

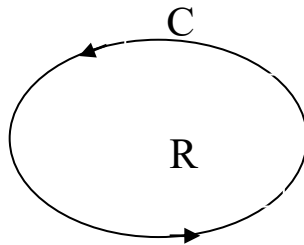
Integral theorems

Green's theorem in the plane

Statement: If R is a closed region in the xy plane bounded by simple closed curve C and M, N are continuous functions of x and y having continuous derivative in R then

$$\oint_C Mdx + Ndy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx dy \quad (\text{Relationship between line integral and area integral})$$

where C is traversed in the positive (counter-clockwise) direction.



Proof:

Suppose

Equation of AEB is $y=Y_1(x)$ and

Equation of AFB is $y=Y_2(x)$

and R is the region bounded by the curve C

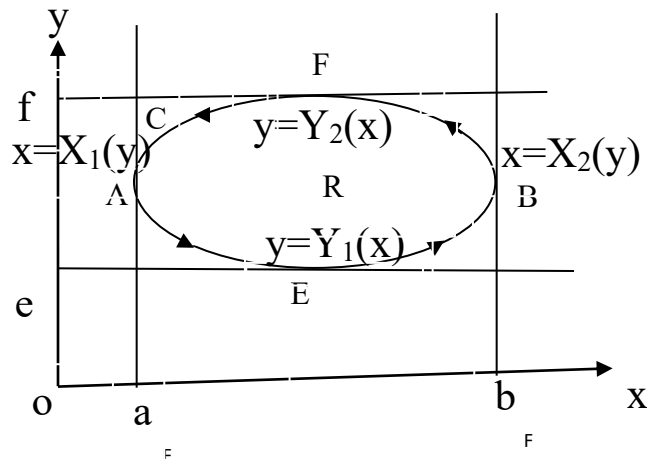


Fig1

$$\begin{aligned}
& \iint_R \frac{\partial M}{\partial y} dx dy \\
&= \int_a^b \left[\int_{y=Y_1(x)}^{y=Y_2(x)} \frac{\partial M}{\partial y} dy \right] dx \\
&= \int_a^b [M(x, y)]_{Y_1(x)}^{Y_2(x)} dx \\
&= \int_a^b [M(x, Y_2(x)) - M(x, Y_1(x))] dx \\
&= - \int_a^b M(x, Y_1(x)) dx - \int_b^a M(x, Y_2(x)) dx \\
&= - \left[\int_a^b M(x, Y_1(x)) dx + \int_b^a M(x, Y_2(x)) dx \right] \\
&= - \oint_C M dx \\
& \oint_C M dx = - \iint_R \frac{\partial M}{\partial y} dx dy
\end{aligned}$$

Again let the equation of the curves EAF and EBF be $x=X_1(y)$ and $x=X_2(y)$.

Now

$$\begin{aligned}
& \iint_R \frac{\partial N}{\partial x} dx dy \\
&= \int_e^f \left[\int_{x=X_1(y)}^{x=X_2(y)} \frac{\partial N}{\partial x} dx \right] dy \\
&= \int_e^f [N(x, y)]_{X_1(y)}^{X_2(y)} dy
\end{aligned}$$

$$\begin{aligned}
 \text{Area} &= \iint_R dx dy \\
 &= \int_0^4 \int_x^{2\sqrt{x}} dy dx \\
 &= \int_0^4 [y]_x^{2\sqrt{x}} dx \\
 &= \int_0^4 (2\sqrt{x} - x) dx = \frac{8}{3}
 \end{aligned}$$

Solution

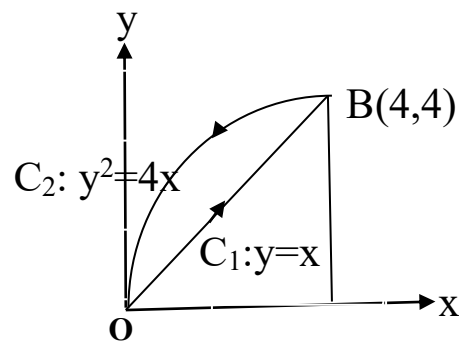


Fig2

$$\begin{aligned}
 \text{Area} &= \iint_R dx dy \\
 &= \frac{1}{2} \oint_C -y dx + x dy \\
 &= \frac{1}{2} \int_{C_1} -y dx + x dy + \frac{1}{2} \int_{C_2} -y dx + x dy, \text{ along } C_2 \quad x = y^2/4, \quad dx = (y/2) dy \\
 &= \frac{1}{2} \int_0^4 -x dx + x dx + \frac{1}{2} \int_4^0 -\frac{y^2}{2} dy + \frac{y^2}{4} dy = \frac{8}{3}
 \end{aligned}$$

Verification of this theorem

Problem-2. Verify Green's theorem for the plane for $\oint_C xydx + x^2dy$ where C is the closed region bounded by $y=x$ and $y=x^2$

