



به نام خدا



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دانشکده مهندسی برق و کامپیوتر  
اصول سیستم های مخابراتی  
تمرین کامپیوتری اول

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## فهرست گزارش سوالات

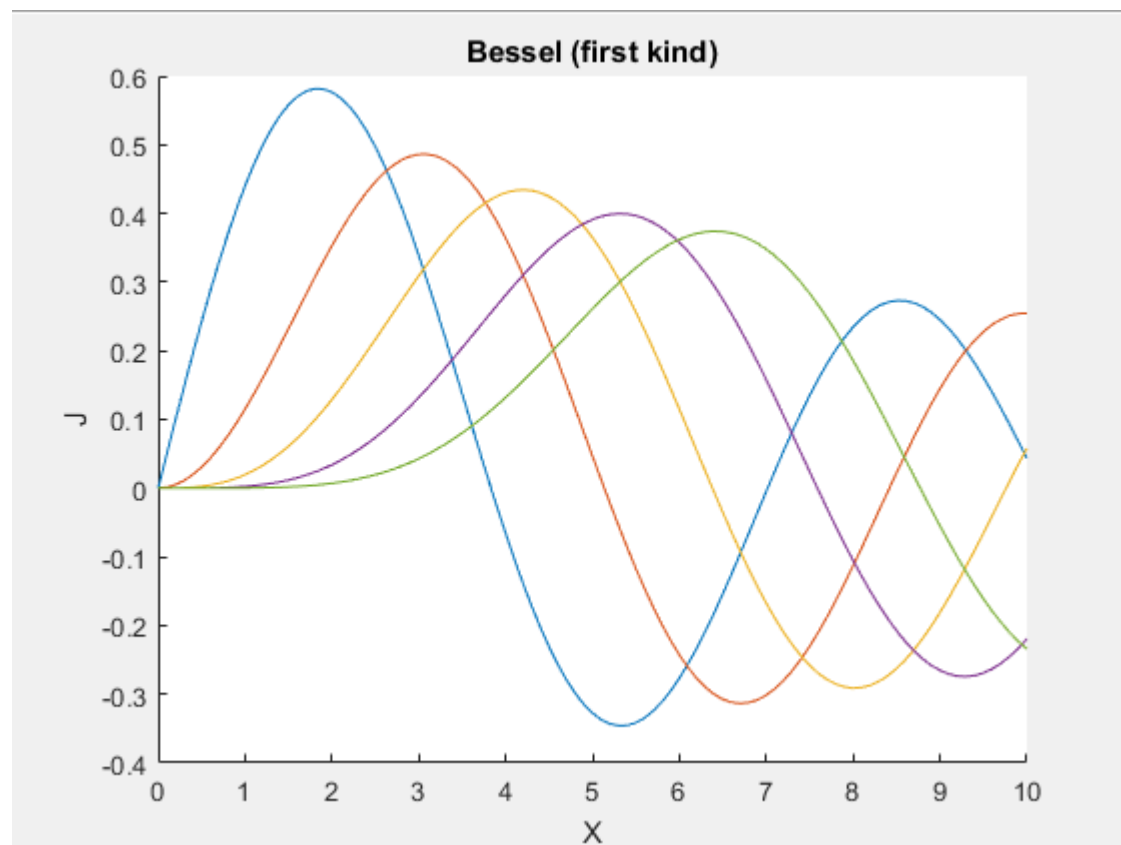
3	Bessel Differential Equations
5	Narrow Band Modulation
8	Single Tone Modulation
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**Bessel first kind :**

```

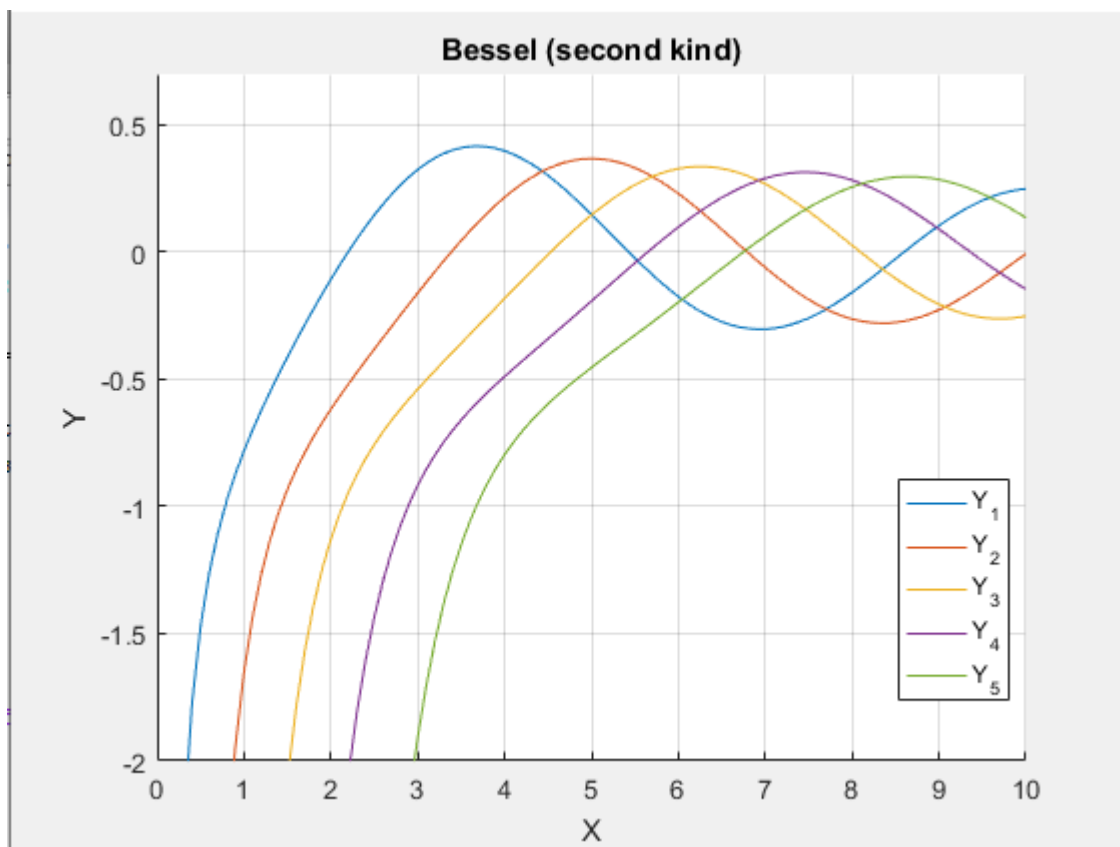
%% Part_1
J = [] ;
Z = [0 : 0.1 : 10] ;
hold on
for nu = 1:5                                %calculate J and plot
    J = besselj(nu,Z) ;
    plot(Z,J) ;
end
title(' Bessel (first kind) ')
xlabel('X');
ylabel('J');
% grid on
% legend('J_1','J_2','J_3','J_4','J_5','Location','Best')
hold off

