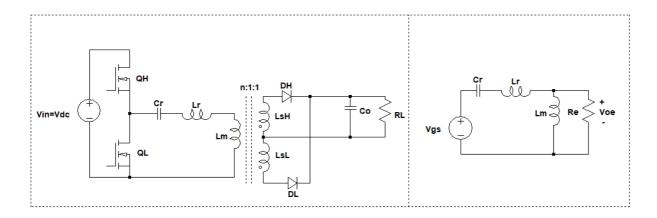
LLC tank pre-design calculations

Voltage Gain - Theoretical Overview



The voltage gain function (normalized) expression is:

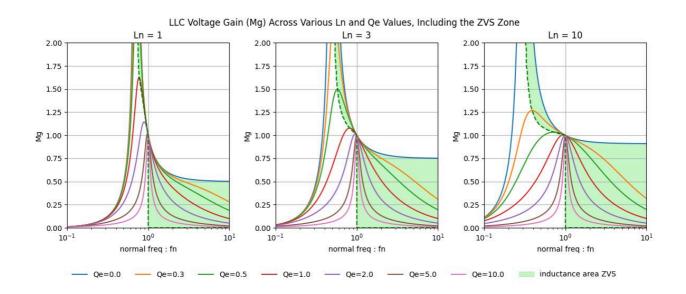
$$M_g = \left| rac{L_n \cdot f_n^2}{\left[(L_n+1) \cdot f_n^2 - 1
ight] + j \left[(f_n^2-1) \cdot f_n \cdot Q_e \cdot L_n
ight]}
ight|$$

With:

$$L_n=rac{L_m}{L_r}, \quad Q_e=rac{\sqrt{rac{L_r}{C_r}}}{R_e}, \quad f_n=rac{f_{sw}}{f_0}, \quad f_0=rac{1}{2\pi\sqrt{L_rC_r}}$$

See page 3 formula (23) [1].

You can found all formula of this chapeter in the same ref



Inputs and Specifications

$$V_{In_{min}} = 360$$
 (v)

$$V_{In_{nom}}=380~\mathrm{(v)}$$

$$V_{In_{max}}=400~
m (v)$$

$$Vo_{min} = 42$$
 (v)

$$Vo_{nom} = 48$$
 (v)

$$Vo_{max} = 54$$
 (v)

$$Power = 1200 \text{ (w)}$$

$$f_{nom} = 100000.000$$
 (Hz)

Inputs data

Transfo ratio and Voltage Gain

$$n = rac{V_{In_{nom}}}{{{
m Vo}_{nom} \cdot 2}} = rac{380}{48 \cdot 2} \hspace{1cm} = 3.958$$

Choose an integer value to simplify the transformer design.

$$n = \text{round}(n) = \text{round}(4) = 4$$

$$Vf = 0.200$$
 (drop voltage in the mos)

$$efficiency = 0.950$$
 (hypothesis)

$$loss = 1 - efficiency = 1 - 0.950$$
 = 0.050

$$Io_{nom} = \frac{Power}{Vo_{nom}} = \frac{1200}{48}$$
 = 25.000 (A)

$$V_{loss} = rac{rac{ ext{Power-loss}}{ ext{efficiency}}}{ ext{Io}_{nom}} = rac{rac{1200 \cdot 0.050}{0.950}}{25.000} = 2.526 ext{ (v)}$$

margin = 0.010

$$\mathrm{Mg}_{min} = n \cdot \frac{\mathrm{Vo}_{min} \cdot (1 - \mathrm{margin}) + \mathrm{Vf}}{\frac{V_{In_{max}}}{2}} = 4 \cdot \frac{42 \cdot (1 - 0.010) + 0.200}{\frac{400}{2}} = 0.836$$

$$\mathrm{Mg}_{max} = n \cdot \frac{\mathrm{Vo}_{max} \cdot (1 + \mathrm{margin}) + \mathrm{Vf} + V_{loss}}{\frac{V_{In_{min}}}{2}} = 4 \cdot \frac{54 \cdot (1 + 0.010) + 0.200 + 2.526}{\frac{360}{2}} = 1.273$$

$$\mathrm{Mg}_{max110} = \mathrm{Mg}_{max} \cdot \left(\frac{110}{100}\right) = 1.273 \cdot \left(\frac{110}{100}\right) \\ = 1.400$$

Lm, Lr, Cr tank

Below we will use grid search to find the best values for Ln and Qe.