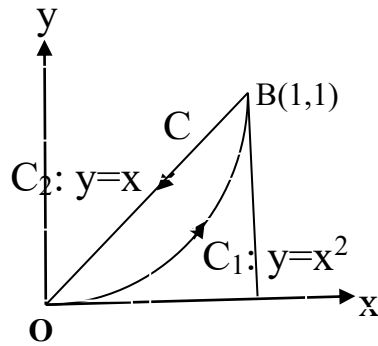


Fig 3

$$\oint_C Mdx + Ndy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx dy$$

$$\begin{aligned} \text{LS} &= \oint_C Mdx + Ndy \\ &= \oint_C xydx + x^2dy \\ &= \oint_{C_1} xydx + x^2dy + \oint_{C_2} xydx + x^2dy \\ &= \int_0^1 xx^2dx + x^2 2xdx + \int_1^0 xx dx + x^2 dx \\ &= 3 \int_0^1 x^3 dx + 2 \int_1^0 x^2 dx \\ &= \frac{1}{12} \end{aligned}$$

$$\begin{aligned} \text{RS} &= \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx dy \\ &= \iint_R (2x - x) dx dy \end{aligned}$$

$$\begin{aligned}
&= \int_0^1 \int_{x^2}^x x dy dx \\
&= \int_0^1 x [y]_{x^2}^x dx \\
&= \int_0^1 x(x - x^2) dx \\
&= \frac{1}{12}
\end{aligned}$$

LS=RS verified

Problem-3. Find the work done in moving a particle along the curve C in the force field $\mathbf{F}=(3x^2-8y^2)\mathbf{i}+(4y-6xy)\mathbf{j}$ where C is the curve $y=x^2$ from (0,0) to (1,1) and the $y^2=x$ from (1,1) to (0,0) using Green,s theorem.

$$\mathbf{F} \cdot d\mathbf{r} = (3x^2-8y^2)dx + (4y-6xy)dy$$

$$\begin{aligned}
\text{Work} &= \int_C \mathbf{F} \cdot d\mathbf{r} = \int_C (3x^2-8y^2)dx + (4y-6xy)dy \\
&= \int_{C_1} (3x^2-8y^2)dx + (4y-6xy)dy + \int_{C_2} (3x^2-8y^2)dx + (4y-6xy)dy
\end{aligned}$$

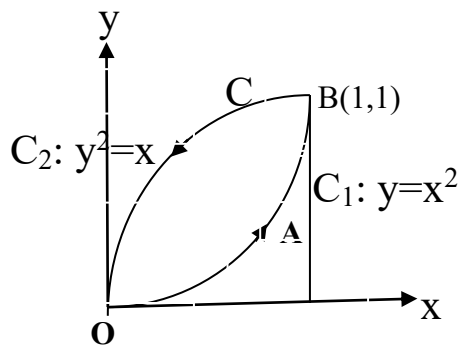


Fig 4

On C_1 , OAB $y=x^2$ so that $dy=2xdx$

$$\begin{aligned}
 \int_{C_1} \mathbf{F} \cdot d\mathbf{r} &= \int_{C_1} (3x^2 - 8y^2)dx + (4y - 6xy)dy \\
 &= \int_0^1 (3x^2 - 8x^4)dx + (4x^2 - 6xx^2)2xdx \\
 &= -1
 \end{aligned}$$

On C_2 BCO $x=y^2$ so that $dx=2ydy$

$$\begin{aligned}
 \int_{C_1} \mathbf{F} \cdot d\mathbf{r} &= \int_{C_1} (3x^2 - 8y^2)dx + (4y - 6xy)dy \\
 &= \int_1^0 (3y^4 - 8y^2)2ydy + (4y - 6y^2y)dy \\
 &= \frac{5}{2}
 \end{aligned}$$

$$\text{Work done} = \int_C \mathbf{F} \cdot d\mathbf{r} = \int_{C_1} \mathbf{F} \cdot d\mathbf{r} + \int_{C_2} \mathbf{F} \cdot d\mathbf{r} = -1 + \frac{5}{2} = \frac{3}{2}$$

Alternative method

This problem can also be done by using Green's theorem

Green's theorem is $\oint_C Mdx + Ndy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dxdy$

$$\text{Work} = \int_C \mathbf{F} \cdot d\mathbf{r} = \int_C (3x^2 - 8y^2)dx + (4y - 6xy)dy \quad M = 3x^2 - 8y^2 \quad N = 4y - 6xy$$

$$\begin{aligned}
 \oint_C Mdx + Ndy &= \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dxdy \\
 &= \iint_R (-6y + 16y) dxdy \\
 &= \iint_R (10y) dxdy \\
 &= 10 \iint_R y dy dx \\
 &= 10 \int_0^1 \int_{x^2}^{\sqrt{x}} y dy dx \\
 &= 10 \int_0^1 \left[\frac{y^2}{2} \right]_{x^2}^{\sqrt{x}} dx
 \end{aligned}$$

$$=10 \int_0^1 \frac{1}{2} (x - x^2) dx$$

$$= \frac{3}{2}$$

C21==A23==B23=====

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Express Green's theorem in the plane in vector form