```



## Bessel second kind :

```
%% Part_2
Y = [] ;
Z = [0 : 0.1 : 10] ;
hold on
for nu = 1:5                                %calculate Y and plot
    Y = bessely(nu,Z) ;
    plot(Z,Y) ;
    axis([0 10 -2 0.7])
end
title(' Bessel (second kind) ')
xlabel('X');
ylabel('Y');
grid on
legend('Y_1','Y_2','Y_3','Y_4','Y_5','Location','Best')
hold off
```



**pmm function :**

```
function y = p3_pmm(x , Ac , fc , kp , fs)
    t = 0 : 1/fs : (1/fs)*(length(x)-1) ;
    y = Ac*cos((2*pi*fc*t)+(x.*kp)) ;
end
```

**nb function :**

```
function y = p4_nb(x , Ac , fc , kp , fs)
    t = 0 : 1/fs : (1/fs)*(length(x)-1) ;
    y = Ac*cos(2*pi*fc*t) - Ac*kp*x.*sin(2*pi*fc*t) ;
end
```

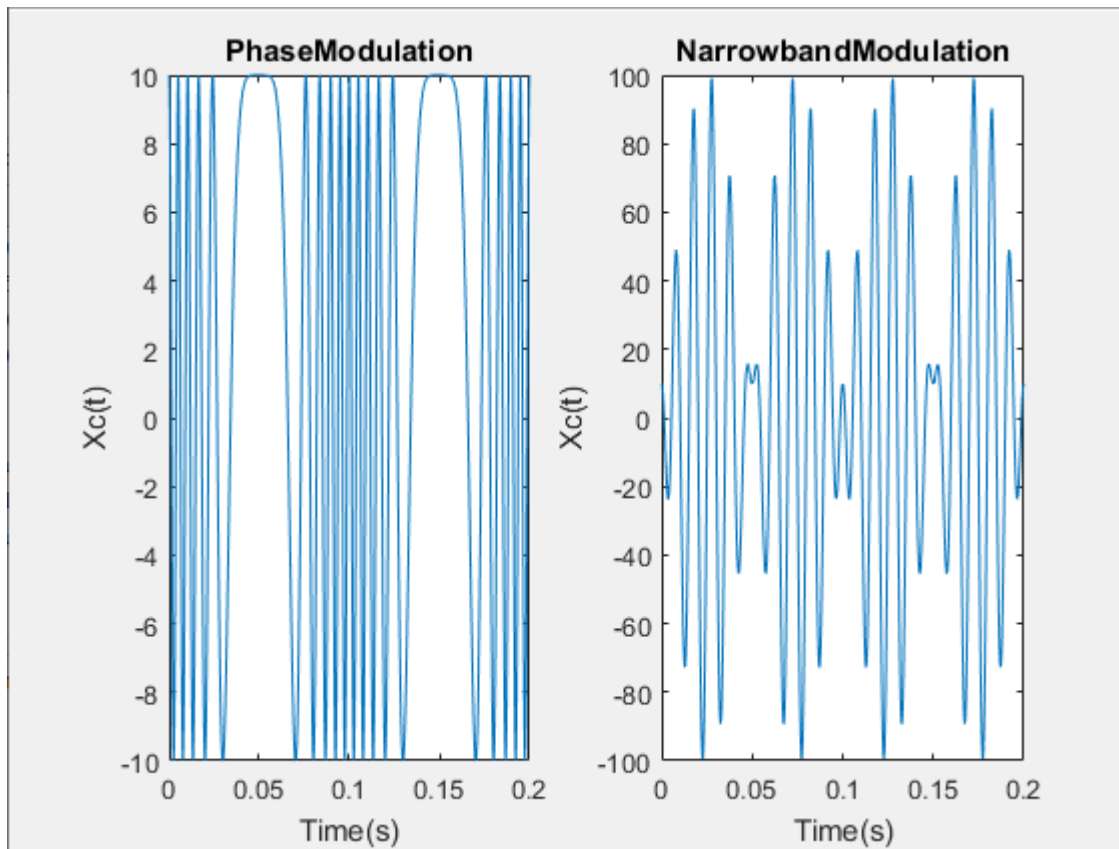
**modulating message signal :**

```
%% Part_5_6_7
fs = 10000 ;
