## Problem (a)

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(a) analytical expressions

$$y = \emptyset, \chi = \begin{bmatrix} \emptyset \\ \emptyset \end{bmatrix}, \emptyset = B^T \theta$$

$$\chi = A \chi + B u, y = C \chi$$

$$\theta = B^T J B u - B^T J D (B^T) d - B^T J \chi_{o} \Lambda (B^T) d$$

$$\vdots \begin{bmatrix} \emptyset \\ \emptyset \end{bmatrix} = \begin{bmatrix} O_5 & I & I_5 \\ -BJ \chi_{o} \Lambda (B)^T - B^T J D (B^T)^T \end{bmatrix} \begin{bmatrix} \emptyset \\ \emptyset \end{bmatrix} + \begin{bmatrix} O_5 \\ B^T J B \end{bmatrix} u$$

$$\chi = \begin{bmatrix} I_5 & O_5 \end{bmatrix} \begin{bmatrix} \emptyset \\ \emptyset \end{bmatrix}$$

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$$\chi = \chi + \chi + \chi + \chi$$

$$\chi = \chi + \chi$$

$$\mathcal{X} = P^{T} \chi, \quad \mathcal{X} = P^{T} \dot{\chi}$$

$$P^{T} \dot{\chi} = AP^{T} \chi + IBu, \quad \mathcal{Y} = CP^{T} \chi.$$

$$\dot{\chi} = PAP^{T} \chi + PIBu \quad \therefore \int AP = PAP^{T} \int BP = PIB$$

$$CP = CP^{T} \chi.$$

### **Numerical verification**

```
% (a)
AA = [zeros(n) eye(n); -B'*inv(J)*v0*Lamda*inv(B') -B'*inv(J)*D*inv(B')];
BB = [zeros(n) ; B'*inv(J)*B];
CC = [eye(n) zeros(n)];
0 1 0 0 0 0 0 0 0; 0 0 0 0 0 0 1 0 0 0;
   0 0 1 0 0 0 0 0 0; 0 0 0 0 0 0 1 0 0;
   0 0 0 1 0 0 0 0 0; 0 0 0 0 0 0 0 1 0;
   0 0 0 0 1 0 0 0 0 0; 0 0 0 0 0 0 0 0 0 1;];
AAA = P*AA*inv(P);
BBB = P*BB;
CCC = CC*inv(P);
load('finaldata.mat')
CheckAp = norm(AAA-Ap)/norm(Ap);
CheckBp = norm(BBB-Bp)/norm(Bp);
CheckCp = norm(CCC-Cp)/norm(Cp);
CheckAp
CheckBp
CheckCp
```

Checking the difference between (A, B, C) from the analytical results with the (Ap, Bp, Cp) by using normalized norm function.

```
CheckAp = 2.6818e-14
CheckBp = 7.0453e-15
CheckCp = 0
```

This result shows that the analytical calculation is verified.

## Problem (b)

torget: 
$$\emptyset = Im[ \vartheta e^{j\omega t}]$$
,

State trajectory:  $\chi(t) = \chi e^{\int t} \eta$ 

Control input:  $u(t) = |U|e^{\int t} \eta$ 

Find analytical expressions for  $\chi$ ,  $V$ ,  $\chi$ ,  $\eta$ 
interms of  $\vartheta$ ,  $w$ ,  $V_0$ , plant parms,

 $\chi = P\chi = P[\vartheta]$ ; from phasor  $\chi = P[I_5] \vartheta$ 

From (1):  $J \vartheta + D \vartheta + \chi \chi \varphi = Bu$ 
 $phasor: \hat{u} = B'(-Jw^2 + j\omega D + \chi_0 \Lambda) (B^T)' \vartheta$ 

Let  $\Gamma = \frac{1}{2} [-\frac{1}{2}]$ ; then  $\chi = [\chi \bar{\chi}] \Gamma$ 
 $V = [\hat{u} \bar{\chi}] \Gamma$ 

## **Numerical verification**

Implement analytical results to the Matlab codes, and by using the norm function, verified the regulator equation.

