Resonance Tank Capacitor and Output Capacitor

Inputs and claculated parameters

Input datas

| V_In_min | 360.0 | | | |
|-------------|--------------|--|--|--|
| V_In_nom | 380.0 | | | |
| V_In_max | 400.0 | | | |
| Vo_min | 42.0 | | | |
| Vo_nom | 48.0 | | | |
| Vo_max | 54.0 | | | |
| Power | 1200.0 | | | |
| f_nom | 100000.0 | | | |
| | Output datas | | | |
| Lnc | 3.000000e+00 | | | |
| Qec | 5.500000e-01 | | | |
| Cr_nF | 1.162090e+02 | | | |
| n | 4.000000e+00 | | | |
| Lr_uH | 2.179700e+01 | | | |
| Lm_uH | 6.539200e+01 | | | |
| fsw_min | 6.017000e+04 | | | |
| fsw_max | 1.562200e+05 | | | |
| lm_rms | 6.992000e+00 | | | |
| lo | 2.500000e+01 | | | |
| loe_rms | 7.636000e+00 | | | |
| los_rms | 3.054500e+01 | | | |
| lr_rms | 1.035400e+01 | | | |
| L_second_uH | 4.087000e+00 | | | |
| Re_nom | 2.490100e+01 | | | |
| Re_110 | 2.263700e+01 | | | |
| Cr | 1.162090e-07 | | | |
| Lr | 2.179700e-05 | | | |
| | | | | |

Output capacitor Co

Lm 6.539200e-05

Formulas

For a resistive load, the output capacitor is determined by

$$C_o \geq C_{o_{min}} = rac{I_o}{8 \cdot f_{sw} \cdot \Delta V_{out}}$$

Where:

- C_o : Output capacitance (Farads, F)
- I_o : Output load current (Amperes, A)
- f_{sw} : Switching frequency of the converter (Hertz, Hz)
- ΔV_{out} : Maximum allowed output voltage ripple (Volts, V)

$$ESR_{max} = rac{\Delta V_{out}}{I_{rect_peak}} = rac{\Delta V_{out}}{rac{\pi}{4} \cdot I_o \cdot 2}$$
 $I_{C_o} = I_o \sqrt{rac{\pi^2}{8} - 1}$

Where:

• I_{C_o} : RMS current of the capacitor @ f_sw = f_nom

See page 26, 27 [1].

By default, you can found all formula of this chapeter in the same ref

Numerical Implementation of the Formulas

We must use fsw min to the worst case

$$\begin{split} & \text{Io} = 25.000 \text{ (A)} \\ & \text{fsw}_{min} = 60170.000 \text{ (Hz)} \\ & \text{DV} = 0.250 \text{ (vpp)} \\ & \text{Co}_{min_{uF}} = 1 \times 10^6 \cdot \frac{\text{Io}}{8 \cdot \text{fsw}_{min} \cdot \text{DV}} = 1 \times 10^6 \cdot \frac{25.000}{8 \cdot 60170.000 \cdot 0.250} \\ & = 207.745 \text{ (uF)} \\ & \text{ESR}_{max_m} = 1 \times 10^3 \cdot \frac{\text{DV}}{\text{Io} \cdot \frac{\pi}{2}} = 1 \times 10^3 \cdot \frac{0.250}{25.000 \cdot \frac{3.142}{2}} \\ & = 6.366 \text{ (m}\Omega) \\ & I_{Co} = \text{Io} \cdot \sqrt{\frac{(\pi)^2}{8} - 1} = 25.000 \cdot \sqrt{\frac{(3.142)^2}{8} - 1} \\ & = 12.086 \text{ (Arms)} \end{split}$$

First proposition

B40910A8127M000 aluminum electrolytic capacitors with Temp_max = 150°C, Below a screenshoot of the datasheet [2].