Ts = 1/fs ;           % Sampling period
time = 0:Ts:0.2 ;
fc = 100 ;
Ac = 10 ;
kp = 10 ;
Xm = sin(20*pi*time) ;
PhaseModulation = p3_pmm(Xm , Ac , fc , kp , fs) ;
NarrowbandModulation = p4_nb(Xm , Ac , fc , kp , fs) ;

figure;
subplot(1,2,1);
plot(time,PhaseModulation) ;
title(' PhaseModulation ')
xlabel('Time(s)');
ylabel('Xc(t)');

subplot(1,2,2);
plot(time,NarrowbandModulation) ;
title(' NarrowbandModulation ')
xlabel('Time(s)');
ylabel('Xc(t)');
```

**modulated signal :**

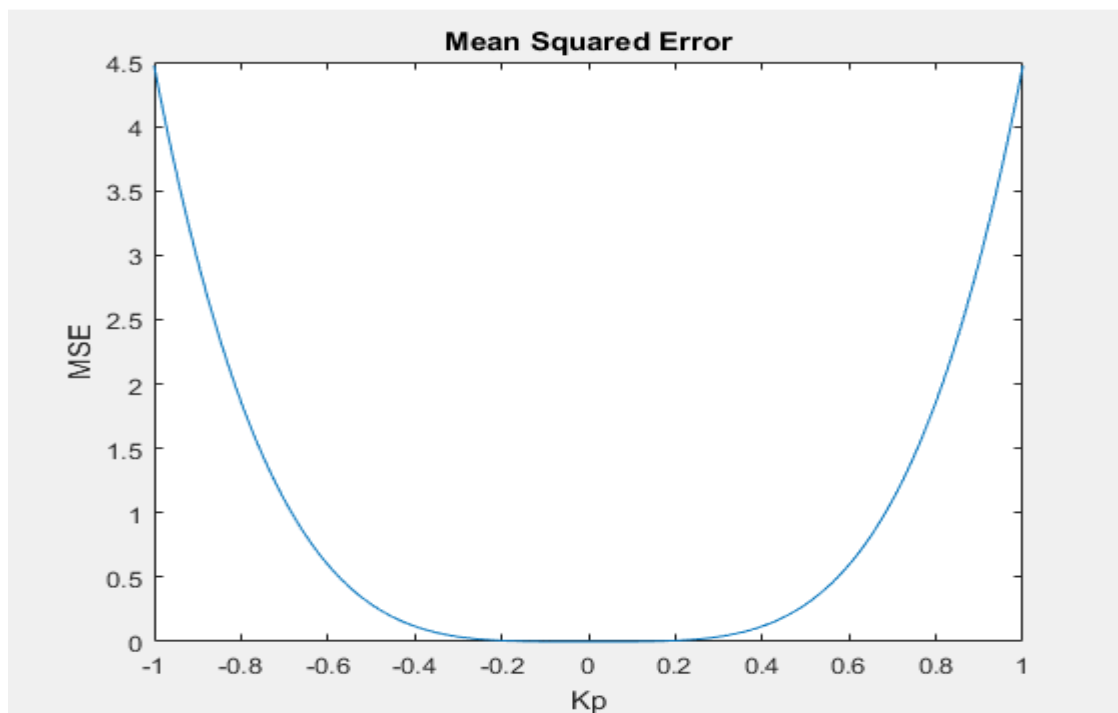


As mentioned in the question, the condition for using the Narrow Band function is that the value of  $\phi$  is small ( $\phi \ll 1$ ) but in this case  $\phi$  is 10 ! so we can no longer use this approximation , And this is the reason for the difference between the two plots .

