

Computational Solid Mechanics Final Project Report

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1. Problem Description

Strong form:

$$\begin{aligned} \text{Given } f_i : \Omega \rightarrow \mathbb{R}, \quad g_i : \Gamma_g \rightarrow \mathbb{R}, \quad h_i : \Gamma_h \\ \text{determine } u_i : \bar{\Omega} \rightarrow \mathbb{R} \text{ s.t.} \\ \sigma_{ij,j} + f_i = 0 \\ u_i = g_i \quad \text{on } \Gamma_g \\ \sigma_{ij} n_j = h_i \quad \text{on } \Gamma_h \end{aligned}$$

Weak form

$$\begin{aligned} \mathcal{S}_i &:= \{u_i : u_i \in H^1, u_i = g_i \text{ on } \Gamma_g\} \\ \mathcal{V}_i &:= \{w_i : w_i \in H^1, w_i = 0 \text{ on } \Gamma_g\} \\ \text{Given } \dots, \text{ find that } u_i \in \mathcal{S}_i, \text{ s.t.} \\ a(\vec{w}, \vec{u}) &= (\vec{w}, \vec{f}) + (\vec{w}, \vec{h})_{\Gamma_h} \\ \text{where } a(\vec{w}, \vec{u}) &:= \int_{\Omega} w_{ij} \sigma_{ij} d\Omega \\ (\vec{w}, \vec{f}) &= \int_{\Omega} w_i f_i d\Omega \\ (\vec{w}, \vec{h})_{\Gamma_h} &= \int_{\Gamma_h} w_i h_i d\Omega \end{aligned}$$

Galerkin formulation

Galerkin formulation and implement

$$\mathcal{V}_i^h = \{ w_i^h : w_i^h(i) = \sum_{A \in \mathcal{T}_B} C_{iA} N_A(x) \}$$

↑
i-th component

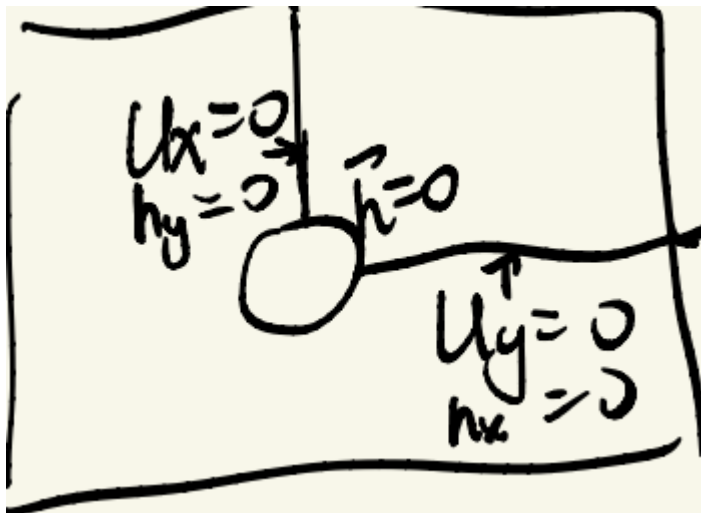
$$\mathcal{S}_i^h = \{ u_j^h = v_j^h + g_j^h, v_j^h = \sum_{B \in \mathcal{T}_B} d_{jB} N_B, g_j^h = \sum_{B \in \mathcal{T}_B} q_{jB} N_B \}$$

$$\sum_{A \in \mathcal{T}_B} C_{iA} \{ a(N_A \vec{e}_i, u^h) = (N_A \vec{e}_i, f) + (N_A \vec{e}_i, h) \Gamma \}$$

$$\Rightarrow a(N_A \vec{e}_i, N_B \vec{e}_j) d_{jB} = \int_{\Omega} N_A f_j d\Omega + \int_{\Gamma_h} N_A h_j da - a(N_A \vec{e}_i, \sum_{B \in \mathcal{T}_B} q_{jB} N_B \vec{e}_j)$$

Boundary condition

For the outer surface, there are Dirichlet BC (e.g. $g = 0$) and Neumann BC (e.g. $h = T$). For inner hole, the BC is $h = 0$. For symmetry surface, the BC is like this



2. The implementation of the element stiffness matrix
I choose $B_a^T D B_b$ implementation. Calculate B matrix first, then get k^e by matrix calculation.
3. Manufactured solution
With given $T_x = 10\text{kPa}$, I calculate 3 stresses at each nodes as manufactured solution, then transfer the polar coordinates into Cartesian coordinates with equations below

$$\sigma_{rr}(r, \theta) = \frac{T_x}{2} \left(1 - \frac{R^2}{r^2} \right) + \frac{T_x}{2} \left(1 - 4 \frac{R^2}{r^2} + 3 \frac{R^4}{r^4} \right) \cos 2\theta,$$

$$\sigma_{\theta\theta}(r, \theta) = \frac{T_x}{2} \left(1 + \frac{R^2}{r^2} \right) - \frac{T_x}{2} \left(1 + 3 \frac{R^4}{r^4} \right) \cos 2\theta,$$

$$\sigma_{r\theta}(r, \theta) = -\frac{T_x}{2} \left(1 + 2 \frac{R^2}{r^2} - 3 \frac{R^4}{r^4} \right) \sin 2\theta.$$

$$\sigma_x = \frac{\sigma_r + \sigma_\theta}{2} + \frac{\sigma_r - \sigma_\theta}{2} \cos 2\theta - \tau_{r\theta} \sin 2\theta$$

$$\sigma_y = \frac{\sigma_r + \sigma_\theta}{2} - \frac{\sigma_r - \sigma_\theta}{2} \cos 2\theta + \tau_{r\theta} \sin 2\theta$$

$$\tau_{xy} = \frac{\sigma_r - \sigma_\theta}{2} \sin 2\theta + \tau_{r\theta} \cos 2\theta$$

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sigma_rr = @(Tx,R,r,theta) Tx./2.*(1 - R.^2./r.^2) + Tx./2.*(1 - 4.*R.^2./r.^2 + 3.*R.^4./r.^4).*cos(2.*theta);
sigma_tt = @(Tx,R,r,theta) Tx./2.*(1 + R.^2./r.^2) - Tx./2.*(1 + 3.*R.^4./r.^4).*cos(2.*theta);
sigma_rt = @(Tx,R,r,theta) -Tx./2.*(1 + 2.*R.^2./r.^2 - 3.*R.^4./r.^4).*sin(2.*theta);
sigma_rr = sigma_rr(Tx,R,r,theta);
sigma_tt = sigma_tt(Tx,R,r,theta);
sigma_rt = sigma_rt(Tx,R,r,theta);
% f
sigma_11 = (sigma_rr + sigma_tt)./2 + (sigma_rr - sigma_tt)./2.*cos(2.*theta) - sigma_rt.*sin(2.*theta);
sigma_22 = (sigma_rr + sigma_tt)./2 - (sigma_rr - sigma_tt)./2.*cos(2.*theta) + sigma_rt.*sin(2.*theta);
sigma_12 = (sigma_rr - sigma_tt)./2.*sin(2.*theta) + sigma_rt.*cos(2.*theta);

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4. The codes are in driver.m