Green's theorem is $\oint_C Mdx + Ndy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dxdy$

$Mdx + Ndy = (M_i + N_j) \cdot (dx i + dy j) = \mathbf{A} \cdot d\mathbf{r}$

where $\mathbf{A} = M_i + N_j$ and $\mathbf{r} = xi + yj$

$$\nabla \times \mathbf{A} = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ M & N & 0 \end{vmatrix} = -\frac{\partial N}{\partial z} i + \frac{\partial M}{\partial z} j + \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) k$$

$$(\nabla \times \mathbf{A}) \cdot k = \frac{\partial N}{\partial x} - \frac{\partial M}{\partial y}$$

Green's theorem can be written as $\oint_C \mathbf{A} \cdot d\mathbf{r} = \iint_R (\nabla \times \mathbf{A}) \cdot k dR$

$dR = dxdy$

This is for two dimensional case.... curve to region

For three dimensional case.....curve to surface which is known as **Stoke's theorem** (it will be considered next)

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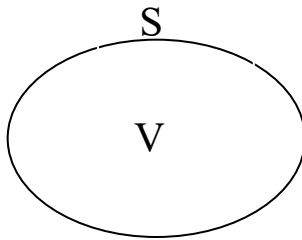
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Gauss divergence theorem

Statement: The surface integral of the normal component of the vector \mathbf{A} taken over a closed surface is equal to the integral of the divergence of \mathbf{A} taken over the volume enclosed by the surface.

If \mathbf{n} be unit outward normal at a point of the boundary of the closed region V and dV be the volume element of the region, then the theorem expresses that

$$\iint_S \mathbf{A} \cdot \mathbf{n} dS = \iiint_V \nabla \cdot \mathbf{A} dV \quad (\text{Relationship between surface and volume integral})$$



Proof:

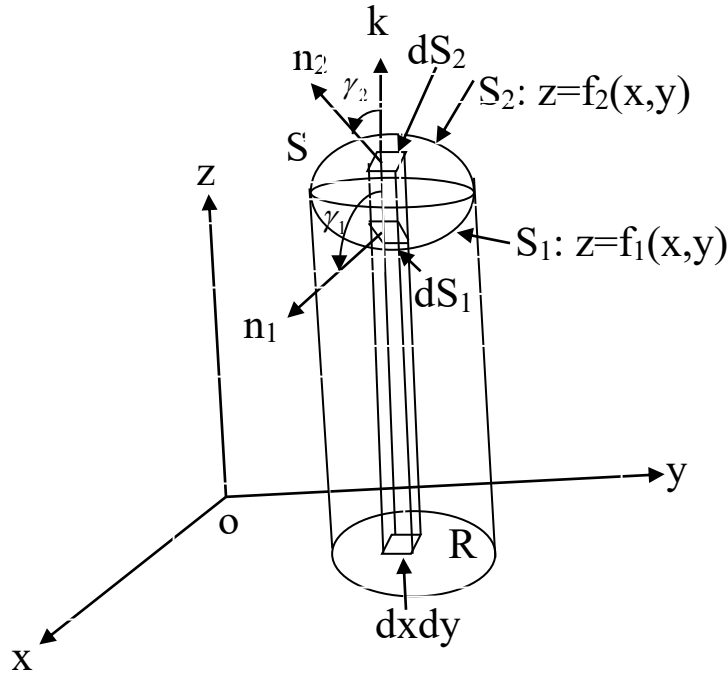


Fig4

If $\mathbf{A} = A_1\mathbf{i} + A_2\mathbf{j} + A_3\mathbf{k}$ then

$$\iint_S \mathbf{A} \cdot \mathbf{n} dS = \iiint_V \nabla \cdot \mathbf{A} dV$$

$$\iint_S (A_1\mathbf{i} + A_2\mathbf{j} + A_3\mathbf{k}) \cdot \mathbf{n} dS = \iiint_V \left(\frac{\partial A_1}{\partial x} + \frac{\partial A_2}{\partial y} + \frac{\partial A_3}{\partial z} \right) dV$$

$$\begin{aligned} \iint_S A_1\mathbf{i} \cdot \mathbf{n} dS + \iint_S A_2\mathbf{j} \cdot \mathbf{n} dS + \iint_S A_3\mathbf{k} \cdot \mathbf{n} dS \\ = \iiint_V \frac{\partial A_1}{\partial x} dV + \iiint_V \frac{\partial A_2}{\partial y} dV + \iiint_V \frac{\partial A_3}{\partial z} dV \end{aligned}$$

Let us suppose that S be a closed surface such that any line parallel to the coordinate axes cuts S in at most two points.