= 12.086 (Arms)



Hybrid polymer aluminum electrolytic capacitors

B40910

Very high ripple current - up to 150 °C

Technical data and ordering codes

| C _R 120 Hz 20 °C µF | Case dimensions ¹⁾ d x I mm | ESR _{max} 100 kHz 20 °C Ω | I _{AC,R} 100 kHz 125 °C A | I _{AC,max} 100 kHz 135 °C A | Ordering code (composition see below) |
|---|--|---|---|---|--|
| V _R = 63 V D | C | | | | |
| 82 | 10 x 10.2 10 x 10.5 | 0.022 | 4.0 | 2.8 | B40910A8826M*** |
| 100 | 10 x 10.2 10 x 10.5 | 0.022 | 4.0 | 2.8 | B40910A8107M*** |
| 100 | 10 x 12.5 10 x 12.8 | 0.017 | 4.6 | 3.2 | B40910B8107M*** |
| 120 | 10 x 12.5 10 x 12.8 | 0.017 | 4.6 | 3.2 | B40910A8127M*** |
| 150 | 10 x 16.5 10 x 16.8 | 0.013 | 5.5 | 3.8 | B40910A8157M*** |
| 180 | 10 x 16.5 10 x 16.8 | 0.013 | 5.5 | 3.8 | B40910A8187M*** |

Figure 1: VRMS

Let's start with a configuration of 5 capacitors in parallel

$$Nb_{capa} = 5$$

$$C_{capa_{nom}} = 120 \; (\mathrm{uF})$$

$$Margin = 20 \ (\\%)$$

$$C_{capa} = C_{capa_{nom}} \cdot \left(1 - rac{ ext{Margin}}{100}
ight) = 120 \cdot \left(1 - rac{20}{100}
ight) = 96.000 \; ext{(uF, Wors)}$$

$$C_{eq} = C_{capa} \cdot \mathrm{Nb}_{capa} = 96.000 \cdot 5 = 480.000 \; (\mathrm{uF} > 208)$$

 $\mathrm{ESR}_{capa} = 17 \ (\Omega \ @ \ 100 \mathrm{kHz})$

$$\mathrm{ESR}_{eq} = rac{\mathrm{ESR}_{capa}}{\mathrm{Nb}_{capa}} = rac{17}{5}$$
 = 3.400 (\Omega < 6.36)

$$Icapa_{max} = 4.600$$

$${\rm Ieq}_{max} = {\rm Icapa}_{max} \cdot {\rm Nb}_{capa} = 4.600 \cdot 5 \\ \hspace*{1.5cm} = 23.000 \ \ (@ \ {\rm Arms} \ @ \ 125\,^{\circ}{\rm C} \ 100 \\ {\rm kHz} > 12.08 \\ {\rm Arms} = 1000 \\ {\rm Color of of other order} = 1000 \\ {\rm Color of other order} = 10000 \\ {\rm Color of other order} = 100000 \\ {\rm Color of other order} = 100000 \\ {\rm Color of other order} = 100000 \\ {\rm Color of other order} = 1$$

Voltage ripples

$$\Delta_{V_{out}} = rac{ ext{Io}}{8 \cdot ext{fsw}_{min} \cdot C_{eq} \cdot 1 imes 10^{-6}} = rac{25.000}{8 \cdot 60170.000 \cdot 480.000 \cdot 1 imes 10^{-6}} \hspace{0.5cm} = 0.108$$

Self heating

Power Dissipation of Each Capacitor

$$I_{each_{capa}} = rac{I_{Co}}{ ext{Nb}_{capa}} = rac{12.086}{5} = 2.417$$

$$P_{selfHeating} = \mathrm{ESR}_{capa} \cdot 1 \times 10^{-3} \cdot \left(I_{each_{capa}}\right)^2$$

= $17 \cdot 1 \times 10^{-3} \cdot (2.417)^2$
= 0.099 (W)

Estimation of Thermal Resistance Rth

$$\Delta_T = 150 - 125$$
 = 25 (°C)

ESR = 0.017

 $I = 4.600 \text{ (Arms)}$
 $P_{dissip} = \text{ESR} \cdot (I)^2 = 0.017 \cdot (4.600)^2$ = 0.360 (W)

