

Multimessenger constraints on outflows from neutron star mergers

A thesis submitted
in partial fulfillment for the award of the degree of

Master of Science

in

Astronomy and Astrophysics

by

B.S.Bharath Saiguhan



**Department of Earth and Space Sciences
Indian Institute of Space Science and Technology
Thiruvananthapuram, India**

May 19, 2021

Certificate

This is to certify that the thesis titled *Multimessenger constraints on outflows from neutron star mergers* submitted by **B.S.Bharath Saiguhan**, to the Indian Institute of Space Science and Technology, Thiruvananthapuram, in partial fulfillment for the award of the degree of **Master of Science in Astronomy and Astrophysics** is a bona fide record of the original work carried out by him/her under my supervision. The contents of this thesis, in full or in parts, have not been submitted to any other Institute or University for the award of any degree or diploma.

Dr. Resmi Lekshmi
Designation

Name of Department Head
Designation

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This thesis is dedicated to ...

Acknowledgements

I acknowledge ...

B.S.Bharath Saiguhan

Abstract

Abstract here.

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Abbreviations

SGRB Short Gamma-Ray Burst

Nomenclature

m Mass of the object
 c Velocity of light

Chapter 1

Introduction

1.1 Outflows from BNS Mergers

Due to the joint electromagnetic and gravitational wave detection of the binary neutron star merger event GW1701817 (see Abbott et al. 2017), there has been renewed interest in SGRBs. Specifically, this detection gives credence to the claim that the central engines of SGRBs are binary neutron star mergers (see Narayan, Paczynski, and Piran 1992). However, there are other aspects of the process that are not as clear. Specifically, several aspects of GW170817 have not been completely explained. The main concerns are as follows Lazzati 2020:

- The outflow of GRB170817A was lower in energy than a typical cosmological SGRB, by a factor of $10^4 - 10^5$, even though the event was one of the closest GW events recorded, at a distance of ~ 40 Mpc. This could be due to two factors :
 - The structured jet was off-axis with respect to the observer.
 - The internal engine powering this SGRB was intrinsically less energetic, and differs from the one observed in other typical SGRBs.
- A clear consensus has not been reached on how the gamma-ray prompt emission was produced. The uncertainty partly comes from the fact that the various delays involved before the prompt emission is observed are not accurately constrained. Models which have been considered include :
 - The structured outflow model, characterised by functions for the Lorentz factor and the energy per unit solid angle, both of which vary with the

angle made with the polar jet axis (θ). This model produces detectable signals even at moderately large off-axis angles.

- The shock breakout model, wherein the leading edge of the wind emits the prompt emission as it breaks out of the cocoon of nuclear matter ejected before the jet was launched. This model has been shown to explain the energetics and spectrum of the prompt emission, although it does require a setup in which the wind is fast enough so that it can reach a large enough distance at breakout.

More light can be shed on these questions by observing more such SGRBs, using both the gravitational wave (GW) and electromagnetic (EM) windows. However, the possibility of joint detections are slim, due to the fact that the EM observations are highly dependent on the viewing angle of the system with respect to the observer (due to relativistic beaming), whereas GW signal amplitudes depend on the distance to the event (see Saleem 2020).

Given that this is the case, it would be expedient to look for constraints on the structure parameters of various models. Furthermore, it would be useful to develop models which are resilient to non-detections, and can produce constraints on the parameters using even upper limits on the flux/fluence observed by the various EM follow-up satellites, such as INTEGRAL, Fermi or Swift.

1.1.1 Modelling outflows from BNS Mergers

As mentioned before, the electromagnetic follow-up of the binary neutron star merger event GW170817 helped measure the various time delays between the time of the GW signal trigger (which roughly is the merger time itself) and the time the gamma-ray signals were picked up. This time delay is denoted $\Delta t_{GW-\gamma}$, and was around 1.75 seconds for this event. The components which make up this delay are as follows Lazzati 2020:

- **Engine Delay** – this is the delay due to a transition mechanism in the central engine which powers the jet (such as a metastable, fast spinning neutron star collapsing into a black hole when its rotation period increases; this process can take years) or due to the time elapsed in amplifying the magnetic field to a

value large enough for jet launching (this process is significantly faster, taking only seconds). This is denoted by Δt_{eng} .