Suppose that

Equation of the lower surface S_1 is $z=f_1(x,y)$ and equation of the upper surface S_2 is $z=f_2(x,y)$

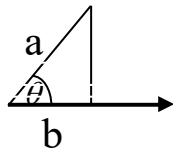
and R is the projection of the surface S on the xy plane

Consider the third integral of the RHS

$$\begin{aligned}
 & \iiint_V \frac{\partial A_3}{\partial z} dV \\
 &= \iiint_V \frac{\partial A_3}{\partial z} dz dy dx \\
 &= \iint_R \left[\int_{z=f_1(x,y)}^{z=f_2(x,y)} \frac{\partial A_3}{\partial z} dz \right] dy dx \\
 &= \iint_R [A_3(x,y,z)]_{z=f_1(x,y)}^{z=f_2(x,y)} dy dx \\
 &= \iint_R [A_3(x,y,f_2) - A_3(x,y,f_1)] dy dx \\
 &= \iint_R A_3(x,y,f_2) dy dx - \iint_R A_3(x,y,f_1) dy dx
 \end{aligned}$$

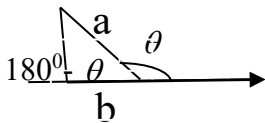
Discussion

When θ is acute



Projection of a is $b = a \cos \theta$

When θ is obtuse

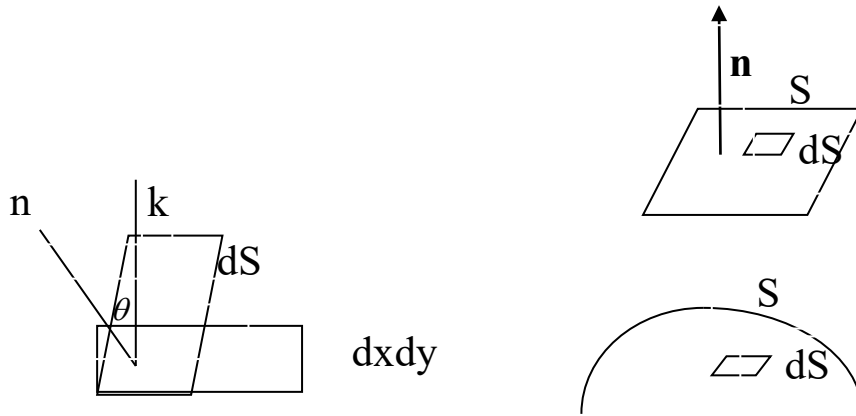


Projection of a is $b = a \cos(180 - \theta) = -a \cos \theta$

We consider the projection on the xy plane

Elementary area in the xy plane is $= dx dy$

The angle between two planes is equal to the angle between their normals



Projection of dS is $dxdy = dS \cos \theta = dS \mathbf{k} \cdot \mathbf{n}$ [$\mathbf{k} \cdot \mathbf{n} = \cos \theta$]

For the upper portion of the surface S_2 , $dxdy = dS_2 \cos \gamma_2 = dS_2 \mathbf{k} \cdot \mathbf{n}_2$ since the outward normal \mathbf{n}_2 to S_2 makes an acute angle γ_2 with \mathbf{k} .

For the lower portion of the surface S_1 , $dxdy = -dS_1 \cos \gamma_1 = -dS_1 \mathbf{k} \cdot \mathbf{n}_1$ since the outward normal \mathbf{n}_1 to S_1 makes an obtuse angle γ_1 with \mathbf{k} .
hence

$$\begin{aligned} \iint_R A_3(x, y, f_2) dy dx &= \iint_{S_2} A_3 \mathbf{k} \cdot \mathbf{n}_2 dS_2 \\ \iint_R A_3(x, y, f_1) dy dx &= - \iint_{S_1} A_3 \mathbf{k} \cdot \mathbf{n}_1 dS_1 \\ \text{Then } \iint_R A_3(x, y, f_2) dy dx - \iint_R A_3(x, y, f_1) dy dx &= \iint_{S_2} A_3 \mathbf{k} \cdot \mathbf{n}_2 dS_2 + \iint_{S_1} A_3 \mathbf{k} \cdot \mathbf{n}_1 dS_1 \\ &= \iint_S A_3 \mathbf{k} \cdot \mathbf{n} dS \end{aligned}$$

$$\iiint_V \frac{\partial A_3}{\partial z} dV = \iint_S A_3 \mathbf{k} \cdot \mathbf{n} dS$$

Similarly $\iiint_V \frac{\partial A_1}{\partial x} dV = \iint_S A_1 \mathbf{i} \cdot \mathbf{n} dS$

And $\iiint_V \frac{\partial A_2}{\partial y} dV = \iint_S A_2 \mathbf{j} \cdot \mathbf{n} dS$