## Mean Squared Error :

```
%% Part_8_9
fs = 10000 ;
Ts = 1/fs ;           % Sampling period
time = 0:Ts:0.2 ;
fc = 100 ;
Ac = 10 ;
Xm = sin(20*pi*time) ;
Kp = -1:0.001:1 ;     % Kp --> [-1 , 1]
MSE = [] ;             % Mean Squared Error
MaxKp = 0 ;            % Maximum Kp to have 1 percent error
for kp = -1:0.001:1
    PhaseModulation = p3_pmm(Xm , Ac , fc , kp , fs) ;
    NarrowbandModulation = p4_nb(Xm , Ac , fc , kp , fs) ;
    MSE(end + 1) = immse( PhaseModulation , NarrowbandModulation ) ;
    if immse( PhaseModulation , NarrowbandModulation ) < 0.1
        MaxKp = kp ;
    end
end

plot(Kp,MSE) ;
title(' Mean Squared Error ')
xlabel('Kp');
ylabel('MSE');
```



As we expected, with increasing the amount of Kp, the difference between the two modulations increases, and finally, the amount of error also increases.

MaxKp = 0.3820

## Single Tone Modulation

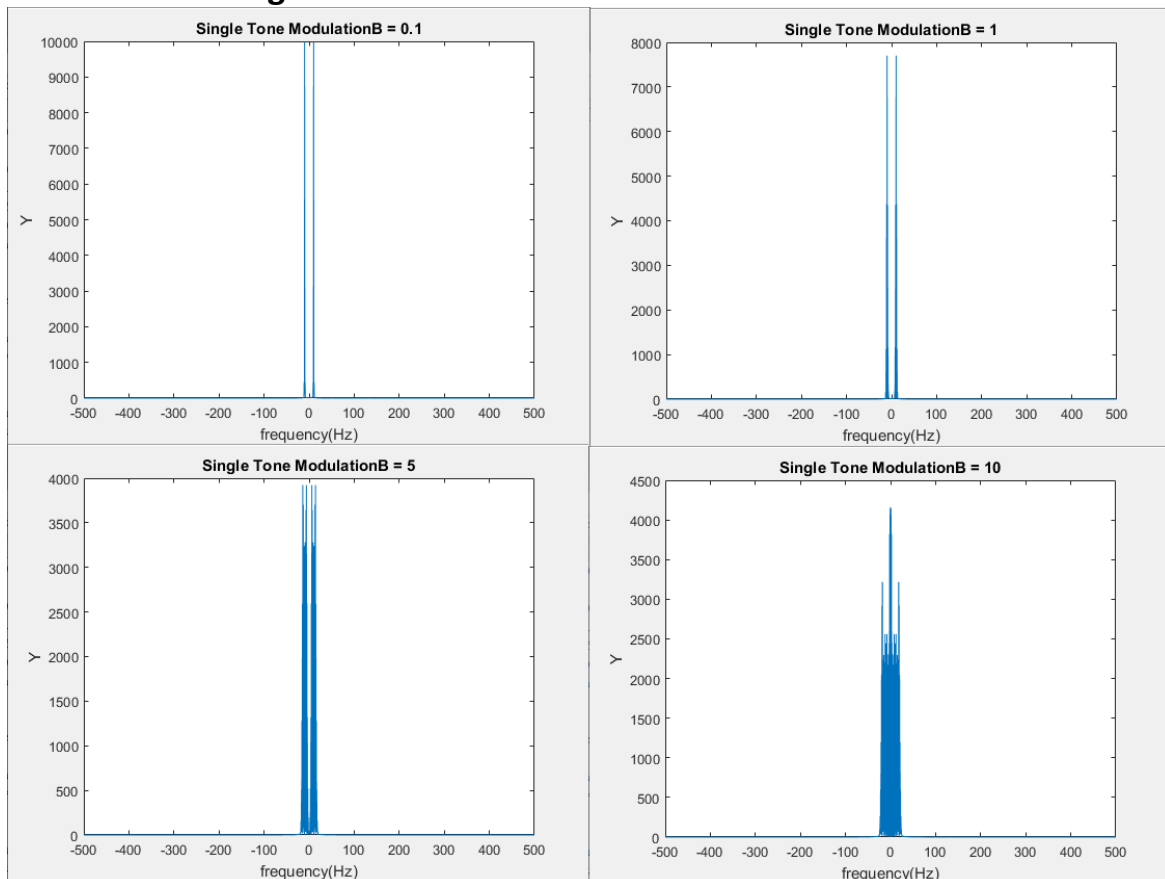
Single Tone Modulation :

```
%% Part_10
fs = 10000 ;
Ac = 10 ;
fc = 100 ;
B = [0.1 ,1 ,5 ,10] ;
Ts = 1/fs ;           % Sampling period
time = 0:Ts:0.2 ;
Xm = sin(20*pi*time) ;
fm = 10 ;
Xc = [] ;
frequency = -500:0.5:500 ;

for Counter = 1:1:4
    Xc = Ac * cos((2*pi*fc*time)+(B(Counter)*sin(2*pi*fm*time))) ;
    Y = fft(Xc) ;
    Y = fftshift(Y) ;
    figure;
    plot(frequency,abs(Y)) ;
    xlim([-30 30])
    title(['Single Tone Modulation','B = ',num2str(B(Counter))])
    xlabel('frequency(Hz)');
    ylabel('Y');
end
```

