

BT209

Bioreaction Engineering

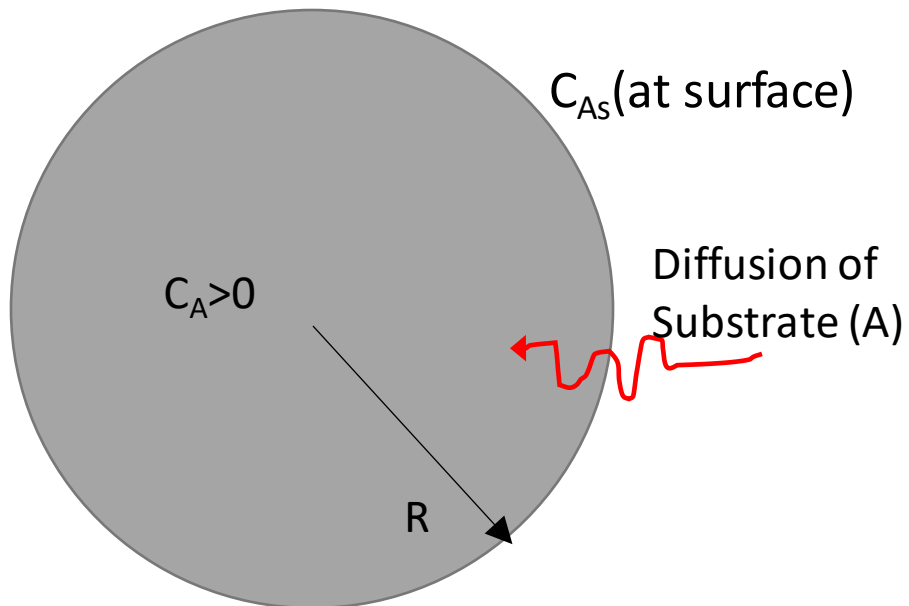
19/04/2023

Heterogeneous reaction

Internal Effectiveness factor (η_i)

- This will give idea the extent to which reaction is affected by the internal mass transfer

$$\eta_i = \frac{\text{observed rate of reaction } (r_{A,obs})}{\text{rate that would occur if } C_A = C_{AS} \text{ everywhere in the particle } (r_{AS}^*)}$$



$$r_{AS}^* = \frac{4}{3} \pi R^3 (k_1 C_{AS}) \quad (\text{maximum rate for 1}^{\text{st}} \text{ order})$$

if $\eta_i = 1$, there is no mass transfer effect

if $\eta_i \ll 1$, there is large mass transfer effect

Objective: prepared immobilized bead having less mass transfer effect

Predict Internal Effectiveness factor (η_i) for first order

$$\eta_i = \frac{\text{observed rate of reaction } (r_{A,obs})}{\text{rate that would occur if } C_A = C_{AS} \text{ everywhere in the particle } (r_{AS}^*)}$$

For first order $r_{A,obs} = 4\pi R \mathcal{D}_{Ae} C_{AS} \left[R \sqrt{k_1 / \mathcal{D}_{Ae}} \coth \left(R \sqrt{k_1 / \mathcal{D}_{Ae}} \right) - 1 \right]$

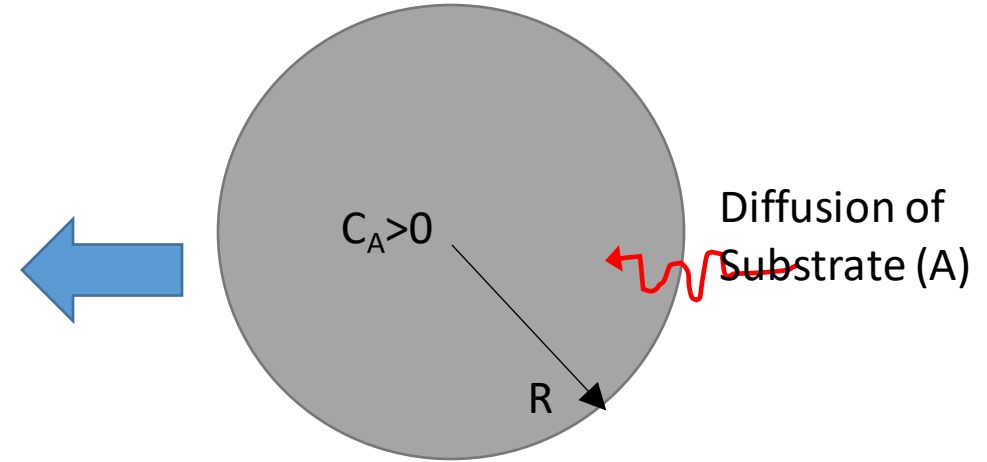
$$\eta_i = \frac{4\pi R D_{Ae} C_{AS} \left[R \sqrt{k_1 / D_{Ae}} \coth \left(R \sqrt{k_1 / D_{Ae}} \right) - 1 \right]}{\frac{4}{3} \pi R^3 k_1 C_{AS}}$$