Adding all these we get

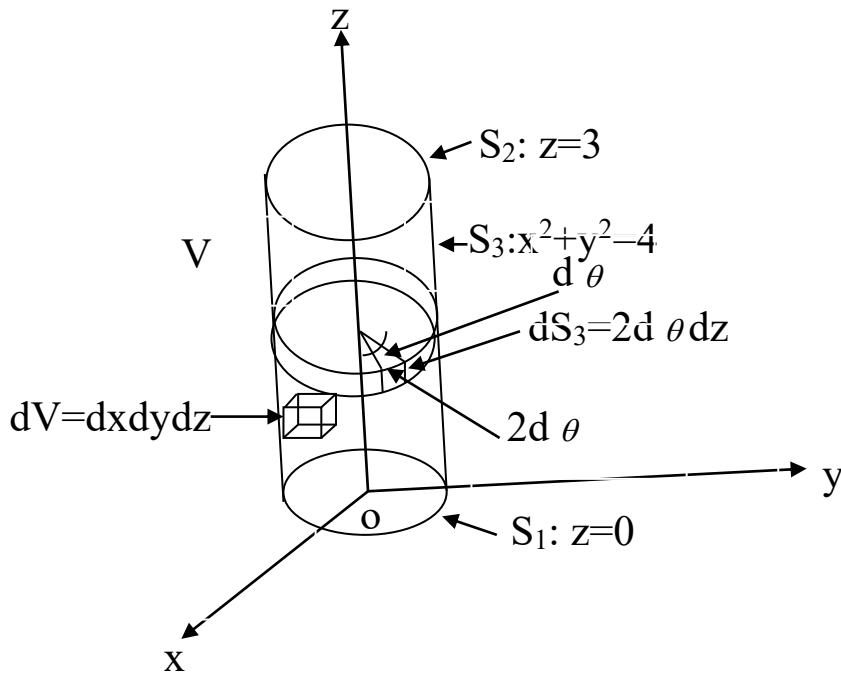
$$\iiint_V \left(\frac{\partial A_1}{\partial x} + \frac{\partial A_2}{\partial y} + \frac{\partial A_3}{\partial z} \right) dV = \iint_S (A_1 \mathbf{i} + A_2 \mathbf{j} + A_3 \mathbf{k}) \cdot \mathbf{n} dS$$

$$\iiint_V \nabla \cdot \mathbf{A} dV = \iint_S \mathbf{A} \cdot \mathbf{n} dS \quad \text{proved}$$

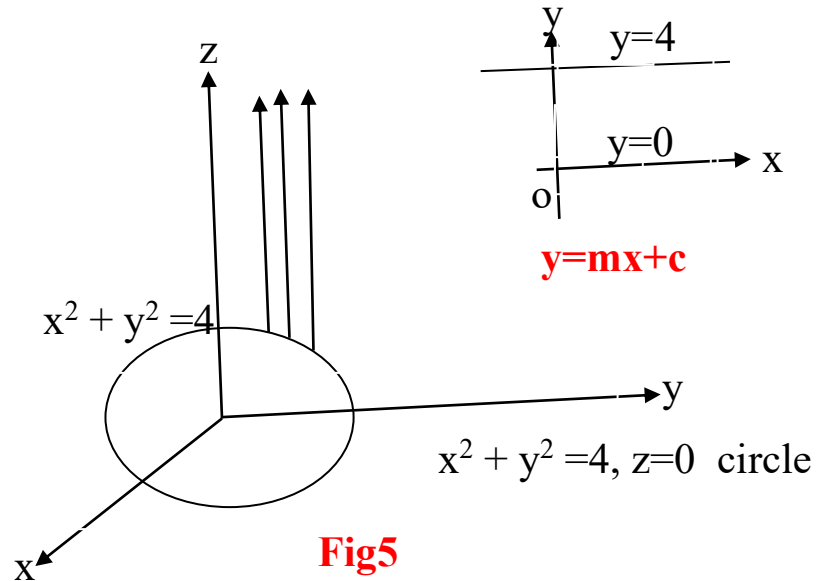
Verification

Problem-4. Verify Gauss divergence theorem for $\mathbf{A} = 4x\mathbf{i} - 2y^2\mathbf{j} + z^2\mathbf{k}$ taken over the region bounded by $x^2 + y^2 = 4$, $z=0$ and $z=3$.

$$\iiint_V \nabla \cdot \mathbf{A} dV = \iint_S \mathbf{A} \cdot \mathbf{n} dS \quad (\text{to be verified})$$



