

Crank-Nicolson method

$\theta = \frac{1}{2}$ & the source term is linear (pg No 289 8.10 eqn)

$$b = S_u + \frac{1}{2} S_p T_p + \frac{1}{2} S_p T_p^0$$

$$a_p T_p = a_E \left[\frac{T_E + T_E^0}{2} \right] + a_W \left[\frac{T_W + T_W^0}{2} \right]$$

$$+ \left[a_p^0 - \left(\frac{a_E}{2} + \frac{a_W}{2} \right) \right] T_p^0 + \underbrace{S_u + \frac{1}{2} S_p T_p^0}_{\text{source}(S_u)}$$

$$a_p = \frac{a_W + a_E}{2} + a_p^0 - \frac{1}{2} S_p$$

$$\times \quad a_p^0 = \rho c \frac{\Delta x}{\Delta t}$$

a_W	a_E
$\frac{k_W}{\Delta x_W}$	$\frac{k_E}{\Delta x_E}$

time step $\Delta t < \rho c \frac{\Delta x^2}{k}$

Given Example problems
Key points

* all coefficients are +ve for realistic & bounded results.

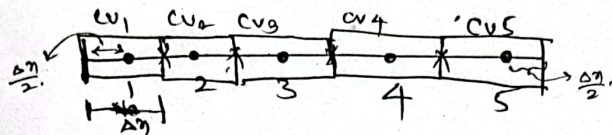
$$a_p^0 > \left(\frac{a_E + a_W}{2} \right)$$

* It's based on the central differencing.
so it's 2nd order accuracy.

* With sufficiently small time steps it's possible to achieve ~~converge~~ great accuracy.

Ex 8.2 267/253
 given time step 8s | by C.N. method
 $\Delta t = 8 \text{ sec}$ $\theta = \frac{1}{2}$

$K = 10 \text{ W/m.K}$; $\rho C = 10 \times 10^6 \text{ J/m}^3 \cdot \text{K}$



the governing eqⁿ

$$\rho C \frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left(K \frac{\partial T}{\partial x} \right) \rightarrow (1)$$

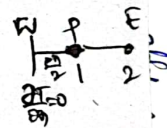
Integrate the eqⁿ (1) wr to Control Volume (CV) & time increments (+) to (+ + Δt)

we have

Now for the Node (1) & CV (1) then we have

$$\rho C \frac{(T_P - T_P^0) \Delta x}{\Delta t} = D \cdot (T_E - T_P) + D \left(\frac{T_E^0 - T_P^0}{2} \right)$$

$$= D \left(\frac{T_E + T_E^0}{2} \right) - \frac{D}{2} T_P^0 - \frac{D}{2} T_P$$



$$\rho C \frac{\Delta x}{\Delta t} T_P - \left(\frac{\rho C \Delta x}{\Delta t} \right) T_P^0 =$$

$$\left(\left(\frac{\rho C \Delta x}{\Delta t} + \frac{D}{2} \right) \right) T_P = D \left(\frac{T_E + T_E^0}{2} \right) + \left(\frac{\rho C \Delta x}{\Delta t} - \frac{D}{2} \right) T_P^0$$

∴ $q_W = 0$; $q_E = \frac{K}{\Delta x} = D$

i.e. $\left(a_P^0 + \frac{a_E}{2} \right) T_P = a_E \left(\frac{T_E + T_E^0}{2} \right) + \left(a_P^0 - \frac{a_E}{2} \right) T_P^0$

$$a_P = \frac{a_E}{2} + a_P^0 //$$

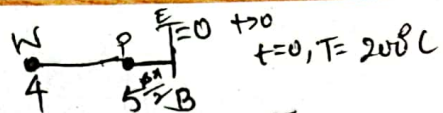
sub
 > 0

if - 1000°C T135U1M + a. d. n. . .