- **Wind Delay** – this is simply a delay in the launching of a non-relativistic wind due to the neutron-rich matter from the progenitor(s) being tidally shredded. For this reason, it can be *negative* as well, since the tidal shredding can occur before the merger itself. This is denoted as Δt_{wind} .
- **Breakout Delay** – if the wind is ejected before the jet, then the latter will have to propagate through the former. This happens at a sub-relativistic speed, whereas the GW signal travels at a relativistic speed. The delay due to this crossing is the breakout delay, and is denoted Δt_{bo} . During this time, jet-wind interactions cause the development of a structured outflow that maintains a bright core but also has energetic wings at large polar angles.
- **Photospheric Delay** – once the jet has crossed the wind, it still needs to propagate out to the photospheric radius, where the outflow becomes transparent and the prompt gamma-ray emission is radiated. The delay from the breakout radius to the photospheric radius is Δt_{ph} . This is given by (for GW170817):

$$\Delta t_{ph} \sim \frac{R_{ph}}{c\Gamma^2} = 1.4 \frac{R_{ph}}{2 \times 10^{12} \text{ cm}} \left(\frac{7}{\Gamma} \right)^2 \text{ s} \quad (1.1)$$

- **Dissipation Delay** – this is a requirement in some models, such as the internal shock synchrotron model, wherein the outflow needs to travel to the internal shock radius before the bulk energy of the flow is dissipated and turned into radiation. The time required to get to this point after crossing the photospheric radius is the dissipation delay, denoted Δt_γ

Several attempts to constrain the various time delay components have been made. However, except for relative comparisons, no conclusions have been arrived upon. For example, one can only say that the photospheric delay is the major component out of all the delays, and that wind delay (if non-zero) has to be lesser than the jet delay, so that the jet catches up to the wind and the jet-wind interaction generates the structured outflow. Fig. 1.1 summarises these delays in the broader context.

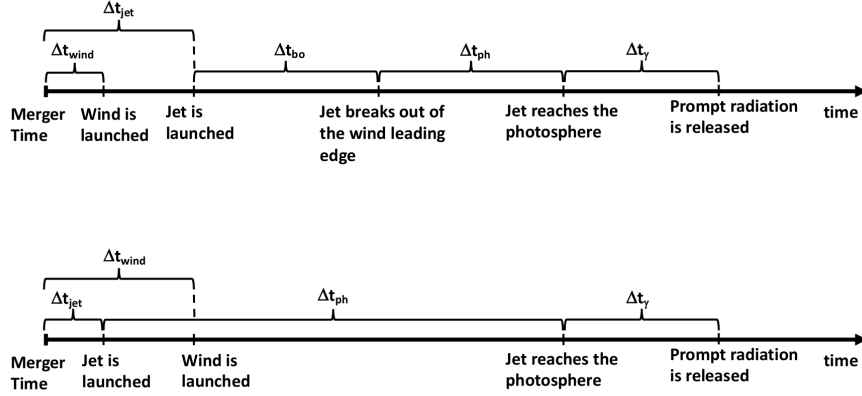


Figure 1.1: Two possible scenarios for the relative positioning of the delays in time, which contribute to $\Delta t_{\text{GW}-\gamma}$. Owing to the requirement of a structured outflow, GW170817 possibly follows the top timeline. The relative contributions of the various delays are debated, but it is agreed that $\Delta t_{\text{wind}} < \Delta t_{\text{jet}} \ll 1$ s, $\Delta t_{\text{bo}} \ll 1$ s, $\Delta t_{\gamma} \sim 0$ and $\Delta t_{\text{ph}} \sim \Delta t_{\text{GW}-\gamma}$.

Due to the uncertainties in the delay terms, several models for the jet can explain the energetics and observed structure. Numerical simulations are also unequivocal about their favouring of one model over the other (see Shibata and Hotokezaka 2019). Some models try to explain the *apparent* structure of the jet, which are the observables seen by a particular observer at a particular viewing angle. Other models are used to explain the *intrinsic* structure, such as the polar angle variation of the bulk Lorentz factor and the energy across the solid angle, in the jet co-moving frame. See Salafia et al. 2015 for a detailed discussion of the differences between the two structures. Some of the models considered are described below (see also Figs. 1.2 and 1.3):

- Top-hat – This model, as used in M. Saleem et al. 2020, assumes that the bulk Lorentz and energy functions drop to zero beyond some cutoff angle, θ_j . Below this threshold, the functions are at their respective on-axis values.
- Gaussian – This model is widely used, in some contexts to explain the apparent jet structure (by Hayes et al. 2020), and in others the intrinsic jet structure (by M. Saleem et al. 2020). The former is simply given by $y_{GJ}(\theta) = e^{-\frac{1}{2}(\frac{\theta}{\theta_{\sigma}})^2}$, since the authors consider only the apparent jet structure, as explained above and θ_{σ} is a structure parameter which is inferred by the authors’ Bayesian inference. In the latter, as the authors consider the intrinsic jet structure, they assume

that $\Gamma\beta(\theta) = \Gamma_0\beta_0 \exp(-\theta^2/2\theta_c^2)$ and that $\epsilon(\theta) \propto \exp(-\theta^2/\theta_c^2)$ ¹, and derive the observed properties (see below).