 $R_{th} = \frac{\Delta_T}{P_{dissip}} = \frac{25}{0.360}$ = 69.498 (°C/W)

The self heating estimation and the max ambiant temp

$$\Delta_T = P_{selfHeating} \cdot R_{th} = 0.099 \cdot 69.498$$
 = 6.903 (°C => low delta temp)

Margin = 30 (°C)

 $T_{max} = 150$
 $T_{amb_{max}} = T_{max} - \Delta_T - \text{Margin} = 150 - 6.903 - 30$ = 113.097 (°C)

 $=69.498 \ (^{\circ}C/W)$

Voltage margin

$$egin{align*} ext{Vo}_{max} &= 54.000 ext{ (VDC)} \ V_{max_{datasheet}} &= 63 ext{ (VDC)} \ Voltage_{Margin} &= 100 \cdot rac{V_{max_{datasheet}} - ext{Vo}_{max}}{V_{max_{datasheet}}} = 100 \cdot rac{63 - 54.000}{63} &= 14.286 ext{ (\\%)} \end{aligned}$$

This solution is acceptable, but the voltage margin is limited.

Second proposition

EMHS101ARA331MMN0S aluminum electrolytic capacitors with Temp_max = 150°C, Below a screenshoot of the datasheet [4].

| wv | Сар | Cid- | ESR (Ω ma | ax./100kHz) | Rated ripple current | Part No. |
|--------------------|---------------|-----------|-----------|-------------|-----------------------|--------------------|
| (V _{dc}) | (μ F) | Size code | 20℃ | −40°C | (mArms/125°C, 100kHz) | Part No. |
| 100 | 110 | KE0 | 0.17 | 2.5 | 920 | EMHS101□RA111MKE0S |
| | 150 | KG5 | 0.13 | 1.8 | 1,030 | EMHS101□RA151MKG5S |
| | 160 | LH0 | 0.098 | 1.3 | 1,640 | EMHS101□RA161MLH0S |
| | 200 | MH0 | 0.091 | 0.98 | 1,720 | EMHS101□RA201MMH0S |
| | 240 | LN0 | 0.063 | 0.80 | 2,230 | EMHS101□RA241MLN0S |
| | 330 | MNO | 0.059 | 0.59 | 2.300 | EMHS101□RA331MMN0S |

Figure 2: VRMS

Let's start with a configuration of 5 capacitors in parallel

$$\mathrm{Nb}_{capa}=10$$

$$C_{capa_{nom}}=330~{
m (uF)}$$

Margin = 20 (
$$\$$
%)

$$C_{capa} = C_{capa_{nom}} \cdot \left(1 - rac{ ext{Margin}}{100}
ight) = 330 \cdot \left(1 - rac{20}{100}
ight)$$

$$= 2640.000 \text{ (uF} > 208)$$

= 264.000 (uF, Wors

$$C_{eq} = C_{capa} \cdot \mathrm{Nb}_{capa} = 264.000 \cdot 10$$

$$\mathrm{ESR}_{capa} = 59 \ (\Omega @ 100 \mathrm{kHz})$$

$$\mathrm{ESR}_{eq} = rac{\mathrm{ESR}_{capa}}{\mathrm{Nb}_{capa}} = rac{59}{10}$$

$$= 5.900 \;\; (\Omega < 6.36)$$

 $Icapa_{max} = 2.300$

$$\mathrm{Ieq}_{max} = \mathrm{Icapa}_{max} \cdot \mathrm{Nb}_{capa} = 2.300 \cdot 10$$

= 23.000 (@ Arms @ 125 °C 100kHz > 12.08Ar



$$\Delta_{V_{out}} = rac{ ext{Io}}{8 \cdot ext{fsw}_{min} \cdot C_{eq} \cdot 1 imes 10^{-6}} = rac{25.000}{8 \cdot 60170.000 \cdot 2640.000 \cdot 1 imes 10^{-6}} \hspace{0.5cm} = 0.020$$

