

 $V_{1} = \pi v_{1}^{2} h_{1} \cdot 2$   $V_{2} = \pi v_{2}^{2} h_{2} \cdot V_{3}$   $V_{3} = \alpha \cdot b \cdot d + \frac{1}{2} \pi r_{3}^{2} d - \pi r_{4}^{2} d$ 

 $m_T = V_T \cdot S_S = 0.79141 \, kg$   $M_T \approx 0.8 \, kg$  (round up) The larger weighs 7919 which for the sake of calculations I will round it up to 800g. This will also add extra margin.

Contracto Robot weight and carry capacity

1CPU : 0. Shy

2 Betteries 2.1ky=2kg

2 Motors 2-0.7 hg=1.4 kg

2 Base / Platform mass 2.0.2 kg = 0.4 kg

2 Wheels 2.0.2 kg = 0.4 kg

2 castor wheels

( ) FISMIN

m= S4. V w= 2700 kg . TL (15mm) 2 10mm =

~ 0.02 kg

I will estimate the caster wheel chassis to be 0.03 kg e

so I wheel will be 0.05kg

2 . 0.05 kg = 0.1 kg

4 Stept vols mass

9 v= 5mm 1. 1an

M= Ss. Vr . 9 = 7800 ms. Tr (Sum). 140 mm =

= 6.68 Skg. + 2 6.34 kg

M=0.5 kg+2 ky+1. Phy +0.9 kg+0.9 kg+0.4 kg+

\*639 lg = 5.24 kg

M ≈ 5.2 kg

I round it up because its beller to overeclimate its weight than to underestimate it.