- **Power Law** – This model is used by Hayes et al. 2020 to explain the apparent structure of the jet, assuming that any variation in the energy is simply because of relativistic beaming and the jet being viewed off-axis. It is given using the shape function $y(\theta)$ (which is multiplied with the on-axis isotropic equivalent energy $E_{iso,0}$ to give $E_{iso}(\theta)$ ²):

$$y(\theta) = \begin{cases} 1, & 0 \leq \theta \leq \theta_c, \\ (\theta/\theta_c)^{-2}, & \theta_c < \theta \leq \theta_j, \\ 0, & \theta_j < \theta \end{cases} \quad (1.2)$$

Here θ_c and θ_j are simply structure parameters, inferred using Bayesian methods.

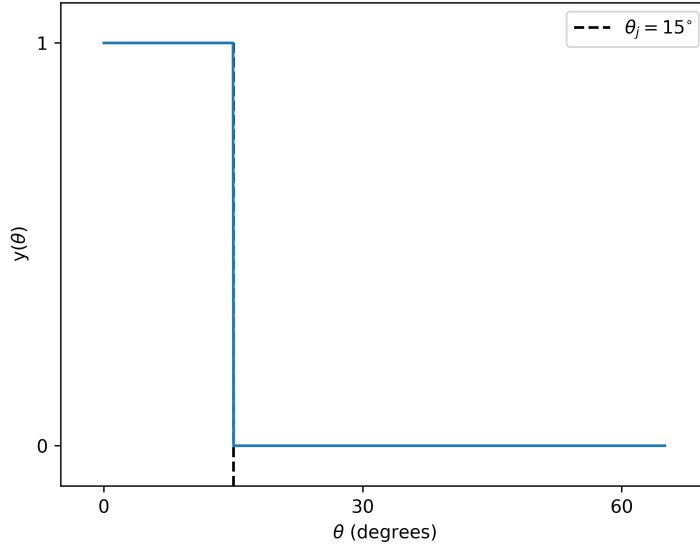


Figure 1.2: Functional form of the tophat jet structure model, as considered in M. Saleem et al. 2020. The dashed line denotes the jet angle $\theta_j = 15^\circ$.

¹This is the normalised energy profile function. The normalisation constant is estimated by the condition $2\pi \int d(\cos \theta) \epsilon(\theta) = E_{tot.,\gamma}$, where $E_{tot.,\gamma}$ is the total energy in gamma-rays.

²Using the equation $E_{iso}(\theta_v) = E_{iso,0} \cdot y(\theta_v)$

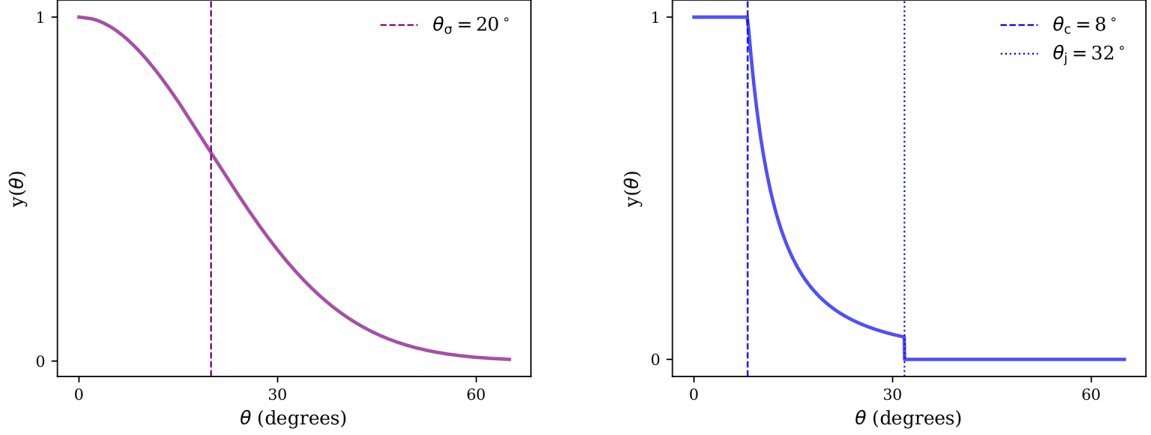


Figure 1.3: Functional forms of the jet structure models, as considered by Hayes et al. 2020. (Left) The gaussian jet structure with a width $\theta_\sigma = 20^\circ$, also marked by the dashed line. (Right) The power-law structure with a core angle $\theta_c = 8^\circ$ and a jet angle $\theta_j = 32^\circ$.

