots of the dynamic simulation of the soft passive walker at times corresponding to those depicted in Figure 6.16. Although slight deviations are noticeable, the overall dynamic characteristics of the locomotion are captured closely by the dynamic FEM model produced using Sorotoki. To further demonstrate the validity of the model, a comparison of the rectilinear displacement of the front leg between the experimental data and the simulated

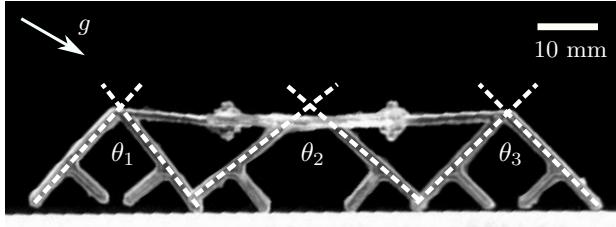


Figure 6.19. Definition of the angular deflection of the three pairs of soft legs, denoted by θ_1 , θ_2 , and θ_3 , respectively. It should be noted that each pair has an intrinsic V-shaped structure, thus their stable equilibrium position during rest is approximately $\theta_i^* \approx 45^\circ$. Raw image obtained from [263].

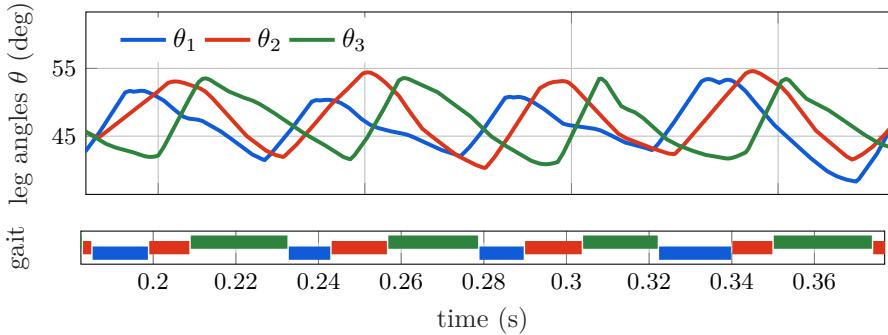


Figure 6.20. Angular deflection of the V-shaped structure of the soft passive walker, simulated with **Sorotoki**. A clear gait cycle is observed in these deflections, indicating synchronization between the deformable structures due to the coupling of the soft body. By analyzing the stable gait cycles, a gait period of approximately $T_{\text{gait}} \approx 47.5$ ms or $f_{\text{gait}} \approx 21.1$ Hz is found.

model is presented in Figure 6.18. The experimental data is obtained from [263] and is shown in Figure 6.18 (in gray). As demonstrated in the figure, the step-like behavior is accurately captured by the numerical model, and the horizontal and vertical distances traveled by the numerical model closely match the original experimental data.

To examine the gait cycle, we introduce state variables $\theta_1, \theta_2, \theta_3$ to represent the joint angles between the V-shaped legs, as depicted in Figure 6.19. The trajectory of these angles over a small time window of 200 ms is shown in Figure 6.20. The angular movements exhibit a clear and consistent "stable" gait cycle, indicating that synchronization indeed occurs between the deformable soft legs due to their interaction with the deformable soft body. An analysis of the stable gait cycle reveals a gait period of approximately $T_{\text{gait}} \approx 47.5$ ms or $f_{\text{gait}} \approx 21.1$ Hz. The numerical simulations presented in this study have effectively demonstrated the capabilities of the **Sorotoki** framework in accurately capturing the complexities commonly encountered in dynamic analysis of soft robots. Furthermore, it has been demonstrated that the methodology proposed by Suzumori et al. [263] can be

efficiently replicated using a minimal amount of code, specifically, approximately 30 lines within the **Sorotoki** framework.

6.6.2 Computational design of bending PneuNet actuator

In this section, we demonstrate the use of finite element models to aid in the design of PneuNet actuators, a popular type of soft robot actuator. PneuNet actuators, which have been in use since the 1980s, utilize a rectangular-shaped actuator with a stiffness differential to achieve a bending motion. Recent developments in the field, such as the work of Mosadegh et al. [195] and Ilievski et al. [122], have proposed modern variations of PneuNet actuators that incorporate an inextensible but flexible bottom layer to further enhance the bending motion. The motion of a soft actuator depends on the interaction between the soft material, structural geometry, and the locations where external loads are applied. In their work, Mosadegh et al. [195] demonstrated the importance of geometry in the performance of PneuNet actuators by proposing a new design, called the fast PneuNet (fPN), that improved upon the earlier slower PneuNet (sPN) designs presented in [122]. The fPN design requires less gas for inflation and thus significantly increases the actuator's performance. Design optimization for PneuNet soft actuators remains an active area of research, as evidenced by recent studies [217, 251]. This demonstrates the continued interest in desing optimizing in soft PneuNet actuators, even decades after its initial development.

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The purpose of this example is to demonstrate the use of **Sorotoki**'s design capabilities to optimize and create a PneuNet actuator. We will apply an inverse design method to find the optimal configuration of a soft material that undergoes pure bending when pressurized. This approach extends upon the work presented in Chapter 3. To extend of our prior study, we aim to show that the optimized designs produced through this computational design method can effectively overcome the Sim2Real hurdles. To find the optimal material arrangement, we will use a nonlinear topology optimization technique, specifically designed for compliant mechanisms.

The objective in the nonlinear topology optimization approach is to find the optimal material distribution $\rho^* = \operatorname{argmin}_{\rho} -\mathbf{L}^\top \mathbf{x}(\rho)$, where \mathbf{L} is a sparse unit vector that selects the nodal displacements that promote bending motion. Once an optimum is found, the material distribution ρ^* can be transformed into a 3D model and manufactured using a commercial 3D printing platform, such as Elastic 80A resin (Formlabs). The optimization algorithm can take into account the specific mechanical properties of the selected printing material, allowing for an optimal design that is tailored to these material properties.

To simplify the problem, we consider a single pressure chamber of the PneuNet actuator. To do this, a rectangular design domain with a size of 15×30 mm is defined using a **Sdf** library within **Sorotoki**. The **Mesh** class is then utilized to generate a mesh, which is used to construct a finite element model (FEM) using the **Fem** class. The **Fem** class takes several arguments to set up the optimization solver

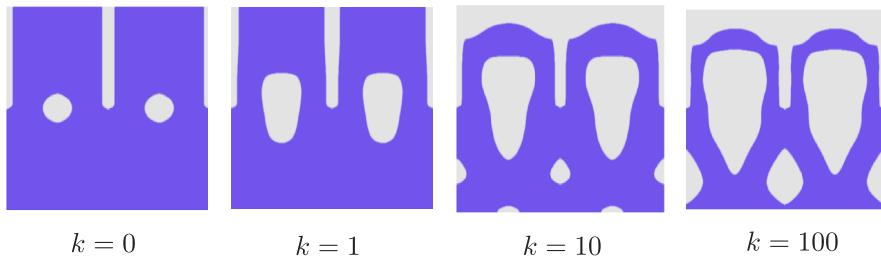


Figure 6.21. Evolution of the topology-based optimization routine in **Sorotoki**. At $k = 0$, we see the initial guess for the PneuNet actuator, and at $k = 100$ we see a converged solution of the optimizer. Observe that the algorithm proposes a solution very similar to the PneuNet, but instead, it has a teardrop shape rather than the classical rectangular shape. It is worth mentioning that the optimizer accounts for the hyperelastic material properties - in this case, Elastic 80A resin by Formlabs.

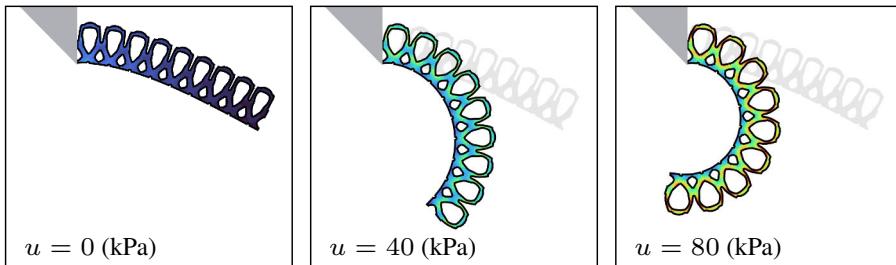


Figure 6.22. Nonlinear finite element simulation of the optimized PneuNet actuator using **Sorotoki**. The system is subjected to a linear ramp upto 80 kPa, and we observe the classical bending behavior of PneuNet actuators. The Von Mises stresses are shown as $\in [0, 10]$ MPa.

conditions, including the volume infill, penalty value, filter radius, time steps, and the maximum number of iterations for the method of moving asymptotes (MMA).

The initial material distribution is set using `fem.initialTopology(sdf)` with `sdf = sCircle(5,[7.5,15])`, which creates a hole in the center of the actuator. The center element of the mesh is designated as an invariant pressure input and influences neighboring elements that satisfy the void conditions (i.e., $\rho_i \leq \varepsilon$ with $\varepsilon = 0.1$) using an efficient flood-fill algorithm. The influenced void elements undergo synchronous volumetric expansion to simulate a positive pressure load. Given its similarities to muscular contraction, the syntax for this function is added as `fem.addMyocyte`. The material properties of the Elastic 80A resin from FormLabs are then specified using `fem.Material = Elastic80A` [316]. Boundary conditions are added to the FEM model using the syntax `fem.addSupport`. Finally, the optimization routine is started using the `fem.optimize` command.

The evolution of the material distribution during the first 100 optimization steps is depicted in Figure 6.21. These interpolated isosurfaces are taken from the discrete FEM mesh and show the intermediate design solutions. Surprisingly, the

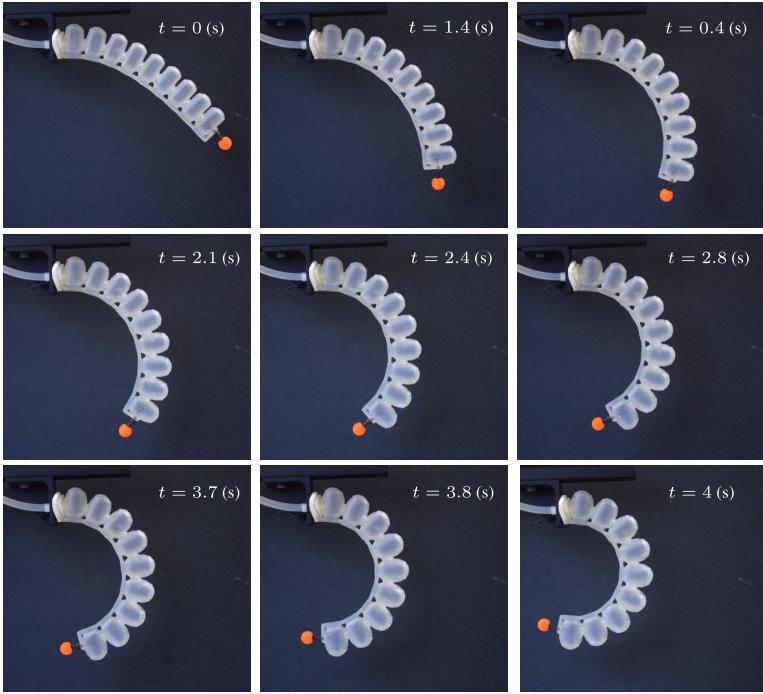


Figure 6.23. Validation study of a 3D-printed *PneuNet* actuator optimized using Sorotoki. The soft actuator is printed using SLA on a Form3+ printer using Elastic 50A UV-resin. Similar to the numerical simulations, we vary the pressure from 0 to 80 kPa with a linear ramp. To measure the planar displacement, an orange marker is placed such that `Vision.m` can be employed.

optimization algorithm generates a design that is reminiscent of the fast PneuNet design presented by Mosadegh et al. [195], but with a bellows-shaped pressure chamber in the form of an upside-down teardrop shape.

Next, the focus shifts to validating the optimization results. The aim is two-fold: (i) to validate that the optimization algorithm indeed produces the desired bending motion, and (ii) to verify if the design suggestion can be successfully transferred to reality (Sim2Real). To do this, the results of the optimization from `fem.optimize` are converted into a triangular mesh using `msh = fem.exportMesh`. Then, boundary conditions are assigned, such as a clamped boundary, gravitational loads, and internal pressure loads for each embedded PneuNet chamber. The same material model for *Elastic80A* resin is chosen. The quasi-static FEM simulation results of the optimized PneuNet actuator for linearly increasing pressure loads of $u = 80$ kPa are shown in Figure 6.22. As can be seen, the desired bending behavior is achieved in the simulation.

Next, the optimized isosurface shown in Figure 6.21 can be transformed into a 3D CAD model and printed as a physical soft actuator using a Form3+ SLA printer

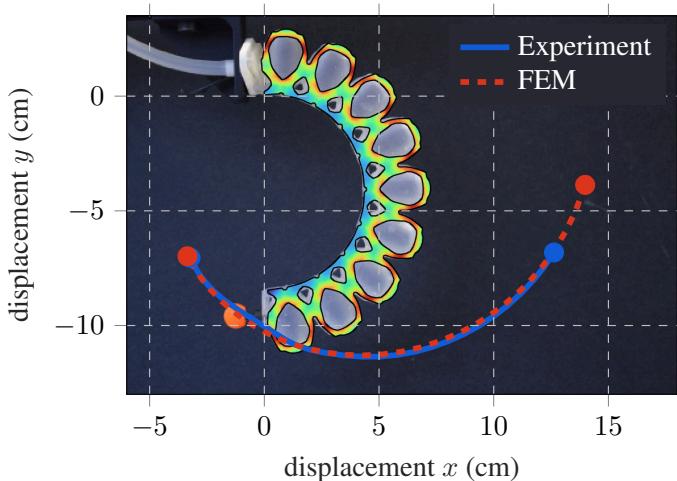


Figure 6.24. Comparison between the numerical simulation in `Sorotoki` and the experimental results where the orange marker is tracked using the `Vision.m` class is shown. The Von Mises stresses are shown as $\in [0, 10]$ MPa. The results indicate a close overall trend between the simulation and experiment. However, a discrepancy in the initial deformation ($u = 0$ kPa) is observed. It is hypothesized that this discrepancy is attributed to the inherent creep of SLA resin materials, which leads to a predeformed continuum due to the slow relaxation of the material upon actuation.

(FormLabs) with Elastic 80A resin. To validate its performance, the soft actuator is subjected to a linearly increasing pressure load of 80 kPa in 5s window. As seen in Figure 6.23, the optimized soft actuator successfully performs the desired bending motion, indicating the feasibility of crossing the Sim2Real barrier.

To quantify the discrepancies between the FEM predictions and the actual system, an optical marker is placed at the tip of the soft actuator. The spatial coordinates of the optical marker are obtained using the `Vision` class of `Sorotoki`, which uses the color-filtered Hough-space circle transformation to return the pixel coordinates of the marker. These measurements are collected using a RealSense D435 RGB-depth camera (Intel). To retrieve the spatial location of the color marker, we use the command `cam = Vision('realsense')` together with the function `cam.getMarker(R,rgb)`, where `R` is an estimate of the color marker radius in pixels, and `rgb` is the RGB color value of the marker.

The comparison between the FEM predictions and experimental results is presented in Figure 6.24. The deformation patterns of the FEM model and the physical system show close agreement, with an average error of ± 2 mm. However, there is a noticeable difference in the initial conditions, as shown in Figure 6.24. For $u = 0$ kPa, under pure gravitational loads, the deformations deviate significantly. The cause of this discrepancy is believed to be related to post-curing and internal stress relaxation of the photopolymerization process. This suggests that the

stress-free configurations of the FEM model and the physical system may differ, but accounting for this stress-relaxation phenomenon in photopolymer printing is outside the scope of this study and the *Sorotoki* toolkit.

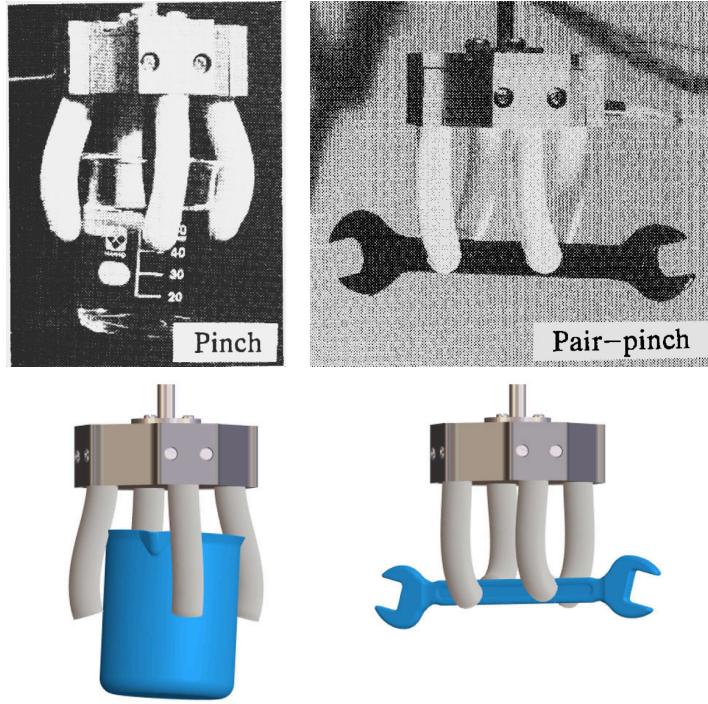
Despite the presence of some differences, the numerical and experimental examples presented in this study highlight the ability of the computational design framework within *Sorotoki* to generate purposeful and useful material distributions with limited prior knowledge of conventional soft robotic design practices. This not only speeds up the design process, but it also opens up the possibility of creating new and innovative soft robot forms.