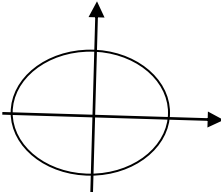
Discussion



$$\begin{aligned}\nabla \cdot \mathbf{A} &= \frac{\partial A_1}{\partial x} + \frac{\partial A_2}{\partial y} + \frac{\partial A_3}{\partial z} \\ &= \frac{\partial(4x)}{\partial x} + \frac{\partial(-2y^2)}{\partial y} + \frac{\partial(z^2)}{\partial z} \\ &= 4 - 4y + 2z\end{aligned}$$

$$\begin{aligned}\text{LS} &= \iiint_V \nabla \cdot \mathbf{A} dV = \iiint_V (4 - 4y + 2z) dV \\ &= \int_{x=-2}^2 \int_{y=-\sqrt{4-x^2}}^{\sqrt{4-x^2}} \int_{z=0}^3 (4 - 4y + 2z) dz dy dx \\ &= \int_{x=-2}^2 \int_{y=-\sqrt{4-x^2}}^{\sqrt{4-x^2}} \left[4z - 4yz + z^2 \right]_0^3 dy dx \\ &= \int_{x=-2}^2 \int_{y=-\sqrt{4-x^2}}^{\sqrt{4-x^2}} (21 - 12y) dy dx \\ &= \int_{x=-2}^2 \left[21y \right]_{-\sqrt{4-x^2}}^{\sqrt{4-x^2}} dx\end{aligned}$$

$$\begin{aligned}
&= \int_{x=-2}^2 \left[42\sqrt{4-x^2} \right] dx \\
&= 2 \int_{x=0}^2 \left[42\sqrt{4-x^2} \right] dx \quad x=2\sin\theta \\
&= 84 \times 4 \int_0^{\frac{\pi}{2}} \sin^2\theta d\theta \\
&= 84 \times 4 \frac{\pi}{4} \\
&= 84\pi
\end{aligned}$$



$$RS = \iint_S \mathbf{A} \cdot \mathbf{n} dS$$

The surface S of the cylinder consists of

S_1 , the plane $z=0$

S_2 , the plane $z=3$

S_3 , the convex surface $x^2+y^2=4$

$$\iint_S \mathbf{A} \cdot \mathbf{n} dS = \iint_{S_1} \mathbf{A} \cdot \mathbf{n} dS_1 + \iint_{S_2} \mathbf{A} \cdot \mathbf{n} dS_2 + \iint_{S_3} \mathbf{A} \cdot \mathbf{n} dS_3$$

On S_1 , $z=0$, $\mathbf{n}=-\mathbf{k}$, $\mathbf{A}=4x\mathbf{i}-2y^2\mathbf{j}$ $\mathbf{A} \cdot \mathbf{n}=0$

Therefore $\iint_{S_1} \mathbf{A} \cdot \mathbf{n} dS_1 = 0$

On S_2 , $z=3$, $\mathbf{n}=\mathbf{k}$, $\mathbf{A}=4x\mathbf{i}-2y^2\mathbf{j}+9\mathbf{k}$ $\mathbf{A} \cdot \mathbf{n}=9$

therefore $\iint_{S_2} \mathbf{A} \cdot \mathbf{n} dS_2 = 9 \iint_{S_2} dS_2 = 9 \times 4\pi = 36\pi$

On S_3 , $x^2+y^2=4$, $\mathbf{n} = \frac{\nabla \phi}{|\nabla \phi|} = \frac{2xi+2yj}{\sqrt{(2x)^2+(2y)^2}} = \frac{xi+yj}{2}$

$\mathbf{A} \cdot \mathbf{n} = (4xi - 2y^2j + z^2k) \cdot \left(\frac{xi+yj}{2}\right) = 2x^2 - y^3$

From fig.

$x = 2\cos \theta \quad y = 2\sin \theta \quad dS_3 = 2d\theta dz$

$$\begin{aligned} \iint_{S_3} \mathbf{A} \cdot \mathbf{n} dS_3 &= \iint_{S_3} (2x^2 - y^3) dS_3 \\ &= \int_{\theta=0}^{2\pi} \int_{z=0}^3 [2(2\cos \theta)^2 - (2\sin \theta)^3] 2dz d\theta \\ &= 48 \int_{\theta=0}^{2\pi} (\cos^2 \theta - \sin^3 \theta) d\theta \\ &= 48 \int_{\theta=0}^{2\pi} \cos^2 \theta d\theta \\ &= 48\pi \end{aligned}$$

$\iint_S \mathbf{A} \cdot \mathbf{n} dS = 0 + 36\pi + 48\pi = 84\pi$

LS=RS verified

Problem-5. Evaluate $\iint_S \mathbf{F} \cdot \mathbf{n} dS$ where $\mathbf{F} = 4xi - 2y^2j + z^2k$ and S is

surface the region bounded by $x^2+y^2=4$, $z=0$ and $z=3$.

Or,

Find the flux of $\mathbf{F} = 4xi - 2y^2j + z^2k$ through the surface S where S is surface the region bounded by $x^2+y^2=4$, $z=0$ and $z=3$.