In order to compute the observed structure given the intrinsic structure, following Granot et al. 2002 we start off by considering the emission profile of a point source moving at some angle with the observer, essentially rendering this scenario off-axis. This will affect the prompt jet emission, as well as the initial afterglow, and so warrants careful analysis. Now, let the initial jet opening angle be θ_0 and let the observer be at an angle θ_{obs} . In general, for a point source moving at any angle θ with respect to the observer, the observed flux is given by :

$$F_\nu = \frac{L'_{\nu'}}{4\pi d_L^2} \left(\frac{\nu}{\nu'} \right)^3 = \frac{1+z}{4\pi d_L^2} \frac{L'_{\nu'}}{\gamma^3 (1 - \beta \cos \theta)^3} \quad (1.3)$$

Here, $L'_{\nu'}$ and ν' are the jet comoving frame spectral luminosity and frequency, d_L is the luminosity distance, $\gamma = (1 - \beta^2)^{-1/2}$ is the jet Lorentz factor. If t and ν are the observed time and frequency for an observer at θ , and t_0 and ν_0 are those for an observer on the axis, then:

$$\frac{t_0}{t} = \frac{\nu}{\nu_0} = \frac{(1 - \beta)}{(1 - \beta \cos \theta)} \equiv a \approx \frac{1}{(1 + \gamma^2 \theta^2)} \quad (1.4)$$

And finally putting Eq. 1.4 into Eq. 1.3 and expanding using a Taylor series approximation upto the leading order:

$$F_\nu(\theta_{obs}, t) = a^3 F_{\nu/a}(0, at) \quad (1.5)$$

This gives us a handle on how to relate observed off-axis quantities to the on-axis ones. Furthermore, this enables us to go from an intrinsic structure to an observed one, which is what was required.

1.2 Outflows from NSBH Mergers

The main difference in the NSBH merger pathway to SGRBs, compared to the case of BNS mergers, is that though there is theoretical and simulational support for the launching of SGRB jets from the merger of a neutron star and a black hole of appropriate mass (see for example Ruiz et al. 2020, Shibata and Hotokezaka 2019, Francois Foucart 2020), there has not been strong observational evidence for the same. In the first half of the third observing run of the LVC (also known as O3a), there have been several triggers which have been reportedly confident NSBH triggers. However, there were no counterpart EM signals picked up, which decreases the credibility of NSBH mergers as the progenitors of SGRBs.

The electromagnetic component from NSBH mergers, is largely decided based on the amount of mass left post-merger, outside the horizon of the black hole. This decides how much matter participates in the subsequent processes, which may be the rapid neutron-capture process which gives rise to the kilonova signal or the magnetic field amplification process via the Magneto-Rotational Instability (MRI) which leads to a SGRB jet.

Qualitatively, for a binary where the neutron star is treated as a test mass and the black hole’s spin is aligned with the orbital angular momentum of the binary, the innermost-stable circular orbit radius r_{ISCO} scales as $r_{ISCO} \sim f(\chi_{BH})GM_{BH}/c^2$ (where f is a function ranging from 1 to 9, decreasing for increasing (prograde) spins; see Bardeen, Press, and Teukolsky 1972) and the radius at which the tidal disruption of the neutron star occurs, r_{dis} scales as $r_{dis} \sim k(M_{BH}/M_{BNS})^{1/3}R_{NS}$ (where k is a constant with a dependence on the black hole spin and the equation of state). Only requiring that $r_{dis} \gtrsim r_{ISCO}$, as a rough requirement for disruption to occur before the neutron star plunges into the black hole, leads to the conclusion that (a.) low-mass black holes (b.) larger NS radii (c.) higher prograde black hole spins favour disruption. This is seen from Fig. 1.7 as well. However, for actual quantitative results simulations need to be performed such the effect of the various components in the problem are correctly taken into account. As seen from the literature, wherein such general-relativistic magnetohydrodynamic simulations are carried out, the matter left

over post-merger heavily depends on (for a summary, see Fig. 1.6):