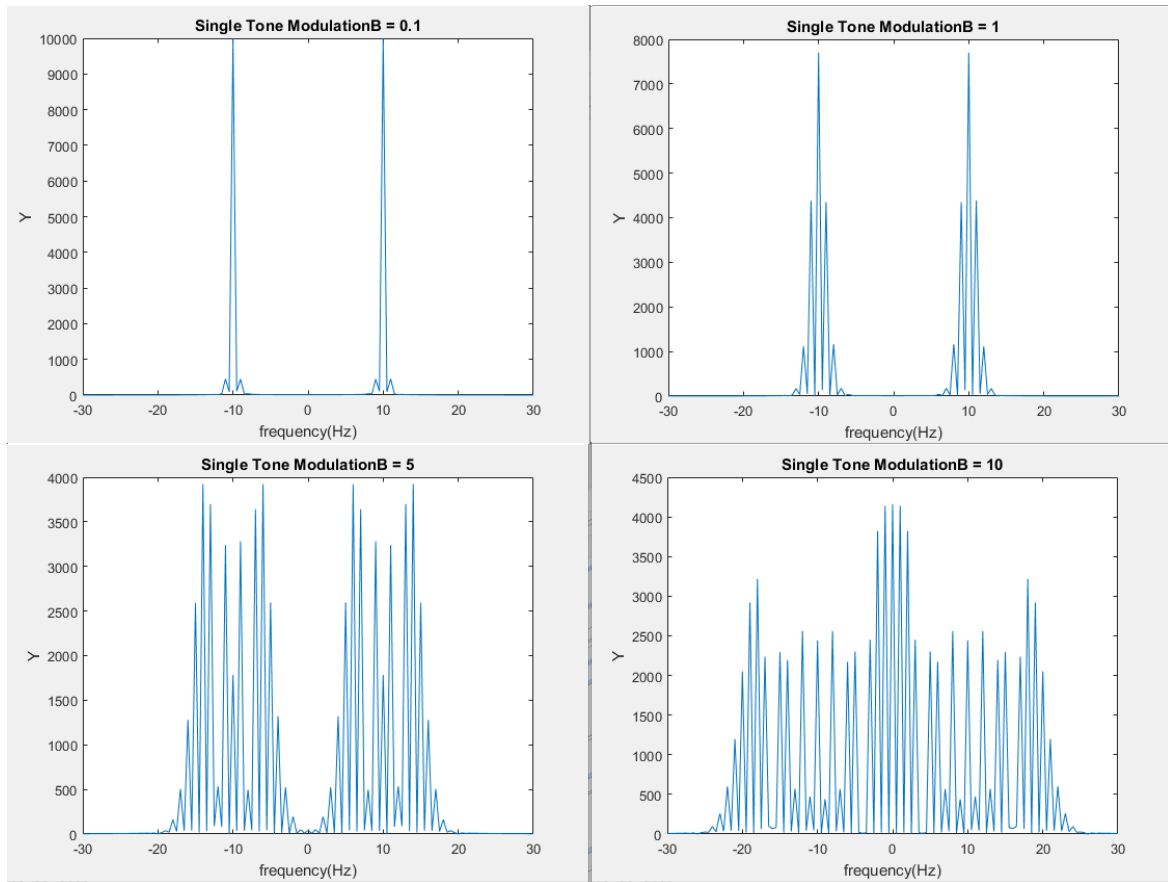
**Note :** To make the diagrams more accurate, we use the “xlim” function to limit the horizontal axis.