6.6.3 Dynamic manipulation of high dexterity soft gripper

In this section, we will examine the use of reduced-order models for soft beams within the context of the *Sorotoki* software. These models are designed for efficient simulation by exploring minimal state representations of the dynamics of continuum systems. To demonstrate the capabilities of the soft beam modeling framework within *Sorotoki*, we will consider a specific example of a soft robotic system proposed by Suzumori and Suzuki in their seminal work [261, 262]. Despite being published in the early 1990s, the work by Suzumori et al. is still recognized as a seminal contribution to the field of soft robotics technology and remains relevant to this day.

In their research, Suzumori et al. developed a highly dexterous soft gripper consisting of four microfluidic soft actuators driven by an electro-pneumatic control system. Each finger has three internal pressure chambers, which together provide three controllable degrees of freedom at the fingertip, including pitch, yaw, and linear stretch. Unlike classic rigid grippers, the soft body of the gripper conforms to external forces, enabling intrinsic adaptation during grasping or manipulation tasks. As an illustration of the static grasping capabilities of this soft gripper, Figure 6.25 depicts two grasping configurations: a pinch grasp for a 40 mm diameter glass beaker (left) and a two-finger pair-pinch grasp for a 5 mm thick metal wrench (right). Suzumori et al. then employed inverse kinematic and compliance control to relate the tip position and compliance to input pressure values. As shown in Figure 6.25, they were able to successfully hold and turn a 10 mm hexagonal bolt, with an average speed of 0.25 revolutions per second. Due to the wide range of dexterous actions performed by the gripper, the soft gripper proposed by [261, 262] remains a seminal contribution to the field of soft robotics, demonstrating the potential of the technology.

The objective of this investigation is to replicate the static grasping and dynamic bolt-screwing experiments as conducted by Suzumori in their published works [261, 262], utilizing the *Sdf*, *Shapes*, and *Model* classes available in the *Sorotoki* software. The soft gripper's design specifications are based on the parameters provided by the available literature, which comprise a radius of $R_0 = 6$ (mm) and an assumed length of $L_0 = 80$ mm for each finger. Although the properties of the soft gripper's material are not mentioned explicitly, we suggest



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Figure 6.25. (top) Pinch and pair-pinch grasping configurations of the soft gripper proposed by Suzumori et al. [261, 262]. The high compliance of each soft finger allows for an adaptive, stable grasp that conforms to the shape of the rigid object. (bottom) A reconstructed soft gripper using the **Sorotoki** framework. To model each soft finger, we utilized the **Shapes** class and composed the entire gripper using the **Model** class. The rigid objects were modeled using the **Sdf** class. We observed a close resemblance between our simulation model and the original experiments performed by Suzumori et al. in [261, 262].

a Neo-Hookean model ansatz to address this issue. The proposed model has an elasticity modulus of $E_0 = 1.0 \text{ MPa}$, Poisson ratio of $\nu_0 = 0.3$, and density of $\rho_0 = 2000 \cdot 10^{-12} \text{ kg mm}^{-3}$. The reduced-order model for each soft finger in interaction with a rigid object, denoted by $\Sigma_{\text{SR},i}$, is described by the following equation:

$$\boldsymbol{M}(\boldsymbol{q}_i)\ddot{\boldsymbol{q}}_i + \boldsymbol{h}(\boldsymbol{q}_i, \dot{\boldsymbol{q}}_i) = \boldsymbol{G}(\boldsymbol{q}_i)\boldsymbol{p}_i + \sum_{j \in \mathcal{S}_{\Omega_{\text{env}}}} \boldsymbol{J}_{v,j}^\top(\boldsymbol{q}_i) [\boldsymbol{\mathcal{F}}_{n,j}(\boldsymbol{q}_i) + \boldsymbol{\mathcal{F}}_{t,j}(\boldsymbol{q}_i, \dot{\boldsymbol{q}}_i)], \quad (6.26)$$

where $\boldsymbol{h}(\boldsymbol{q}_i, \dot{\boldsymbol{q}}_i)$ represents the collection of nonlinear internal forces, \boldsymbol{p}_i is the prescribed pressure input, $\boldsymbol{J}_v(\boldsymbol{q}) := [\boldsymbol{J}(L, \boldsymbol{q})]_3$ is the linear velocity part of the generalized Jacobian matrix of the tip, $\mathcal{S}_{\Omega_{\text{env}}}$ represents the nodal indices that penetrates the object, and $\boldsymbol{\mathcal{F}}_n = -\mu_e \boldsymbol{d} \cdot \boldsymbol{e}_n$ and $\boldsymbol{\mathcal{F}}_t = -\mu_v |\boldsymbol{\mathcal{F}}_n| \text{sgn}(\dot{\boldsymbol{d}}) \cdot \boldsymbol{e}_t$ denoting

the normal and tangent contact forces between the i -th finger and the rigid object, respectively. The parameters $\mu_e, \mu_v > 0$ represent the contact coefficients. The distance between the finger and the object is given by $d = \text{sdf}_{\Omega_{\text{env}}}(\gamma_L(\mathbf{q}))$, where $\text{sdf}_{\Omega_{\text{env}}}(\cdot)$ represents the signed distance function of the rigid object and $\gamma_L(\mathbf{q})$ the finger's tip position.

In this study, we utilize a third-order Chebyshev polynomial basis to model the deformation of the pneumatic soft robot's finger. The basis is sampled over $N_p = 100$ uniform nodes and is assembled into a matrix using the command `pod = Basis(100,3,'chebyshev')`. It is assumed that only free strains occur in the bending, while elongation and torsion are neglected. Each strain mobility vector is characterized by three modes of the Chebyshev basis, specified as `dof = [0,3,3,0,0,0]`, leaving the κ_x and κ_y curvatures free. The dynamic model for each finger is constructed using the command `shp = Shapes(pod,dof)`. The material properties are assigned using `shp.Material = NeoHookean(1.0, 0.3)`. To set the geometry of each finger, we call `shp.setLength(80)` to set its length, and `shp.setGeometry(sCircle(6))` to set a circular cross-section of radius 6 (mm). Each finger of the soft gripper model is equipped with three fluidic chambers that are radially distributed along its circumference. As such, the input map \mathbf{G} for each finger becomes a nonlinear, non-square matrix. We assume that these distributed forces can be represented by a tangent bundle of linear forces that are positioned 3 (mm) away from the center axis. To assign these forces, the `shp.addFluidic(@p)` command can be utilized, which requires an anonymous function `@p` that describes the path of the soft actuator.

The full soft gripper model, composed of four identical finger `Shapes` classes, can be assembled using a for-loop routine. In this process, a class representing each finger is copied and assigned a unique SE(3) base frame to each instance. Each finger is placed in a circular array with a radius of 37.5 (mm) relative to the center axis of the gripper body. The contact domain for each finger is specified using the method `shp.addContact(sdf)`, where `sdf` denotes the signed distance field of the contact object. For the beaker example, a cylindrical SDF with dimensions $40 \times 40 \times 60$ (mm) is considered, while for the wrench, a rectangular SDF with dimensions $5 \times 10 \times 100$ (mm) is used. Subsequently, each instance of the `Shapes` class is appended to the `Model` class constructor using the `mdl.addSystem(shp)`.

Once the global model of the soft gripper has been assembled, it can be controlled using an open-loop controller. In the case of a static grasping scenario with a glass beaker and wrench, we apply pressure ramps to each pressure chamber of the soft gripper through an auxiliary anonymous function, `@(mdl) Control(mdl)`. The function takes in a time variable and outputs a column vector of pressure signals, represented by $\mathbf{u} = (\mathbf{p}_1, \mathbf{p}_2, \mathbf{p}_3, \mathbf{p}_4)^\top$. The controller is then assigned to the `Model` class using the command `mdl.addControl(@Control)`, which is executed at each simulation step. The forward dynamics of the soft gripper's interaction with the object are implicitly solved through the `mdl.simulate()` routine. The simulated grasping configurations are shown in Figure 6.25. It is evident that there is close agreement with the experiments in [261, 262].

Subsequently, we aim to reproduce the hexagonal bolt screwing experiment of [261, 262], which involves a more complex simulation than the previous scenario due to the dynamic interaction between the environment and the soft robot. To accurately depict this interaction, we must also incorporate dynamics into the signed distance field describing the hexagonal bolt screw. We assume a rotational mass-damper system, represented by the following equation:

$$I_{\Omega} \ddot{\theta} = -\mu_{\Omega} \dot{\theta} - \sum_{i=1}^{N_{\text{finger}}} \sum_{j \in \mathcal{S}_{\Omega}} \mathbf{r}_j(\mathbf{q}_i) \times \mathcal{F}_{t,j}(\mathbf{q}_i, \dot{\mathbf{q}}_i) \cdot \mathbf{e}_3, \quad (6.27)$$

where I_{Ω} is the inertia of the hex-bolt, $\mu_{\Omega} = 2.5$ its friction coefficient, and \mathbf{r} the relative position vector from the point of contact and the central turning axis of the screw. Note that we only include the tangential force components \mathcal{F}_t that are responsible for motion, as the normal forces are assumed to have a net zero-torque contribution. The model described in equation (6.27) is incorporated into the simulation by using the command `mdl.addSystem(@f)`, where `@f(x,u,t)` is an anonymous function that represents the state space. The required input u for equation (6.27) is connected to the soft gripper by utilizing the `mdl.addController(@Controller)` command, which inputs tangential reaction forces into the screw model. The controller also includes the prescribed pressure profile $p_{1,2,3,4}$ for each of the four soft fingers.

The qualitative comparison between the experiments conducted by Suzumori et al. [261, 262] and our numerical model programmed using Sorotoki is depicted in Figure 6.27. Similar to the simulation of the static object grasping scenario, the simulation of the Suzumori soft gripper's screwing experiment qualitatively reflects the real-world experiment performed in the 1980's. Not only do we observe similar deformation characteristics in the soft finger, but we also observe the step-like turning of the bolt screw, as reported in [262]. To highlight these rotational

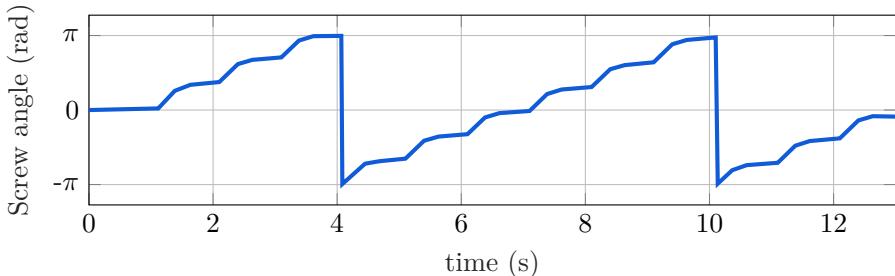


Figure 6.26. The evolution of the hexagonal bolt angle $\theta(t)$ is depicted, where the stair-like trajectory of the screwing motion, as observed in Suzumori's experiment, is apparent. Through careful parameter and input shaping, a bolt-screwing motion of 0.16 rps was achieved. This is slightly slower than the reported rate of 0.25 rps, however, the underlying morphological characteristics are accurately captured.

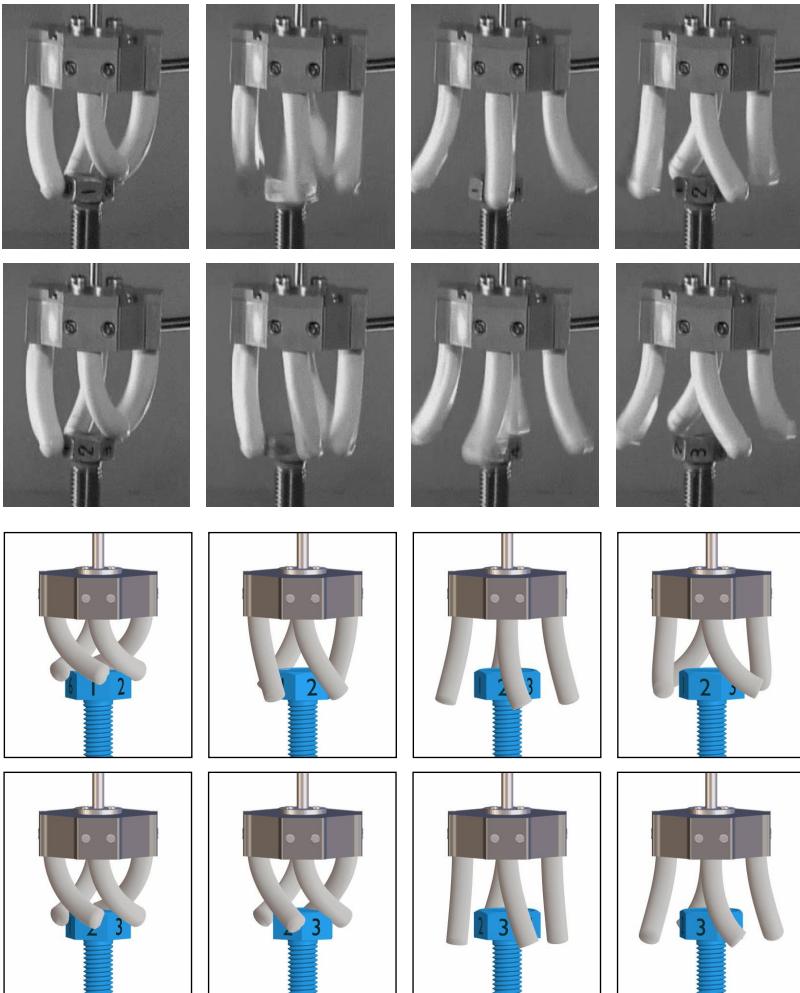


Figure 6.27. (top) Snapshots of the bolt screwing experiment with the soft gripper, as presented in the work of Suzumori et al. [261, 262], are displayed. The soft gripper periodically switches through a predefined set of configurations, enabling the holding and manipulation of a hexagonal bolt screw. In the experiment, a bolt turning rate of 0.25 rps was achieved. (bottom) The bolt screwing experiment was reproduced using *Sorotoki*. In the simulation, each finger was modeled utilizing the class `Shapes` and assembled together into `Model`. The contact interaction with the bolt was modeled using signed distance functions, and a rotational mass-damper model was used to describe the dynamics of the bolt. By utilizing solely the frictional interaction between the fingers and the screw, the experiment of Suzumori et al. was successfully reproduced.

trajectories, we present the rotation angle $\theta(t)$ in Figure 6.26, which shows that an average bolt-screwing speed of 0.16 rps is achieved. Although this rate is slightly slower than the reported rate of 0.25 rps, it is believed that the underlying morphological characteristics are accurately captured. Note that although the system is of highly complex nature, the simulation program contains less than 100 lines of code (including visualization).

6.6.4 Impedance control of soft robot manipulator with static environmental interaction

The subsequent section will focus on the development of controllers utilizing the `Model` and `shapes` classes. In prior experiments, the Suzumori et al. gripper was governed in an open-loop fashion, with complications arising from the interplay between the model and dynamic object. Our investigation will now examine the feasibility of model-derived controllers in the `Sorotoki` scenario, drawing upon Della Santina et al.'s work [71] as a prospective case study.

Their work presents a design for model-based controllers for soft robot manipulators, highlighting two control architectures: dynamic tracking and surface tracking. The authors proposed a Cartesian impedance controller for the latter architecture, which actively regulates the desired compliance behavior of the soft robot's end-effector in a static environment. Additionally, the work presented a contact path planning algorithm that initially brings the robot close to a desired setpoint on the surface (Phase 1: Approach), and then adjusts the setpoint to maintain contact with the surface (Phase 2: Explore). The proposed controller was validated both numerically and experimentally on a six-link soft robot manipulator, demonstrating that model-based controllers can lead to higher-level performances in soft robotic systems.

To maintain high computational bandwidth, the impedance controllers used in Della Santina et al.'s study [71] incorporate an augmented rigid body model. This model employs Constant-Curvature kinematics to approximate the center of mass of the continuously deformable robot by projecting its mass distribution into a lumped mass description. This leads to an Euler-Lagrangian representation similar to the commonly used Denavit-Hartenberg (DH) parametrization models in rigid robotics. Moreover, this approach maintains classical properties, such as positive semi-definiteness of the inertia matrix and passivity properties, which are valuable for stability analysis.