- **The mass ratio of the system.** This is defined as $q = M_{BH}/M_{NS}$ so that $q > 1$ always. Fully general relativistic, magnetohydrodynamic simulations (such as Ruiz et al. 2020) show that in cases where the mass ratio is 3:1, regardless of the neutron spin, a collimated outflow is observed, whereas the same is not realised in cases where the mass ratio is 5:1 or higher.
- **The spin of the components of the system.** In geometrized units (where $G = c = 1$), these are prescribed in terms of a_{BH}/M_{BH} or a_{NS}/M_{NS} , and whether these two spins align (prograde) or are anti-aligned (retrograde) decides whether the neutron star would be tidally disrupted, and hence participate in the processes mentioned previously, or not. Via simulations, it is seen that the more the prograde spin of the neutron star, the farther out the neutron star is tidally disrupted, albeit this is only observed for the case of $q = 3:1$ (comparing say, Figs. 1.4 and 1.5). Also, this leads to long tidal tails, which produces a baryon-loaded environment and thus the magnetic field of the tidally disrupted matter must overcome the baryon ram pressure to launch the jet. This process hence delays the launching of the jet.

Aside from the SGRB jet, which requires magnetic field amplification (via MRI) as well as thermal pair production (from the disk remnant) followed by the Blandford-Znajek process, there is a possibility that NSBH mergers can produce kilonovae signatures. For this, the dynamically ejected mass has to be between $10^{-4.5} - 10^{-2}(M_{NS}/1.4M_{\odot})M_{\odot}$ (see Ruiz et al. 2020 for more details), and this will lead to kilonovae potentially detectable by the Large Synoptic Survey Telescope (LSST).

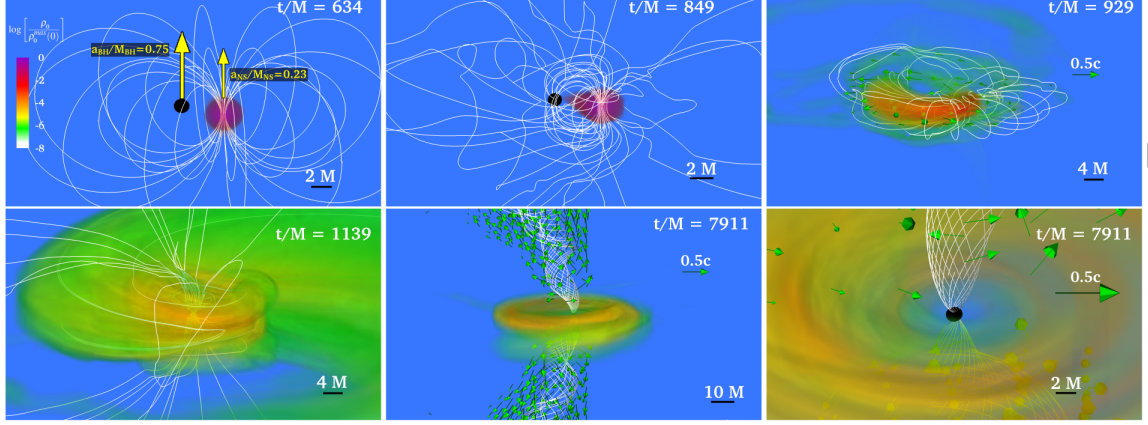


Figure 1.4: Volume rendering of the rest mass density (ρ_0) (in log scale), normalized to the NS maximum value $\rho_0 = 8.92 \times 10^{14} (1.4 M_\odot / M_{NS})^2 \text{ g/cm}^3$, for particular times for a magnetized neutron star, with $q = 3:1$ and a prograde NS spin of 0.23. Top three panels highlight the inspiral and the tidal disruption, whereas the bottom three panels highlight the appearance of the magnetically-driven jet. White lines denote the magnetic field, arrows denote the fluid velocity and the BH's apparent horizon is the black sphere. Here $M = 2.5 \times 10^{-2} (M_{NS} / M_{1.4 M_\odot}) \text{ ms} = 7.58 (M_{NS} / M_{1.4 M_\odot}) \text{ km}$ (in geometrized units). From Ruiz et al. 2020.