25 T_E⁰

T135U1M

Node (5) ie for CV(5)



$$\rho C \left(\frac{T_P - T_P^0}{\Delta t} \right) \Delta \eta = \frac{1}{2} \left[\frac{k}{\Delta \eta} (T_B - T_P) - \frac{k}{\Delta \eta} (T_P - T_W) \right] + \frac{1}{2} \left[\frac{k}{\Delta \eta} (T_B^0 - T_P^0) - \frac{k}{\Delta \eta} (T_P^0 - T_W^0) \right]$$

$$= \frac{1}{2} [2D(T_B) - 2DT_P - DT_P + DT_W] + \frac{1}{2} [2DT_B^0 - 2DT_P^0 - DT_P^0 + DT_W^0]$$

$$\rho C \frac{\Delta \eta}{\Delta t} T_P - \rho C \frac{\Delta \eta}{\Delta t} T_P^0 = DT_B - DT_P - \frac{D}{2} T_P + \frac{D}{2} T_W + DT_B^0 - DT_P^0 - \frac{D}{2} T_P^0 + \frac{D}{2} T_W^0$$

$$\left[\rho C \frac{\Delta \eta}{\Delta t} + \frac{a_w}{2} + D \right] T_P = a_w \left(\frac{T_W + T_W^0}{2} \right) + \left[\rho C \frac{\Delta \eta}{\Delta t} - \frac{a_w}{2} - D \right] T_P^0 + D(T_B + T_B^0)$$

$$\therefore (a_p^0 + \frac{a_w}{2} + D) T_P = a_w \left(\frac{T_W + T_W^0}{2} \right) + (a_p^0 - \frac{a_w}{2} - D) T_P^0 + D(T_B + T_B^0)$$

$$\text{Now } a_p^0 = \rho C \frac{\Delta \eta}{\Delta t} \quad | \quad D = 0 \quad | \quad S_u = D(T_B + T_B^0)$$

$$\text{Now } D = \frac{k}{\Delta \eta} ; \text{ coeff of } T_P^0 = a_p^0 - \frac{a_w}{2} - D$$

Now for Nodes 2, 3, 4 ie for CV 2, 3, 4, 4m,

$$\rho C \left(\frac{T_P - T_P^0}{\Delta t} \right) \Delta \eta = \frac{1}{2} \left[\frac{k}{\Delta \eta} (T_E - T_P) - \frac{k}{\Delta \eta} (T_P - T_W) \right] + \frac{1}{2} \left[\frac{k}{\Delta \eta} (T_E^0 - T_P^0) - \frac{k}{\Delta \eta} (T_P^0 - T_W^0) \right]$$

$$\therefore (a_p^0 + \frac{a_w}{2} + \frac{a_E}{2}) T_P = a_E \left(\frac{T_E + T_E^0}{2} \right) + a_w \left(\frac{T_W + T_W^0}{2} \right) + (a_p^0 - \frac{a_w}{2} - \frac{a_E}{2}) T_P^0$$

$$\therefore a_E = a_w = \frac{k}{\Delta \eta} ; \quad a_p^0 = \rho C \frac{\Delta \eta}{\Delta t}$$

$$a_p = \left(a_p^0 + \left(\frac{a_w + a_E}{2} \right) \right) \quad \text{coeff of } T_P^0 = a_p^0 - \frac{a_w}{2} - \frac{a_E}{2}$$

Node

au

ae

ap

$ap^0 = pc \frac{\Delta T}{\Delta t}$

sp

su

1

0

$\frac{k}{\Delta x}$

$\frac{ae}{2} + ap^0$

0

0

2.

$\frac{k}{\Delta x}$

$\frac{k}{\Delta x}$

$\frac{ae}{2} + \frac{au}{2} + ap^0$

0

0

3.

$\frac{k}{\Delta x}$

$\frac{k}{\Delta x}$

$\frac{ae}{2} + \frac{au}{2} + ap^0$

0

0

4.

$\frac{k}{\Delta x}$

$\frac{k}{\Delta x}$

$\frac{ae}{2} + \frac{au}{2} + ap^0$

0

0

5.

$\frac{k}{\Delta x}$

0

$\frac{au}{2} + ap^0 + \frac{sp}{ae}$

$\frac{k}{\Delta x}$

$\frac{k}{\Delta x} (T_B + T_B^0)$

(3+1)

$$\text{Node (1)} \quad a_{PTP} = a_E \left(\frac{T_E + T_E^0}{2} \right) + \left(a_p^0 - \frac{a_E}{2} \right) T_p^0$$

$$a_p = \frac{a_E}{2} + a_p^0;$$

$$a_p = \frac{2500}{2} + 20,000 \Rightarrow a_p = 21250$$

$$a_{PTP} = \frac{a_E T_E}{2} + \frac{a_E T_E^0}{2} + \left(a_p^0 - \frac{a_E}{2} \right) T_p^0$$