$$\eta_i = \frac{3 D_{Ae}}{R^2 k_1} \left[R \sqrt{k_1 / D_{Ae}} \coth \left(R \sqrt{k_1 / D_{Ae}} \right) - 1 \right]$$

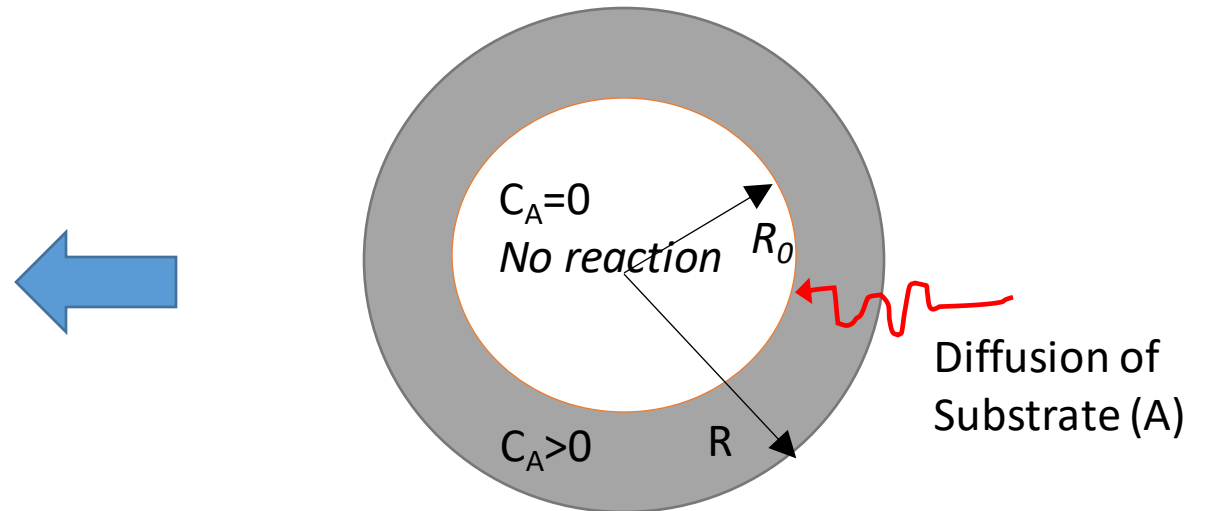
Predict Internal Effectiveness factor (η_i) for zero order

$$\eta_i = \frac{\text{observed rate of reaction } (r_{A,obs})}{\text{rate that would occur if } C_A = C_{AS} \text{ everywhere in the particle } (r_{AS}^*)}$$

$$\eta_i = \frac{\frac{4}{3} \pi R^3 k_0}{\frac{4}{3} \pi R^3 k_0} = 1 \quad (\text{Rate independent of concentration})$$



$$\eta_i = \frac{\frac{4}{3} \pi (R^3 - R_0^3) k_0}{\frac{4}{3} \pi R^3 k_0} = 1 - \left(\frac{R_0}{R}\right)^3$$