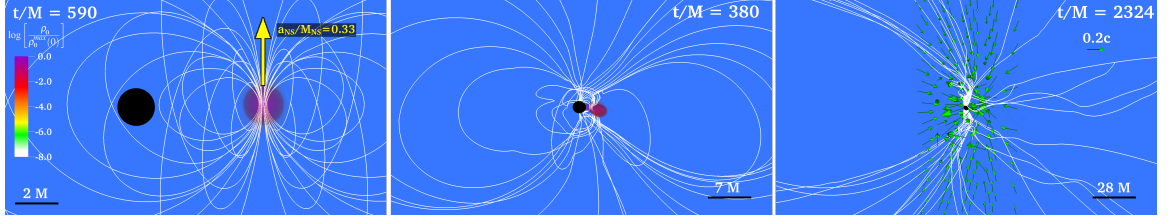


Figure 1.5: Similar to Fig. 1.4, however with the NS spin being 0.33, the BH spin being 0 and $q = 5:1$. In this case, no strong collimation of the magnetic field is observed from the merger remnant, and so a magnetically-driven jet is also not observed. From Ruiz et al. 2020.

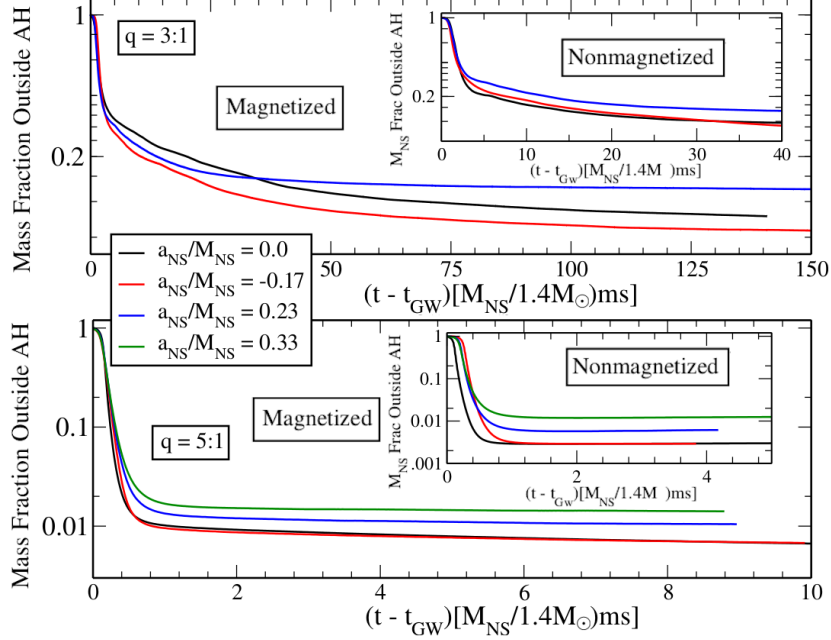


Figure 1.6: Fraction of rest-mass of the NS outside the apparent horizon of the black hole as a function of coordinate time, for the various configurations considered in Ruiz et al. 2020. The inset figures report the same for non-magnetized cases, and the coordinate time is shifted such that the merger time coincides with 0.

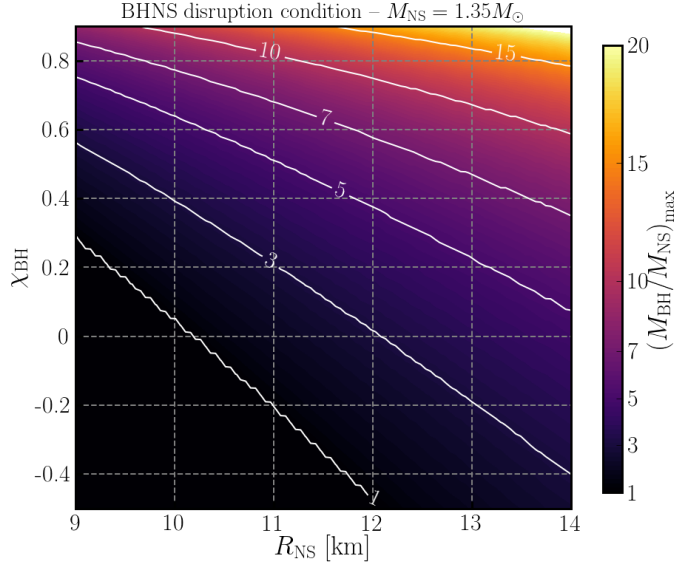


Figure 1.7: Maximum value of the mass-ratio (M_{BH}/M_{NS}) for which a NSBH system disrupts, as a function of the neutron star radius R_{NS} , and the aligned component of the dimensionless black hole spin χ_{BH} , assuming $M_{NS} = 1.35M_{\odot}$. Results for other neutron star masses can be obtained by rescaling considering the disruption condition at constant compaction $C_{NS} = GM_{NS}/R_{NS}c^2$. From Francois Foucart 2020.