$$21250 T_p = 1250 T_E + 18750 T_p^0 + 1250 T_E^0$$

$$a_p^0 = \int c \frac{\Delta T}{\Delta t}$$

$$D = \frac{1C - 1B}{\Delta T} = \frac{10}{0.004}$$

$$a_E = \frac{P}{\Delta T} = 2500$$

$$a_p^0 = \int c \frac{\Delta T}{\Delta t} = \frac{10 \times 10^6 \times 0.004}{2}$$

$$a_p^0 = 20,000$$

$$\left(\frac{a_E}{2} = 1250 \right)$$

$$\text{Node (5)} \quad a_{PTP} = a_W \left(\frac{T_W + T_W^0}{2} \right) + \left(a_p^0 - \frac{a_W}{2} - s_p \right) T_p^0 + D(T_B + T_B^0)$$

$$a_p = a_p^0 + \frac{a_W}{2} + s_p = 20000 + 1250 + 2500 = 23750$$

$$a_{PTP} = \frac{a_W T_W}{2} + \frac{a_W T_W^0}{2} + \left(a_p^0 - \frac{a_W}{2} - s_p \right) T_p^0 + D(T_B + T_B^0)$$

$$23750 T_p = 1250 T_W + 1250 T_W^0 + 16250 T_p^0 + 2500 T_B + 2500 T_B^0$$

Node (2) (3) (4)

$$a_{PTP} = a_E \left(\frac{T_E + T_E^0}{2} \right) + a_W \left(\frac{T_W + T_W^0}{2} \right) + \left[a_p^0 - \left(\frac{a_W}{2} + \frac{a_E}{2} \right) \right] T_p^0$$

$$a_p = a_p^0 + \left(\frac{a_W}{2} + \frac{a_E}{2} \right) = 20000 + 2500 = 22500$$

$$22500 T_p = \frac{a_E T_E}{2} + \frac{a_W T_W}{2} + \frac{a_E T_E^0}{2} + \frac{a_W T_W^0}{2} + \left[a_p^0 - \left(\frac{a_W}{2} + \frac{a_E}{2} \right) \right] T_p^0$$

$$22500 T_p = 1250 T_E + 1250 T_W + 1250 T_E^0 + 1250 T_W^0 + 17500 T_p^0$$

2

Node(1) $21250T_P - 1250T_E = 18750T_P^0 + 1250T_E^0$

$\times \begin{matrix} P & E \\ 1 & 2 \end{matrix}$

(3)

~~Node(2)~~

$2125T_P - 125T_E = 1875T_P^0 + 125T_E^0$

Node(2)

$-1250T_W + 22500T_P - 1250T_E = 1250T_E^0 + 1250T_W^0 + 1750T_P^0$

Node(3)

(1) $\sim \begin{matrix} W & P & E \\ 2 & 3 & 1 \end{matrix}$

$\begin{matrix} P & E \\ 1 & 2 & 3 \\ W & & E \end{matrix}$

Node(4)

(1) $\begin{matrix} W & P & E \\ 3 & 4 & 5 \end{matrix}$

Node(5)

~~12500~~ $\begin{matrix} W & P & E \\ 4 & 5 & 1 \end{matrix}$

$125T_W + 2375T_P = 125T_W^0 + 1625T_P^0 + 2500T_B^0$

The matrix $A \vec{T} = b \cdot \vec{x}$

$$\begin{bmatrix} 21250 & -1250 & 0 & 0 & 0 \\ -1250 & 22500 & -1250 & 0 & 0 \\ 0 & -1250 & 24250 & -1250 & 0 \\ 0 & 0 & -1250 & 24250 & -1250 \\ 0 & 0 & 0 & -1250 & 23750 \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \\ T_3 \\ T_4 \\ T_5 \end{bmatrix} = \begin{bmatrix} 18750T_1^0 + 1250T_2^0 \\ 1250T_1^0 + 1750T_2^0 + 1250T_3^0 \\ 1250T_2^0 + 1750T_3^0 + 1250T_4^0 \\ 1250T_3^0 + 1750T_4^0 + 1250T_5^0 \\ 1250T_4^0 + 1625T_5^0 + 2500T_B^0 + 2500T_B \end{bmatrix}$$