Our aim in this section is to replicate the results of the closed-loop controlled multi-link soft robot during dynamic contact that were presented in the study by Della Santina et al. [71]. Instead of employing the augmented rigid body model used in their work, we explore a reduced-order beam model, in which each link is represented as an inextensible, continuous PCC segment. This approach extends their work to a distributed mass robotic system. As a template for the soft manipulator model, we again utilize the `Shapes` class. According to [71], each CC segment of the soft manipulator has an intrinsic length of $\delta L_0 = 60$ mm and

a mass of $m_0 = 334$ g. The robot has a rounded rectangular cross-section of 60×20 mm, which is described using `sdf = sSquircle`. The density of the soft robot manipulator, given its length and geometry, is approximated to be $\rho_0 = 1200 \cdot 10^{-12}$ (kg mm^{-3}).

A crucial aspect of the simulation is the dynamic interaction with the environment. Therefore, a static environment must be assigned to the dynamic model. While [71] presents multiple examples of dynamic contact, this study focuses on the experiment with a 40° slanted surface with wave indentations, as shown in Figure 6.28. The surface features were extracted from the image data presented in [71] and the `env = sPolyLine(V)` function was used to generate the SDF environment, where `V` is a polyline vector. The environment is then added using `Shapes.addContact(env)`. Once all settings are assigned to the class `Shapes`, the model is constructed by `mdl = Model(Shapes)`.

Given the `Model` class, we can now start deriving the control law. For conciseness, let $\mathbf{J}(\mathbf{q}) := \mathbf{J}(L, \mathbf{q})$ be the geometric Jacobian of the end-effector. We also introduce the Cartesian inertia matrix as $\mathbf{\Lambda} := (\mathbf{J}^\top \mathbf{M}^{-1} \mathbf{J}^\top)^{-1}$. Then, the proposed Cartesian stiffness controller given in [71] can be written as:

$$\boldsymbol{\tau} = \mathbf{J}^\top \left[\mathbf{J}_M^{+\top} \mathbf{f}_e + \mathbf{f}_g + \mathbf{J}^\top \boldsymbol{\eta}_C (\mathbf{I} - \mathbf{J}_M^{+\top} \mathbf{J}) \dot{\mathbf{q}} \mathbf{J}^\top (\mathbf{K}_c (\boldsymbol{\gamma}_d - \boldsymbol{\gamma}_L) - \mathbf{D}_c \mathbf{J} \dot{\mathbf{q}}) \right], \quad (6.28)$$

where $\boldsymbol{\gamma}_d$ and $\boldsymbol{\gamma}_L$ represent the desired and true end-effector positions, respectively; and \mathbf{K}_c and \mathbf{D}_c are the desired stiffness and damping of the end-effector. The closed-loop controller employs a so-called "*dynamically consistent pseudo-inverse*" of the Jacobian, denoted as \mathbf{J}_M^+ , which is defined as $\mathbf{J}_M^+ := \mathbf{M}^{-1} \mathbf{J}^\top \mathbf{\Lambda}$. The controller also utilizes the Cartesian Coriolis terms, denoted as $\boldsymbol{\eta}_C(\mathbf{q}, \dot{\mathbf{q}})$, which are expressed in the Cartesian frame and given by:

$$\boldsymbol{\eta}_C = \mathbf{\Lambda}(\mathbf{J}\mathbf{M}^{-1}\mathbf{C} - \dot{\mathbf{J}}) \quad (6.29)$$

The closed-loop controller, implemented as an anonymous function, is derived from four system matrices: the inertia matrix $\mathbf{M}(\mathbf{q})$, the Coriolis matrix $\mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})$, the Jacobian \mathbf{J} , and its time derivative $\dot{\mathbf{J}}$. In Sorotoki, these matrices are automatically computed at each solver step and stored in a data structure named `shp.log`. The closed-loop controller can access this data structure.

It is noteworthy that the controller above uses the command `shp.isContact` to detect if the robotic system is in contact. Similar to path planning in [68], upon contact, a new desired equilibrium position is adopted. These desired equilibrium positions for the end-effector are in line with the approach presented in [71]. Subsequently, the implicit solver is invoked by calling `mdl.simulate` to solve the closed-loop dynamics. Snapshots of the dynamics have been presented in Figure 6.28 which are produced by calling the function `shp.render`. Figure 6.29 shows the trajectory of the end-effector (dashed lines are the desired setpoints), Figure 6.30 shows the evolution of the states, and Figure 6.31 shows the control action $\boldsymbol{\tau}$ from (6.28).

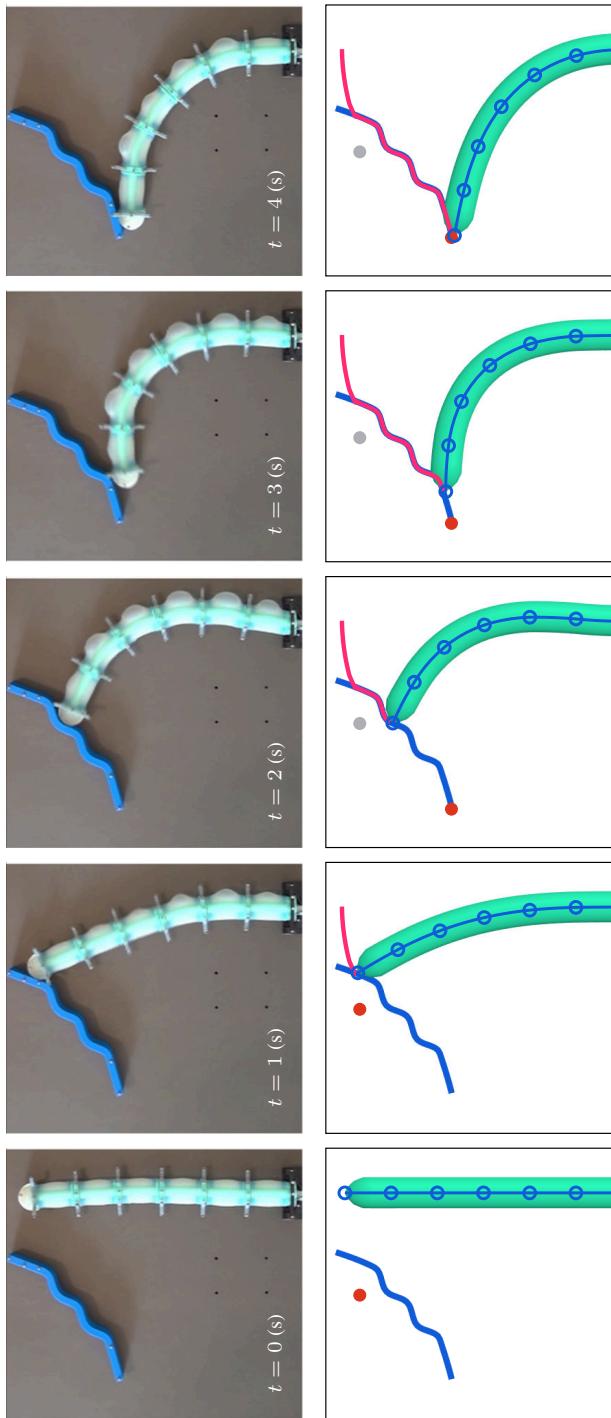


Figure 6.28. (top) The experimental results presented in the work of Della Santina et al. [68] show a six-link soft manipulator controlled by the control law described in (6.28). The manipulator is in contact with a static environment. The controller first ensures that the soft robot approaches the environment (Phase 1: Approach) and then follows the rigid wavy surface (Phase 2: Explore). (bottom) The numerical simulations performed using the Sorotoki toolkit are inspired by the work of Della Santina et al. [68]. In the simulation, the active setpoints are denoted by (●) and the de-activated setpoints are denoted by (○). The end-effector trajectory is shown in (—) and the environment is shown in (—). The results of the simulation truthfully reflect the approaching and surface tracking behavior as seen in the experiments.

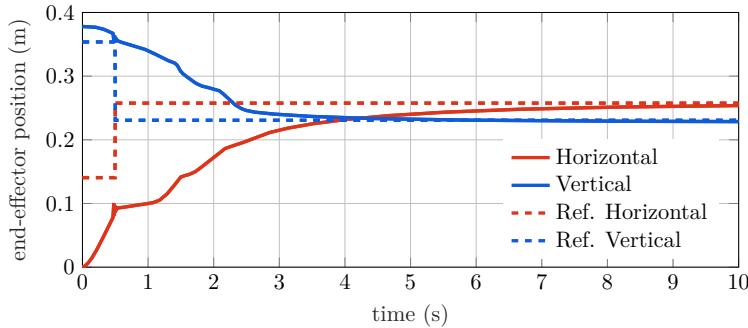


Figure 6.29. The end-effector trajectories of the six-link soft manipulator, where $\{\text{---}\}$, $\{-\}$ denote the horizontal and vertical position, respectively. The setpoints assigned by the controller are indicated by the dashed lines. Note that at $t \approx 0.88$ (s), the point of contact, the controller switches setpoint.

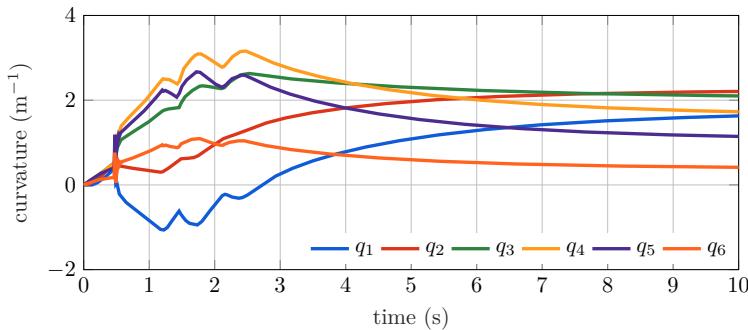


Figure 6.30. State evolutions of the six-link soft manipulator, where the states represent the planar curvature of each individual soft link.

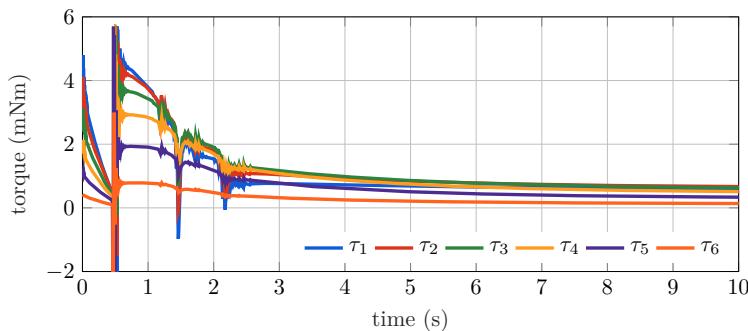


Figure 6.31. The control inputs τ in (mNm) produced by the control law in (6.28) exhibit a significant peak at the point of contact. This is due to two factors: (i) the sudden change of setpoint and (ii) the switch in control strategy to accommodate for compliance.

When comparing the experimental results reported by Della Santina et al. [68] and the numerical simulations produced by **Sorotoki**, we observe similar deformation characteristics in both systems. Most notably, the numerical implementation of the impedance Cartesian stiffness controller also follows the inclined surface until the setpoint is reached. These similarities highlight the reliability of **Sorotoki** in accurately reflecting true soft robotic systems, even in closed-loop scenarios.

6.6.5 Contact robust shape sensing of elastomer soft actuator (PneuNet) using a FEM-based modal basis

In the next section, our focus shifts from simulation to the experimental domain. Our primary focus will be on the **Vision** and **Control** classes, and we aim to provide experimental validation for the Data-driven Variable Strain (DVS) basis approach detailed in Section 6.5.4. The objectives of this study case are (*i*) to derive a finite-dimensional Cosserat beam model of the PneuNet actuator and (*ii*) to implement a real-time shape sensing algorithm that is robust against external forces through the exploration of model information.

We begin our investigation by conducting a nonlinear dynamics analysis of a soft PneuNet actuator, the geometry of which has been selected to match that described in the work of Mosadegh et al. [195]. The soft actuator is suspended vertically in order to produce minimal deformation under zero-input conditions. In pursuit of high-accuracy simulation, we first perform a Finite Element simulation. The generation of the mesh is performed using the function `msh = Mesh('PneuNet.png')`, which utilizes an image of a PneuNet cross-section as input. The finite element model is then formed using `fem = Fem(msh)`, and the appropriate material properties (*i.e.*, Dragonskin10) and boundary conditions are assigned. The system is subjected to a linearly increasing and decreasing pressure ramp of 40 (kPa), and the dynamics are solved using `fem.simulate`. In accordance with the procedure outlined in Section 6.5.4, a third-order DVS basis for pure bending is then constructed, which are used to construct the **Shapes** class. The curvature-bending modes are shown in Figure 6.32.

Given that the **Shapes** class has been constructed, we can now tailor the real-time estimation algorithm. This is achieved through the utilization of an inverse kinematics algorithm, as described in Section 22. The algorithm can be invoked using the function `Shapes.IK(pos, q0)`, where `pos` represents the desired position (such as a camera measurement) and `q0` is an initial estimate. The inverse kinematics solver is then repeatedly called in the real-time control loop. To ensure that the inverse kinematics solution aligns with the true system behavior, we also consider the null-space subtask projection. In this case, the gradient of the subtask is assumed to be $\nabla \Psi_{\text{sub}}(\mathbf{q}) = \mathbf{K}\mathbf{q} + \mathbf{f}_g(\mathbf{q}) - \mathbf{G}(\mathbf{q})u$, where $u = 30 \cdot \text{sat}[\sin(t)]$ (kPa) is the prescribed pressure input assigned by the open-loop controller. This subtask serves to minimize the internal residual forces – and thus is nothing more than a quasi-static deformation solver that is guided by the camera measurements. Note that model parameter have been pre-tuned to align with the experimental

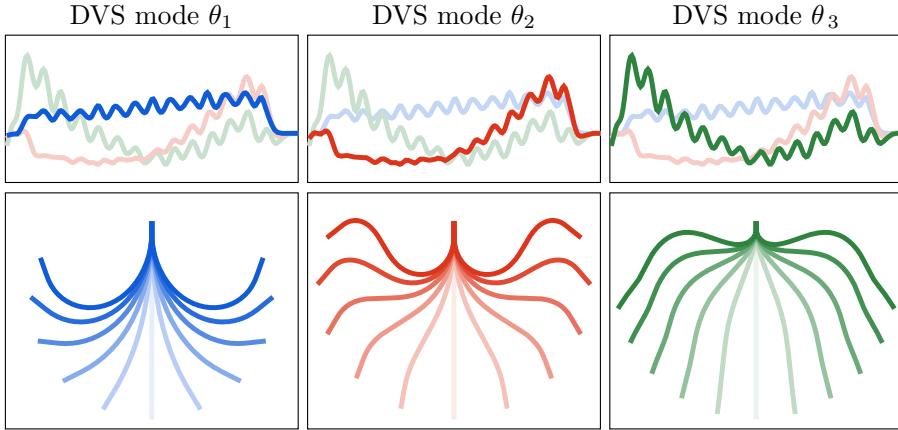


Figure 6.32. (top) The first three DVS modes of the soft PneuNet actuator in vertical hanging condition, where the ordering is {—, —, —}. (bottom) The respective deformation for each strain mode of the PneuNet actuator. Note that these differ from the DVS basis in Section 6.5.4.

6

system presented in Figure 6.33. However, certain initial estimates of the system parameters have been used that are produced by the Finite Element model.

To instantiate the camera class, we call `cam = Vision('realsense')` and establish a Secure Shell (SSH) connection with the control platform through `brd = Control('ip','pwd')`. Once the connection with the control platform is established, a real-time while-loop containing the necessary shape estimation algorithms to be executed.

Figure 6.33 shows the experiment and overlayed on top are the real-time shape estimations from the inverse kinematics algorithm that uses a combination with the Data-driven Variable Strain (DVS) basis. Figure 6.34 shows the state trajectories and the time instance of contact. Despite the significant impact of contact forces on the soft actuator, the shape estimation algorithm qualitatively matches the deformation profile of the real soft robotic system. This is due to its relatively low state dimension of $\text{dim}(\mathbf{q}) = 3$, enabling it to achieve a bandwidth of +60 Hz with ease.