Motor torque = 3Nm

Wheel vadius = 75 mm = 0.075m

T= v · Em weler Em = T

 $F_m = \frac{3Nm}{0.075m} = 40N$ 

because we have 2 wheels

bal Fr = 80N

 $F = m \cdot q$  ,  $F = m \cdot g$   $m = \frac{F}{g}$ 

 $m = \frac{80N}{9.81 \, \text{m}^2} = 8.15 \, \text{kg}$ 

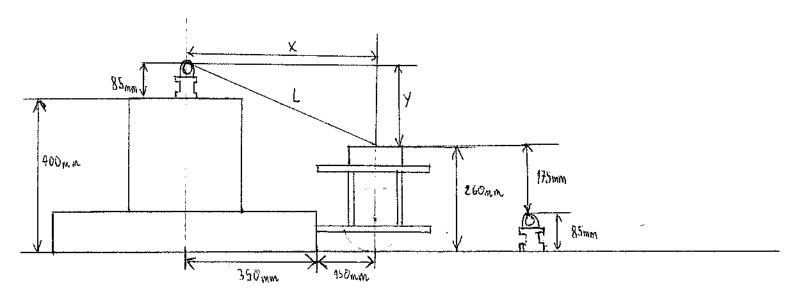
8.15 kg - 5.2 kg = 2.95 kg

The robot can carry additional 2.95 kg

Assuming target weight of 800g we have 2.15 kg to

build the arm

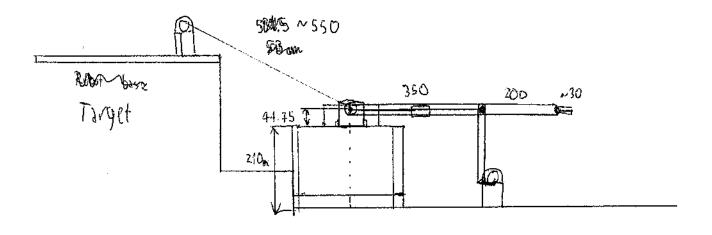
Page 2



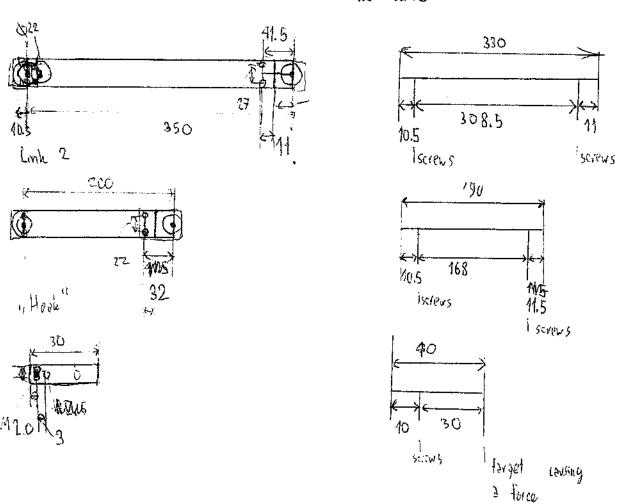
The arm should be able to place the target on top of the destination with a length of 55cm if it was attached directly on top of the CPU a and in a straight line. This means that depending on the mounting system the arm can be even shorter.

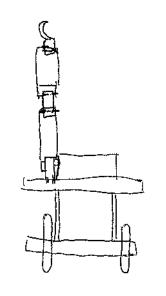
If link first link is horizontal the second link has to be 175mm long to leach the target on the floor

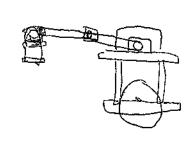
Design of arm (mm)



Link 1 2 Beams on either site of the servo





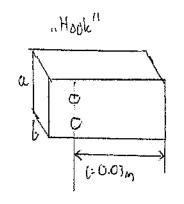


Limitations: - Robot carry weight (2.15 kg)

- Am mght put vobet GAT belance

The robot has to reach the thousand the target on the floor and on the destination

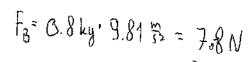
-The arm is 2 link with a controlled "hock" at the end, so the wolors have to be powerfull enough to lift 800g on a 55cm rod and support their weight



G = beam height a 6 = beam with , C = beam length 9 = bean material density (185) Page 1040 kg a=0.015m b=0.015an

The right side of the size will not experience syntiant bods.

The right side will have most of the bods. The screw position will be a fixed end, since there is 2 screws. The list will be of the end to account for the worst case (0.8kg target)



$$W = \frac{m \cdot q}{L} = \frac{a \cdot b \cdot l \cdot \beta \cdot q}{L} = ab \beta q \qquad W = 0.015 \cdot 0.015 \cdot 1040. \quad 9.81 = 6$$

$$F_A = W + F_B = 0 \qquad \qquad V = 2.3 \frac{W}{m}$$

FA=7.8N+0.069N & 7.9N & 7.9N

GA MA \*- WZiz-FBt = 0 MA = 6.0395 + 0.234

MA ≈ 0, 24 Nm

SF between A and B , at B F= FA-2.3.0.03=0.069 20.1

M et A Ma = 7.8N. 6.03 m + 2.356.05: 0015 m = 0.23 Act 6.00035 m

M<sub>A</sub> ≈ 0.2 # + Nm M<sub>3</sub>=0

Highest bending moment is at the sever location M=0.137 Nm

M=0.24 Nm

Stress in "Hook"

 $\frac{M}{J} = \frac{G}{J} = \frac{E}{R}$   $G = \frac{My}{J}$ 

 $y = \frac{1}{2}a$ ,  $J = \frac{6a^3}{12}$  M = 0.249Nn a = 6 = 0.015 n

for PR; Gy = 43 MPa = 93000000 Pa

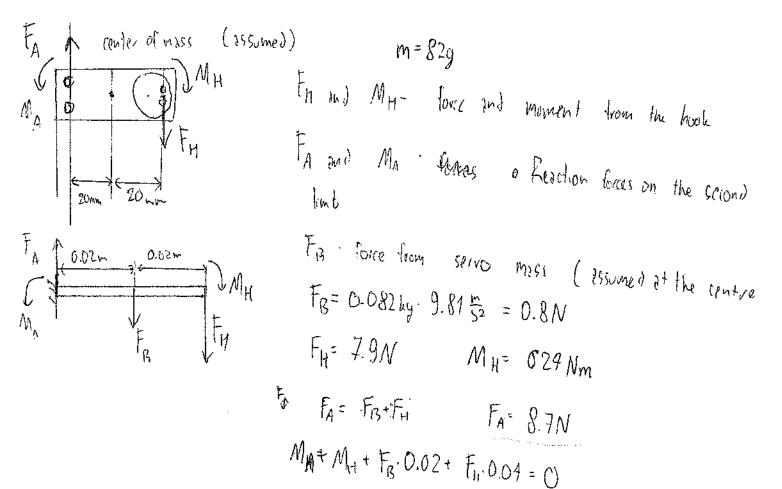
 $\sigma = \frac{\alpha \cdot 34 \, \text{Nm·6.0075m}}{(0.015)^{2} \cdot 12} = \frac{M \cdot \frac{1}{2} \alpha}{\frac{1}{12}} = \frac{M \cdot 6}{\alpha^{3}} = \frac{0.214 \, \text{Nm·6}}{(0.015 \, \text{m})^{3}} =$ 