**Plots before using “xlim” :**





**Plots after using “xlim” :**



**As mentioned in the question, with increasing beta, the number of sentences increases and we can not ignore some sentences, which is why the signal is wider.**

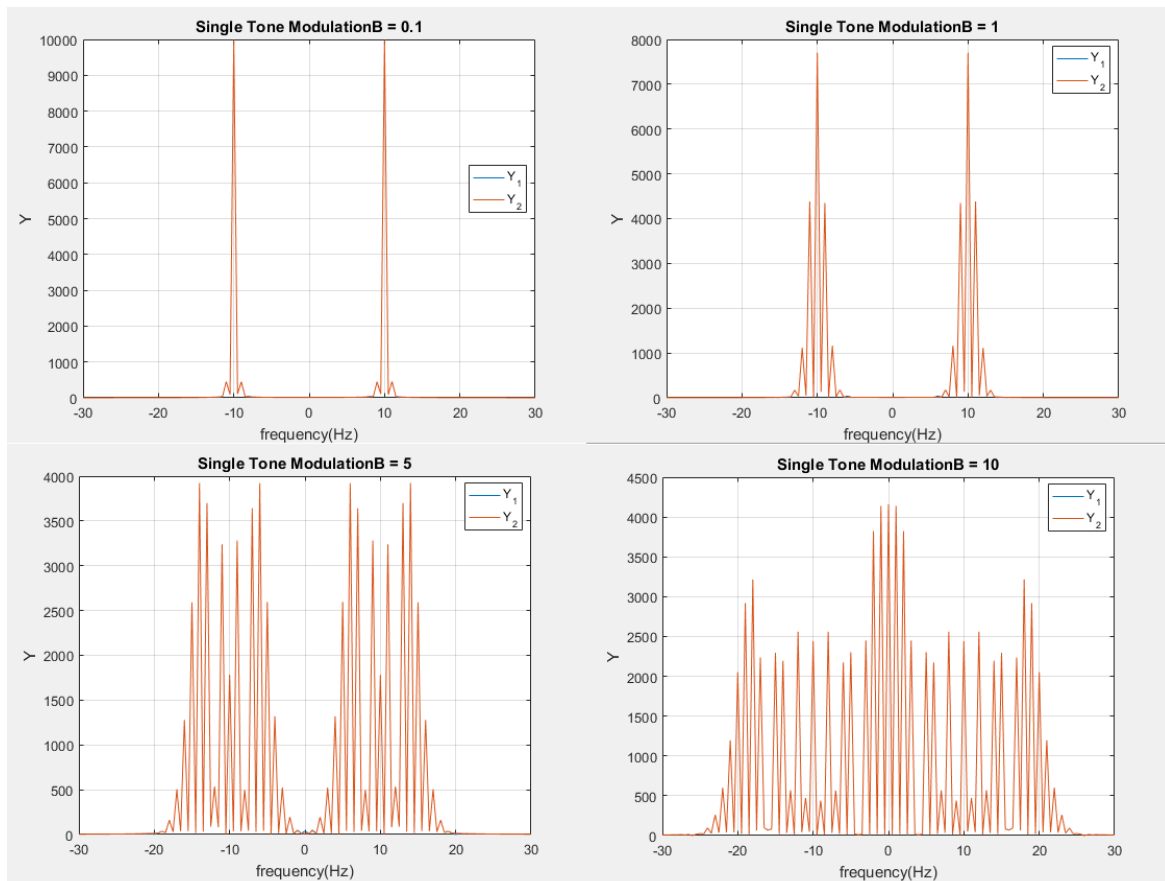
## modulating message signal using functional expansion :

```
%% Part_11_12
fs = 10000 ;
Ac = 10 ;
fc = 100 ;
B = [0.1 , 1 , 5 , 10] ;
Ts = 1/fs ;           % Sampling period
time = 0:Ts:0.2 ;
Xm = sin(20*pi*time) ;
fm = 10 ;
Xc = [] ;
Bc = [] ;
N = [1 , 3 , 9 , 23] ;
frequency = -500:0.5:500 ;

for Counter = 1:1:4
    Xc = Ac * cos((2*pi*fc*time)+(B(Counter)*sin(2*pi*fm*time))) ;
    Y = fft(Xc) ;
    Y = fftshift(Y) ;
    figure;
    plot(frequency,abs(Y)) ;
    hold on
    title(['Single Tone Modulation','B = ',num2str(B(Counter))])
    xlabel('frequency(Hz)');
    ylabel('Y');

    Xc = 0 ;
    for n = -N(Counter):1:N(Counter)
        Xc = Xc + (besselj(n,B(Counter)) * cos(2*pi*(fc + n*fm)*time)) ;
    end
    Xc = Xc * Ac ;
    Y = fft(Xc) ;
    Y = fftshift(Y) ;
    plot(frequency,abs(Y)) ;
    grid on
    legend('Y_1','Y_2','Location','Best')
    hold off
    Bc(Counter) = 2 * (B(Counter) + 1) * fm ;
end
```