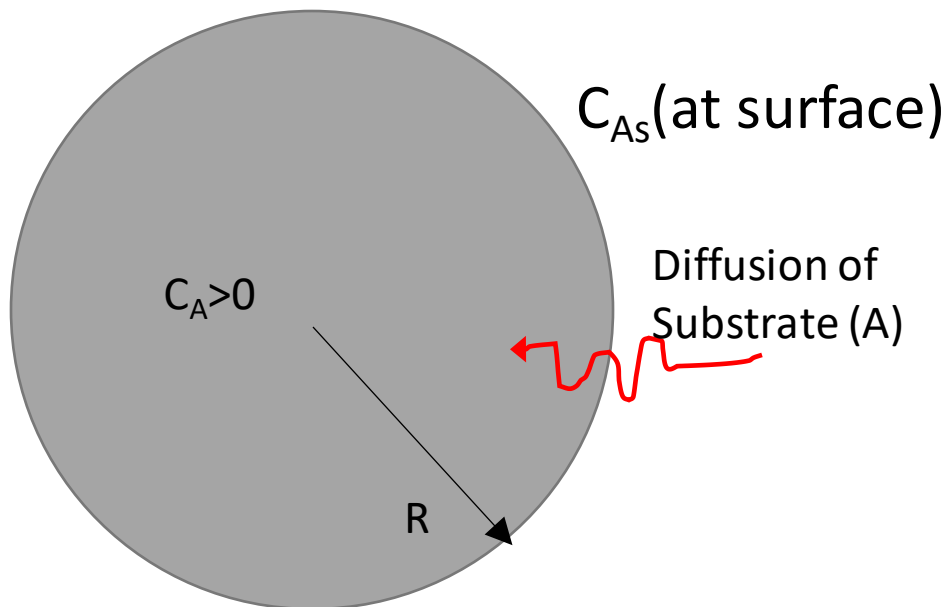
Predict Internal Effectiveness factor (η_i) for Michaelis–Menten kinetics type reaction

$$\eta_i = \frac{\text{observed rate of reaction } (r_{A,obs})}{\text{rate that would occur if } C_A = C_{As} \text{ everywhere in the particle } (r_{As}^*)}$$

$$r_{As}^* = \frac{4}{3} \pi R^3 \left(\frac{v_{max} C_{As}}{K_m + C_{As}} \right) \quad (\text{maximum rate})$$

Thiele modulus

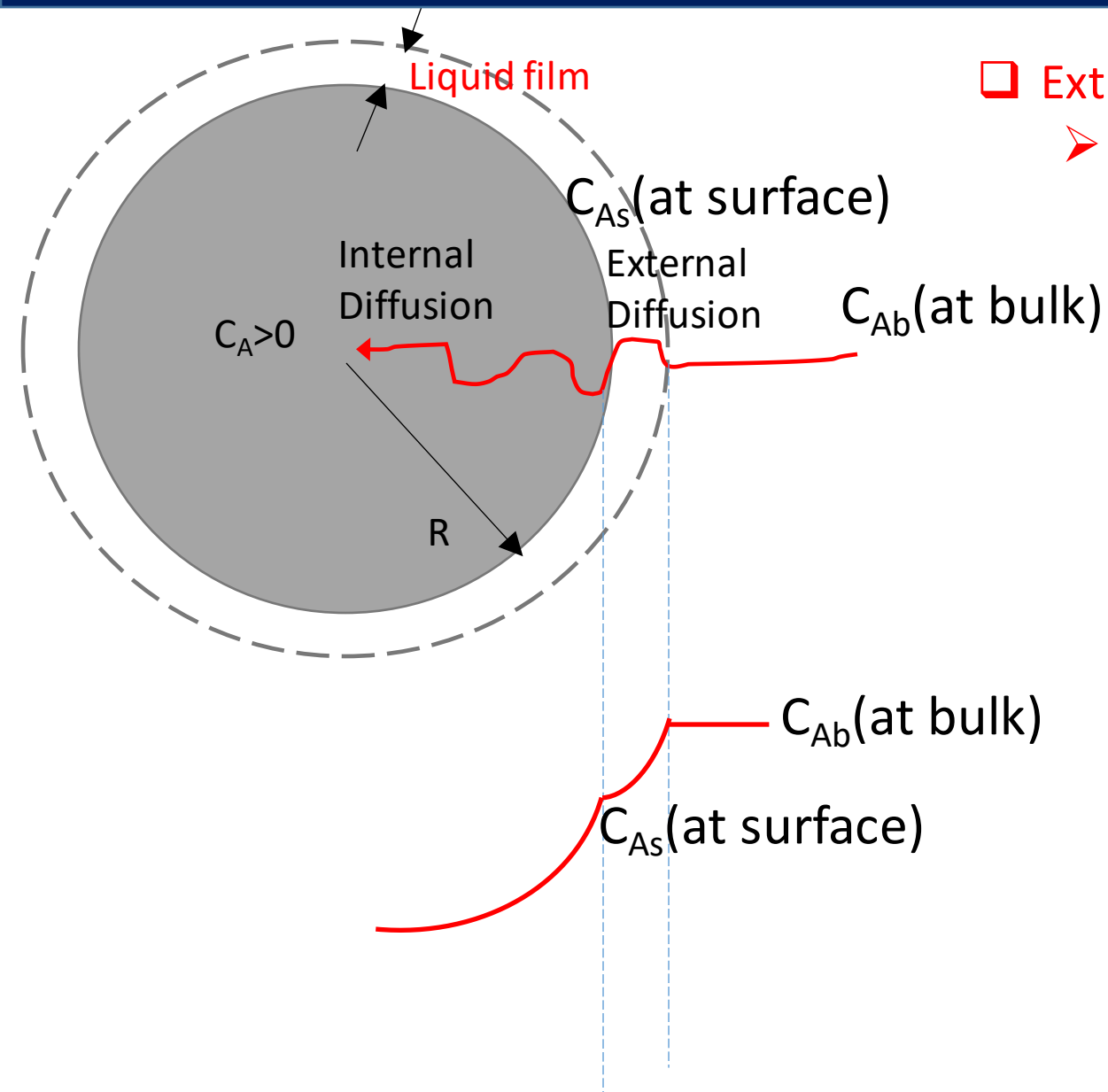
$$\phi^2 = \frac{\text{surface reaction rate (maximum)}}{\text{internal diffusion rate}}$$