The idea:

- Change Ln in the range: start = 1, stop = 10, step = 0.01 (around 100 points)
- Change Qe in the range: start = 0.1, stop = 1, step = 0.01 (around 10 points)

We will select the Ln and Qe values that give an Mg value closest to Mg_max110.

Top 6 (Ln, Qe) Combinations Matching Mg_max110

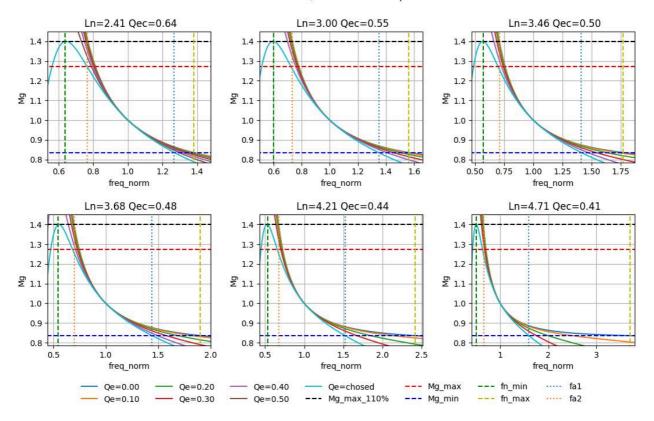
The following 6 values of Ln and Qe closely match the target voltage gain Mg_max110.

These rows were selected based on the criterion that Mg_ape is nearly equal to Mg_max110.

$$Mg_{max110} = 1.400$$

	Lnc	Qec	Lm_uH	Lr_uH	Cr_nF	fn_min	fn_max	fsw_min	fsw_max	Mg_ape
0	2.41	0.64	61.127	25.364	99.867314	0.6375	1.3790	63750.0	137900.0	1.400142
1	3.00	0.55	65.392	21.797	116.209238	0.6017	1.5622	60170.0	156220.0	1.400062
2	3.46	0.50	68.562	19.816	127.830162	0.5707	1.7698	57070.0	176980.0	1.399923
3	3.68	0.48	70.005	19.023	133.156419	0.5471	1.9035	54710.0	190350.0	1.400284
4	4.21	0.44	73.413	17.438	145.261548	0.5324	2.4133	53240.0	241330.0	1.400277
5	4.71	0.41	76.532	16.249	155.890441	0.5077	3.6928	50770.0	369280.0	1.400231

Grid search for Ln and Qe to find the best pair of values.



Lnc = 3

Qec = 0.550

Lnc = 3 and Qec = 0.55 represent an optimal compromise due to the following:

• Moderate gain slope (ΔM/Δf):

In the inductive region, the gain rises gradually with frequency, enabling stable control without abrupt sensitivity shifts.

• Limited frequency span (f_min to f_max):

These parameters restrict the switching frequency range, simplifying component design, controller implementation, and consistent ZVS operation.

Equivalent resistor

$$\operatorname{Re}_{nom} = 8 \cdot (n)^2 \cdot \frac{\operatorname{Vo}_{nom}}{(\pi)^2 \cdot \operatorname{Io}_{nom}} = 8 \cdot (4)^2 \cdot \frac{48}{(3.142)^2 \cdot 25.000} = 24.901$$

$$Re_{nom} = round(Re_{nom}, 3) = round(24.901, 3)$$
 = 24.901

$$Re_{110} = 8 \cdot (n)^{2} \cdot \frac{Vo_{nom}}{(\pi)^{2} \cdot Io_{nom} \cdot 1.1} = 8 \cdot (4)^{2} \cdot \frac{48}{(3.142)^{2} \cdot 25.000 \cdot 1.1} = 22.637$$

$$P_{re_{110}} = rac{\left(rac{V_{In_{nom}}}{2}
ight)^2}{\mathrm{Re}_{nom}} = rac{\left(rac{380}{2}
ight)^2}{24.901} = 1449.741$$

Lm, Lr, Cr values

$$\operatorname{Cr}_{nF} = \frac{1 \times 10^9}{2 \cdot \pi \cdot \operatorname{Qec} \cdot f_{nom} \cdot \operatorname{Re}_{nom}} = \frac{1 \times 10^9}{2 \cdot 3.142 \cdot 0.550 \cdot 100000.000 \cdot 24.901} = 116.209 \text{ (nF)}$$