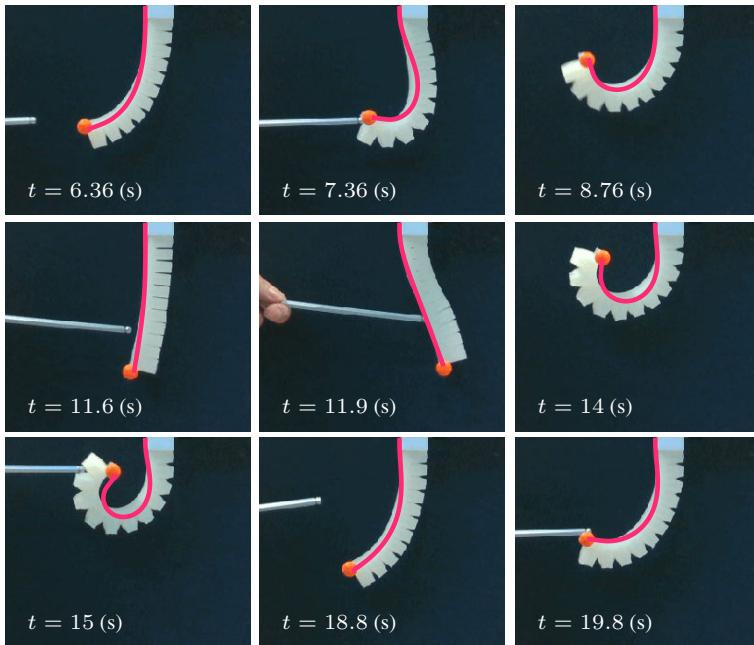


Figure 6.33. Real-time shape estimation using the **Shapes** inverse kinematics algorithm in combination with the Data-driven Variable Strain (DVS) basis. The reconstructed backbone curve is depicted in (—). Despite the presence of substantial contact forces on the soft actuator, the shape estimation algorithm accurately reflects the behavior of the real soft robotic system. Due to the relatively small state dimension of $\dim(\mathbf{q}) = 3$, the algorithm achieves a bandwidth of +60 Hz.

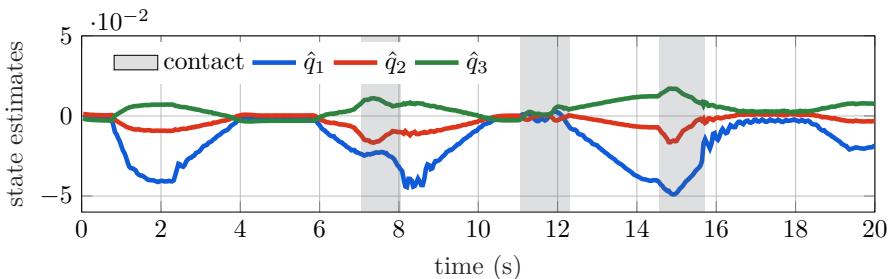


Figure 6.34. Evolution of the state estimations during the PneuNet experiment, where the ordering is given by {—, —, —}. Note that the joint variables represent the modal coefficients of the DVS basis related to curvature-bending.

6.7 Conclusion and future work

This paper introduces the *Sorotoki* is an open-source toolkit in MATLAB that provides a comprehensive and modular programming environment to address the complex interdependencies associated with the design and control of soft robots. The toolkit consists of seven Object-Oriented classes that are designed to work together to solve a wide range of soft robotic problems. We hope the versatility and flexibility of *Sorotoki* make it a valuable resource for many researchers and practitioners in the field of soft robotics. The toolkit has been demonstrated to be effective through a range of case studies encompassing a broad range of issues within the field of soft robotics, including inverse design of soft actuators, passive and active soft locomotion, object manipulation with soft grippers, meta-materials, model reduction, model-based control of soft robots, and shape estimation. A unique aspect of the software package is that it does not follow the traditional linear relationship between the complexity of soft robotics systems and the length of code needed to represent them. Instead, complex system behavior can be effectively modeled using a minimal number of lines of code. The *Sorotoki* software package is particularly notable for its ability to succinctly represent complex soft robotics systems. Despite the intricacy of soft robotics, the accompanying software package is highly effective in modeling complex system behavior with minimal code, making it accessible to individuals with limited programming knowledge. Furthermore, the toolkit provides access to four open-hardware soft robotic systems that can be easily fabricated using commercially available 3D printers.

Nevertheless, the framework presents opportunities for improvement and can be expanded to make it more comprehensive, extensive, and to achieve faster simulation times. This is particularly significant in the field of control, where computational performance is a recurring challenge. The software package *Sorotoki* addresses this challenge by converting MATLAB code to its equivalent in `c++` using the compilation method. Real-time computation is attainable, yet the produced `.mex` functions frequently face limitations due to inadequate memory allocation and a lack of parallel processing. This can result to subpar performance. An alternative solution could be to explore other languages with better computational performance, such as `Python` (via `pybind`) and `Julia`. Especially those with a stronger (open-access) community. An early `Julia`-port of *Sorotoki* is found at github.com/BJCaasenbrood/Sorotoki.jl, which has already shown performance improvements.

7

Conclusions, recommendations, and future outlook

In recent years, the scientific community has shown an increasing interest in soft robotics owing to its utilization of soft materials that augment the dexterity, mobility and resilience of robots. The field has demonstrated potential for various applications in both industrial and academic settings, such as reliable and safe manipulation, adaptable gripping, and environmental exploration under uncertainties. Despite the advancements made in soft robotics, there is still a considerable gap between this field and traditional rigid robotics as well as biological systems. As highlighted in the introduction, successful implementation of embodied intelligence in soft robotics necessitates the holistic consideration of the entire embodiment of the bio-inspired system, which harmonizes design and control aspects of soft robots.

The primary objective of this thesis is to develop new and systematic tools for the design, modeling, and control of soft robots, with the aim of improving their overall performance by considering these aspects as a collective body. In this section, we provide an overview of the key contributions of the thesis, along with recommendations for future research directions.

7.1 Conclusions

Design synthesis of soft actuators. Chapter 3 of the thesis proposes a new framework for synthesizing soft robot topologies from hyperelastic materials. The optimal design of actively deformable soft structures is a complex task due to the presence of numerous nonlinearities arising from material properties and fluid-structure interactions that result in state-dependent loads. It is crucial to consider these effects when designing such structures, as doing so ensures that the final soft topology is both efficient and effective in meeting its intended motion requirements.

Moreover, *ad-hoc* human-driven design methods for soft robots may not always be desirable. Firstly, the iterative process of designing, fabricating, and testing of soft robots can be excessively time-consuming for users. Secondly, accurately predicting the continuum-bodied motion of soft actuators without performing structural analysis is challenging, particularly when various material nonlinearities are present.

We address the challenges associated with designing fluid-driven soft structures by exploring the nonlinear Finite Element Method (FEM) using polygonal elements in conjunction with gradient-based topology optimization. The presented approach involves numerical free-form optimization to identify optimal topologies for fluidic soft actuation with predefined motion criteria set by the user. By exploring the mesh connectivity and volumetric dilation of polygonal elements, we have demonstrated that our approach provides a precise representation of fluid-structure interactions in soft robots, which is currently lacking in traditional structural optimization techniques. Through numerical analysis, we demonstrate that the optimization framework can generate meaningful design suggestions based on the desired actuator motion and material choice. Consequently, this capability significantly reduces the workload involved in developing pressure-driven soft robots. It is interesting to observe that the optimized topologies align with prevalent designs often utilized in soft robotics, such as the bellows and the well-known PneuNet actuator. Although some distinctions may appear minor, they emphasize the importance of achieving an optimal design in soft robotics. To illustrate, our approach yields concave configurations of bellows that effectively amplify the actuator's stroke. Alternatively, the bellows featured in the PneuNet actuator assume a tear-shaped morphology that obviates the need for an inextensible layer located at the base.

Modeling for control of soft manipulators. Chapter 4 addresses the necessity of bridging the gap between modeling and control-oriented research in soft robotics. The chapter proposes developing accurate dynamic models for continuum soft robots to explore model-based control. However, such dynamic models tailored towards continuum soft robots must maintain real-time performance for transferring model-based control to physical systems. To achieve this goal, we use a minimal set of coordinates related to the differential geometry of spatial curves to express high-dimensional continuum deformation, building upon existing *Piecewise-Constant Curvature* (PCC) formulations. To improve computational efficiency further, we propose a reduced-order integration scheme for fast forward dynamic simulations. Through numerical benchmarking, we demonstrate its ability to achieve real-time performance. In continuation, we introduce high-fidelity FEM data to enhance the representation of state-dependent compliance resulting from hyperelasticity and structural geometry in our models. We also introduce simplified models capable of capturing viscoelastic behavior, specifically creep. Our aim is to offer a more precise depiction of soft robots' compliant nature when compared to conventional Hookean options. To qualitatively evaluate our modifications, we conduct experiments that highlight a significant accuracy improvement

for static and dynamic conditions.

Following, our modeling approach is applied on a physical, pneumatic soft robot that has been produced using Additive Manufacturing techniques. The resulting continuum dynamic model exhibits good correspondence with the physical system and enables real-time simulations with varying degrees of motion. The similar model structures of soft robots and rigid robots facilitate the adoption of conventional control theory. We propose a passivity-based adaptive controller that provides exceptional tracking capabilities, despite encountering parameter uncertainties, including tip-loads and material parameters. Additionally, the controller gradually enhances the precision of these estimations over time, given that the unknown parameters remain persistently excited.

Chapter 5 centers on hyper-redundant soft robots and their capacity to imitate intricate morphological movements observed in nature. Previous PCC models exhibit various kinematic artifacts that hinder the actual hyper-redundancy commonly present in soft robots. In light of this, a modeling framework for Cosserat beams is presented, which leads to a finite-dimensional system in a port-Hamiltonian structure. An energy-shaping controller is proposed that ensures the closed-loop potential energy is minimal at the desired set-point. The numerical model is developed for several bio-inspired soft robots, such as an octopus' tentacle and an elephant's trunk with distributed control inputs. The key challenges are capturing hyper-flexibility, dealing with inherent under-actuation, and exploiting hyper-redundancy to achieve control tasks. The model-based controller yields smooth convergence of the soft robot's end-effector while accounting for under-actuation. Our findings reveal that adjusting the controller gains enables the adjustment of the intrinsic stiffness of the soft body, resulting in diverse quasi-static joint solutions for the set-point problem with varying structural compliance.

Furthermore, we explore the potential of our proposed modeling and control method to imitate biological creatures. By incorporating an energy-shaping control law that minimizes geodesic distance anywhere the curve, we are able to create closed-loop soft robots that demonstrate bending propagation patterns similar to those observed in octopi. This outcome underscores the significance of model-based control when striving to develop robotic systems with biomimetic characteristics, which leverage inherent structural flexibility to optimize task efficiency and potentially reduce energy consumption.

Software development for the soft robotics community. In Chapter 6, the thesis introduces Sorotoki, a modular and comprehensive MATLAB® toolkit that enables the design, modeling, and control of soft robots. This toolkit serves as a compilation of all previous components described in the dissertation. The toolkit encompasses a library of Object-Oriented classes that has been specifically devised to address a diverse array of problems in soft robotics, encompassing inverse design of soft actuators, passive and active soft locomotion, object manipulation with soft grippers, model reduction, model-based control of soft robots, and shape estimation. Its most significant feature is its ability to represent complex soft robotics systems using minimal code and a straightforward syntax. In theory, this

lowers the barrier of entry for individuals with diverse academic backgrounds to utilize the toolkit effectively. The chapter also presents a stable modeling platform for soft robotic systems that accommodates various shape functions designed for unique joint mobility imposed by the soft robot's design. Previous works in the modeling literature often select these functions without proper consideration, such as using polynomial bases (Chapter 5). This thesis proposes a geometric modal decomposition approach that extracts geometric strain modes from higher-fidelity FEM simulations to construct generic low-dimensional models that accurately encode the features and elasticity of soft bodies. This approach introduces a new strain parametrization called the "*Data-driven Variable Strain*" (DVS) basis. Finally, the toolkit also presents four open-hardware soft robotic systems that can be easily fabricated using commercially available 3D printers, further enabling soft robotic technology for the community. Overall, Sorotoki is a versatile and flexible resource that can benefit many researchers and practitioners of soft robotics.

7.2 Recommendations

Three-dimensional inverse design: Chapter 3 demonstrates the implementation of gradient-based design for soft robots using topology optimization. The process involves the application of straightforward optimization techniques to identify locally *optimal* structures that align with the desired morphology. However, due to computational limitations, only optimizations of planar mechanical structures have been considered. Hence, additional steps are imperative for transforming the found topology into functional structures of soft actuators. One suggestion for enhancing the optimization techniques discussed in this thesis is to broaden their scope to encompass three-dimensional domains. This expansion is highly recommended as it simplifies the post-processing of the resulting topological structure, which can then be more readily transferred to a 3D-printing platform. It is important to acknowledge that the computational complexity of finite element models experiences an increase of $\mathcal{O}(n^3)$ as n , the global degrees of freedom (DOF) of the mesh, grows. Due to this substantial computational burden, it is strongly advised that forthcoming investigations delve into the use of GPU parallel computation or cluster computation.

An alternative to consider is the potential integration of the Material Point Method (MPM). The MPM offers certain benefits over FEM, including its capability to handle significant mesh distortions and superior preservation of mass and momentum. Furthermore, complex geometries can be handled more explicitly without necessitating remeshing. Although MPM is more computationally intensive than FEM, there are software packages available that offer parallel computing on multi-GPU (Graphics Processing Unit) or cloud-computing architectures. Recent studies have demonstrated encouraging utilization of MPM in the context of free-form soft robots, particularly with regards to co-optimization for locomotion.

Extension towards active and multi-materials optimization: Another intriguing improvement upon Chapter 3 can be found in the area of multi-material

topology optimization. One common issue with soft robots is that their supporting structures experience limited force transmissibility without suffering from structural buckling instabilities. Conducting research on multi-materials offers a promising solution, where the use of diverse materials, inspired for instance by natural muscular-skeletal systems, can result in a broader range of mechanical operation, eventually benefiting potential applications such as locomotion. Additionally, advancements in multi-material printing technology have made it easier to consolidate soft, rigid, and flexible conductive materials, or even mixtures thereof. This presents an opportunity to incorporate skeletal function along with proprioceptive sensing capabilities that can be directly integrated into the optimization.

We believe that the integration of "*rigid*" and "*soft*" materials in soft robotics will be instrumental in facilitating the development of "*near-biological*" soft robot, especially when energy consumption is critical. To achieve this, an architectural hierarchy comprising mechanical rigid and soft components can be utilized to perform distinct functions such as motion transmission, body support, and energy storage and release. Extending such design philosophy further, we could start designing robots that are neither completely rigid nor completely soft, but instead explore a spectrum of material composites that enable embedded intelligence through smart use of materials and structural elements.

Free-floating and compositional soft bodies. In Chapters 4 and 5, we introduce techniques for modeling soft continuum robot manipulators, which can also be utilized for other slender, elastic structures. As demonstrated in Chapter 6, this method can be applied to soft grippers, *e.g.*, those described in seminal works like [244, 262]. Yet, a significant limitation of our modeling methodology is that the soft beam's structural foundation yield zero velocity and acceleration inherently. Consequently, this limitation partially restricts the applicability of the model and it cannot be directly applied to soft robotic systems designed for locomotion, closed-chain soft robots, or a composition of soft robots on mobile platforms (*e.g.*, drones or robot end-effectors). Other potential applications include academic study cases that relate to control theory, such as swing-up control for soft pendulums [67, 305]. This modeling restriction arises from the projection into the desirable Lagrangian formulation by means of pre-multiplication of the geometric Jacobian matrix, which effectively eliminates the boundary conditions at the foundation (*i.e.*, the constraint wrenches) in the model and thereby ensures that the state's evolution always satisfies the imposed kinematic behavior.

In order to relax the model, we recommend extending it to incorporate the rigid-body dynamics of the entire soft structure subjected to general motion. This can be done by introducing a free inertial coordinate frame that is affixed at a specific location on the body, following a similar Lie group representation. Although the selection of this inertial coordinate frame can be chosen arbitrary, opting for the base of the beam constitutes a reasonable choice inline with prior chapters. The equation of motions can be written using a Newton-Euler formulation, akin to the approach presented in Chapter 5. Consequently, this necessitates a separate solver that calculates the inertia tensor, which accounts for changes of the center

of mass upon deformation, and the lumped integration of all inertial wrench responsible for rigid-body motion. In theory, it is feasible to optimize the spatial integration of Lagrangian matrices along with rigid-body inertial dynamics by developing a single Matrix Differential Equation (MDE), which aims to expedite the computational process. However, additional investigation is necessary to explore the numerical efficiency of these methodologies. This is imperative for enabling online model-based control, which can be implemented in areas such as locomotion.