Checkreg = 5.2538e-11

This result shows that the analytical calculation is verified.

(c) Design a network of coupled n-AHO w state 
$$g_{i}(t) \in \mathbb{R}^{2}(i=1,2..n)$$
 $g_{i}=h_{i}$  with  $h_{i}(t)=\begin{bmatrix}\delta M \log t + \beta_{i} \\ Cos (\omega t + \beta_{i})\end{bmatrix}$ ,  $\beta_{i}=c$   $\delta_{i}$ 
 $(i-1)-i-(i+1)$  nearest neighbor

So, I designed  $\Delta$  based on  $\{\Delta 1=0\}$   $=$   $\{\Delta 1=1\}$   $=$   $=$   $\{\Delta 1=1\}$   $=$   $\{\Delta 1=$ 

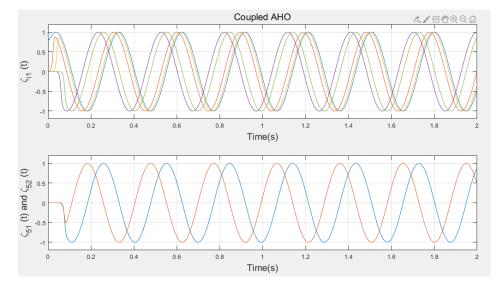
For Simulation, I set d=1, u=200 (Increase M -> AHO converges toss fast)

#### Simulation codes

#### **ODE function**

```
\Box function cdx = cdx(\underline{t},x,Beta, 0)
      x1 = x(1:2,:); x2 = x(3:4,:); x3 = x(5:6,:); x4 = x(7:8,:); x5 = x(9:10,:);
      beta1 = Beta(1); beta2 = Beta(2); beta3 = Beta(3); beta4 = Beta(4); beta5 = Beta(5);
      mu = 200;
      A1 = -0 + eye(2)*(mu)*(1-norm(x1)^2);
      A2 = -0 + eye(2)*(mu)*(1-norm(x2)^2);
      A3 = -0 + eye(2)*(mu)*(1-norm(x3)^2);
      A4 = -0 + eye(2)*(mu)*(1-norm(x4)^2);
      A5 = -0 + eye(2)*(mu)*(1-norm(x5)^2);
      R1 = [\cos(beta1) - \sin(beta1); \sin(beta1) \cos(beta1)];
      R2 = [\cos(beta2) - \sin(beta2); \sin(beta2) \cos(beta2)];
      R3 = [\cos(beta3) - \sin(beta3); \sin(beta3) \cos(beta3)];
      R4 = [cos(beta4) -sin(beta4);sin(beta4) cos(beta4)];
      R5 = [cos(beta5) -sin(beta5);sin(beta5) cos(beta5)];
      R = [-eye(2) R1'*R2 zeros(2) zeros(2) zeros(2);
          R2'*R1 -2*eye(2) R2'*R3 zeros(2) zeros(2);
          zeros(2) R3'*R2 -2*eye(2) R3'*R4 zeros(2);
          zeros(2) zeros(2) R4'*R3 -2*eye(2) R4'*R5;
          zeros(2) zeros(2) zeros(2) R5'*R4 -eye(2)];
      cdx = (blkdlag(A1,A2,A3,A4,A5) + R)*x;
 -end
```

## Figure (c)



From trial and error, found that larger mu make the oscillator converges to steady-state faster. Thus, the designed AHO converges almost immediately.

(d) Design a decentralized output regulator of the form.

$$u = U_s^2 + O_1(y - exs), \quad g = e(s)$$

optimal goit  $z(t) \to ze^{nt}y$ 
 $(x, u) \in z = xH, \quad W = uH$ 
 $h = He^{nt}y = \begin{bmatrix} Sin(uvt + \beta_1) \\ Cus(uvt + \beta_2) \end{bmatrix} = \begin{bmatrix} Misin v_1 & M_1 & Gis v_1 \\ Ginut & Gis v_2 \end{bmatrix} \begin{bmatrix} Cosut & -sin v_1 \\ Ginut & Gis v_3 \end{bmatrix} \begin{bmatrix} Cosut & -sin v_1 \\ Ginut & Gis v_4 \end{bmatrix} \begin{bmatrix} 1 \\ Ginut & Gis v_4 \end{bmatrix} \begin{bmatrix}$ 

From the mechanical equation analysis, the control gain K derived a diagonal matrix and has positive components. Then in the simulation, I found seems proper K by trial and error process.

K = diag(0.0002, 0.0002, 0.0002, 0.0002, 0.0002)

#### Simulation codes

```
beta1 = Beta1(1); beta2 = Beta1(2); beta3 = Beta1(3); beta4 = Beta1(4); beta5 = Beta1(5);
X1 = X(1:2,:); X2 = X(3:4,:); X3 = X(5:6,:); X4 = X(7:8,:); X5 = X(9:10,:);
U1 = U(1,:); U2 = U(2,:); U3 = U(3,:); U4 = U(4,:); U5 = U(5,:);
h1 = [sin(beta1) cos(beta1); sin(beta1+90) cos(beta1+90)];
h2 = [sin(beta2) cos(beta2); sin(beta2+90) cos(beta2+90)];
h3 = [sin(beta3) cos(beta3);sin(beta3+90) cos(beta3+90)];
h4 = [sin(beta4) cos(beta4);sin(beta4+90) cos(beta4+90)];
h5 = [sin(beta5) cos(beta5);sin(beta5+90) cos(beta5+90)];
H = [h1;h2;h3;h4;h5];
XX = blkdiag(X1*inv(h1), X2*inv(h2), X3*inv(h3), X4*inv(h4), X5*inv(h5));
UU = blkdiag(U1*inv(h1),U2*inv(h2),U3*inv(h3),U4*inv(h4),U5*inv(h5));
YY = Cp*XX;
options=odeset('RelTol',1e-4,'Refine',5);
simtime=[0 2];
xinit=[sin(beta1);cos(beta1);sin(beta2);cos(beta2);sin(beta3);
   cos(beta3);sin(beta4);cos(beta4);sin(beta5);cos(beta5);
   0;0;0;0;0;0;0;0;0;0;0];
Beta = unwrap(angle(phih))*(360/(2*pi));
K = blkdlag(0.00009, 0.00009, 0.00009, 0.00009);
[tt,xx]=ode45(@(tt,xx) ddx(tt,xx,K,P,Bp,Cp,XX,UU,Beta,O,phih),simtime,xinit);
```

At t = 0, set the initial zeta to the desired oscillator state H\*eta.

Then, Zeta(0) = H\*eta.

#### **ODE function**

```
\neg function ddx = ddx(tt,xx,K,P,Bp,Cp,XX,\lorW,Beta1,0,phih)
      % Define Constants
      n = 5;
      m = 0.001; % kg
      I = 0.1; % m
     cni = 0.009; % N/(m/s)
      cti = 0.0006; % N/(m/s)
      ct0 = 0.0006; % N/(m/s)
      li = 1/(2*n+2); mi = m/(n+1);
     10 = 1/(2*n+2); m0 = m/(n+1);
     y0 = -0.15; \% m/s
      % Define matrices
      B = diag(-ones(n,1)) + diag(ones(n-1,1),1);
      A = diag(ones(n,1)) + diag(ones(n-1,1),-1);
      e = ones(n,1);
      L = diag(li*ones(n,1)); M = diag(mi*ones(n,1));
      Ct = diag(cti*ones(n,1)); Cn = diag(cni*ones(n,1));
      CO = Cn-Ct;
      F = inv(B')*A*L;
      h = F'*M*e;
      Lamda = F'*C0 + diag((F'-e*h'/m)*Ct*e);
      J = L*M*L/3 + F'*M*F;
      D = L*Cn*L/3 + F'*Cn*F;
```