if ϕ high, Internal diffusion rate low ,
—process is internal mass transfer control

if ϕ low, reaction rate low ,
—process is reaction control

External Mass transfer (liquid film mass transfer)



- ❑ External barrier/resistance: Liquid film outside the solid
- External diffusion/External mass transfer

$$1^{\text{st}} \text{ order } C_A = C_{As} \frac{R}{r} \frac{\sinh(r \sqrt{k_1 / \mathcal{D}_{Ae}})}{\sinh(R \sqrt{k_1 / \mathcal{D}_{Ae}})}$$

$$0^{\text{th}} \text{ order } C_A = C_{As} + \frac{k_0}{6 \mathcal{D}_{Ae}} (r^2 - R^2)$$

- Very difficult to measure C_{As} (at surface)
- ✓ Predict C_{As}

Cont.

The rate of mass transfer across the external film

$$N_A = k_S a (C_{Ab} - C_{As})$$

k_S : the liquid-phase mass transfer coefficient

a : is the external surface area of the catalyst (some times per unit volume)

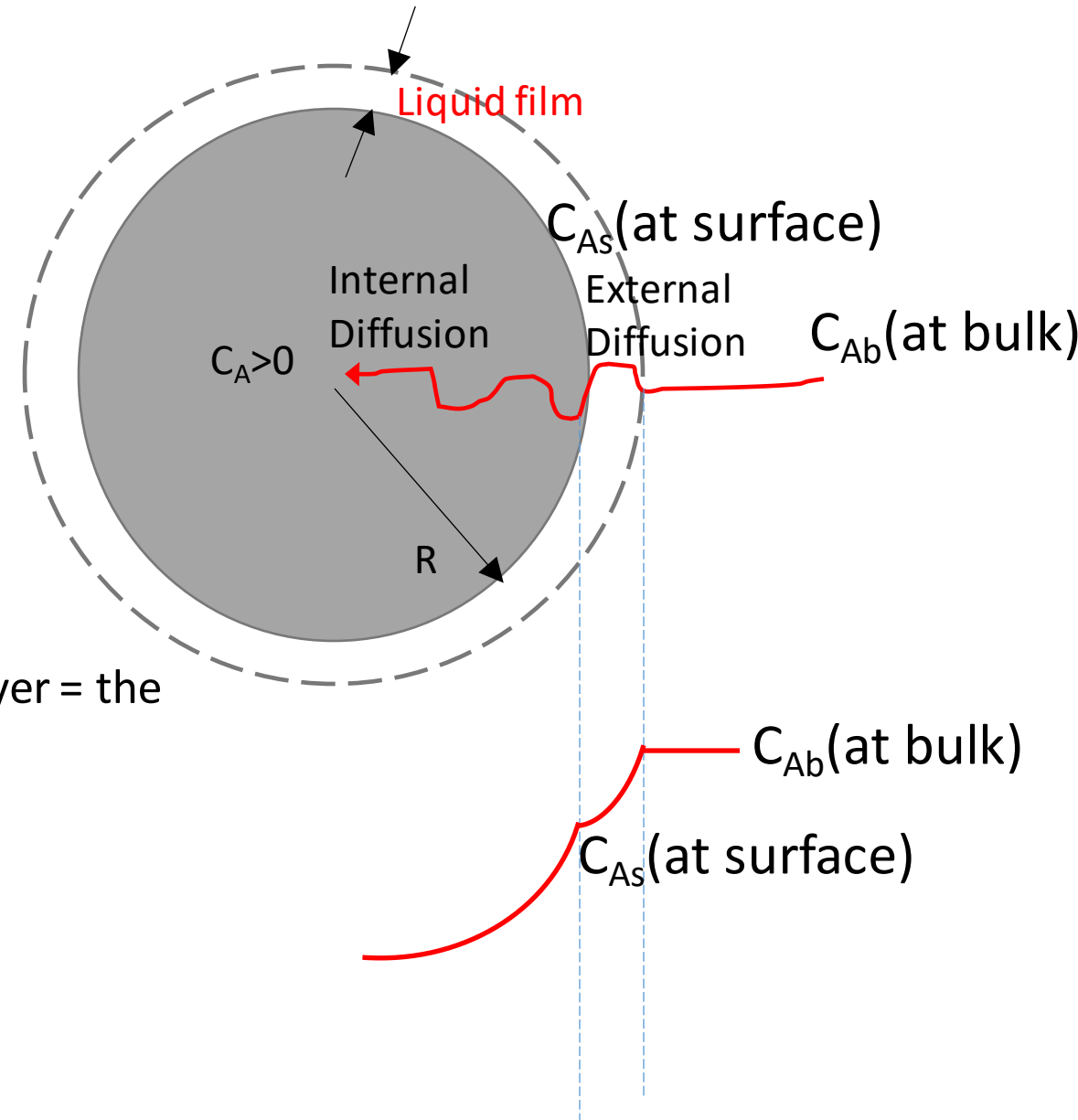
$$a = \frac{S_X}{V_P} = \frac{\text{External surface area}}{\text{volume of the particle}}$$

At steady state

the rate of substrate transfer across the boundary layer = the rate of substrate consumption by the catalyst, $r_{A,obs}$.