=  $486666 \, \frac{N}{m^2} = \frac{486666 \, P_d}{1} \quad T = \frac{F}{A} = \frac{7.9 \, N}{(0.015 \, m)^2} \approx 35411 \, P_d$ 

5-7 426 666 P2 + 6147 35111P2 ≈ 0.01 5-7 = 93

Whis & The real stress to would stress ratio is almost without withstand the stress ~90

Assuming the screw holes



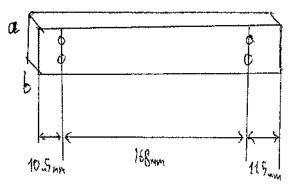
The serve is a dynamical XM 430-W350

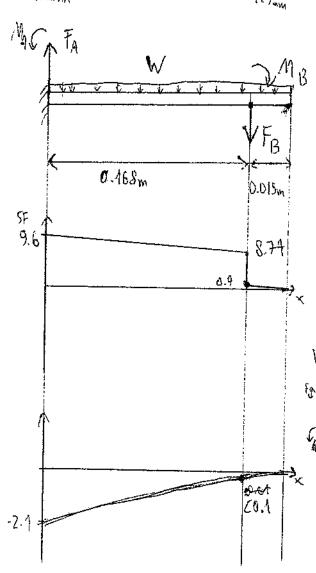
Serve with 4.1 Nm Stall torque. Since

Mm C 7.1 Nm the serve should work

fine.

MA= 0.6 Nm





a= 33,5mm= 0.0335m 6= \$5 mm = C. 015m L= 168+11.5 (un): 179. Sun < 6.1795m PAISS = 1090 443

FR-force from the moch including the larget and serve MB-Moment from hook with larget and serve

Englan 665.063.090) + 682.68 28.7N

Mg=10.615-0045-0.05-1040 by:

$$F_B = 8.7N$$
  $M_B = 0.6N_m$ 

$$W = a6 Sg = 0.0335.0.045.1090.9.81 = 5.1 \left(\frac{\pi}{m}\right)$$

$$F_{A} * F_{B} * WL = 0 - F_{A} = 8.7 + 5.1 \cdot 0.1795 = 9.6N$$

$$F_{A} * M_{A} * M_{B} *$$

$$M_A = 5.4 \pm (0.1795)^2 + 8.7 \cdot 0.168 + 0.6 = 2.1 N_m$$

Mmz = 2.1 Nm

Second limb stress

$$G = \frac{M \cdot \frac{1}{2}\alpha}{\frac{12}{12}} = \frac{6M}{\alpha^2 b} = \frac{6 \cdot 2.1 \, \text{Nm}}{(6.0335 \, \text{M}^2 \cdot 6.015 \, \text{m})} = 748496 \, P_2$$

$$T = f_3 \qquad 96N$$

The yield stress to stress ratio is 156, so the stress needs to be 56 times larger to break the material. This leaves enough room to add screw holes without compromising the integrity.

L. Bann

$$9_{\text{max}} = \frac{FL^3}{3EJ} + \frac{WL^4}{8EJ} + \frac{ML^2}{2EJ}$$

$$y_{max} = \frac{8FL^3 + 3wL^4 + 12ML^2}{29EI} = \frac{L^2(8FL + 3wL^2 + 12M_B)}{29EI} = \frac{29EI}{12}$$

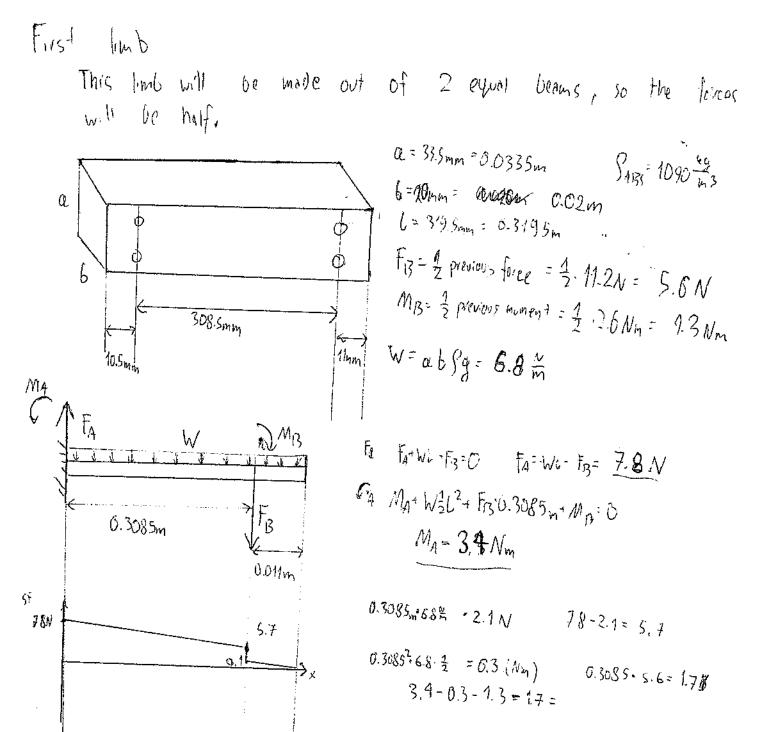
$$= \frac{6.168^{2} (8.8.7 \cdot 0.168) + 3.5.1 \cdot 6.168^{2} + 12 \cdot 6.6)}{24 \cdot 2.3 \cdot 10^{9} \cdot \frac{6.0335^{3} \cdot 6.015}{12}} = \frac{0.545}{2594.1}$$

= 6.0002m ~ 6.2 mm

Foress in second limb to first limb serve assumed control of mass in the control m=165g FR= 0.165.9681 = 1.6N mass FH= 9.6N MH= 2.1Nm 26mm 26.5mm. F2 FA+ FB+FH= O FA= 1.6N+ 9.6N=11.2N FA \$ 0.026m (6.0265m) \ MH A MA+ MH+ FHOR (0.6265+6026) n+ Fg-6.026m = 0

MA= RUMMENT a GNA metricips = 2.6 Nm

The servo is a dynamical XM S40 - W270 - T/R Ja has a stall torque of 10.6 Nm, so it shord have no issues operating.



0.4%

-3.91

First limb stress

The yield stiess to stress ratio is 97. Earn Remembering that there is two saturbasiums thus should be enough.

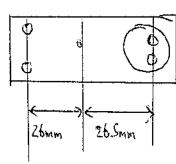
Limb 1 deflection

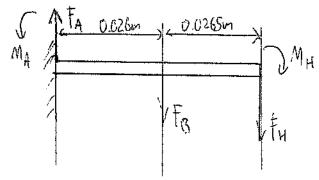
L= 308.5mm

$$\frac{v_{\text{max}}}{24} = \frac{8FL^3 + 3WL^4 + 12ML^2}{24 \cdot E} = \frac{L^2 \left(8F_B L + 3WL^2 + 12M_B\right)}{24 \cdot E} = \frac{24 \cdot E}{24 \cdot E}$$

$$= \frac{0.3085^{2}(8.7.8.0.3085 + 3.68.6.3085^{2} + 12.1.3)}{29.2.3.10^{9} \cdot 0.02.0.0335^{3}} = \frac{3.502}{3458.77}$$

= 6.00101m # 1mm



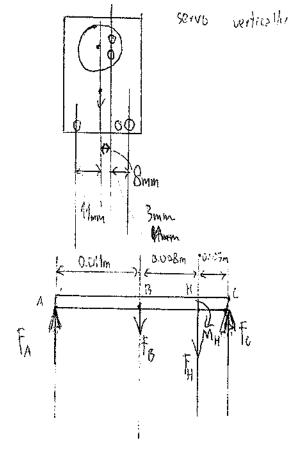


m=165g

$$F_{R}=0.165.9.81=1.6(N)$$
 mass

 $F_{H}=2.1681 \text{ kmb fore}=2.7.8 N=15.6 N$ 
 $M_{H}=2.1681 \text{ kmb moment}=2.3.4 Nm=6.8 Nm$ 

C MA + FR'0.026n + FH(6.0265,0026n) + MH = 0 MA = 7.7 Nm

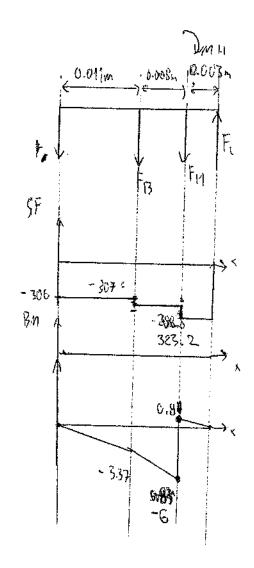


Franks Fut = 0 Fc = Fa-Fs-FH

Fc = 44009 323.2 (N)

FOREN FROM THE FOOD WHY

RESPONSE THE THE STATE OF THE ST

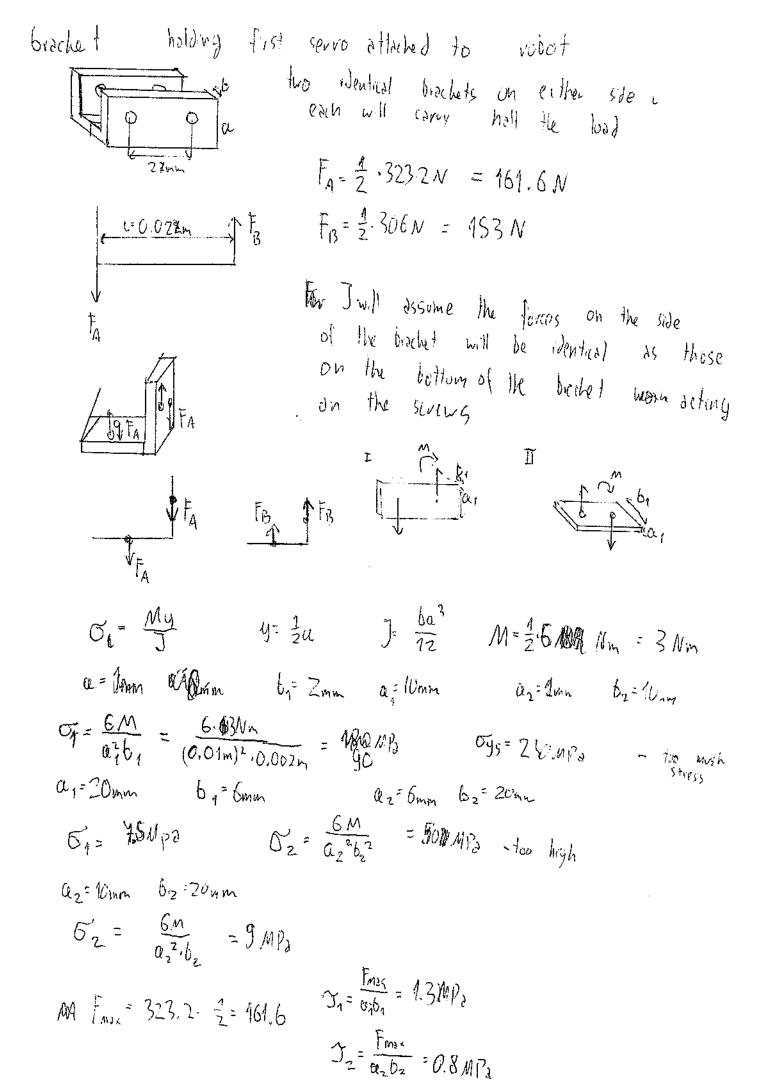


$$F_{A} = 306 N$$
  $-306 \cdot 0.041 = -3.37 (Nm)$   
 $F_{B} = 46N$   $-323.2 \cdot 0.008 = -2.39 (Nm)$   
 $F_{H} = 15.6N$   $-3.37 = 2.59 = 5.96 (Nm)  $\approx 6 Nm$   
 $F_{C} = 323.2 N$   $-306 + 6.8 = 0.8 Nm$$ 

Those forces apply to the brechet

The serve is also a dynamical XM 540-W270-T/R, so it should operate with no issues.