**Note :** To make the diagrams more accurate, we use the “xlim” function to limit the horizontal axis.



**fmm function :**

```
function y = p3_fmm(x , Ac , fc , kf , fs)
    N = 100 ;
    Integral = 0 ;
    for Counter = 1:1:N
        Integral = Integral + x(N) + x(N+1) ;
    end
    Integral = ((0.2-0)/(2*N)) * Integral ;
    Phi = 2*pi*kf*Integral ;
    y = p3_pmm(Phi , Ac , fc , 1 , fs) ;
end
```

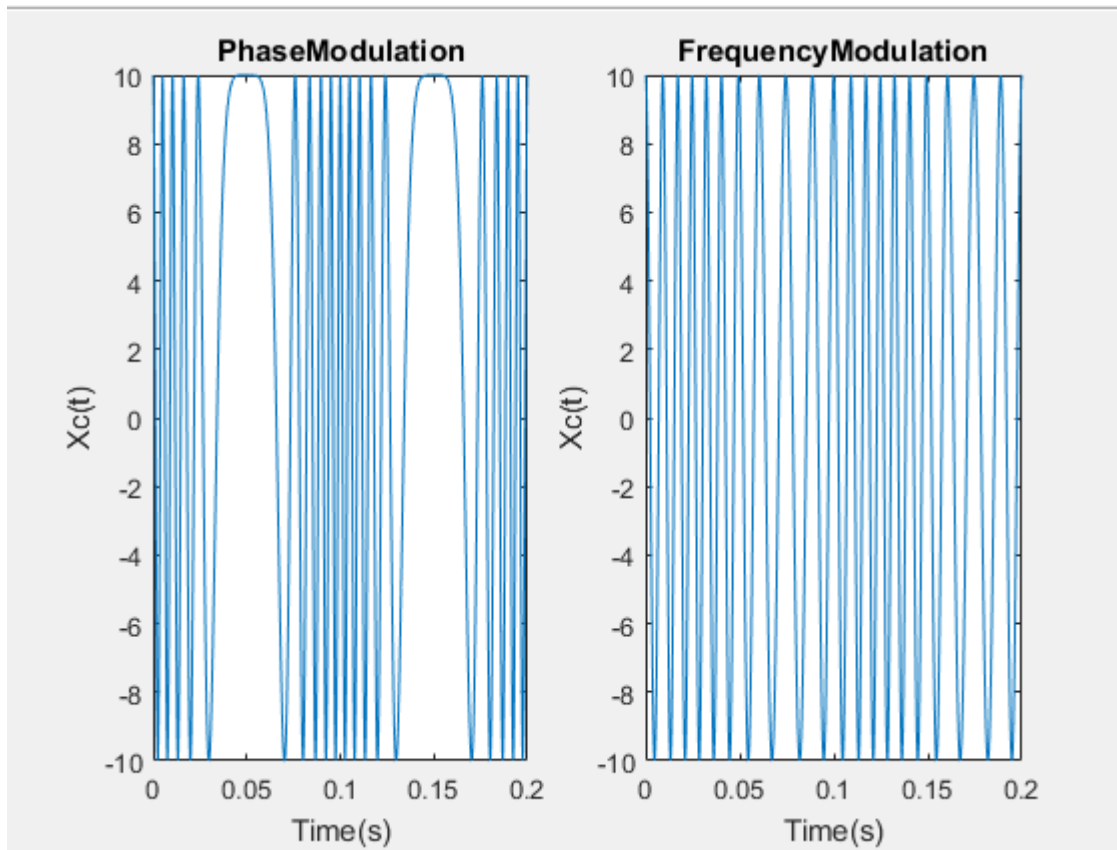
**pm modulation and fm modulation :**

```
%% Part_14
fs = 10000 ;
Ts = 1/fs ;           % Sampling period
time = 0:Ts:0.2 ;
fc = 100 ;
Ac = 10 ;
kp = 10 ;
kf = 100 ;
Xm = sin(20*pi*time) ;
PhaseModulation = p3_pmm(Xm , Ac , fc , kp , fs) ;
FrequencyModulation = p3_fmm(Xm , Ac , fc , kf , fs) ;

figure;
subplot(1,2,1);
plot(time,PhaseModulation) ;
title(' PhaseModulation ')
xlabel('Time(s)');
ylabel('Xc(t)');

subplot(1,2,2);
plot(time,FrequencyModulation) ;
title(' FrequencyModulation ')
xlabel('Time(s)');
ylabel('Xc(t)');
```

---



## Armstrong Indirect Method

در فرکانس میچ جلد به صورت جدا از  $x(t)$  تولید می شود و در یک پهنای باند محدود قرار دارد.