$$r_{A,obs} = k_S \frac{S_x}{V_p} (C_{Ab} - C_{As})$$

$$\frac{C_{As}}{C_{Ab}} = 1 - \frac{V_p}{S_x} \frac{r_{A,obs}}{k_S C_{Ab}}$$

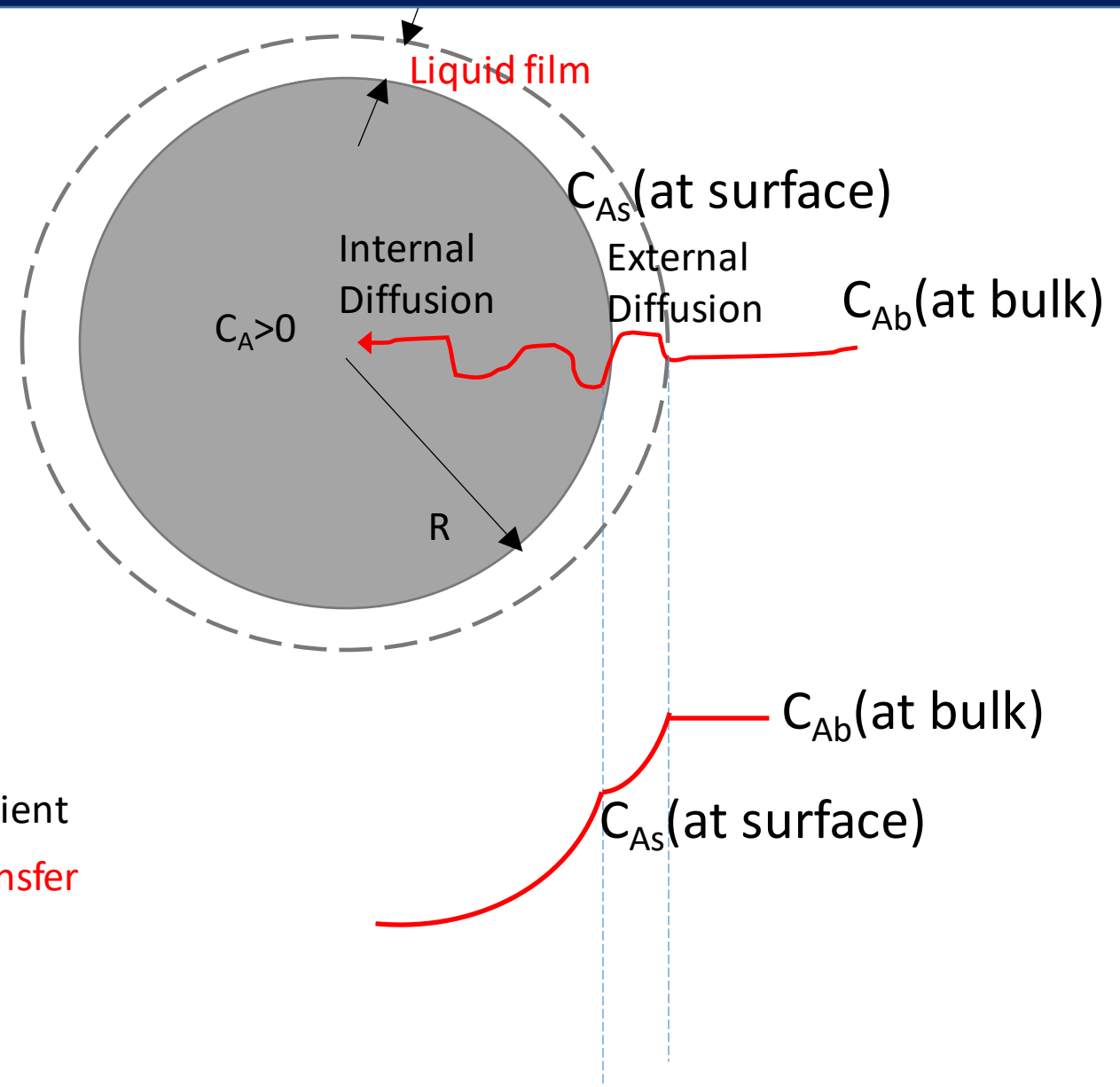


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$$\frac{C_{As}}{C_{Ab}} = 1 - \frac{V_p}{S_x} \frac{r_{A,obs}}{k_S C_{Ab}}$$

$\frac{C_{As}}{C_{Ab}} \approx 1$, indicates no or negligible external mass transfer limitations, as the substrate concentration at the surface is approximately equal to that in the bulk

$\frac{C_{As}}{C_{Ab}} \ll 1$, indicates a very steep concentration gradient in the boundary layer and severe external mass transfer effects



Total effectiveness factor (η_T)