Set parameters and state of the ODE function.

```
beta1 = Beta1(1); beta2 = Beta1(2); beta3 = Beta1(3); beta4 = Beta1(4); beta5 = Beta1(5);
mu = 200;
A1 = -0 + eye(2)*(mu)*(1-norm(x1)^2);
A2 = -0 + eye(2)*(mu)*(1-norm(x2)^2);
A3 = -0 + eye(2)*(mu)*(1-norm(x3)^2);
A4 = -0 + eye(2)*(mu)*(1-norm(x4)^2);
A5 = -0 + eye(2)*(mu)*(1-norm(x5)^2);
R1 = [cos(beta1) -sin(beta1);sin(beta1) cos(beta1)];
R2 = [cos(beta2) -sin(beta2);sin(beta2) cos(beta2)];
R3 = [cos(beta3) -sin(beta3);sin(beta3) cos(beta3)];
R4 = [cos(beta4) -sin(beta4);sin(beta4) cos(beta4)];
R5 = [cos(beta5) -sin(beta5);sin(beta5) cos(beta5)];
R = [-eye(2) R1'*R2 zeros(2) zeros(2);
   R2'*R1 -2*eye(2) R2'*R3 zeros(2) zeros(2);
    zeros(2) R3'*R2 -2*eye(2) R3'*R4 zeros(2);
    zeros(2) zeros(2) R4'*R3 -2*eye(2) R4'*R5;
    zeros(2) zeros(2) zeros(2) R5'*R4 -eye(2)];
% get Zeta dot
ddx(1:10,:) = (blkdiag(A1,A2,A3,A4,A5) + R)*x0;
```

Add the oscillator that designed in problem (c) and by using this, zeta dot is calculated.

```
% get feedback u
w = 0(2,1);
h1 = [sin(beta1) cos(beta1);sin(beta1+90) cos(beta1+90)];
h2 = [sin(beta2) cos(beta2);sin(beta2+90) cos(beta2+90)];
h3 = [sin(beta3) cos(beta3);sin(beta3+90) cos(beta3+90)];
h4 = [sin(beta4) cos(beta4);sin(beta4+90) cos(beta4+90)];
h5 = [sin(beta5) cos(beta5);sin(beta5+90) cos(beta5+90)];
uhat = inv(B)*(-J*w^2+1i*w*D+v*Lamda)*inv(B')*phih;
Gamma = 0.5*[-1i 1; 1i 1];
U = [uhat conj(uhat)]*Gamma;
U1 = U(1,:); U2 = U(2,:); U3 = U(3,:); U4 = U(4,:); U5 = U(5,:);
UU = blkdiag(U1*inv(h1),U2*inv(h2),U3*inv(h3),U4*inv(h4),U5*inv(h5));
rho = 0.05*sin(300*tt); % noise
y = (1+rho)*Cp*x6;
u = UU*x0-K*(y-Cp*XX*x0);
```

Because velocity v(t) is not a constant value anymore and U has v inside, newly update U.

Then, the sensor noise rho is calculated and added feedback control equation.

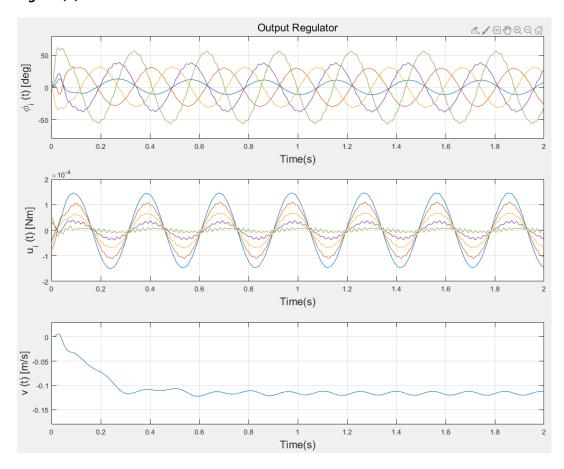
```
% get state dot from nonlinear plant dynamics
AA = [zeros(n) eye(n);-B'*inv(J)*v*Lamda*inv(B') -B'*inv(J)*D*inv(B')];
AAA = P*AA*inv(P);
ddx(11:20,:) = AAA*x6 +Bp*u;
```

Because the plant dynamic has v inside, update Ap for every iteration.

```
% get v dot
thetadot = inv(B')*[xx(12,:);xx(14,:);xx(16,:);xx(18,:);xx(20,:)];
theta = inv(B')*[xx(11,:);xx(13,:);xx(15,:);xx(17,:);xx(19,:)];
dtheta = ct0 +e'*Ct*e+theta'*C0*theta;
ddx(21,:) = (-dtheta*v-thetadot'*Lamda*theta)/m;
```

v dot is calculated by second line of the equation (1).

# Figure (d)



The simulator sufficiently compensated noise and reached steady-state quickly.

## Problem (e)

## Modification of the simulation codes from (d)

```
LL = blkdiag([100:100],[100:100],[100:100],[100:100],[100:100]);
eps = 0.1;
```

Designed block diagonal matrix L (LL in the code) and epsilon by trial and error.

```
% With disturbance without Q2
[ttt,xxx]=ode45(@(ttt,xxx) edx1(ttt,xxx,K,P,Bp,Cp,XX,UU,Beta,0,phih,LL,eps),simtime2,xinit);

% With disturbance with Q2
[tttt,xxxx]=ode45(@(tttt,xxxx) edx2(tttt,xxxx,K,P,Bp,Cp,XX,UU,Beta1,0,phih,LL,eps),simtime2,xinit);
```

# Modification of the ODE function from (d)

```
% add disturbance
d = 20;
if 2 <= tttt
    if tttt <= 2.1
        u = d*(UU*x0-K*(y-Cp*XX*x0));
else
        u = UU*x0-K*(y-Cp*XX*x0);
end
else
    u = UU*x0-K*(y-Cp*XX*x0);
end</pre>
```

Add disturbance to the system from 2s to 2.1s.

```
% get Zeta dot with feedback L
edx2(1:10,:) = (blkdiag(A1,A2,A3,A4,A5) + R)*x0 + eps*LL*(y-Cp*XX*x0);
```

For the feedback case, add the Q2 in the oscillator equation.

# Figure1 (e)

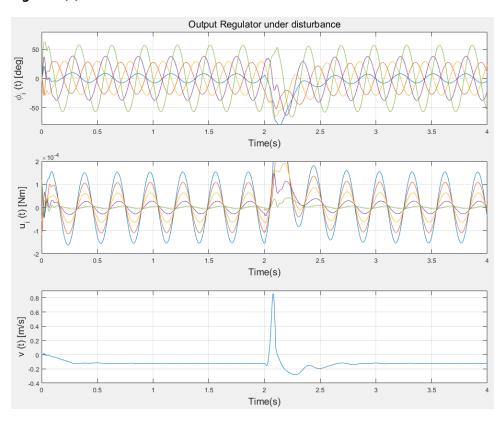
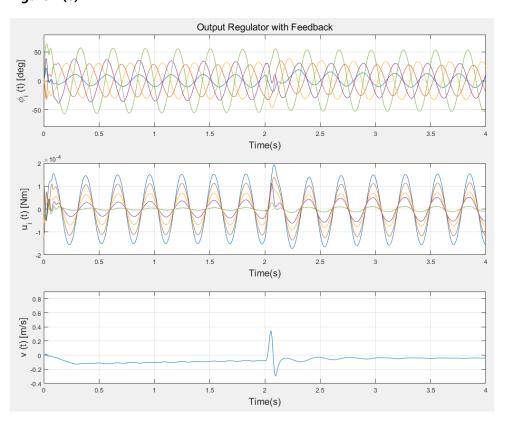


Figure2 (e)



In the first system, disturbance at 2s breaks stable gait easily. And it takes almost 0.4 seconds to recover the unstable

state. The same system with proper Q2 feedback attenuates disturbance much more quickly. Indeed, the system is not much affected by disturbance. This result shows that the second system with Q2 feedback is more robust than the first one.