Self heating

Power Dissipation of Each Capacitor

$$I_{each_{capa}} = rac{I_{Co}}{ ext{Nb}_{capa}} = rac{12.086}{10} = 1.209$$

$$P_{selfHeating} = \mathrm{ESR}_{capa} \cdot 1 \times 10^{-3} \cdot \left(I_{each_{capa}}\right)^2 = 59 \cdot 1 \times 10^{-3} \cdot \left(1.209\right)^2 = 0.086 \,\,\,\mathrm{(W)}$$

Estimation of Thermal Resistance Rth

$$\Delta_T = 150 - 125$$
 = 25 (°C)

$$egin{aligned} P_{dissip} &= ext{ESR}_{capa} \cdot 1 imes 10^{-3} \cdot (ext{Icapa}_{max})^2 \ &= 59 \cdot 1 imes 10^{-3} \cdot (2.300)^2 \ &= 0.312 \; ext{(W)} \end{aligned}$$

$$R_{th} = \frac{\Delta_T}{P_{dissip}} = \frac{25}{0.312}$$
 = 80.100 (°C/W)

The self heating estimation and the max ambiant temp

$$\Delta_T = P_{selfHeating} \cdot R_{th} = 0.086 \cdot 80.100$$
 = 6.903 (°C => low delta temp)

Margin = 30 (°C)

 $T_{max} = 150$
 $T_{amb_{max}} = T_{max} - \Delta_T - \text{Margin} = 150 - 6.903 - 30$ = 113.097 (°C)

 $V_{max} = 54.000 \text{ (VDC)}$
 $V_{max_{datasheet}} = 100 \text{ (VDC)}$

Voltage $_{Margin} = 100 \cdot \frac{V_{max_{datasheet}} - \text{Vo}_{max}}{V_{max_{datasheet}}} = 100 \cdot \frac{100 - 54.000}{100}$ = 46.000 (\%)

Comparaison

| | requirements | Solutio1 | Solutio2 |
|----------------|--------------|----------|----------|
| ESR_eq | 6.37 | 3.40 | 5.90 |
| C_eq | 207.74 | 480.00 | 2640.00 |
| leq_max | 12.09 | 23.00 | 23.00 |
| VmaxDC | 54.00 | 63.00 | 100.00 |
| Delta_V_out | 0.25 | 0.11 | 0.02 |
| C_capa | NaN | 96.00 | 264.00 |
| Nb_capa | NaN | 5.00 | 10.00 |
| P_selfHeating | NaN | 0.10 | 0.09 |
| T_amb_max | NaN | 113.10 | 113.10 |
| Voltage_Margin | NaN | 14.29 | 46.00 |

The margin in the first solution is limited (16% in the worst case). However, I propose we proceed with this option, given the number of parallel capacitors. Care must be taken in control to prevent any overshoot or transient voltage, especially when Vout is at Vout_max.

Resonanat capacitor Cr

Chosing a capacitor for Cr

The inputs data

$$Cr_{nF} = 116.209 \text{ (nF)}$$

$$V_{In_{max}} = 400.000 \;\; {
m (V)}$$

$$fsw_{min} = 60170.000 \text{ (Hz)}$$

The RMS voltage of the resonant capacitor

$$X_{Cr} = rac{1}{2 \cdot \pi \cdot \mathrm{fsw}_{min} \cdot \mathrm{Cr}_{nF} \cdot 1 \times 10^{-9}} = rac{1}{2 \cdot 3.142 \cdot 60170.000 \cdot 116.209 \cdot 1 \times 10^{-9}} = 22.761 \; \; ext{(Ohm)}$$

$$V_{Cr} = \text{Ir}_{rms} \cdot X_{Cr} = 10.354 \cdot 22.761$$
 = 235.672 (V)

$$V_{Cr_{rms}} = \sqrt{\left(rac{V_{In_{max}}}{2}
ight)^2 + \left(V_{Cr}
ight)^2} = \sqrt{\left(rac{400.000}{2}
ight)^2 + \left(235.672
ight)^2} \ = 309.098 \; ext{ (vrms)}$$

{ "Cr_nF": Cr_nF, "V_In_max": V_In_max, "fsw_min":fsw_min, "V_Cr_rms":V_Cr_rms, "Ir_rms":Ir_rms, }

Starting with the B3267*L film capacitors, the maximum rated DC voltage is 2000 V. [2].