For reactions affected by both internal and external mass transfer restrictions,

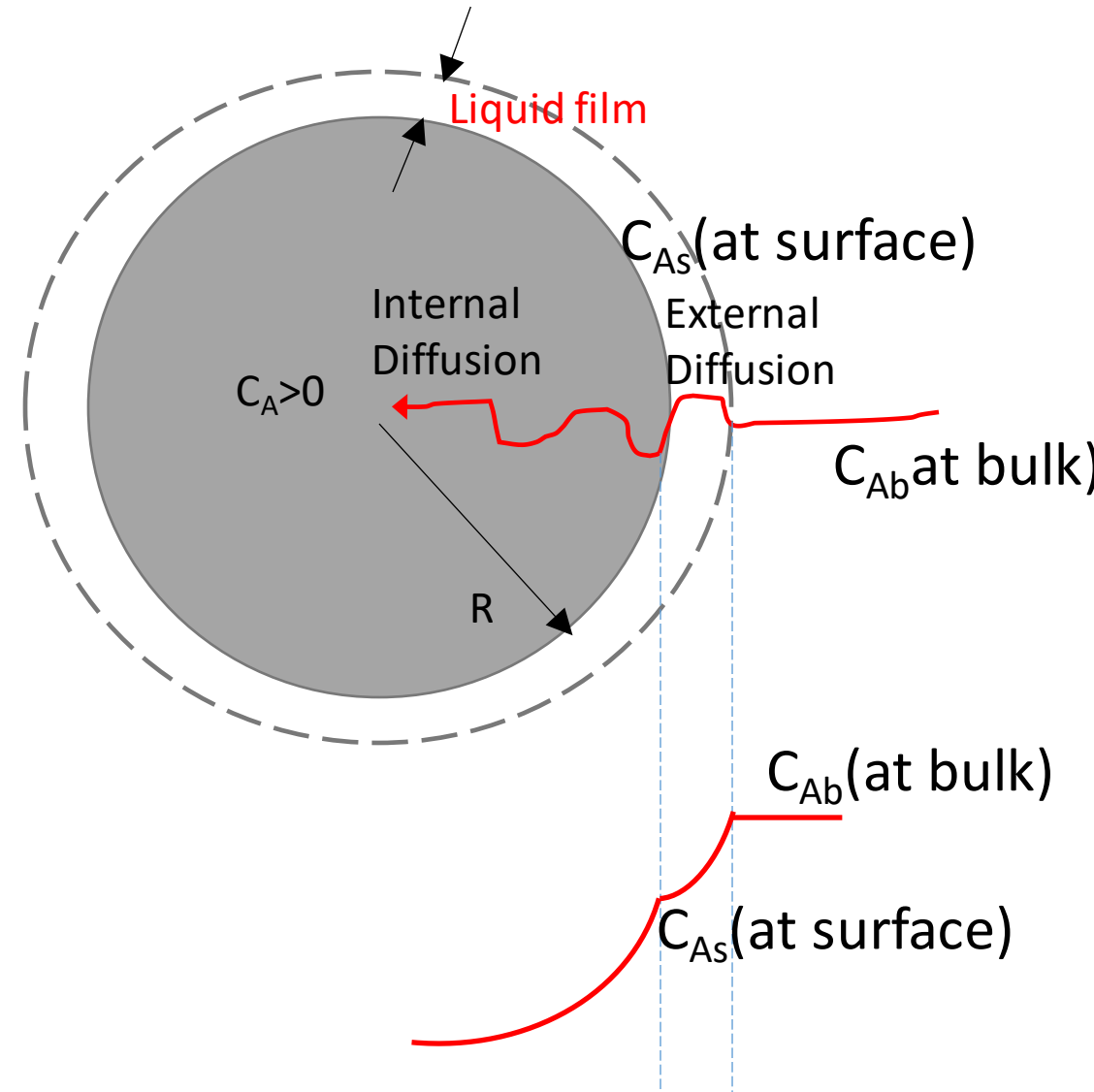
Total effectiveness factor η_T :

$$\eta_T = \frac{r_{A,obs}}{r_{Ab}^*} = \frac{\text{(observed rate)}}{\left(\text{rate that would occur if } C_A = C_{Ab} \text{ everywhere in the particle} \right)}$$

External effectiveness factor (η_e)

$$\eta_e = \frac{r_{As}^*}{r_{Ab}^*} = \frac{\left(\text{rate that would occur if } C_A = C_{As} \text{ everywhere in the particle} \right)}{\left(\text{rate that would occur if } C_A = C_{Ab} \text{ everywhere in the particle} \right)}$$

$$\eta_T = \left(\frac{r_{A,obs}}{r_{As}^*} \right) \left(\frac{r_{As}^*}{r_{Ab}^*} \right) = \eta_i \eta_e$$