Or,

Find the flow of fluid through the surface S where S is surface the region bounded by $x^2+y^2=4$, $z=0$ and $z=3$, if the fluid velocity is $\mathbf{v} = 4xi - 2y^2j + z^2k$

Or,

Find the flow of heat through the surface S where S is surface the region bounded by $x^2+y^2=4$, $z=0$ and $z=3$, if the heat flux $\mathbf{q}=4xi-2y^2j+z^2k$

Find the flow of current through the surface S where S is surface the region bounded by $x^2+y^2=4$, $z=0$ and $z=3$, if the current density $\mathbf{J}=4xi-2y^2j+z^2k$

These problems can be done either directly or by using Gauss divergence theorem

$$\iiint_V \nabla \cdot \mathbf{A} dV = \iint_S \mathbf{A} \cdot \mathbf{n} dS$$

Directly (using surface integral)

$$\iint_S \mathbf{A} \cdot \mathbf{n} dS = 84\pi \quad (\text{done previously})$$

Or,

by using Gauss divergence theorem

$$\iint_S \mathbf{A} \cdot \mathbf{n} dS = \iiint_V \nabla \cdot \mathbf{A} dV$$

$$\iiint_V \nabla \cdot \mathbf{A} dV = 84\pi \quad (\text{done previously})$$

Stoke's theorem

Statement: The line integral of the tangential component of a vector \mathbf{A} taken around a simple closed curve C is equal to the surface integral of the normal component of the curl of \mathbf{A} taken over any Surface S having C as its boundary.

Mathematically

$$\oint_C \mathbf{A} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{A} \cdot \mathbf{n} dS \quad (\text{Relation between line and surface integral})$$

$$\mathbf{A} \cdot d\mathbf{r} = \mathbf{A} \cdot \mathbf{T} ds$$

Proof:

Let S be a surface such that its projection on the xy, yz and zx planes are the regions bounded by simple closed curves and suppose that the equation of the surface can be written as $z=f(x,y)$, $x=g(y,z)$ and $y=h(z,x)$ where f, g, and h are single valued continuous and differentiable function.

Fig6

Let If $\mathbf{A} = A_1\mathbf{i} + A_2\mathbf{j} + A_3\mathbf{k}$ and $\mathbf{r} = x\mathbf{i} + y\mathbf{j} + z\mathbf{k}$

Then the theorem expresses that

$$\oint_C A_1 dx + A_2 dy + A_3 dz = \iiint_S \nabla \times (A_1\mathbf{i} + A_2\mathbf{j} + A_3\mathbf{k}) \cdot \mathbf{n} dS$$

$$\oint_C A_1 dx + \oint_C A_2 dy + \oint_C A_3 dz = \iiint_S \nabla \times (A_1\mathbf{i}) \cdot \mathbf{n} dS + \iiint_S \nabla \times (A_2\mathbf{j}) \cdot \mathbf{n} dS + \iiint_S \nabla \times (A_3\mathbf{k}) \cdot \mathbf{n} dS$$

Consider the first term on the right $\iiint_S \nabla \times (A_1\mathbf{i}) \cdot \mathbf{n} dS$

$$\nabla \times (A_1\mathbf{i}) = \begin{vmatrix} \mathbf{i} & \mathbf{j} & \mathbf{k} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ A_1 & 0 & 0 \end{vmatrix} = \frac{\partial A_1}{\partial z} \mathbf{j} - \frac{\partial A_1}{\partial y} \mathbf{k}$$

$$[\nabla \times (A_1 \mathbf{i})] \cdot \mathbf{n} dS = \left(\frac{\partial A_1}{\partial z} j \cdot \mathbf{n} - \frac{\partial A_1}{\partial y} k \cdot \mathbf{n} \right) dS$$

Choosing $z=f(x,y)$ as the equation of the surface S , the position vector \mathbf{r} of any point of S is given by

$$\mathbf{r} = x\mathbf{i} + y\mathbf{j} + z\mathbf{k} = x\mathbf{i} + y\mathbf{j} + f(x,y)\mathbf{k}$$

$$\frac{\partial \mathbf{r}}{\partial y} = \mathbf{j} + \frac{\partial z}{\partial y} \mathbf{k}$$

$\frac{\partial \mathbf{r}}{\partial y}$ is a vector tangent to S , therefore it must be perpendicular to \mathbf{n}

$$\mathbf{n} \cdot \frac{\partial \mathbf{r}}{\partial y} = \mathbf{n} \cdot \mathbf{j} + \mathbf{n} \cdot \frac{\partial z}{\partial y} \mathbf{k} = 0 \quad \mathbf{n} \cdot \mathbf{j} = - \frac{\partial z}{\partial y} \mathbf{n} \cdot \mathbf{k}$$

$$\begin{aligned} [\nabla \times (A_1 \mathbf{i})] \cdot \mathbf{n} dS &= \left(- \frac{\partial A_1}{\partial z} \frac{\partial z}{\partial y} \mathbf{n} \cdot \mathbf{k} - \frac{\partial A_1}{\partial y} k \cdot \mathbf{n} \right) dS \\ &= - \left(\frac{\partial A_1}{\partial z} \frac{\partial z}{\partial y} + \frac{\partial A_1}{\partial y} \right) \mathbf{n} \cdot \mathbf{k} dS \end{aligned}$$