Robustness of modal discretization for soft beam, a Chicken-and-Egg problem. Although the prospect of exploring locomotion is fascinating, it presents a challenge that is not immediately apparent. Namely, there is no guarantee that a chosen modal strain discretization is representative of the true spatial dynamics of the soft beams. Since robots often operate in unstructured environments, there are infinite possible force wrenches of varying amplitudes and frequencies that can disturb the system. Due to our inadequate understanding of the interaction between the soft robotic system and the unknown environment, it is difficult, if not impossible, to select an appropriate strain basis *a-priori*. This challenge was previously discussed in Chapter 5, where it was referred to as the "Chicken-and-Egg" problem, primarily from the viewpoint of state feedback. The implementation of model-based feedback loops, or feedback in general, has the potential to evoke strain modes that were not considered during modeling. This might paradoxically lead to unintended errors being introduced. The implementation of model-based control leads to circular reasoning of cause-and-effect in regards to this phenomenon. Furthermore, ascertaining whether the closed-loop system can stabilize such unmodeled modes through rigorous mathematical analysis is challenging, since various numerical approximations of the PDE model are introduced.

A recommendation for future research involves conducting a rigorous mathematical analysis on the stability and robustness of control laws derived from the Cosserat PDE model. Chapter 5 showed that controllers with state dimension significantly smaller than the plant, can lead to good closed-loop performance under conservative conditions (*e.g.*, static setpoint). The finding may suggest that the role of modal truncation (or the choice of model basis) in the performance of model-based control for soft robots may be less significant. We believe soft robots inherently possess sufficient redundancy to effectively counteract for modeling imperfections. This issue is directly linked to the selection of control gains, for which we currently lack a systematic approach to determine suitable values aside from *ad-hoc* tuning. Deriving control gains with stability guarantees may prove challenging, but offers substantial advantages for the future application of soft robots. On the other hand, Chapter 6 experimentally demonstrated that the DVS strain method is sufficiently robust to accommodate (moderate) unmodeled disturbances that manifest as point contacts at multiple locations on a soft body. This suggests that these models possess a certain degree of disturbance rejection. Our hypothesis is that soft body may act as spatial low-pass filter that structurally penalizes high-order modes, thus a sufficiently large collection of ordered

strain modes will alleviate the Chicken-and-Egg problem. This may provide an explanation for the successful performance of control structures that are based on the Piecewise-Constant Strain assumption thus far. One possible area of investigation is the application of frequency-based stability analysis to the closed-loop PDE system. Another potential avenue for research involves the exploration of adaptive basis representations that can dynamically adjust their truncations based on observable model errors. This approach is partially inspired by the adaptive control methodology described in Chapter 3. One potential recommendation could be to consider utilizing a vast library of orthonormal spatial modes, potentially even data-driven. To achieve a balance between precision and efficiency, an adaptive decision variable can be introduced that determines whether or not to include a strain mode in the recursive numerical solver of the dynamic model, thereby optimizing computational resources.

Soft sensing applied to control. An important area of control for robotics is sensing. While the main focus of this thesis centers around the modeling of soft actuation and mechanical structures, little emphasis is given on the topic of soft sensing. Although Chapter 5 and 6 discusses sensing solution based on body-markers, proprioceptive sensing is not explored. A possible recommendation can be to explore strain-sensitive materials that are directly embedded into the soft structures to recover the spatial modes of the soft robot. This aligns with a popular research topic in control of PDE systems: "*sensor placement*". In general, such problem is formulated as an observability problem. Observability can be considered as a measure of well-posedness for the estimation of system states using sensor information as well as additional system knowledge [133]. However, when considering soft robot models, which are often represented by high-dimensional discretized PDEs with many state variables, the traditional notion of observability is not directly applicable. For example, FEM models often have million DoFs, where certain state variables may exhibit strong observability, while others may display weak observability. Similar reasoning holds for high-order Cosserat beam models. Hence, one often refers to *partial observability* [58, 133] – the observability of a finite number of modes that are important, while neglecting less important states which are irrelevant to the control task.

The relationship between the system output and partial observability lies within the choice of sensors, their location and orientation, but also the respective dynamics of the sensor network. The concept of "*optimal sensor placement*" aims to minimize the sensor nodes of the network while strategically determining their optimal positions to enhance the quantitative measure of partial observability; a crucial consideration given the finite capacity for incorporating (soft) sensors within a soft robotic structure. Upon reviewing the prior literature, it is apparent that this particular area of research is relatively new and has yet to be extensively explored. Moreover, similar to the concept of soft actuation, there is a plethora of sensor technologies available for the implementation of soft sensing. The available alternatives encompass magnetic sensors [16, 80, 81], inertial sensors, color-altering (meta)-materials [235], or embedded stretchable liquid metal channels [208, 269].

Of particular interest is the latter, as the proposed soft beam modeling can be readily expanded to assess the deformation of an complex network of micro-channels. Yet, it is possible that a single alternative may be inadequate and therefore necessitate the use of multiple embedded sensing strategies with robust online sensor fusion for state estimation. Irrespective of the chosen soft sensor, it is crucial to model the input-output behavior, which may even exhibit some degree of memory (*e.g.*, creeping or plasticity).

I

Appendices

A

List of definitions

In this appendix, we present a compilation of the definitions and terminologies proposed in Chapter 1 and Chapter 6. It should be noted that these definitions may diverge from those commonly used in literature. Nevertheless, we consider them essential to address the multi-disciplinary perspective inherent in the scientific field of soft robotics.

Soft materials are a class of homogeneous materials with a Young's modulus (*i.e.*, the modulus of elasticity) typically lower than $E \leq 10^9$ Pa. Following, the word 'soft' or 'softness' refers to the collection of mechanical properties that are often associated with these low moduli materials.

Soft robotics is a subclass of robotics with purposefully designed compliant actuators embedded into their soft body whose goal is to enable the robot control over its ability to perform bio-inspired behavior.

Soft actuators are controllable flexible actuation units of the constitute soft robot that through external stimuli are responsible for natural motion within the system or a change in its compliance.

(Proprioceptive) soft sensors are flexible measurements units embedded into the soft robotic body that through external stimuli measure the (local) changes of the system. Softness here implies that the sensor minimally alters the global mechanical behavior of the robot.

Hyper-elasticity is a branch of continuum mechanics that deals with the behavior of materials that exhibit large elastic deformations. In hyper-elastic materials,

the stress-strain relationship is nonlinear and the material response depends on the deformation history. Hyper-elasticity is an important concept in the field of soft robotics, as many soft robots are made from hyper-elastic materials and their behavior must be accurately modeled for effective design and control.

Hyper-redundancy refers to a design principle in robotics where the number of Degrees of Freedom (DoF) in a robot is significantly greater than what is required for a given task. This redundancy allows the robot to perform the same task in multiple ways, providing increased flexibility and adaptability.

Under-actuation is a term used to describe a system whose Degrees of Freedom (DoF) cannot be matched (anywhere) by the number of inputs. In other words, there exist joint configurations, or whole sets of configurations, where the robot cannot realize all joint acceleration via the input alone. Although continuum-bodied motions enable increased flexibility and adaptability in the soft robot's movements, but also presents challenges in controlling the system since not all setpoint are globally reachable. Since only a finite number of actuators can be embedded in a continuum, but possess infinite DoF, soft robots are intrinsically underactuated systems

Under-sensed refers to the situation where the robot's sensors are not able to capture all the relevant information about its environment or its own state. This can lead to incomplete or inaccurate perception of the world, which in turn can affect the robot's ability to perform effectively. Undersensing can occur due to limitations in the sensing hardware, environmental factors such as occlusions or lighting conditions, or the complexity of the task itself. Similar to under-actuation, only a finite number of sensors can be embedded in a continuum, and thus soft robots are intrinsically undersensed.

B

Appendices to Chapter 3

B.1 Wachspress shape functions for polygons

The finite element method involves the reduction of an infinite-dimensional problem to a finite-dimensional one through the utilization of local spatial interpolation. This is achieved by assigning states to the exterior of the finite element and employing specialized basis functions to locally interpolate the continuum. These shape functions must be tailored towards the chosen elemental discretization, and thus researchers often rely on common element types, including triangular elements (*e.g.*, Tet3 or Tet6) and quadrilateral elements (*e.g.*, Quad8) [19, 75, 115, 146, 220]. In the present work, we investigate polygonal elements called PolyN, resulting in a finite element mesh composed of heterogeneous mesh elements.

To find a suitable shape function for these PolyN elements, we explore a technique called *barycentric coordinates* [83, 84]. Let $P_k \subset \mathbb{R}^2$ be a convex polygon viewed as an open set, which is spanned by a set of vertices $\{\mathbf{v}_i\}_{i=1}^k$ (anti-clockwise ordering) where k is the degree of the polygon. Then, any function $N_i : P_k \rightarrow \mathbb{R}$ is considered a barycentric coordinate if for all $\boldsymbol{\sigma} \in P_k$, it holds that

- It is strictly positive, *i.e.*, $N_i(\boldsymbol{\sigma}) > 0$,
- Its sum is equal to one, *i.e.*, $\sum_{i=1}^k N_i(\boldsymbol{\sigma}) = 1$,
- And $\sum_{i=1}^k N_i(\boldsymbol{\sigma}) \mathbf{v}_i \geq \boldsymbol{\sigma}$,

A common function that satisfies such conditions for any $k \geq 3$ is called the Wachspress shape function given as follows:

$$N_i^k(\boldsymbol{\sigma}) = \frac{w_i(\boldsymbol{\sigma})}{\sum_{j=1}^k w_j(\boldsymbol{\sigma})}, \quad (\text{B.1})$$

with w_i the shape interpolation weights given by

$$w_i(\boldsymbol{\sigma}) = \frac{A(\mathbf{v}_{i-1}, \mathbf{v}_i, \mathbf{v}_{i+1})}{A(\mathbf{v}_{i-1}, \mathbf{v}_i, \boldsymbol{\sigma}) A(\mathbf{v}_i, \mathbf{v}_{i+1}, \boldsymbol{\sigma})}, \quad (\text{B.2})$$

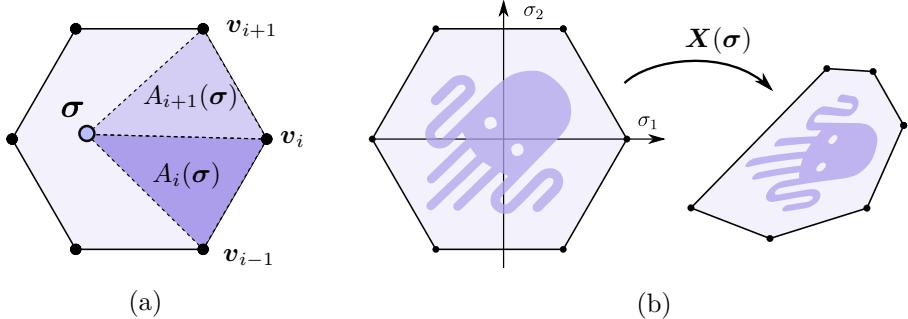


Figure B.1. (a) Illustration of the triangular areas $A_i(\sigma) := A(\mathbf{v}_{i-1}, \mathbf{v}_i, \sigma)$ used in the computation of (B.2). The figure is adopted from Talischi et al. [267, 268]. (b) Example of an isoparametric mapping from natural to global coordinates.

where A is the signed area spanned by its three arguments (see Figure B.1). By convention, we use $\mathbf{v}_{n_p+1} = \mathbf{v}_1$ in (B.2). From a numerical standpoint, the computation of this area can be achieved in an efficient manner by evaluating [268]:

$$A(\mathbf{v}_i, \mathbf{v}_{i+1}, \boldsymbol{\sigma}) = \frac{1}{2} \begin{vmatrix} \sigma_1 & \sigma_2 & 1 \\ v_{1,i-1} & v_{2,i-1} & 1 \\ v_{1,i} & v_{2,i} & 1 \end{vmatrix} \quad (\text{B.3})$$

Since we consider regular polygonal elements where $\mathbf{v}_i = (\cos(\frac{2\pi i}{k}), \sin(\frac{2\pi i}{k}))$, it follows that $A(\mathbf{v}_{i-1}, \mathbf{v}_i, \mathbf{v}_{i+1})$ is constant for all i in the summation for (B.1), and can therefore be factored out of the expression. By adopting the notation $A_i(\boldsymbol{\sigma}) := A(\mathbf{v}_{i-1}, \mathbf{v}_i, \boldsymbol{\sigma})$ and $\alpha_i = [A_i A_{i+1}]^{-1}$, we can simplify the expression for the Wachspress shape function in (B.1) further to

$$N_i^k = \frac{[A_i A_{i+1}]^{-1}}{\sum_{j=1}^k [A_j A_{j+1}]^{-1}} = \frac{\alpha_i}{\sum_{j=1}^k \alpha_i}, \quad (\text{B.4})$$

Remark B.1 Let it be clear that (B.4) is expressed in the natural coordinates $\boldsymbol{\sigma} \in P_k$ as opposed to $\mathbf{X} \in \mathcal{B}_0$. The idea of using reference interpolation functions N_i^k is due to convenience because it is unnecessary to build different shape functions for the elements with an identical topology. The only difference between elements is the mapping from global to natural coordinates. So, given such isoparametric elements, their coordinate transformation and displacement can be expressed by

$$\mathbf{X}(\boldsymbol{\sigma}) \approx \sum_{i=1}^k N_i^k(\boldsymbol{\sigma}) \mathbf{X}_i^e; \quad \mathbf{d}(\boldsymbol{\sigma}, T) \approx \sum_{i=1}^k N_i^k(\boldsymbol{\sigma}) \mathbf{x}_i^e$$

where $\mathbf{X}_i^e = (X_1^e, X_2^e)^\top$ and $\mathbf{x}_i^e = (x_1^e, x_2^e)^\top$ are the nodal coordinates and the nodal displacement vector related to the i -th node of the element \mathcal{V}_e , respectively. We provided an illustration of the isoparametric mapping using a polygonal element of degree $k = 5$ in Figure B.1.

Finally, the element-wise derivative of the Wachspress shape function with respect to the natural coordinates is given by [268]:

$$\frac{\partial N_i^k}{\partial \sigma_j} = \frac{1}{\sum_{q=1}^k \alpha_q} \left(\frac{\partial \alpha_i}{\partial \sigma_j} - N_i^k \sum_{q=1}^k \frac{\partial \alpha_q}{\partial \sigma_j} \right) \quad (\text{B.5})$$

Again, note that the (B.5) is given in terms of the natural coordinates $\boldsymbol{\sigma} = [\sigma_1, \sigma_2] \in P_k$. Yet, we are interested in the partial derivatives with respect to the global coordinates, for instance, the deformation gradient $\mathbf{F} = \mathbf{I} + \nabla_0 \mathbf{d}$, or the Piola stress tensor $\mathbf{S} = \frac{\partial \Psi}{\partial \boldsymbol{\varepsilon}}$. Let us introduce the Jacobian matrix of the isoparametric mapping as

$$\mathbf{J} = \frac{\partial \mathbf{X}}{\partial \boldsymbol{\sigma}} = \sum_{i=1}^k \mathbf{X}_i^e \left(\frac{\partial N_i^k}{\partial \sigma_1}, \frac{\partial N_i^k}{\partial \sigma_2} \right). \quad (\text{B.6})$$

Then, using (B.6), it can be shown that the spatial derivatives of shape functions are related by the Jacobian matrix as $\partial N / \partial \mathbf{X} = (\partial N / \partial \boldsymbol{\sigma}) \mathbf{J}^{-1}$ [146]. In this context, spatial derivatives can be calculated using an isoparametric reference element and then converted to the global coordinate frame. This approach allows for faster computation of the global system matrices as each element in the mesh follows the same numerical procedure and thus enables parallel computation.

B.2 Element formulation for the Lagrangian strain

When solving finite element numerically, it is often more convenient to utilize matrix-vector notation as opposed to tensor notation. This approach involves representing second-order symmetric tensors using vectors, while fourth-order symmetric tensors are represented using matrices. Given the two-dimensional formulation of the finite element problem described in Chapter 3, it is possible to define the Green-Lagrange strain tensor and second Piola stress strain tensor, which are both symmetric second-order tensors, as vector in \mathbb{R}^3 following the Voigt notation:

$$\boldsymbol{\varepsilon} = \begin{bmatrix} \varepsilon_{11} & \cdot & \cdot \\ \varepsilon_{12} & \varepsilon_{22} & \cdot \\ \varepsilon_{13} & \varepsilon_{23} & \varepsilon_{33} \end{bmatrix} \implies \text{voigt}_{2D}(\boldsymbol{\varepsilon}) = (E_{11}, E_{22}, 2E_{12})^\top, \quad (\text{B.7})$$

$$\mathbf{S} = \begin{bmatrix} S_{11} & \cdot & \cdot \\ S_{12} & S_{22} & \cdot \\ S_{13} & S_{23} & S_{33} \end{bmatrix} \implies \text{voigt}_{2D}(\mathbf{S}) = (S_{11}, S_{22}, S_{12})^\top, \quad (\text{B.8})$$

where the two-dimensional reduction follows from the plane strain conditions in which $\varepsilon_{i3} = \varepsilon_{3i} = 0$ for all $i = \{1, 2, 3\}$; and $S_{i3} = S_{3i} = 0$ for $i = \{1, 2\}$. For convenience, we will introduce the following $\underline{\boldsymbol{\varepsilon}} := \text{voigt}_{2D}(\boldsymbol{\varepsilon})$ and $\underline{\mathbf{S}} := \text{voigt}_{2D}(\mathbf{S})$.