Special remarks on zero order reaction

- **For zero-order reactions, $(-r_A = k_0)$**

$$\eta_e = \frac{r_{As}^*}{r_{Ab}^*} = \frac{\left(\begin{array}{c} \text{rate that would occur if } C_A = C_{As} \\ \text{everywhere in the particle} \end{array} \right)}{\left(\begin{array}{c} \text{rate that would occur if } C_A = C_{Ab} \\ \text{everywhere in the particle} \end{array} \right)}$$

- $\eta_e = 1$ as long as $C_{As} > 0$ and $C_{Ab} > 0$

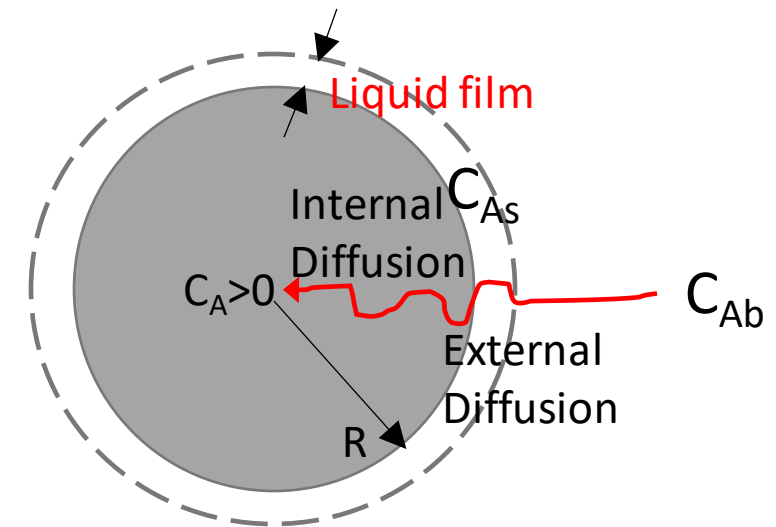
- $\eta_e = 1$ does not imply that an external boundary layer does not exist.

Because r_{As}^* and r_{Ab}^* are independent of C_A

- $\eta_e = 1$ even when there is a reduction in concentration across the external film.

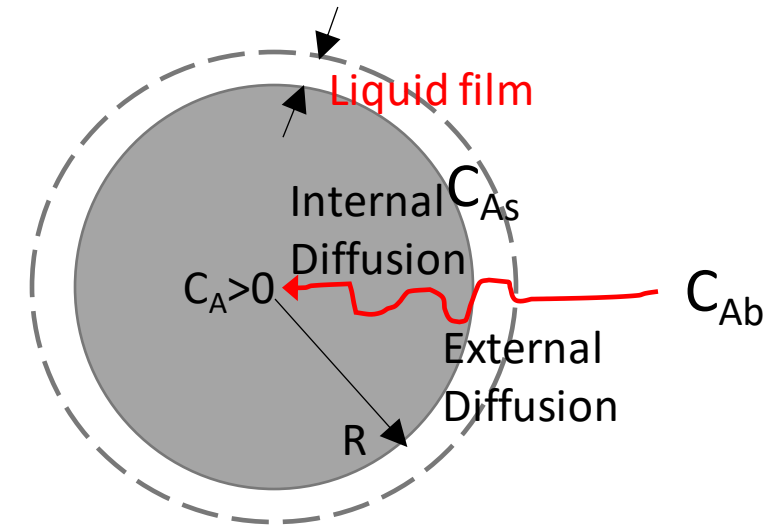
- Furthermore, $\eta_e = 1$ **does not imply that eliminating the external boundary layer** could not improve the observed reaction rate.

- Removing the boundary layer would increase the value of C_{As} , thus establishing a greater driving force for internal mass transfer and reducing the likelihood of C_A falling to zero inside the particle.



Minimizing internal mass transfer effects

- Internal mass transfer effects are eliminated when the internal effectiveness factor (η_i) is equal to 1.
 - Reducing the size of the catalyst (travel path length decrease)
 - Increasing the effective diffusivity D_{Ae} (gel permeability and porosity increase)
 - Increasing the surface substrate concentration C_{As}



Minimizing external mass transfer effects

The rate of external mass transfer (across the external boundary layer)

$$N_A = k_S a (C_{Ab} - C_{As})$$

- Increasing the mass transfer coefficient k_S
 - By increasing the bulk liquid velocity
- Increasing the bulk substrate concentration C_{Ab}