The design value of Cr is 116.2 nF Below are some possible combinations for constructing this resonant capacitor:

| | Nominal_capa_nF | Nb capas in parallel | total capa nF | error % |
|----|-----------------|----------------------|---------------|---------|
| 0 | 6.2 | 19 | 117.8 | 1.4 |
| 1 | 6.8 | 17 | 115.6 | -0.5 |
| 2 | 8.2 | 14 | 114.8 | -1.2 |
| 3 | 10.0 | 12 | 120.0 | 3.3 |
| 4 | 12.0 | 10 | 120.0 | 3.3 |
| 5 | 15.0 | 8 | 120.0 | 3.3 |
| 6 | 22.0 | 5 | 110.0 | -5.3 |
| 7 | 33.0 | 4 | 132.0 | 13.6 |
| 8 | 47.0 | 2 | 94.0 | -19.1 |
| 9 | 56.0 | 2 | 112.0 | -3.6 |
| 10 | 68.0 | 2 | 136.0 | 17.0 |

The current of each element capacitor

$$\mathrm{Ir}_{rms_1}=1.294$$

The 15 nF, 15 mm, 2000 VDC TDK MKP capacitor meets both the Vrms and Irms requirements.

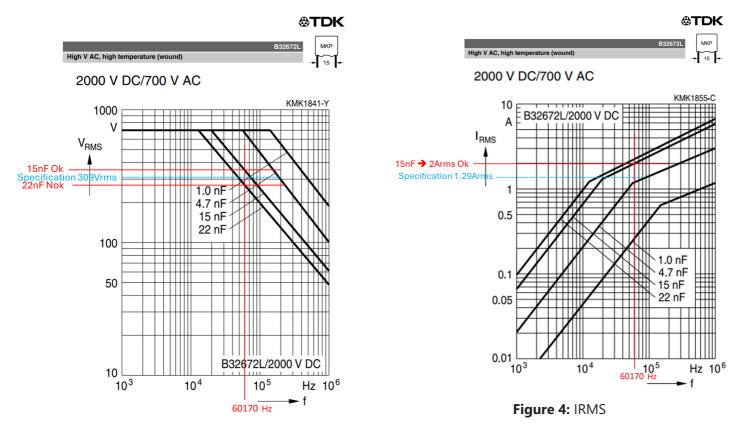


Figure 3: VRMS

Below is a screenshot from the B32672L datasheet. The ref B32672L8153 is a 15 nF capacitor.



Ordering codes and packing units (lead spacing 15 mm)