1.2.1 Modelling outflows from NSBH Mergers

As mentioned before, the outflows from NSBH mergers depend on the amount of mass left outside the event horizon post-merger. In the work done by Francois Foucart, Hinderer, and Nissanke 2018, the authors consider a suite of 75 numerical relativity simulations of NSBH mergers over the parameter space $\mathcal{Q} \in [1, 7]$, $\chi_{BH} \in [-0.5, 0.97]$, $C_{NS} \in [0.13, 0.182]^3$ and fit the results for the *remnant mass* M_{rem} (sometimes also denoted as M_{out}), as a function of the binary parameters (masses, spins of the components, tidal deformability of the neutron star etc). This fit is given as follows:

$$M_{\text{out}} = M_{NS}^b \cdot \max \left(\alpha \frac{1 - 2\rho}{\eta^{1/3}} - \beta \hat{R}_{\text{ISCO}} \frac{\rho}{\eta} + \gamma, 0 \right)^\delta \quad (1.6)$$

where:

- The baryonic mass of the neutron star is given by the equation

$$M_{NS}^b = M_{NS} \left(1 + \frac{0.6C_{NS}}{1 + 0.5C_{NS}} \right)$$

- The tidal deformability of the neutron star is given by Λ_{NS} and $\rho = (15\Lambda_{NS})^{-1/5}$. It is also related to the compactness of the neutron star via the C-Love relation (see Yagi and Yunes 2017):

$$C_{NS} = \sum_{k=0}^2 a_k (\ln \Lambda_{NS})^k \quad (1.7)$$

where $a_0 = 0.360$, $a_1 = -0.0335$, $a_2 = 0.000705$.

- η is the symmetric mass ratio, given by $\eta = \frac{\mathcal{Q}}{(1 + \mathcal{Q})^2}$.
- $\hat{R}_{\text{ISCO}} = c^2 R_{\text{ISCO}} / GM_{BH}$ is the normalized ISCO radius for a spinning black hole, given in Bardeen, Press, and Teukolsky 1972 as :

$$\begin{aligned} \hat{R}_{\text{ISCO}} &= 3 + Z_2 - \text{sgn}(\chi_{BH}) \sqrt{(3 - Z_1)(3 + Z_1 + 2Z_2)} \\ &\hookrightarrow Z_1 = 1 + (1 - \chi_{BH}^2)^{1/3} [(1 + \chi_{BH})^{1/3} + (1 - \chi_{BH})^{1/3}] \\ &\hookrightarrow Z_2 = \sqrt{3\chi_{BH}^2 + Z_1^2} \end{aligned} \quad (1.8)$$

³Here, $\mathcal{Q} = M_{BH}/M_{NS}$ is the mass-ratio, $\chi_{BH} = c|\mathbf{S}|/GM_{BH}^2$ is the effective spin of the black hole and $C_{NS} = GM_{NS}/R_{NS}c^2$ is the compactness of the neutron star.

- $(\alpha, \beta, \gamma, \delta) \equiv (0.308, 0.124, 0.283, 1.536)$ are the fit coefficients.

Similarly, Kawaguchi et al. 2016 fit to the results of 45 numerical relativity simulations over the parameter space $\mathcal{Q} \in [3, 7]$, $\chi_{\text{BH}} \in [0, 0.90]$, $C_{\text{NS}} \in [0.138, 0.180]$. This fit produces a formula for the *dynamic* mass M_{dyn} , which is the unbound mass ejected at the time of disruption, in terms of the binary parameters. This fit is given as follows:

$$\frac{M_{\text{dyn}}}{M_{\text{NS}}^b} = \max \left\{ a_1 Q^{n_1} (1 - 2C_{\text{NS}}) C_{\text{NS}}^{-1} - a_2 Q^{n_2} \hat{R}_{\text{ISCO}}(\chi_{\text{BH}}) + a_3 \left(1 - \frac{M_{\text{NS}}}{M_{\text{NS}}^b} \right) + a_4, 0 \right\} \quad (1.9)$$

where the symbols have their usual meanings, and additionally:

$$\begin{aligned} a_1 &= 4.464 \times 10^{-2} & a_2 &= 2.269 \times 10^{-3} \\ a_3 &= 2.431 & a_4 &= -0.4159 \\ n_1 &= 0.2497 & n_2 &= 1.352 \end{aligned}$$