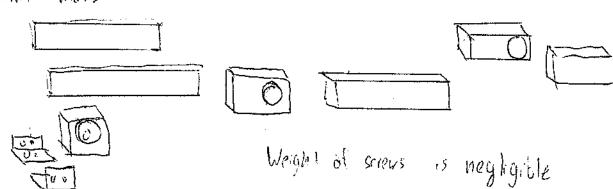
Since 10.6 Nm > 6.8 Nm



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Brochet stress

vield sleess to strais ratio in the bracket sections of 28 and 28 should be sufficient.



Breizets Mg= 2-(0.02:0.006:6.022:7800 + 0.01.0.02.0022:7800) = 0.11 kg

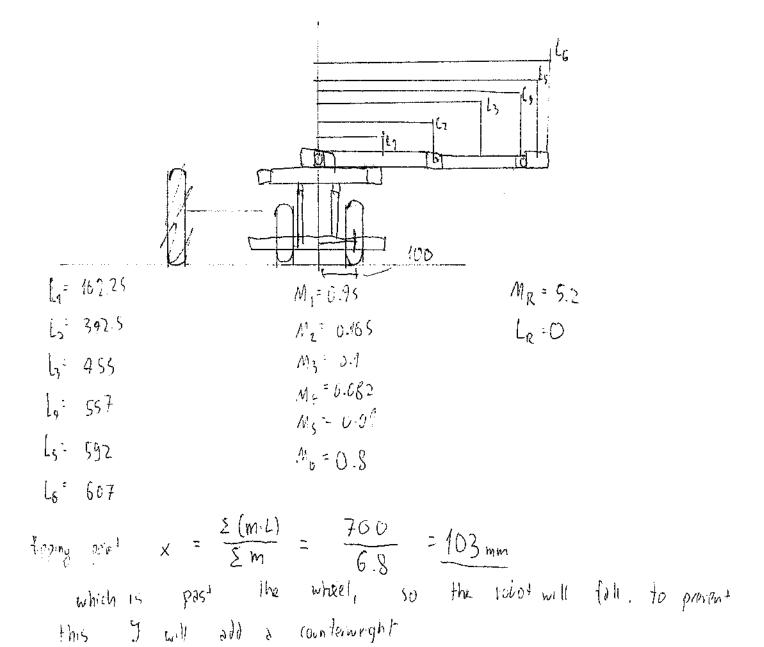
Limbi ML = 2-(0.0335. 0.02.6.3195. 1090) = 6.95 kg Servo 2 = 1659 = 0.165 kg

Limbo MLz = 0.0335 · 0.015 · 0.1799 · 1090 = 0.1 hg

Servo 3 = 82g = 0.082 kg

Limb 3 (hosh) MH = 0.015.0.015.0.09 .1090 = 0.01hg

EM = G.11 + 0.165 + 0.45 + 0.105 + 6.1 + 0.082 + 0.01 = 1.169which is less than the meximum 2.15 ky meaning the robot can still move





$$x = \frac{700 + 0.5 \cdot (-130)}{7.3} = 87 \text{ mm}$$

which is within the volot tipping point.
The counterwight will be just a steel bluck (whee)
glued to the volot 130mm from the centre.
It shouldn't experience any forces and thus stay in place

Cube dimentions:

$$m = V \cdot S_{S}$$
  $V = \frac{m}{S_{S}}$   $a = \frac{3}{S_{S}}$   $a = \frac{3}{S_{$ 

The counterweight will brought the robot weight by O.Shy, leaving the extra carry weight to be 0.65 hy, so the robot should still be able to fully more.