| V _{RMS} | V_R | C _R | Max. dimensions | Ordering code | Ammo | Reel | Untaped |
|------------------|-------|----------------|-------------------------------|------------------|----------|----------|----------|
| f≤1 kHz | | | $w \times h \times I$ | (composition see | pack | | |
| V AC | V DC | nF | mm | below) | pcs./MOQ | pcs./MOQ | pcs./MOQ |
| 700 | 2000 | 1.0 | $5.0 \times 10.5 \times 18.0$ | B32672L8102+*** | 4680 | 5200 | 4000 |
| | | 1.2 | $5.0 \times 10.5 \times 18.0$ | B32672L8122+*** | 4680 | 5200 | 4000 |
| | | 1.5 | $5.0 \times 10.5 \times 18.0$ | B32672L8152+*** | 4680 | 5200 | 4000 |
| | | 2.2 | $5.0 \times 10.5 \times 18.0$ | B32672L8222+*** | 4680 | 5200 | 4000 |
| | | 2.7 | $5.0 \times 10.5 \times 18.0$ | B32672L8272+*** | 4680 | 5200 | 4000 |
| | | 3.3 | $5.0 \times 10.5 \times 18.0$ | B32672L8332+*** | 4680 | 5200 | 4000 |
| | | 3.9 | $5.0 \times 10.5 \times 18.0$ | B32672L8392+*** | 4680 | 5200 | 4000 |
| | | 4.7 | $5.0\times10.5\times18.0$ | B32672L8472+*** | 4680 | 5200 | 4000 |
| | | 5.6 | $6.0 \times 11.0 \times 18.0$ | B32672L8562+*** | 3840 | 4400 | 4000 |
| | | 6.2 | $6.0 \times 11.0 \times 18.0$ | B32672L8622+*** | 3840 | 4400 | 4000 |
| | | 6.8 | $6.0 \times 11.0 \times 18.0$ | B32672L8682+*** | 3840 | 4400 | 4000 |
| | | 8.2 | $6.0 \times 12.0 \times 18.0$ | B32672L8822+*** | 3840 | 4400 | 4000 |
| | | 10 | $7.0 \times 12.5 \times 18.0$ | B32672L8103+*** | 3320 | 3600 | 4000 |
| | | 12 | $8.5 \times 14.5 \times 18.0$ | B32672L8123+*** | 2720 | 2800 | 2000 |
| | | 15 | $8.5\times14.5\times18.0$ | B32672L8153+*** | 2720 | 2800 | 2000 |
| | | 22 | $9.0 \times 17.5 \times 18.0$ | B32672L8223+*** | 2560 | 2800 | 2000 |
| | | 33 | $11.0\times18.5\times18.0$ | B32672L8333+*** | _ | 2200 | 1200 |

Figure 5: VRMS

The ESR and Power dissipation



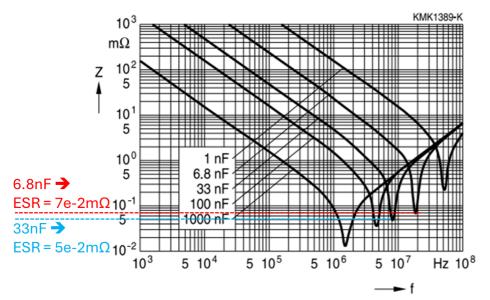
B3267*L

Capacitors for Snubbering, Resonant Circuits, Power Factor Correction (PFC)

High V AC, high temperature (wound)

Impedance Z versus frequency f

(typical values)



$$\begin{split} I_{RMS}\left(T_{A}\right) &= I_{RMS,T_{A} \leq 100} \, {^{\circ}_{C}} \cdot \, F_{T}\!\left(T_{A}\right) \\ V_{RMS}\left(T_{A}\right) &= V_{RMS,T_{A} \leq 100} \, {^{\circ}_{C}} \cdot \, F_{T}\!\left(T_{A}\right) \\ And \, F_{T} \, is given by the following curve: \end{split}$$

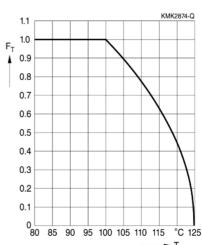


Figure 6: VRMS

From the below

 $6.8nF ESR = 70\mu\Omega$

33nF ESR=50μΩ

By linear interpolation, the ESR of a 15 nF capacitor can be estimated as 63.74 $\mu\Omega$

The power dissipation of each capacitor

$$\mathrm{ESR}_u = 63.740 \; (\mu\Omega)$$

$$Ir_{rms_1} = 1.294$$
 (Arms)

$${
m Ir}_{rms_{max}}=2~{
m (Arms)}$$

$$PD_{uW} = ESR_u \cdot (Ir_{rms_1})^2 = 63.740 \cdot (1.294)^2$$
 = 106.771 (uW)

