# Distillation

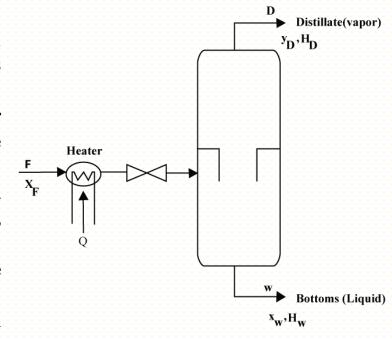
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#### Lecture 3: Flash Distillation

#### **Definition & Purpose:**

- Flash distillation (sometimes called "flash vaporization" or "equilibrium distillation") is a single stage separation technique.
- A liquid mixture feed is pumped at higher pressure through a heater to raise the temperature and enthalpy of the mixture.
- Mixture flows to the flush drum through a throttling valve under reduced pressure, causing the liquid to partially vaporize.
- Once the mixture enters the "flash drum", the liquid and vapor separate.
- The vapor and liquid are allowed to reach equilibrium.
- Vapor and liquid phases are separated and removed from the system



- ✓ Separation by flash vaporization are very common in industry, e.g., petroleum refining.
- ✓ Even when some other method of separation is to be used, it is not uncommon to use a "pre-flash" to reduce the load on the separation itself.
- ✓ When designing a flash drum it is important to provide enough space in the drum for disengagement of liquid and vapor. Drums can be designed as cyclone type.

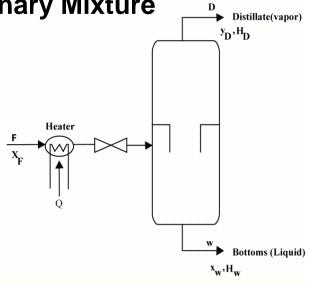
• Consider a binary mixture of components A and B.

• Flow rates, composition and enthalpy of feed are: F,  $z_F$ ,  $H_F$ 

• Flow rates, composition and enthalpy of distillate (top product) are: D, z<sub>D</sub>, H<sub>D</sub>

• Flow rates, composition and enthalpy of bottom product are: W, z<sub>w</sub>, H<sub>w</sub>

• Let Q be the rate of supply of heat to the heat exchanger.



Following are the assumptions:

1. No heat losses to surroundings, 2. Ideal gas behavior for vapor, 3. Perfect mixing

Materials and energy balance equations for a steady-state flash vaporization unit:

**Total material balance:** F = D + W (1)

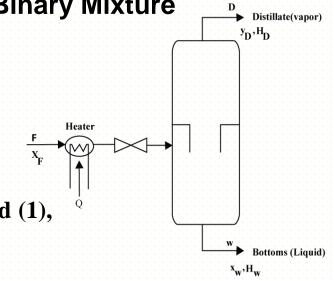
**Component balance:**  $Fz_F = Dy_D + Wx_W$  (2)

**Energy balance:**  $FH_F + Q = DH_D + WH_W$  (3)

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Using equations (2) and (1), we have

$$(D+W)z_F = Dy_D + Wx_W$$

$$\Rightarrow D(z_F - y_D) = W(x_W - z_F)$$

$$\Rightarrow -\frac{W}{D} = \frac{y_D - z_F}{x_W - z_F} \tag{4}$$

Using equations (3) and (1), we have

$$FH_F + Q = (F - W)H_D + WH_W$$

$$\Rightarrow \frac{W}{F} (H_D - H_W) = H_D - \left( H_F + \frac{Q}{F} \right)$$
 (5)

Similarly, using equations (3) and (1) again, we have

$$FH_F + Q = DH_D + (F - D)H_W$$

$$\Rightarrow \frac{D}{F} (H_W - H_D) = H_W - \left( H_F + \frac{Q}{F} \right) \tag{6}$$

Dividing eq (5) by eq (6) we have,

$$-\frac{W}{D} = \frac{H_D - (H_F + Q/F)}{H_W - (H_F + Q/F)}$$
 (7)

We'll consider a different rearrangement of the steady state model. These will be useful in some of the solution methods.

Let the *fraction vaporized* of the feed as f=D/F.

**Material balance can be rewritten as:** 
$$1 = \frac{D}{F} + \frac{W}{F} = f + \frac{W}{F}$$
  $\Rightarrow \frac{W}{F} = 1 - f$  (8)

Component balance can then be written as: 
$$z_F = \frac{D}{F} y_D + \frac{W}{F} x_W = f y_D + (1 - f) x_W$$
 (9)

There are two unknown in eq (9). A second equation between the unknown must be available. This is provided by equilibrium curve or equation based on relative volatility,  $\alpha$ . For binary system:

$$\alpha_{AB} = \frac{y_A / x_A}{y_B / x_B}$$
 where  $x_A = 1-x_A$  and  $y_B = 1-y_A$ 

The above equation can be rearranged to get:

$$y = \frac{\alpha x}{1 + (\alpha - 1)x}$$

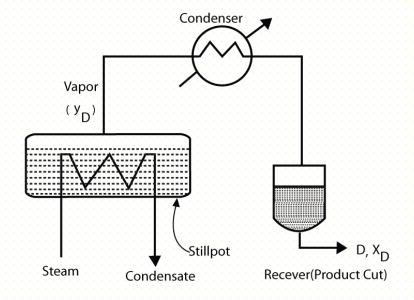
#### **Calculation Techniques**

- > To solve a flash distillation problem, one simultaneously solves the operating and equilibrium equations.
- > Flash calculations can be solved directly, but usually require an iterative solution.
- > Graphical techniques are also common.
- Often, the choice of technique depends on the available form of the equilibrium relationship.