On the Surface S $A_1(x,y,z) = A_1(x,y,f(x,y)) = F(x,y)$ (say)
 $A_1(x,y,z) = F(x,y)$

Differentiating partially with respect to y

$$\frac{\partial A_1}{\partial y} + \frac{\partial A_1}{\partial z} \frac{\partial z}{\partial y} = \frac{\partial F}{\partial y}$$

$$[\nabla \times (A_1 \mathbf{i})] \cdot \mathbf{n} dS = - \frac{\partial F}{\partial y} \mathbf{n} \cdot \mathbf{k} dS = - \frac{\partial F}{\partial y} dx dy$$

$$\iint_S \nabla \times (A_1 \mathbf{i}) \cdot \mathbf{n} dS = - \iint_R \frac{\partial F}{\partial y} dx dy$$

where R is the projection of S on the xy plane

Now by Green's theorem in the plane region R

$$\oint_C M dx + N dy = \iint_R \left(\frac{\partial N}{\partial x} - \frac{\partial M}{\partial y} \right) dx dy$$

If C_1 is the boundary of R then

$$\oint_{C_1} Fdx + 0dy = \iint_R \left(\frac{\partial 0}{\partial x} - \frac{\partial F}{\partial y} \right) dxdy = - \iint_R \left(\frac{\partial F}{\partial y} \right) dxdy$$

$$\iint_S \nabla \times (A_1 \mathbf{i}) \cdot \mathbf{n} dS = \oint_{C_1} F dx$$

Since at each point (x,y) of C_1 , the value of F is the same as the value of A_1 at each point (x,y,z) of C and since dx is same for both the curves, we have

$$\oint_{C_1} F dx = \oint_C A_1 dx$$

$$\iint_S \nabla \times (A_1 \mathbf{i}) \cdot \mathbf{n} dS = \oint_C A_1 dx$$

Similarly

$$\iint_S \nabla \times (A_2 \mathbf{j}) \cdot \mathbf{n} dS = \oint_C A_2 dy$$

$$\iint_S \nabla \times (A_3 \mathbf{k}) \cdot \mathbf{n} dS = \oint_C A_3 dz$$

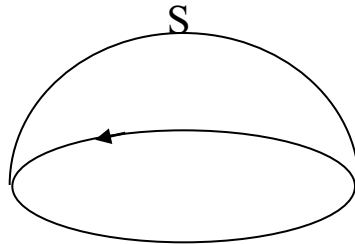
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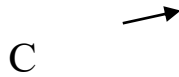
$$\iint_S \nabla \times (A_1 \mathbf{i} + A_2 \mathbf{j} + A_3 \mathbf{k}) \cdot \mathbf{n} dS = \oint_C A_1 dx + A_2 dy + A_3 dz$$

$$\iint_S \nabla \times \mathbf{A} \cdot \mathbf{n} dS = \oint_C \mathbf{A} \cdot d\mathbf{r} \quad \text{proved}$$

Verification

Problem-6. Verify Stoke's theorem for $\mathbf{A} = (2x-y)\mathbf{i} - yz^2\mathbf{j} - y^2z\mathbf{k}$ where S is the upper half surface of the sphere $x^2 + y^2 + z^2 = 1$ and C is its boundary.





The boundary C of S is a circle in the xy plane of radius one and centre at the origin The parametric equation of the circle is $x=\cos t$, $y=\sin t$, $z=0$, $0 \leq t \leq 2\pi$.

We are to show that $\oint_C \mathbf{A} \cdot d\mathbf{r} = \iint_S \nabla \times \mathbf{A} \cdot \mathbf{n} dS$

$$LS = \oint_C \mathbf{A} \cdot d\mathbf{r} = \oint_C (2x-y)dx - yz^2 dy - y^2 z dz = \int_0^{2\pi} (2\cos t - \sin t)(-\sin t) dt = \pi$$

$$RS = \iint_S \nabla \times \mathbf{A} \cdot \mathbf{n} dS$$

$$\nabla \times \mathbf{A} = \begin{vmatrix} i & j & k \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial z} \\ 2x-y & -yz^2 & -y^2z \end{vmatrix} = \mathbf{k}$$

$$\iint_S \nabla \times \mathbf{A} \cdot \mathbf{n} dS$$

$$= \iint_S \mathbf{k} \cdot \mathbf{n} dS$$

$$= \iint_R dx dy$$

$$= \int_{x=-1}^{x=1} \int_{y=-\sqrt{1-x^2}}^{y=\sqrt{1-x^2}} dy dx$$

$$= 4 \int_{x=0}^{x=1} \int_{y=0}^{y=\sqrt{1-x^2}} dy dx$$

$$= 4 \int_{x=0}^{x=1} \sqrt{1-x^2} dx$$

$$= \pi$$

$LS=RS$ verified

END