From these two quantities, we can derive the disc mass M_{disc} as :

$$M_{\text{disc}} = \max\{M_{\text{out}} - M_{\text{dyn}}, 0\} \quad (1.10)$$

However, due to the fact that these two fits are derived from simulations over different regions of the input parameter space, care must be taken while applying them together. This is to ensure that $M_{\text{dyn}} \leq M_{\text{out}}$ always, so that the disc mass is non-negative. This validation is performed by considering the ratio $M_{\text{out}}/M_{\text{dyn}}$. Another constraint is imposed, which is motivated by the fact that NSBH simulations carried out by F. Foucart et al. 2019 in the near-equal mass ratio regime found an unbound component no more massive than roughly 30% of the total remnant mass (note that one expects maximal tidal disruption in this regime, given a fast spinning black hole). Thus we set:

$$M_{\text{dyn,max}} = f \cdot M_{\text{rem}} = 0.3 \cdot M_{\text{rem}} \quad (1.11)$$

Additionally, the masses of the other wind ejecta, namely the neutrino-driven and

viscosity-driven wind ejecta, are derived from that of the disc mass:

$$\begin{aligned} M_{\text{vis}} &= \xi_{\text{vis}} M_{\text{disc}} = 0.2 M_{\text{disc}} \\ M_{\nu} &= \xi_{\nu} M_{\text{disc}} = 0.01 M_{\text{disc}} \end{aligned} \quad (1.12)$$

To model the SGRB jet, the procedure of Zhu et al. 2020 is followed. The kinetic energy of the jet is decided by the disc mass and the black hole spin as follows:

$$E_{\text{K,jet}} = \epsilon(1 - \xi_{\text{vis}} - \xi_{\nu}) M_{\text{disc}} c^2 \Omega_H^2 f(\Omega_H) \quad (1.13)$$

where:

- The dimensionless angular velocity at the horizon of the black hole is given by:

$$\Omega_H = \frac{\chi_{BH}}{2(1 + \sqrt{1 + \chi_{BH}^2})} \quad (1.14)$$

- $f(\Omega_H)$ is a high-spin correction factor given by

$$f(\Omega_H) = 1 + 1.38\Omega_H^2 - 9.2\Omega_H^4$$

- ϵ is a fudge factor which depends on the large-scale geometry of the magnetic field, disc aspect ratio and the ratio of the magnetic field energy density to disc pressure at saturation.

In order to set it to a definite value, it is noted that the maximum disc mass cannot exceed the total NS baryonic mass i.e. $M_{\text{disc}} \lesssim 2M_{\odot}$. Also, the spin-dependent factor $\Omega_H^2 f(\Omega_H)$ cannot exceed 0.2 (since $\chi_{BH} \in [-1, 1]$). Furthermore, the most energetic of SGRBs has had a $E_{\gamma,\text{iso}} \sim 7.4 \times 10^{52}$ erg, and if one assumes a 10% conversion efficiency of kinetic to gamma-ray energy along with a typical jet opening angle of 5° , this corresponds to a kinetic energy of $E_{\text{K,jet}} \sim 3 \times 10^{52}$ erg.

Based on this, once can calculate $\boxed{\epsilon \approx 0.015}$.

Using this we can define the structure of the SGRB jet, given by the following equations:

$$\frac{dE(\theta)}{d\Omega} = \frac{E_{\text{K,jet}}}{\pi\theta_{\text{c,E}}^2} e^{-(\theta/\theta_{\text{c,E}})^2} \quad (1.15)$$

$$\Gamma(\theta) = (\Gamma_c - 1)e^{-(\theta/\theta_{c,E})^2} + 1 \quad (1.16)$$

$$E_{\text{iso}}(\theta_v) = \eta \int \frac{\delta^3}{\Gamma} \frac{dE}{d\Omega} d\Omega \quad (1.17)$$

where:

- $\Gamma_c = 100, \theta_{c,E} = 0.1, \theta_{c,\Gamma} = 0.2$. See Salafia et al. 2015 and Barbieri et al. 2019.
- η is the conversion efficiency of gamma-ray energy to kinetic energy, which is traditionally taken to be 10%.
- δ is the Doppler factor, given by

$$\delta = \frac{1}{\Gamma[1 - \beta \cos \alpha_v]}$$

where α_v is the angle between the jet element at (θ, ϕ) and the observer's direction.

Chapter 2

Population Synthesis

Write related work here.

2.1 Summary

Chapter 3

Conclusions

Conclusions here.

Chapter 4

Performance Analysis

4.1 Experimental Setup

4.2 Summary

References

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