**EXAMPLE:** A mixture of liquid containing 50 mole % n-hexane and 50% n-heptane is subjected to flash distillation at 1 atm total pressure and 40°C to vaporize 50 mol% of feed. The relative volatility of n-hexane in the mixture is 2.36. Calculate the composition of vapor and liquid leaving the flash chamber considering an equilibrium stage.

#### Lecture 4: Batch Distillation

- In batch distillation, a tank is charged with feed and then heated using steam jacket or steam coil.
- Vapor flows overhead, is condensed and collected in a receiver.
- The liquid remaining in the tank is generally called the residue. T
- he composition of the material collected in the receiver varies with time, so the composition of the product is an average of all the material collected.
- Often, the receiver will be emptied or switched several times during a distillation to collect separate cuts of product.



A batch process is inherently dynamic -- it cannot be modeled steady state.

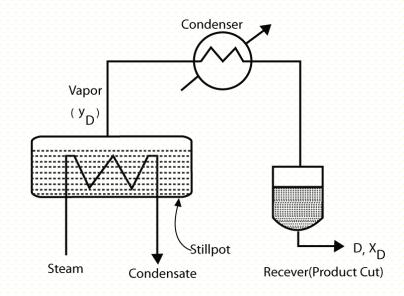
Batch distillation can be conducted with or without reflux. When reflux is used, any of several different operating *policies* may be used -- you might use a constant reflux rate, you might vary it, etc.

#### **Batch distillation is most common:**

- in small capacity plants
- when feed or products vary widely and frequently (as in specialty chemical production)
- for test runs on new products
- when the feed is the result of batch processing
- when the process requires frequent cleaning which would interrupt continuous processing

We want to consider one main variant -- without reflux. Other variant --with reflux will be considered later.

Batch distillation without reflux is often called differential distillation. Because there is no reflux, the vapor product is assumed in equilibrium with the liquid residue in the tank at any given time.



Let L= number of moles of liquid in still pot at any time t

x = mol fraction of more volatile component A

D = moles of condensate accumulated

y\* = concentration of equilibrium vapor

Differential mass balance is as follows:

Total material balance: -dL = dD (1)

Component A balance:  $-d(Lx) = y^* dD$ 

 $\Rightarrow$  -Ldx - x dL = y\* dD



$$-Ldx + x dD = y^* dD$$

$$\Rightarrow$$
 -Ldx = (y\*-x) dD

Now again using eq.1

$$-Ldx = (y^*-x) dL$$

$$\Rightarrow \frac{dL}{L} = \frac{dx}{(y^* - x)}$$

If F = amount of feed, moles

 $z_F$  = concentration of feed

W = moles of residue

 $x_W$  = concentration of more volatiles in the residue Then,

Vapor ( y<sub>D</sub>)

Steam

Condensate

Condenser

D, X<sub>D</sub>

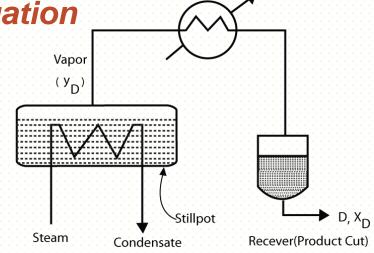
Recever(Product Cut)

$$\int_{F}^{W} \frac{dL}{L} = \int_{z_{F}}^{x_{W}} \frac{dx}{(y^{*}-x)} \qquad \Longrightarrow \ln \frac{F}{W} = \int_{x_{W}}^{z_{F}} \frac{dx}{(y^{*}-x)}$$

This is the *Rayleigh Equation* which relates the amount of residue to the composition.

$$\ln \frac{F}{W} = \int_{x_W}^{z_F} \frac{dx}{(y^* - x)}$$
 Rayleigh Equation

- If equilibrium data (x-y\*) are available in tabular form, graphical integration of the RHS is possible
- If algebraic relation between x and y is available then analytical integration is possible.



Condenser

**Example** 
$$y^* = \frac{\alpha x}{1 + (\alpha - 1)x}$$

$$\ln \frac{F}{W} = \int_{x_W}^{z_F} \frac{dx}{\left(\frac{\alpha x}{1 + (\alpha - 1)x} - x\right)} = \frac{1}{\alpha} \ln \frac{z_F}{x_W} \left(\frac{1 - x_W}{1 - z_F}\right) + \ln \left(\frac{1 - x_W}{1 - z_F}\right) \qquad \qquad \ln \frac{Fz_F}{Wx_W} = \alpha \ln \frac{F}{W} \left(\frac{1 - z_F}{1 - x_W}\right)$$

#### More convenient form

$$\ln \frac{Fz_F}{Wx_W} = \alpha \ln \frac{F}{W} \left( \frac{1 - z_F}{1 - x_W} \right)$$

Average conc. (y<sub>D,avg</sub>) of the accumulated distillate can be obtained by material balance:  $F z_F = D y_{D,avg} + W x_W$  and F = D + W

**EXAMPLE:** A liquid mixture of 150 mol containing 40 mole% n-hexane and 60 mole% n-heptane is to be batch-distilled at 1 atm total pressure.

- (a) If 50 mol is distilled, what is the average composition of the distillate and the composition of the liquid left in the still?
- (b) If the accumulated vapor is 90% n-hexane, calculate the amount of distillate. The relative volatility of the n-hexane in the mixture is 2.36.

**SOLUTION:** (a) Given, F = 150 mol,  $Z_F = 0.4$ , Distillate, D = 50, W = 100 mol

100 mol, 
$$y_{D, avg}$$
=?

$$FZ_F = Dy_{D,avg} + Wx_W$$





→ Composition of the Distillate