Our goal now is to derive an expression for the (nonlinear) strain-displacement matrix $\mathbf{B}(\mathbf{d})$ which relates the displacement field and the variation of the Lagrangian strain as $\delta\boldsymbol{\varepsilon} = \mathbf{B}(\mathbf{d})\delta\mathbf{d}$. To do so, we explore the elemental interpolation using the Wachspress shape function that we derived previously in Appendix B.1. The derivation for the Piolla stress is dependent on the constitutive material models, thus we presented its derivation separately in Appendix B.14.

The following vector form of the displacement gradient is defined first

$$\text{voigt}_{2D}(\nabla_0 \mathbf{d}) = \left(\frac{\partial d_1}{\partial X_1}, \frac{\partial d_1}{\partial X_2}, \frac{\partial d_2}{\partial X_1}, \frac{\partial d_2}{\partial X_2} \right)^\top, \quad (\text{B.9})$$

$$\begin{aligned} \text{voigt}_{2D}(\mathbf{F}) &= (F_{11}, F_{12}, F_{21}, F_2)^\top \\ &= \left(1 + \frac{\partial d_1}{\partial X_1}, \frac{\partial d_1}{\partial X_2}, \frac{\partial d_2}{\partial X_1}, 1 + \frac{\partial d_2}{\partial X_2} \right)^\top. \end{aligned} \quad (\text{B.10})$$

Then, the symmetric second-order Lagrangian strain tensor defined as $\boldsymbol{\varepsilon} = \frac{1}{2}(\mathbf{F}^\top \mathbf{F} - \mathbf{I})$ expressed using the Voigt notation can be calculated by

$$\boldsymbol{\varepsilon} = \begin{pmatrix} \frac{\partial d_1}{\partial X_1} + \frac{1}{2} \left(\frac{\partial d_1}{\partial X_1} \frac{\partial d_1}{\partial X_1} + \frac{\partial d_2}{\partial X_1} \frac{\partial d_1}{\partial X_2} \right) \\ \frac{\partial d_2}{\partial X_2} + \frac{1}{2} \left(\frac{\partial d_1}{\partial X_2} \frac{\partial d_2}{\partial X_1} + \frac{\partial d_2}{\partial X_2} \frac{\partial d_2}{\partial X_2} \right) \\ \frac{\partial d_1}{\partial X_2} + \frac{\partial d_2}{\partial X_1} + \frac{\partial d_1}{\partial X_2} \frac{\partial d_1}{\partial X_1} + \frac{\partial d_2}{\partial X_1} \frac{\partial d_2}{\partial X_2} \end{pmatrix}. \quad (\text{B.11})$$

Since we can estimate the displacement derivatives through shape interpolation functions, *i.e.*, $\frac{\partial \mathbf{d}}{\partial X_i} \approx \sum_j^k \frac{\partial N_j^k}{\partial X_i} \mathbf{x}_j^k$, we can obtain an expression for the nonlinear displacement-strain matrix, which connects variational displacement with strain variations, given by $\delta\boldsymbol{\varepsilon} = \mathbf{B}\delta\mathbf{d}$. This nonlinear displacement-strain matrix is given by

$$\mathbf{B}_e = (\mathbf{B}_1, \mathbf{B}_2, \mathbf{B}_3, \dots, \mathbf{B}_k), \quad (\text{B.12})$$

with

$$\mathbf{B}_i = \begin{pmatrix} F_{11} \frac{\partial N_i}{\partial X_1}, & F_{12} \frac{\partial N_i}{\partial X_2}, & F_{11} \frac{\partial N_i}{\partial X_2} + F_{12} \frac{\partial N_i}{\partial X_1} \\ F_{21} \frac{\partial N_i}{\partial X_1}, & F_{22} \frac{\partial N_i}{\partial X_2}, & F_{21} \frac{\partial N_i}{\partial X_2} + F_{22} \frac{\partial N_i}{\partial X_1} \end{pmatrix}^\top, \quad (\text{B.13})$$

where again k denotes the polygonal degree of the element. Then, (B.4), (B.10) and (B.12) combined, allow for the numerical computation of the residual force vector of the discretized PDE system given in (3.9). The derivation of the second Piolla stress tensor, denoted as $\boldsymbol{\sigma}$, is presented in the subsequent section.

B.3 Piolla stress tensor and stress-strain tangent for the nearly incompressible Yeoh model

In the following section, we will derive the second Piolla stress tensor and the stress-strain tangent tensor which are derived from the constitutive material model Ψ . Previously, we have introduce the nearly incompressible Yeoh model expressed as

$$\Psi(J_1, J) = \sum_{i=1}^3 c_i (J_1 - 3)^i + \sum_{j=1}^3 \frac{1}{d_j} (J - 1)^{2j}, \quad (\text{B.14})$$

where $J_1 = J^{-\frac{2}{3}} I_1$ with $I_1 = \text{trace}(\mathcal{E})$ the first true strain invariant and $J = \det(\mathbf{F})$ the volumetric change, and c_i and d_i material parameters. To express the second Piolla-Kirchhoff stress tensor, denoted by \mathcal{S} , and the fourth-order tangent stiffness tensors, \mathbb{D} , it is necessary to obtain the partial derivatives of J and J_1 with respect to the Green-Lagrangian strain tensor \mathcal{E} . These derivatives are provided in the works [146, 220] as follows:

$$\frac{\partial J}{\partial \mathcal{E}} = J \mathcal{C}^{-1}, \quad \frac{\partial J_1}{\partial \mathcal{E}} = \mathbf{I} - \frac{1}{3} \mathcal{C}^{-1}. \quad (\text{B.15})$$

Taking the derivative of the constitutive material model Ψ with respect to \mathcal{E} , and substitution of the strain invariant derivatives into (B.14) leads to

$$\mathcal{S} = 2\beta_1 J^{-\frac{2}{3}} \left[\mathbf{I} - \frac{I_1}{3} \mathcal{C}^{-1} \right] + \beta_2 J \mathcal{C}^{-1}, \quad (\text{B.16})$$

where $\beta_1 = \sum_{i=1}^3 i c_i (J_1 - 3)^{i-1}$ and $\beta_2 = \sum_{j=1}^3 \frac{2j}{d_j} (J - 1)^{2j-1}$ are scalar functions of the strain variants. In order to solve nonlinear structures using the finite element method, it is necessary to calculate the stress-strain tangent operator \mathbb{D} in order to construct the tangent stiffness matrix \mathbf{K}_T . First, let us introduce the following tensor operation between two second-order tensors \mathcal{A} and \mathcal{B} as:

$$(\mathcal{A} \otimes \mathcal{B})_{ijkl} = A_{ij} B_{kl}, \quad (\mathcal{A} \overline{\otimes} \mathcal{B})_{ijkl} = \frac{1}{2} (A_{ik} B_{jl} + A_{il} B_{jk}) \quad (\text{B.17})$$

for indices $i, j, k, l \in \{1, 2, 3\}$. Then, the derivative of the second Piolla stress tensor in (B.16) with respect to the Lagrangian strain \mathcal{E} is gives the stress-strain tangent tensor \mathbb{D} which is a fourth-order tensor calculated as follows [220]:

$$\begin{aligned} \mathbb{D} = & 4J^{-\frac{4}{3}} \gamma_1 \left[\mathbf{I} - \frac{I_1}{3} \mathcal{C}^{-1} \right] \otimes \left[\mathbf{I} - \frac{I_1}{3} \mathcal{C}^{-1} \right] \\ & - \frac{4}{3} J^{-\frac{2}{3}} \beta_1 \left[\mathcal{C}^{-1} \otimes \mathbf{I} + \mathbf{I} \otimes \mathcal{C}^{-1} + \frac{I_3}{3} \mathcal{C}^{-1} \otimes \mathcal{C}^{-1} - I_1 \mathcal{C}^{-1} \overline{\otimes} \mathcal{C}^{-1} \right] \\ & + \gamma_2 J^2 \mathcal{C}^{-1} \otimes \mathcal{C}^{-1} + \beta_2 J [\mathcal{C}^{-1} \otimes \mathcal{C}^{-1} - 2\mathcal{C}^{-1} \overline{\otimes} \mathcal{C}^{-1}], \end{aligned} \quad (\text{B.18})$$

where $\gamma_1 = \sum_{i=2}^3 i(i-1)c_i(J_1-3)^{i-2}$ and $\gamma_2 = \sum_{j=1}^3 \frac{2j(2j-1)}{d_j} (J-1)^{2j-2}$ are scalar functions. It is important to note that the stress-strain tangent tensor has major and minor symmetries, *i.e.*, $\mathbb{D}_{ijkl} = \mathbb{D}_{klji}$ and $\mathbb{D}_{jijl} = \mathbb{D}_{jilk}$ [115, 146]. Hence, by utilizing the Voigt notation, these symmetries can be leveraged to compactly represent the fourth-order stress-strain tangent tensor as an equivalent matrix of size 6 by 6 as follows:

$$\mathbf{D} = \begin{pmatrix} \mathbb{D}_{1111} & \mathbb{D}_{1122} & \mathbb{D}_{1133} & \mathbb{D}_{1123} & \mathbb{D}_{1113} & \mathbb{D}_{1112} \\ \cdot & \mathbb{D}_{2222} & \mathbb{D}_{2233} & \mathbb{D}_{2223} & \mathbb{D}_{2213} & \mathbb{D}_{2212} \\ \cdot & \cdot & \mathbb{D}_{3333} & \mathbb{D}_{3323} & \mathbb{D}_{3313} & \mathbb{D}_{3312} \\ \cdot & \cdot & \cdot & \mathbb{D}_{2323} & \mathbb{D}_{2313} & \mathbb{D}_{2312} \\ \cdot & \cdot & \cdot & \cdot & \mathbb{D}_{1313} & \mathbb{D}_{1312} \\ \cdot & \cdot & \cdot & \cdot & \cdot & \mathbb{D}_{1212} \end{pmatrix}. \quad (\text{B.19})$$

Furthermore, considering the plane strain conditions and utilizing the Voigt notation for two-dimensional problems (refer to Section B.2), we obtain that

$$\underline{\mathbf{D}} := \text{voigt}_{2\text{D}}(\mathbf{D}_0) = \begin{pmatrix} \mathbb{D}_{1111} & \mathbb{D}_{1122} & 0 \\ \mathbb{D}_{2211} & \mathbb{D}_{2222} & 0 \\ 0 & 0 & \mathbb{D}_{1212} \end{pmatrix}, \quad (\text{B.20})$$

where we use that $\mathbb{D}_{ij12} = 0$ for all $i, j \in \{1, 2, 3\}$ except $i = 1$ and $j = 2$. Applying a reduced formulation, we obtain the tangent stiffness matrix by evaluating the Jacobian of the conservative elastic forces with respect to the state displacements \mathbf{x} . The expression for this matrix is as follows:

$$\begin{aligned} \mathbf{K}_T &:= \frac{\partial}{\partial \mathbf{x}} \left[\sum_{e=1}^n \int_{\mathcal{V}_e} \mathbf{B}_e^\top \underline{\mathcal{S}}_e \, dV \right] = \sum_{e=1}^n \int_{\mathcal{V}_e} \frac{\partial \mathbf{B}_e^\top}{\partial \mathbf{x}} \underline{\mathcal{S}}_e + \mathbf{B}_e^\top \frac{\partial \underline{\mathcal{S}}_e}{\partial \boldsymbol{\epsilon}} \frac{\partial \boldsymbol{\epsilon}}{\partial \mathbf{x}} \, dV \\ &= \sum_{e=1}^n \int_{\mathcal{V}_e} \frac{\partial \mathbf{B}_e^\top}{\partial \mathbf{x}} \underline{\mathcal{S}}_e + \mathbf{B}_e^\top \underline{\mathbf{D}} \mathbf{B}_e \, dV. \end{aligned} \quad (\text{B.21})$$

We should mention that the numerical computation of the tangent stiffness matrix is considerable, and often the numerical bottleneck for fast FEM simulation. It is thus often wise to optimize the computation above, for instance, using GPU parallel computation. Alternatively, there exist methods that circumvent extensive computations. The BFGS method is an iterative method that aims to find the minimum (or maximum) of a nonlinear objective function [115]; or the secant-stiffness method [146]. Both approximate the inverse Hessian matrix of the objective function by updating it at each iteration, saving computational cost considerably.

C

Appendices to Chapter 4

C.1 Adjoint actions on SE(3) and se(3)

Given the position vector $\gamma \in \mathbb{R}^3$ and the homogeneous rotation matrix $\Phi \in \text{SO}(3)$, the adjoint action of the homogeneous transformation $\mathbf{g} = (\gamma, \Phi) \in \text{SE}(3)$ is then defined as

$$\mathbf{Ad}_{\mathbf{g}(\sigma, \mathbf{q})} := \begin{pmatrix} \Phi(\sigma, \mathbf{q}) & \mathbf{0}_{3 \times 3} \\ \gamma^\times(\sigma, \mathbf{q}) \Phi(\mathbf{q}, \sigma) & \Phi(\sigma, \mathbf{q}) \end{pmatrix}. \quad (\text{C.1})$$

Note that the operator $(\cdot)^\times$ denotes the isomorphism from $\mathbb{R}^3 \rightarrow \text{SO}(3)$ see Murray et al. [197]. In continuation, given the velocity twist $\boldsymbol{\eta}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) = (\boldsymbol{\omega}^\top, \mathbf{v}^\top)^\top \in \mathbb{R}^6 \cong \text{se}(3)$, being the aggregate of $\boldsymbol{\omega}$ and \mathbf{v} , the angular and linear velocities, respectively. Then, the adjoint action on the algebra $\text{se}(3)$ is defined as

$$\mathbf{ad}_{\boldsymbol{\eta}(\sigma, \mathbf{q}, \dot{\mathbf{q}})} := \begin{pmatrix} \mathbf{v}^\times(\sigma, \mathbf{q}, \dot{\mathbf{q}}) & \mathbf{0}_{3 \times 3} \\ \boldsymbol{\omega}^\times(\sigma, \mathbf{q}, \dot{\mathbf{q}}) & \mathbf{v}^\times(\sigma, \mathbf{q}, \dot{\mathbf{q}}) \end{pmatrix}. \quad (\text{C.2})$$

These adjoint representation on the group $\text{SE}(3)$ and its algebra $\text{se}(3)$ are analogous to the conventional notations in modern robotics mathematics, such as the work of Murray et al. [197].

C.2 Passivity properties of the inertia matrix

To show $\dot{\mathbf{M}} - 2\mathbf{C}$ is skew-symmetric in the chosen coordinates, we start by computing the time-derivative of the inertia matrix. For sake of clarity, lets abbreviate $\mathbf{J}(\sigma, \mathbf{q}) = \mathbf{J}$ and $\dot{\mathbf{J}}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) = \dot{\mathbf{J}}$. Through chain differentiation of the inertia matrix, we find

$$\dot{\mathbf{M}} = \int_{\mathbb{X}} \dot{\mathbf{J}}^\top \mathcal{M} \mathbf{J} + \mathbf{J}^\top \mathcal{M} \dot{\mathbf{J}} \, d\sigma, \quad (\text{C.3})$$

Then, calculating $\dot{M} - 2C$ leads to

$$\dot{M} - 2C = \int_{\mathbb{X}} \dot{\mathbf{J}}^\top \mathbf{M} \mathbf{J} - \mathbf{J}^\top \mathbf{M} \dot{\mathbf{J}} - 2\mathbf{J}^\top \mathbf{C}_\eta \mathbf{J} d\sigma. \quad (\text{C.4})$$

Since $\mathbf{J}^\top \mathbf{C} \mathbf{J}$ is skew-symmetric, the remainder of the proof consists of showing that the matrix $S = \dot{\mathbf{J}}^\top \mathbf{M} \mathbf{J} - \mathbf{J}^\top \mathbf{M} \dot{\mathbf{J}}$ also satisfies skew-symmetry. Since $\mathbf{M} = \mathbf{M}^\top$, we can easily show this holds true:

$$\begin{aligned} S &= \dot{\mathbf{J}}^\top \mathbf{M}^\top \mathbf{J} - \mathbf{J}^\top \mathbf{M}^\top \dot{\mathbf{J}}, \\ &= -\left(\dot{\mathbf{J}}^\top \mathbf{M}^\top \mathbf{J} - \mathbf{J}^\top \mathbf{M} \dot{\mathbf{J}}\right)^\top = -S^\top. \end{aligned} \quad (\text{C.5})$$

Therefore, the matrix $\dot{M} - 2C$ is skew-symmetric.