Cr = 116.209

$$Cr = round(Cr, 3) = round(116.209, 3)$$
 = 116.209

$$ext{Lr} = rac{1}{\left(2 \cdot \pi \cdot f_{nom}
ight)^2 \cdot ext{Cr} \cdot 1 imes 10^{-9}} = rac{1}{\left(2 \cdot 3.142 \cdot 100000.000
ight)^2 \cdot 116.209 \cdot 1 imes 10^{-9}} = 0.000$$

$$\operatorname{Lr}_{uH} = \operatorname{Lr} \cdot 1 \times 10^6 = 0.000 \cdot 1 \times 10^6 = 21.797 \text{ (uH)}$$

$$Lr_{uH} = round(Lr_{uH}, 3) = round(21.797, 3)$$
 = 21.797

$$Lm = Lr \cdot Lnc = 0.000 \cdot 3$$

$$Lm_{uH} = Lm \cdot 1 \times 10^6 = 0.000 \cdot 1 \times 10^6$$
 = 65.392 (uH)

Verification

$$ext{Qcal} = rac{\sqrt{rac{ ext{Lr}}{ ext{Cr} \cdot 1 imes 10^{-9}}}}{ ext{Re}_{110} \cdot 1.1} = rac{\sqrt{rac{0.000}{116.209 \cdot 1 imes 10^{-9}}}}{22.637 \cdot 1.1} = 0.550$$

$$Qec = 0.550$$

Fsw limites and primary secondary currents

$$\begin{aligned} &\text{fsw}_{min} = \text{round}(\text{fn}_{min} \cdot f_{nom}, \ 2) = \text{round}(0.602 \cdot 100000.000, \ 2) &= 60170.000 \ \text{(Hz)} \\ &\text{fsw}_{max} = \text{round}(\text{fn}_{max} \cdot f_{nom}, \ 2) = \text{round}(1.562 \cdot 100000.000, \ 2) &= 156220.000 \ \text{(Hz)} \\ &\text{wmin} = 2 \cdot \pi \cdot \text{fsw}_{min} = 2 \cdot 3.142 \cdot 60170.000 &= 378059.260 \ \text{(rad/s)} \\ &\text{wmax} = 2 \cdot \pi \cdot \text{fsw}_{max} = 2 \cdot 3.142 \cdot 156220.000 &= 981559.209 \ \text{(rad/s)} \\ &\text{Im}_{rms} = 2 \cdot \sqrt{2} \cdot n \cdot \frac{\text{Vo}_{nom}}{\pi \cdot \text{Lm} \cdot \text{wmin}} = 2 \cdot \sqrt{2} \cdot 4 \cdot \frac{48}{3.142 \cdot 0.000 \cdot 378059.260} &= 6.992 \ \text{(Arms)} \\ &\text{Io} = 25.000 \ \text{(Arms)} \\ &\text{Ioe}_{rms} = 1.1 \cdot \pi \cdot \frac{\text{Io}}{n \cdot 2 \cdot \sqrt{2}} = 1.1 \cdot 3.142 \cdot \frac{25.000}{4 \cdot 2 \cdot \sqrt{2}} &= 7.636 \ \text{(Arms)} \oplus 110\% \\ &\text{Ios}_{rms} = \text{Ioe}_{rms} \cdot n = 7.636 \cdot 4 &= 30.545 \ \text{(Arms)} \\ &\text{Ir}_{rms} = \sqrt{(\text{Im}_{rms})^2 + (\text{Ioe})^2} = \sqrt{(6.992)^2 + (7.636)^2} &= 10.354 \ \text{(Arms)} \\ &\text{L}_{second_{uH}} = \frac{\text{Lm}_{uH}}{(n)^2} = \frac{65.392}{(4)^2} &= 4.087 \ \text{(uH)} \end{aligned}$$

Output data

```
{'Lnc': 3.0,
 'Qec': 0.55,
 'Cr_nF': 116.209,
'Lr_uH': 21.797,
 'Lm_uH': 65.392,
 'fsw min': 60170.0,
 'fsw_max': 156220.0,
 'Im rms': 6.992,
 'Io': 25.0,
 'Ioe_rms': 7.636,
'Ios_rms': 30.545,
 'Ir_rms': 10.354,
 'I second rms': 27.969,
 'L_second_uH': 4.087,
 'Re nom': 24.901,
 'Re_110': 22.637}
```

References

[1] Hong Huang, *Designing an LLC Resonant Half-Bridge Power Converter*. Available: https://bbs.dianyuan.com/upload/community/2013/12/01/1385867010-65563.pdf