The Rth estimation

$$T_{max} = 125$$

$$T_{100} = 100$$

$$\Delta_T = T_{max} - T_{100} = 125 - 100$$
 = 25

$$ext{PD}_{uW_{max}} = ext{ESR}_u \cdot (ext{Ir}_{rms_{max}})^2 = 63.740 \cdot (2)^2$$
 = 254.962

$$R_{TH} = rac{\Delta_T}{ ext{PD}_{uW_{max}}} = rac{25}{254.962} = 0.098 \ (^{\circ} ext{C/uW})$$

Each capacitor's self-heating and the maximum permissible ambient temperature.

$$\Delta_T = PD_{uW} \cdot R_{TH} = 106.771 \cdot 0.098$$
 = 10.469

$$T_{amb_{max}} = 125 - \Delta_T = 125 - 10.469$$
 = 114.531 (°C)

Understanding the Derating Curve of the Capacitors

One point calculation

$$Ta = 105$$

$$\Delta_T = T_{max} - \mathrm{Ta} = 125 - 105$$
 = 20

$$ext{PD}_{uW_{max}} = rac{\Delta_T}{R_{TH}} = rac{20}{0.098} = 203.969$$

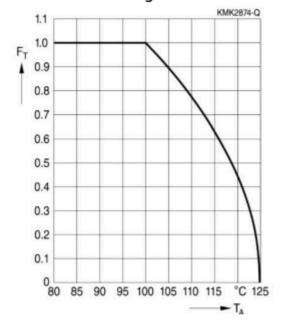
$${
m Ir}_{rms_{max_{Ta}}}=1.789$$

$$\operatorname{Fa} = \frac{\operatorname{Ir}_{rms_{max_{Ta}}}}{\operatorname{Ir}_{rms_{max}}} = \frac{1.789}{2} = 0.894$$

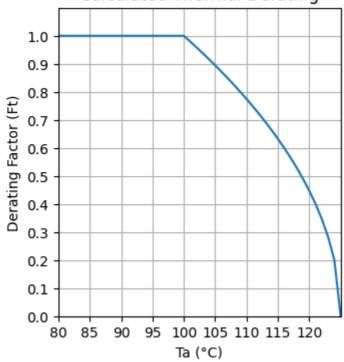
The same calculation is repeated to construct the derating curve.

(80.0, 125.0)

Thermal Derating from datasheet



Calculated Thermal Derating



Resonant capacitors configuration

There are two possible configurations for the resonant capacitors:

• All capacitors in parallel:

which is the classic LLC configuration and offers simplicity in layout.

• Dividing the capacitors between the high side and low side:

which helps balance HV+ and HV-.

Below is a simulation of both solutions. We can see that the voltage and current of each capacitor are almost identical in both configurations, and all other voltages and currents are also very similar.

You can donwload the LTSPICE file using this Link.

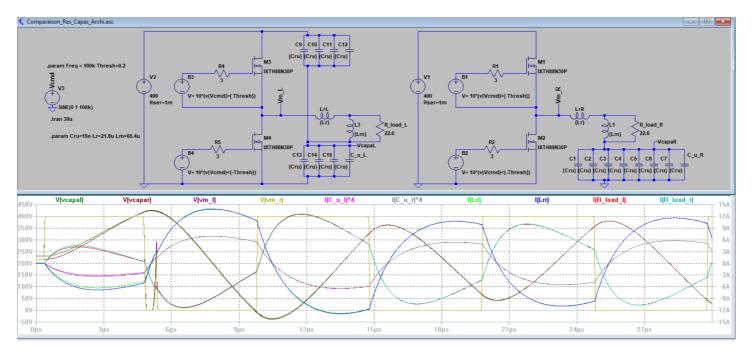


Figure 7: VRMS

References

- [1] Hong Huang, *Designing an LLC Resonant Half-Bridge Power Converter*. Available: https://bbs.dianyuan.com/upload/community/2013/12/01/1385867010-65563.pdf
- [2] B40910 Aluminum electrolytic capacitors datasheet
- [3] B3267*L Film Capacitors
- [4] EMHS Aluminum electrolytic capacitors datasheet