C.3 Implicit trapezoidal time integration

Here, we detail an numerical approach to efficiently find the solutions to the approximated dynamic model $\mathbf{M}(\mathbf{q})\ddot{\mathbf{q}} + \mathbf{C}(\mathbf{q}, \dot{\mathbf{q}})\dot{\mathbf{q}} + \mathbf{f}_e(\mathbf{q}, \dot{\mathbf{q}}) + \mathbf{f}_g(\mathbf{q}) = \boldsymbol{\tau}$. We emphasize that the control input $\boldsymbol{\tau}(\cdot, t)$ could be state-dependent if closed-loop controllers are considered; for instance, the proposed passivity-based controller in (4.54). First, consider a new state vector defined as $\mathbf{z} := (\mathbf{q}^\top, \dot{\mathbf{q}}^\top)^\top$ such that we can rewrite the Lagrangian model in state-space form:

$$\dot{\mathbf{z}} = \mathbf{f}(\mathbf{z}, t), \quad (\text{C.6})$$

where $\mathbf{f}(\cdot, \cdot)$ is a nonlinear vector-valued function given by

$$\mathbf{f}(\mathbf{z}, t) = \begin{pmatrix} \dot{\mathbf{q}} \\ \mathbf{M}^{-1}[\boldsymbol{\tau} - \mathbf{C}\dot{\mathbf{q}} - \mathbf{f}_e - \mathbf{f}_g] \end{pmatrix}. \quad (\text{C.7})$$

The objective here is to compute the solutions to the system above over the finite horizon $\mathbb{T} = [0, T]$ efficiently such that real-time control applications are possible. To do so, we consider an implicit trapezoidal scheme which is given by

$$\mathbf{z}_{i+1} = \mathbf{z}_i + \frac{\Delta t}{2} (\mathbf{f}(\mathbf{z}_i, t_i) + \mathbf{f}(\mathbf{z}_{i+1}, t_{i+1}),) \quad (\text{C.8})$$

where \mathbf{z}_i is the state solution at time instance t_i , and $\Delta t = t_{i+1} - t_i$ the timestep. The advantage of implicit schemes over explicit ones is the improved numerical stability for coarser temporal discretization at the mere cost of numerical precision. Let us be clear that evaluating nonlinear vector function $\mathbf{f}(\cdot, \cdot)$ is numerically expensive, as it requires the computation of \mathbf{M} , \mathbf{C} and \mathbf{f}_g . Therefore, it is advantageous to minimize its calls by using coarser timesteps while retaining stability using an implicit scheme. By fixing \mathbf{z}_i and aiming to seek the intermediate state

solutions $\mathbf{w} := \mathbf{z}_{i+1}$, we can define the residual dynamics on the time interval $[t_i, t_{i+1}]$ as

$$\mathbf{e}(\mathbf{w}) := \mathbf{w} - \mathbf{z}_i - \frac{\Delta t}{2} (\mathbf{f}_i + \mathbf{f}_{i+1}(\mathbf{w})). \quad (\text{C.9})$$

By aiming to find the root of the residual dynamics $\mathbf{e}(\mathbf{w}) = 0$ and choosing $\mathbf{w}_0 = \mathbf{z}_i$ as initial guess, we can employ an iterative Newton-Raphson procedure:

$$\mathbf{w}_{j+1} = \mathbf{z}_i - \alpha^+ [\nabla_{\mathbf{w}} \mathbf{e}(\mathbf{w}_j)]^{-1} \mathbf{e}(\mathbf{w}_j), \quad (\text{C.10})$$

where j is the iteration index for finding the intermediate state solution $\mathbf{w} = \mathbf{z}_{i+1}$, and $0 < \alpha^+ \leq 1$ a constant for controlling the update step. Once the residual dynamics converges on the sub-interval, i.e., $\|\mathbf{e}(\mathbf{w})\|_2 \ll 1$, we repeat the procedure above until the solutions to $\mathbf{z}(t)$ are recovered for the finite time horizon \mathbb{T} . Now the key here is that a rough approximation of the hessian $\mathbf{H}(\mathbf{w}) = \nabla_{\mathbf{w}} \mathbf{e}$ can suffice for numerical convergence. This implies we do not need a close approximation of hessian – which can significantly speed-up simulation speed. This process, however, might require more iterations for the solutions to converge, but it outweighs computing the Hessian directly. Therefore, let us consider the first Taylor approximation of the Hessian:

$$\begin{aligned} \mathbf{H}(\mathbf{w}) &\simeq \widetilde{\mathbf{H}}(\mathbf{w}), \\ &:= \mathbf{I}_{2n} - \frac{\Delta t}{2} \begin{pmatrix} 0 & \mathbf{I}_n, \\ -\mathbf{M}^{-1} \widetilde{\mathbf{K}} & -\mathbf{M}^{-1} \widetilde{\mathbf{D}} \end{pmatrix}, \end{aligned} \quad (\text{C.11})$$

where the matrices $\widetilde{\mathbf{K}} = \nabla_{\mathbf{q}} \mathbf{f}_e + \nabla_{\mathbf{q}} \mathbf{f}_g + \nabla_{\mathbf{q}} \boldsymbol{\tau}$ and $\widetilde{\mathbf{D}} = \mathbf{C} + \nabla_{\dot{\mathbf{q}}} \mathbf{f}_e + \nabla_{\dot{\mathbf{q}}} \boldsymbol{\tau}$ are a-priori approximations of the Hessians w.r.t. \mathbf{q} and $\dot{\mathbf{q}}$, respectively. Note that the Jacobians $\nabla_{\mathbf{q}} \boldsymbol{\tau}$ and $\nabla_{\dot{\mathbf{q}}} \boldsymbol{\tau}$ can be nonzero, especially in a closed-loop control setting. To approximate these partial derivatives of the control input, we employ a finite-difference scheme. Again, the Hessian does not need to be exact, as such an a-priori computation of the controller Jacobians can be performed before the start of the implicit solver.

D

Appendices to Chapter 5

D.1 Preliminaries on Lie group theory

Here we briefly discuss some notation and basic operations on the Lie groups $\text{SO}(3)$ and $\text{SE}(3)$, and their respective Lie algebras $\text{so}(3)$ and $\text{se}(3)$. This appendix serves a compact comprehensive introduction in the context of robotics, and the appendix is based on the comprehensive work of Bullo and Murray [35].

D.1.1 Basic definition(s)

Here, we focus first on the (Lie) group of rigid-body transformations about the origin of \mathbb{R}^3 denoted by $\text{SE}(3)$. Let $G = \text{SE}(3)$ be a matrix Lie group and its respective algebra $\mathfrak{g} = \text{se}(3)$, also known as the Lie algebra. Then, the evolution of a general rigid body under motion with pose $\mathbf{g} \in G$ can be described using

$$\dot{\mathbf{g}} = \mathbf{g} \hat{\boldsymbol{\eta}}^b \iff \dot{\mathbf{g}} = \hat{\boldsymbol{\eta}}^s \mathbf{g}. \quad \hat{\boldsymbol{\eta}}^b, \hat{\boldsymbol{\eta}}^s \in \mathfrak{g} \quad (\text{D.1})$$

where the velocity twist relative its body frame is given by $\hat{\boldsymbol{\eta}}^b$ or to a spatial frame by $\hat{\boldsymbol{\eta}}^s$. Since $\dot{\mathbf{g}} = \mathbf{g} \hat{\boldsymbol{\eta}}^b$ is invariant under left multiplication by constant matrices, we call it *left invariant*; and correspondingly $\dot{\mathbf{g}} = \hat{\boldsymbol{\eta}}^s \mathbf{g}$ is said to be *right invariant*. Let it be clear that the geometric strain $\boldsymbol{\xi}(\sigma, t)$ and velocity twist $\boldsymbol{\eta}(\sigma, t)$ in (5.2) and (5.3) are thus expressed in the body frame. Next, let us discuss the adjoint actions. For all $\mathbf{g} \in G$ and any $\mathbf{X}, \mathbf{Y} \in \mathfrak{g}$, the adjoint action $\mathbf{Ad}_{\mathbf{g}}$ and the matrix commutator or adjoint action on the algebra $\mathbf{ad}_{\mathbf{X}}$ are defined as

$$\mathbf{Ad}_{\mathbf{g}} \mathbf{X} = \mathbf{g} \mathbf{X} \mathbf{g}^{-1} \quad (\text{D.2})$$

$$\mathbf{ad}_{\mathbf{X}} \mathbf{Y} = [\mathbf{X}, \mathbf{Y}] = \mathbf{X} \mathbf{Y} - \mathbf{Y} \mathbf{X}. \quad (\text{D.3})$$

Now, on $\text{SE}(3)$ and $\text{se}(3)$ we represent a matrix group element $\mathbf{g} = (\Phi, \gamma) \in \text{SO}(3) \times \mathbb{R}^3 \cong \text{SE}(3)$ and a (velocity) twist vector field $\hat{\boldsymbol{\eta}} = (\boldsymbol{\Omega}, \mathbf{V}) \in \text{se}(3)$ using

homogenous coordinates,

$$\mathbf{g} := \begin{pmatrix} \Phi & \gamma \\ \mathbf{0}_3^\top & 1 \end{pmatrix}; \quad \hat{\boldsymbol{\eta}} := \begin{pmatrix} \boldsymbol{\Omega}^\times & \mathbf{V} \\ \mathbf{0}_3^\top & 1 \end{pmatrix}. \quad (\text{D.4})$$

where the operator $(\cdot)^\times : \mathbb{R}^3 \rightarrow \text{so}(3)$ is defined such that $\mathbf{x}^\times \mathbf{y} = \mathbf{x} \times \mathbf{y}$ for all $\mathbf{x}, \mathbf{y} \in \mathbb{R}^3$, and $(\cdot)^\wedge : \mathbb{R}^6 \rightarrow \text{se}(3)$. Now, representing the geometric twist as a column vector $\boldsymbol{\eta}^\wedge \rightarrow \boldsymbol{\eta}$, it straightforwardly follows from (D.2) and (D.3) that the adjoint actions can be written in the form:

$$\text{Ad}_{\mathbf{g}} := \begin{pmatrix} \Phi & \mathbf{0}_{3 \times 3} \\ \gamma^\times \Phi & \Phi \end{pmatrix}; \quad \text{ad}_{\boldsymbol{\eta}} := \begin{pmatrix} \mathbf{V}^\times & \mathbf{0}_{3 \times 3} \\ \boldsymbol{\Omega}^\times & \mathbf{V}^\times \end{pmatrix}. \quad (\text{D.5})$$

The notation above are analogous to the notations used in Chapter 4.

D.1.2 Exponential and logarithmic map

An important operation in Lie group theory, is the exponential and logarithmic maps that serve as transformations between the groups and their respective algebras. Lets start with the exponential map. Given $\boldsymbol{\Omega}^\times \in \text{so}(3)$ and $\boldsymbol{\eta} = (\boldsymbol{\Omega}, \mathbf{V}) \in \text{se}(3)$, the exponential maps for the orientation group $\exp_{\text{SO}(3)} : \text{so}(3) \rightarrow \text{SO}(3)$ and the rigid-body transformation group $\exp_{\text{SE}(3)} : \text{se}(3) \rightarrow \text{SE}(3)$ are given respectively by

$$\exp_{\text{SO}(3)}(\boldsymbol{\Omega}) = \mathbf{I} + \sin\|\boldsymbol{\Omega}\| \frac{\boldsymbol{\Omega}^\times}{\|\boldsymbol{\Omega}\|} + (1 - \cos\|\boldsymbol{\Omega}\|) \frac{\boldsymbol{\Omega}^\times \boldsymbol{\Omega}^\times}{\|\boldsymbol{\Omega}\|^2}; \quad (\text{D.6})$$

$$\exp_{\text{SE}(3)}(\boldsymbol{\xi}) = \begin{pmatrix} \exp_{\text{SO}(3)}(\boldsymbol{\Omega}) & A(\boldsymbol{\Omega})\mathbf{V} \\ \mathbf{0}_3^\top & 1 \end{pmatrix}, \quad (\text{D.7})$$

where $\|\cdot\|$ stands for the Euclidean norm and the operator $A(\boldsymbol{\Omega})$ is given By

$$A(\boldsymbol{\Omega}) = \mathbf{I} + \left(\frac{1 - \|\boldsymbol{\Omega}\|}{\|\boldsymbol{\Omega}\|} \right) \frac{\boldsymbol{\Omega}^\times}{\|\boldsymbol{\Omega}\|} + (1 - \sin\|\boldsymbol{\Omega}\|) \frac{\boldsymbol{\Omega}^\times \boldsymbol{\Omega}^\times}{\|\boldsymbol{\Omega}\|^2}. \quad (\text{D.8})$$

Note that we have seen equation (D.6) earlier which is known as the Rogdrigues' formula. Referring to [35], in an open neighborhood of the origin in G , we define $\boldsymbol{\eta} = \log(\mathbf{g}) \in \mathfrak{g}$ to be the "*exponential coordinates*" of the group element \mathbf{g} . Then, the logarithmic map can be regarded as the local chart of the manifold G . As such, let $\mathbf{g} = (\Phi, \gamma) \in \text{SO}(3) \times \mathbb{R}^3$ be such that $\text{trace}(\Phi) \neq -1$. Then, the logarithmic map $\log_{\text{SO}3} : \text{SO}(3) \rightarrow \text{so}(3)$ is given by

$$\log_{\text{SO}(3)}(\Phi) = \frac{\theta}{2 \sin \theta} (\Phi - \Phi^\top), \quad (\text{D.9})$$

where the angle θ satisfies $\cos \theta = \frac{1}{2}(\text{trace}(\boldsymbol{\Phi}) - 1)$ and is bounded by $|\theta| < \pi$. Following (D.9), and logarithmic map $\log_{SE3} : SE(3) \rightarrow se(3)$ is then given by

$$\log_{SE(3)}(\mathbf{g}) = \begin{pmatrix} \boldsymbol{\Omega}^\times & A^{-1}(\boldsymbol{\Omega})\boldsymbol{\gamma} \\ \mathbf{0}_3^\top & 1 \end{pmatrix}, \quad (\text{D.10})$$

where $\boldsymbol{\Omega}^\times = \log_{SO(3)}(\boldsymbol{\Phi})$ and the mapping $A^{-1}(\boldsymbol{\Omega})$ is given By

$$A^{-1}(\boldsymbol{\Omega}) = \mathbf{I} - \frac{1}{2}\boldsymbol{\Omega}^\times + \left[1 - \frac{\|\boldsymbol{\Omega}\|}{2}\cot\left(\frac{\|\boldsymbol{\Omega}\|}{2}\right)\right] \frac{\boldsymbol{\Omega}^\times\boldsymbol{\Omega}^\times}{\|\boldsymbol{\Omega}\|^2}, \quad (\text{D.11})$$

where $\cot : \mathbb{R} \rightarrow \mathbb{R}$ is the co-tangent function.

D.2 Time-differentiation of the geometric Jacobian for continuum deformable robots

The mapping from generalized coordinates $\dot{\mathbf{q}} \in \mathbb{R}^n$ to the velocity-twist vector $\dot{\boldsymbol{\eta}} = \mathbf{g}^{-1}\dot{\mathbf{q}} \in \mathbb{R}^3 \cong \mathbb{R}^6$ for a point σ is given by $\boldsymbol{\eta} = \mathbf{J}\dot{\mathbf{q}}$, where \mathbf{J} is the geometric Jacobian. The k -th order truncation of the exact geometric Jacobian is given by:

$$[\mathbf{J}]_k = \text{Ad}_{[\mathbf{g}]_k}^{-1} \int_0^\sigma \text{Ad}_{[\mathbf{g}]_k} \boldsymbol{\Theta} ds. \quad (\text{D.12})$$

Unlike rigid robotics, note that the geometric Jacobian matrix here is time and space-variant. Following the chain rule, the partial time-derivative of the geometric Jacobian matrix yields

$$[\dot{\mathbf{J}}]_k = \left(\dot{\text{Ad}}_{[\mathbf{g}]_k}^{-1} \right) \int_0^\sigma \text{Ad}_{[\mathbf{g}]_k} \boldsymbol{\Theta} ds + \text{Ad}_{[\mathbf{g}]_k}^{-1} \int_0^\sigma (\dot{\text{Ad}}_{[\mathbf{g}]_k}) \boldsymbol{\Theta} ds. \quad (\text{D.13})$$

Given the differential relations of the adjoint action mapping on the Lie group, that is, $d/ds(\text{Ad}_{\mathbf{g}}) = \text{Ad}_{\mathbf{g}} \text{ad}_{\boldsymbol{\Upsilon}}$ given a twist $\boldsymbol{\Upsilon} = (\mathbf{g}^{-1}d\mathbf{g}/ds)^\vee$, we can express the time-derivative of the adjoint action and its inverse as

$$\frac{\partial}{\partial t} (\text{Ad}_{\mathbf{g}}) = \text{Ad}_{\mathbf{g}} \text{ad}_{\boldsymbol{\eta}}, \quad (\text{D.14})$$

$$\frac{\partial}{\partial t} (\text{Ad}_{\mathbf{g}^{-1}}) = -\text{ad}_{\boldsymbol{\eta}} \text{Ad}_{\mathbf{g}^{-1}}. \quad (\text{D.15})$$

Substituting the truncated variations of (D.14) and (D.15) into (D.13), we find the complete expression of the time-derivative of the geometric Jacobian matrix

$$[\dot{\mathbf{J}}]_k = -\text{ad}_{[\boldsymbol{\eta}]_k} [\mathbf{J}]_k + \text{Ad}_{[\mathbf{g}]_k}^{-1} \int_0^\sigma \text{Ad}_{[\mathbf{g}]_k} \text{ad}_{[\boldsymbol{\eta}]_k} \boldsymbol{\Theta} ds. \quad (\text{D.16})$$

Since $\text{ad}_{\boldsymbol{\eta}}(\mathbf{J}\dot{\mathbf{q}}) = \text{ad}_{\boldsymbol{\eta}}\boldsymbol{\eta} = \mathbf{0}_6$ by definition, the first right-hand term vanishes if (D.16) is post-multiplied with the generalized velocities $\dot{\mathbf{q}}$, thus leading to the acceleration twist $[\ddot{\boldsymbol{\eta}}]_k$ in (5.19).

D.3 Derivation of the generalized linear stiffness and damping matrix for continuum robots

In this section, we will derive the expression for the generalized stiffness matrix \mathbf{K} and the generalized stiffness matrix \mathbf{D} as given in (5.30) and (5.31), respectively. Their formulation follow directly from the derivation of the generalized conservative material forces, computed by spatial integration of the internal material wrenches \mathcal{F}_{mat} as in (5.26). Recall that the expression is given by

$$\mathbf{f}_{\text{mat}}(\mathbf{q}, \dot{\mathbf{q}}) = \int_{\mathbb{X}} [\mathbf{J}(\sigma, \mathbf{q})]_k^{\top} \mathcal{F}_{\text{mat}}(\sigma, \mathbf{q}, \dot{\mathbf{q}}) d\sigma. \quad (\text{D.17})$$

The generalized material forces described in the aforementioned expression can be represented by a linear model $\mathbf{f}_{\text{mat}}(\mathbf{q}, \dot{\mathbf{q}}) = \mathbf{K}\mathbf{q} + \mathbf{D}\dot{\mathbf{q}}$ when a Hookean material model is assumed. We will demonstrate that this statement hold true through the following derivation.

Drawing from the existing work on geometric Cosserat models [29, 102, 222], the material wrench can be expressed as $\mathcal{F}_{\text{mat}} = \partial \mathcal{S} / \partial \sigma - \text{ad}_{\xi}^{\top} \mathcal{S}$, where \mathcal{S} represents the internal stress wrench resulting from deformation of the continuum body. Before substitution of the internal stress into \mathcal{F}_{mat} , it is necessary to first establish the spatial derivative of the inverse adjoint action, akin to (D.15). This derivative can be expressed as follows:

$$\frac{\partial}{\partial \sigma} (\text{Ad}_{g^{-1}}) = -\text{ad}_{\xi} \text{Ad}_{g^{-1}}. \quad (\text{D.18})$$

Given that $\text{Ad}_{g^{-1}}^{-\top} \equiv \text{Ad}_g^{\top}$, we can rewrite the expression in (D.18) and obtain a new expression for the adjoint action $-\text{ad}_{\xi}^{\top} = \text{Ad}_g^{\top} \frac{\partial}{\partial \sigma} (\text{Ad}_{g^{-1}}^{-\top})$. By utilizing this expression, it is possible to simplify the expression $\partial \mathcal{S} / \partial \sigma - \text{ad}_{\xi}^{\top} \mathcal{S}$ via the chain rule as follows:

$$\begin{aligned} \mathcal{S}' - \text{ad}_{\xi}^{\top} \mathcal{S} &= \frac{\partial \mathcal{S}}{\partial \sigma} + \text{Ad}_{[g]_k}^{\top} \frac{\partial}{\partial \sigma} (\text{Ad}_{[g]_k}^{-\top}) \mathcal{S}, \\ &= \underbrace{\text{Ad}_{[g]_k}^{\top} \text{Ad}_{[g]_k}^{-\top} \frac{\partial \mathcal{S}}{\partial \sigma}}_{I_6} + \text{Ad}_{[g]_k}^{\top} \frac{\partial}{\partial \sigma} (\text{Ad}_{[g]_k}^{-\top}) \mathcal{S}, \\ &= \text{Ad}_{[g]_k}^{\top} \left(\text{Ad}_{[g]_k}^{-\top} \frac{\partial \mathcal{S}}{\partial \sigma} + \frac{\partial}{\partial \sigma} (\text{Ad}_{[g]_k}^{-\top}) \mathcal{S} \right), \\ &= \text{Ad}_{[g]_k}^{\top} \frac{\partial}{\partial \sigma} (\text{Ad}_{[g]_k}^{-\top} \mathcal{S}). \end{aligned} \quad (\text{D.19})$$

Substitution of (D.19) and the geometric Jacobian (5.18) into (D.17), we find

$$\mathbf{f}_{\text{mat}} = \int_{\mathbb{X}} \left(\int_0^{\sigma} \Theta^{\top} \text{Ad}_{[g]_k}^{\top} ds \right) \frac{\partial}{\partial \sigma} (\text{Ad}_{[g]_k}^{-\top} \mathcal{S}) d\sigma \quad (\text{D.20})$$

By virtue of the integration by parts and applying the appropriate boundary conditions of the net wrenches at the base $\sigma = 0$ and $\sigma = L$ (*i.e.*, force balance), the generalized material forces can be compactly written as $\mathbf{f}_{\text{mat}} = \int_{\mathbb{X}} \Theta^T \mathcal{S} d\sigma$ which is nothing more than a projection of the stress wrench onto the truncated modal basis $\{\boldsymbol{\theta}_i\}_{i=1}^k$. By selecting a Hookean model, the internal stress wrench can be expressed as

$$\mathcal{S} = \mathcal{K}([\xi]_k - \xi^\circ) + \mathcal{D}[\dot{\xi}]_k, \quad (\text{D.21})$$

where $\mathcal{K} \in \text{se}^*(3) \times \text{se}(3)$ and $\mathcal{D} \in \text{se}^*(3) \times \text{se}(3)$ represent the stiffness and damping material tensor, respectively. Recall that $[\xi]_k = \Theta \mathbf{q} + \xi^\circ$ and $[\dot{\xi}]_k = \Theta \dot{\mathbf{q}}$ denote the geometric strain and strain-rate, respectively. This yields $\mathcal{S} = \mathcal{K} \Theta \mathbf{q} + \mathcal{D} \Theta \dot{\mathbf{q}}$; and consequently, the generalized conservative forces caused by material deformation can be expressed as a linear model in the following way:

$$\mathbf{f}_{\text{mat}} = \underbrace{\int_{\mathbb{X}} \Theta^T \mathcal{K} \Theta d\sigma}_{\mathbf{K}} \mathbf{q} + \underbrace{\int_{\mathbb{X}} \Theta^T \mathcal{D} \Theta d\sigma}_{\mathbf{D}} \dot{\mathbf{q}}. \quad (\text{D.22})$$

The quadratic form of the given matrices implies that they are positive definite, *i.e.*, $\mathbf{K} \succ 0$ and $\mathbf{D} \succ 0$.

E

Appendices to Chapter 6

E.1 Newmark- β solver

The Newmark- β method is an implicit numerical integration scheme extensively used to solve high-dimensional structural dynamic problem [115, 202]. We briefly explain the algorithm implemented in the function `Fem.simulate`. First, let us subdivide the time domain such that $(0, \dots, T)$ with uniform timesteps $\Delta t = t_{i+1} - t_i$. Then, given the initial conditions for (6.3), we wish to compute the state evolution $\mathbf{x}(t_i)$ and $\dot{\mathbf{x}}(t_i)$. For conciseness, let us write the discrete states of the FEM model as $\mathbf{x}(t_i) = \mathbf{x}^{(i)}$. Through the extended mean value theorem, we can formulate the general Newmark- β scheme as

$$\dot{\mathbf{x}}^{(i+1)} = \dot{\mathbf{x}}^{(i)} + \Delta t \left[(1 - \beta_1) \ddot{\mathbf{x}}^{(i)} + \Delta t \beta_1 \ddot{\mathbf{x}}^{(i+1)} \right], \quad (\text{E.1})$$

$$\mathbf{x}^{(i+1)} = \mathbf{x}^{(i)} + \Delta t \left[\dot{\mathbf{x}}^{(i)} + \left(\frac{1}{2} - \beta_2 \right) \ddot{\mathbf{x}}^{(i)} + \beta_2 \ddot{\mathbf{x}}^{(i+1)} \right], \quad (\text{E.2})$$

where $\beta_1, \beta_2 \geq \frac{1}{2}$. Now, in the expressions above only the forward-time acceleration $\ddot{\mathbf{x}}^{(i+1)}$ is the unknown partial solution, hence we conveniently write $\mathbf{w} := \ddot{\mathbf{x}}^{(i+1)}$. Substitution into the flow (6.3), we find:

$$\mathbf{r}(\mathbf{w}) := \mathbf{w} + \nabla_{\mathbf{x}} \mathcal{H}(\mathbf{w}) + \mathbf{R} \nabla_{\dot{\mathbf{x}}} \mathcal{H}(\mathbf{w}) - \mathbf{G} \mathbf{u}^{(i+1)}, \quad (\text{E.3})$$

where \mathcal{H} is the Hamiltonian. Following, the residual vector (E.3) forms an optimization problem in the form $\operatorname{argmin}_{\mathbf{w}} \|\mathbf{r}(\mathbf{w})\|_2$ for unknown accelerations \mathbf{w} . This implicit relation can be solved numerically using a recursive Newton Raphson method. Given the n -th iteration, the recursive solver reads

$$\mathbf{w}^{(n+1)} = \mathbf{w}^{(n)} + \alpha_+ \left[\mathbf{A}(\mathbf{w}^{(n)}) \right]^{-1} \mathbf{r}(\mathbf{w}^{(n)}), \quad (\text{E.4})$$

where $\mathbf{A} := [\mathbf{I} + \beta_1 \Delta t \mathbf{R} + \beta_2 \Delta t^2 \mathbf{K}_T \mathbf{M}]$ is the hessian matrix, and $0 < \alpha_+ \leq 1$ an update coefficient. The matrix \mathbf{K}_T denotes the tangent stiffness related to the local gradient of the elasticity force, given by $\mathbf{K}_T := \nabla_{\mathbf{x}} \mathbf{f}_e$.

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List of publications

Peer-reviewed journal articles

- Caasenbrood B.J., Pogromsky A.Y., and Nijmeijer, H., “*Sorotoki: A Matlab Toolkit for Design, Modeling, and Control of Soft Robots*”, IEEE Access. (*in preparation for journal submission*);
- Caasenbrood B.J., Pogromsky A., and Nijmeijer, H., “*Generative Design of Soft Robotic Actuators – a Gradient-based Approach*”, Frontiers in Robotics and AI. (*in preparation for journal submission*);
- Caasenbrood B.J., Pogromsky A.Y., and Nijmeijer H., “*Energy-shaping Controllers for Soft Robot Manipulators through Port-Hamiltonian Cosserat Models*”, SN Computer Science Springer, 2022;
- Caasenbrood B.J., Pogromsky A.Y., and Nijmeijer, H., “*Control-oriented Models for Hyper-elastic Soft Robots through Differential Geometry of Curves*”, Soft Robotics, 2022.

Peer-reviewed articles in conference proceedings

- Chu H., Caasenbrood B., Keyvanara M., Kuling I., and Nijmeijer H. (2023). “*Full-body Grasping Strategy for Planar Underactuated Soft Manipulators using Passivity-based Control*”. IEEE International Conference on Soft Robotics (RoboSoft). IEEE.
- Proper B., Caasenbrood B., and Kuling I. (2023). “*Easy Cleaning of 3D SLA/DLP Printed Soft Fluidic Actuators with Complex Internal Geometry*”. 2023 IEEE International Conference on Soft Robotics (RoboSoft). IEEE.
- Caasenbrood B., van Beek, F., Khanh Chu, H., and Kuling, I., “*A Desktop-sized Platform for Real-time Control Applications of Pneumatic Soft Robots*,” IEEE International Conference on Soft Robotics, RoboSoft 2022, pp 217-223.
- Amoozandeh Nobaveh A., and Caasenbrood B., “*Design Feasibility of an Energy-efficient Wrist Exoskeleton using Compliant Beams and Soft Actuators*”, Proceedings of the 18th International Consortium for Rehabilitation Robotics, 2022.
- Caasenbrood B.J., Pogromsky A., and Nijmeijer, H., “*Energy-based control for Soft Robots using Cosserat-beam models*”, Proceedings of the 18th International Conference on Informatics in Control, Automation and Robotics, 2021, pp. 311–319.
- Caasenbrood B.J., Pogromsky A., and Nijmeijer, H., “*A Computational Design Framework for Pressure-driven Soft Robots through Nonlinear Topology Optimization*,” 2020 3rd IEEE International Conference on Soft Robotics, 2020, pp. 633-638.

- Caasenbrood B.J., Pogromsky A., and Nijmeijer, H., “*Dynamic modeling of hyper-elastic soft robots using spatial curves,*” IFAC World Congress, IFAC-Papers OnLine, 2020, pp. 9238-9243.

Ancillary publications

In addition to the aforementioned work, the author has made contributions to the following publications that have not been explicitly discussed in the dissertation.

- Bertens T., Caasenbrood B., Saccon A., and Jalba A, "*Symmetry-Induced Ambiguity in Orientation Estimation from RGB Images*", IEEE Transaction on pattern Analysis and Machine Intelligence, (*in preparation for journal submission*).
- Amiri, A., Caasenbrood, B., van de Wouw, N., and Lopez Arteaga, I. "*A replacement model to simulate the nonlinear dynamics of electro-responsive liquid crystal coatings*", AIP Advances, 2022.

Talks, workshops, and non peer-reviewed abstracts

- Caasenbrood, B.J., invited student talk on “*Design and Control tools for fluidic soft robots,*” 4TU Federation’s Symposium on Soft Robotics, Twente University, 2023.
- Caasenbrood, B.J., invited talk on “*3D-printed Soft Robotics,*” Symposium on Robotic Technologies, Ultimaker, 2022. (invited speaker).
- Caasenbrood B.J., invited student speaker on **SOROTOKI: an open-source MATLAB toolkit for Design, Modeling and Control of Soft Robots,**” 4TU Federation’s Symposium on Soft Robotics, Delft University, 2022.
- Caasenbrood B.J., “*SOROTOKI: an Open-source Toolkit for Soft Robotics written in MATLAB,*” IEEE International Conference on Soft Robotics, RoboSoft 2022, Edinbrugh. (poster presentation). Received the Best Poster Award during the workshop on "Software for Soft Robotics Research".
- Caasenbrood B.J., C. Della Santina, and A. Pogromsky, “*Workshop on Model-based Control of Soft Robots,*” European Control Conference (ECC), 2021. (main workshop organizer).
- Caasenbrood B.J., talk on “*Towards Design and Control of Soft Robotics,*” 4TU Symposium on Soft Robotics (digital), 2020. (invited speaker).
- Caasenbrood B.J., talk on “*3D-printed Soft Robotics,*” Symposium on Robotic Technologies, 2019. (invited speaker).
- Caasenbrood B.J., Pogromsky A.Y, and Nijmeijer H., talk on “*Forward Dynamics of Hyper-elastic Soft Robotics,*” 39th Benelux Meeting on Systems and Control, 2019. (abstract).
- Caasenbrood B.J., Pogromsky A.Y, and Nijmeijer H., talk on “*Dynamical modeling and control of continuum soft robots,*” 37th Benelux Meeting on Systems and Control, 2018. (abstract).

About the author

Brandon Caasenbrood was born in Roermond, the Netherlands, on April 29th, 1993. After finishing high school in 2011 at the Broekhin college in Roermond, he studied mechanical engineering at the Eindhoven University of Technology (TU/e) in Eindhoven, the Netherlands. In 2016, he did an internship project at the RMIT Melbourne University under the supervision of Liuping Wang focusing on nonlinear Kalman filters for autonomous drones using onboard inertial and ultrasound sensor measurements. He obtained his BSc and MSc degrees (with honors) at the Eindhoven university in 2014 and 2017, respectively.



In September 2017, he started as a junior researcher within the Dynamics and Control group at the Department of mechanical engineering of the TU/e. Later, in February 2018, he started his PhD on the topic of design, modeling and control of soft robots under the supervision of Alexander Pogromsky (Sasha) and Henk Nijmeijer. The work focuses on both theoretical and practical aspects related to the design, modeling and control of soft robots. This research is part of the Wearable Robotics perspective program, a Dutch research program funded by the Nederlandse Organisatie voor Wetenschappelijk Onderzoek (NWO). The main results of his research are presented in this dissertation.