① NBPM → ② NBFM → ③ ضرب کننده فرکانس → WBFM →  $f_i$  →  $x_n$  →  $f_o$

① narrowband PM:  $w_c$  فرکانس میچ جلد:  $w_c \rightarrow f_c$   $n f_i = f_o$

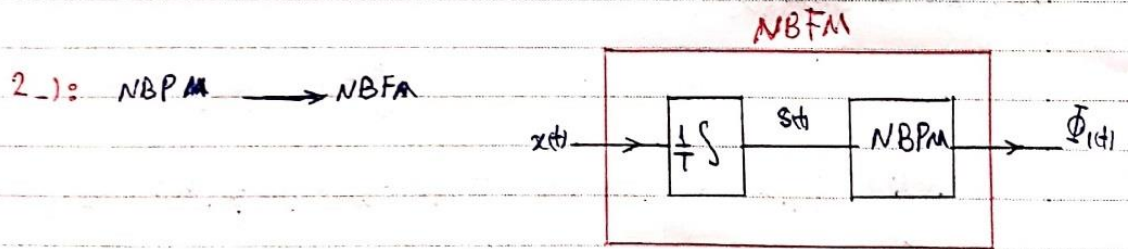
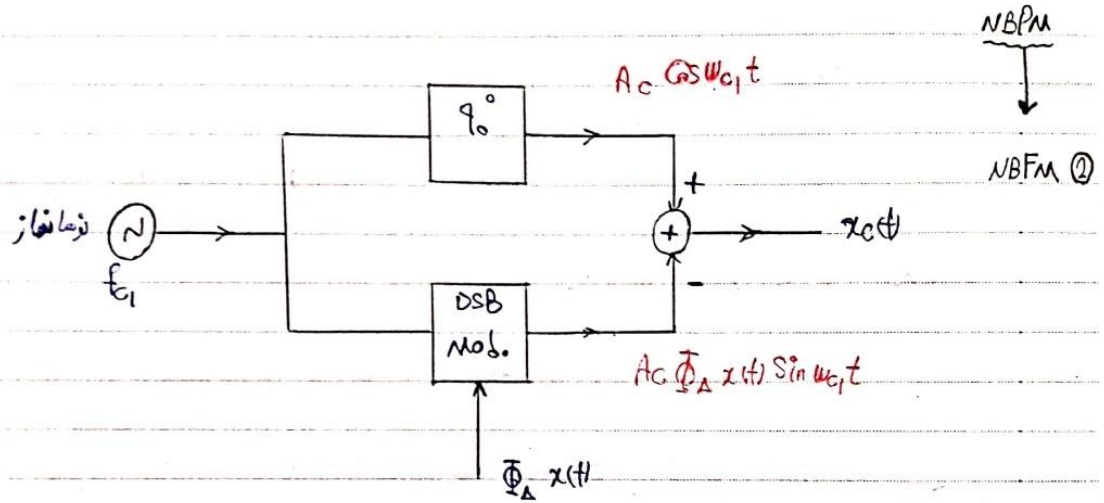
$$x_c(t) = A_c \cos[\omega_c t + \phi(t)] = A_c \cos[\omega_c t + \phi_\Delta x(t)]$$

NB:  $\phi_\Delta x(t) \ll 1$   $x_c(t) = A_c \cos(\phi_\Delta x(t)) \cos \omega_c t = A_c \sin(\phi_\Delta x(t)) \sin \omega_c t$

بنابراین  $\frac{\phi_\Delta x(t)}{1}$  ضرایب

باید ولتاژ DSB سیگنال این شکل مرجع را تولید کرد...

$$x_c(t) = A_c \cos \omega_c t - A_c \bar{\Phi}_A x(t) \sin \omega_c t$$



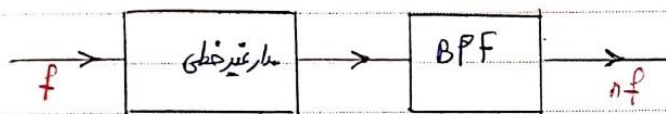
$$S(t) = \frac{1}{T} \int x(\lambda) d\lambda$$

$$\Phi_1(t) = \Phi_\Delta S(t) = \frac{\Phi_\Delta}{T} \int x(\lambda) d\lambda$$

$$f_1(t) = f_c + \left( \frac{\Phi_\Delta}{k_f T} \right) x(t) \rightarrow f_\Delta$$

3- ضرب کننده فرکانس: باید عنصر غیرخطی فرکانس را  $N$  برابر می کنیم.

← غالباً ترکیبی از ۲ برابر کننده و ۳ برابر کننده فرکانس است.



۱۰۰۰ برابر کننده فرکانس: ۱۰۰۰ برابر کننده

مثال: برای اینکه  $f_2$  برابر مقدار فاصله شده یعنی  $f_\Delta$  باشد  $n$  باید خیلی بزرگ باشد:

