

**7 NOVEMBER 2024**

# **ASE 367K: FLIGHT DYNAMICS**

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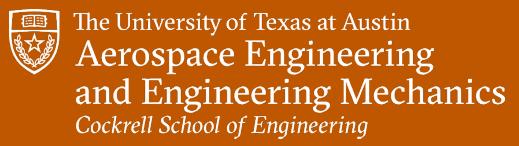
TTH 09:30-11:00  
CMA 2.306

**JOHN-PAUL CLARKE**

Ernest Cockrell, Jr. Memorial Chair in Engineering, The University of Texas at Austin

# Topics for Today

- Topic(s):
  - Rocket (Launch Vehicle) Aerodynamics and Stability
  - Computing the Location of the Center of Pressure



# ROCKET AERODYNAMICS AND STABILITY

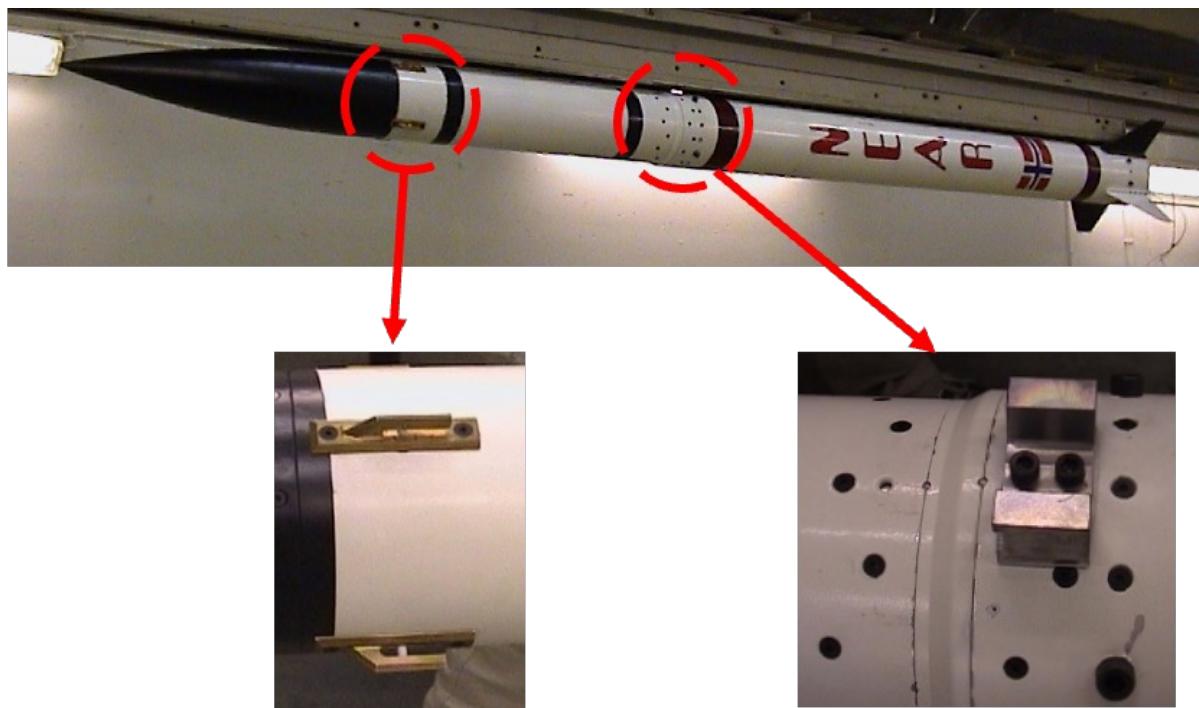
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# What Affects Aerodynamic Drag?

- The Object
  - Size
  - Shape
- Motion
  - Inclination
  - Speed
- Atmosphere
  - Mass
  - Compressibility
  - Viscosity



× 33

# Air Flow Around Objects

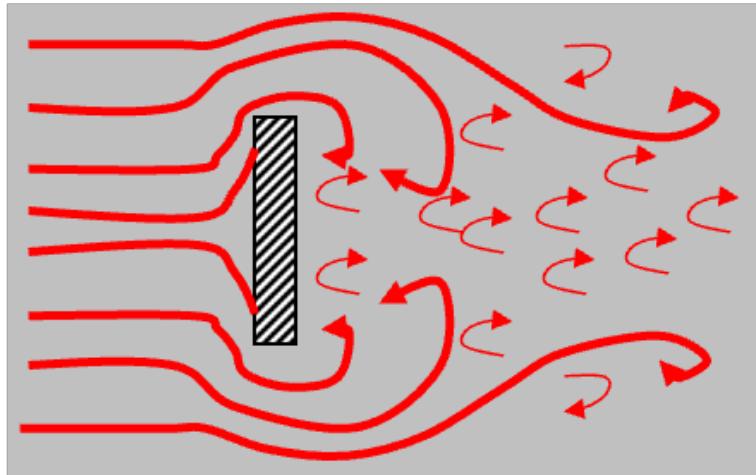
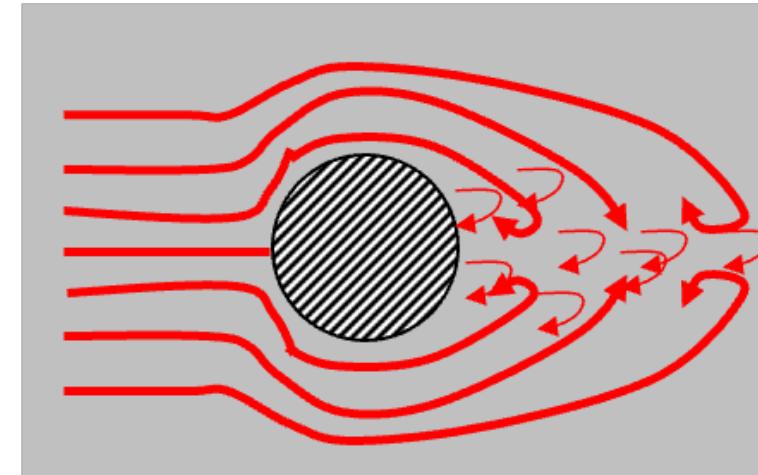
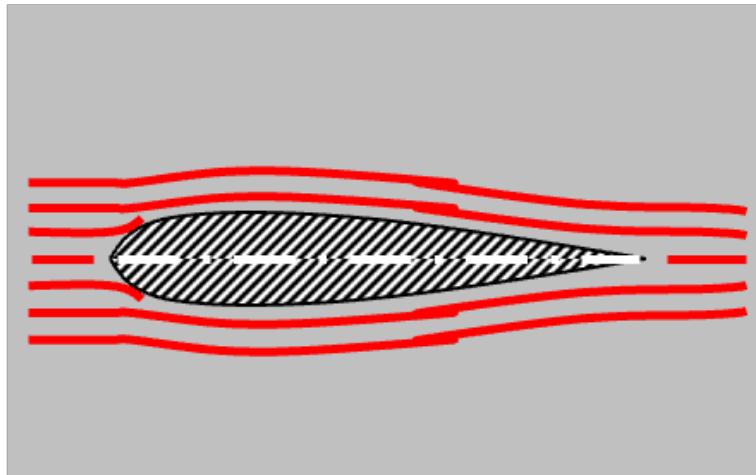


Plate - Induce large resistance



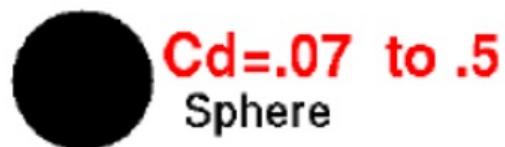
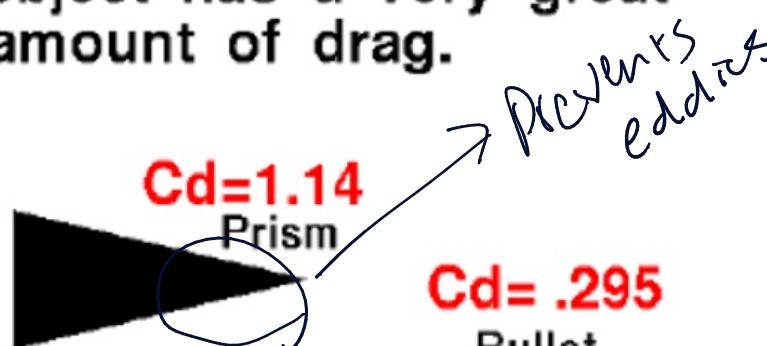
Cylindrical Rod - Lower resistance



Symmetrical wing profile ( $\text{Alpha} = 0^\circ$ ) - Least resistance

# Air Flow Around Objects

The shape of an object has a very great effect on the amount of drag.



$$C_d = \frac{D}{\rho A V^2 / 2}$$

$A = \text{frontal area}$

All objects have the same frontal area.

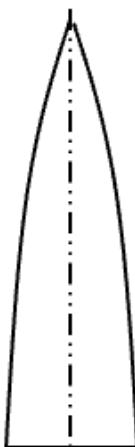


Almost factor 30 better than the flat plate!



# Drag Coefficients for Various Noses

**Cd for different nose design (subsonic velocity) and zero alpha:**



**Cd:** <0.05

>0.01

**0.20**

**0.20**

**0.34**

**0.90**

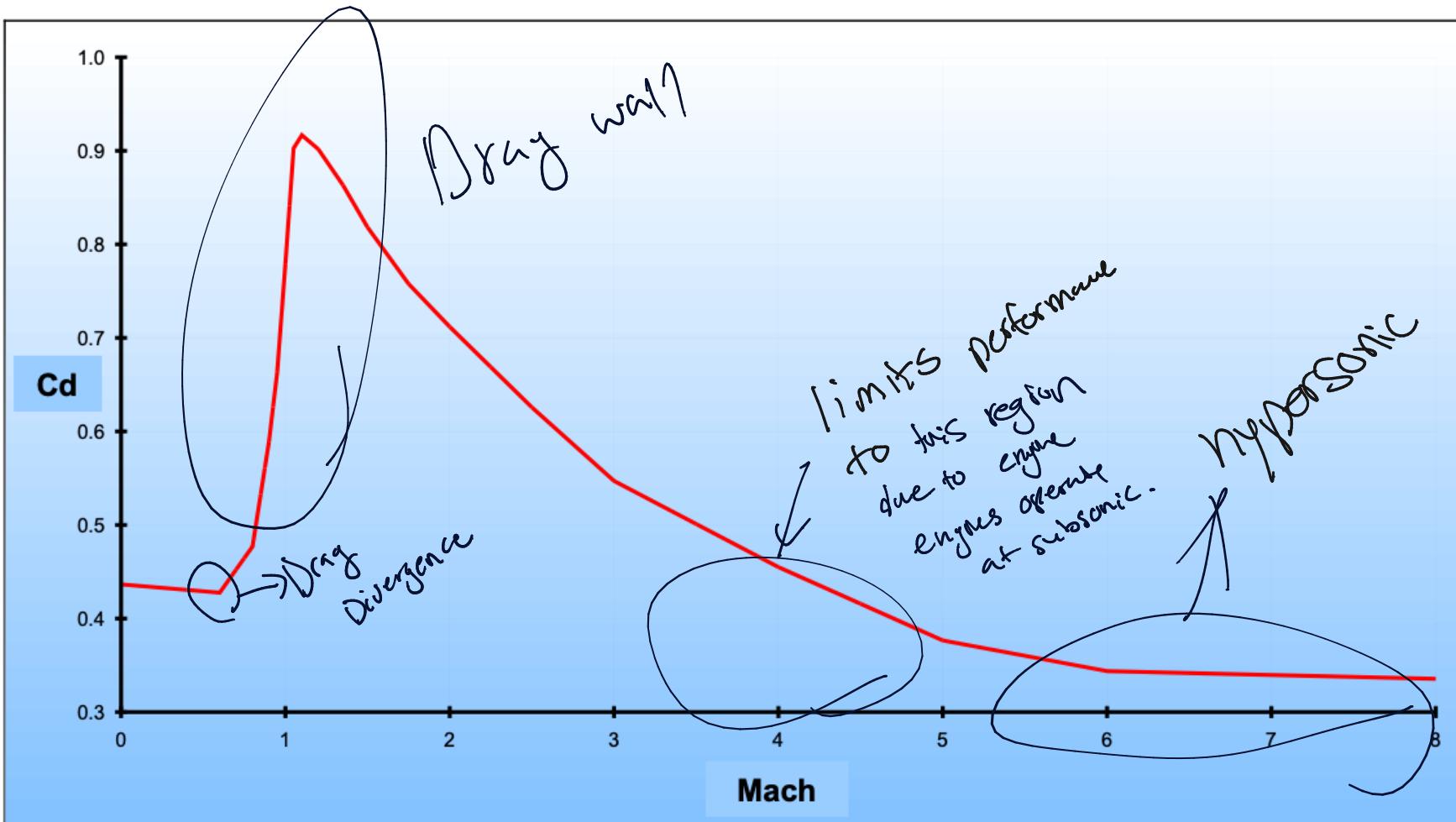
**1.00**

**4:1**

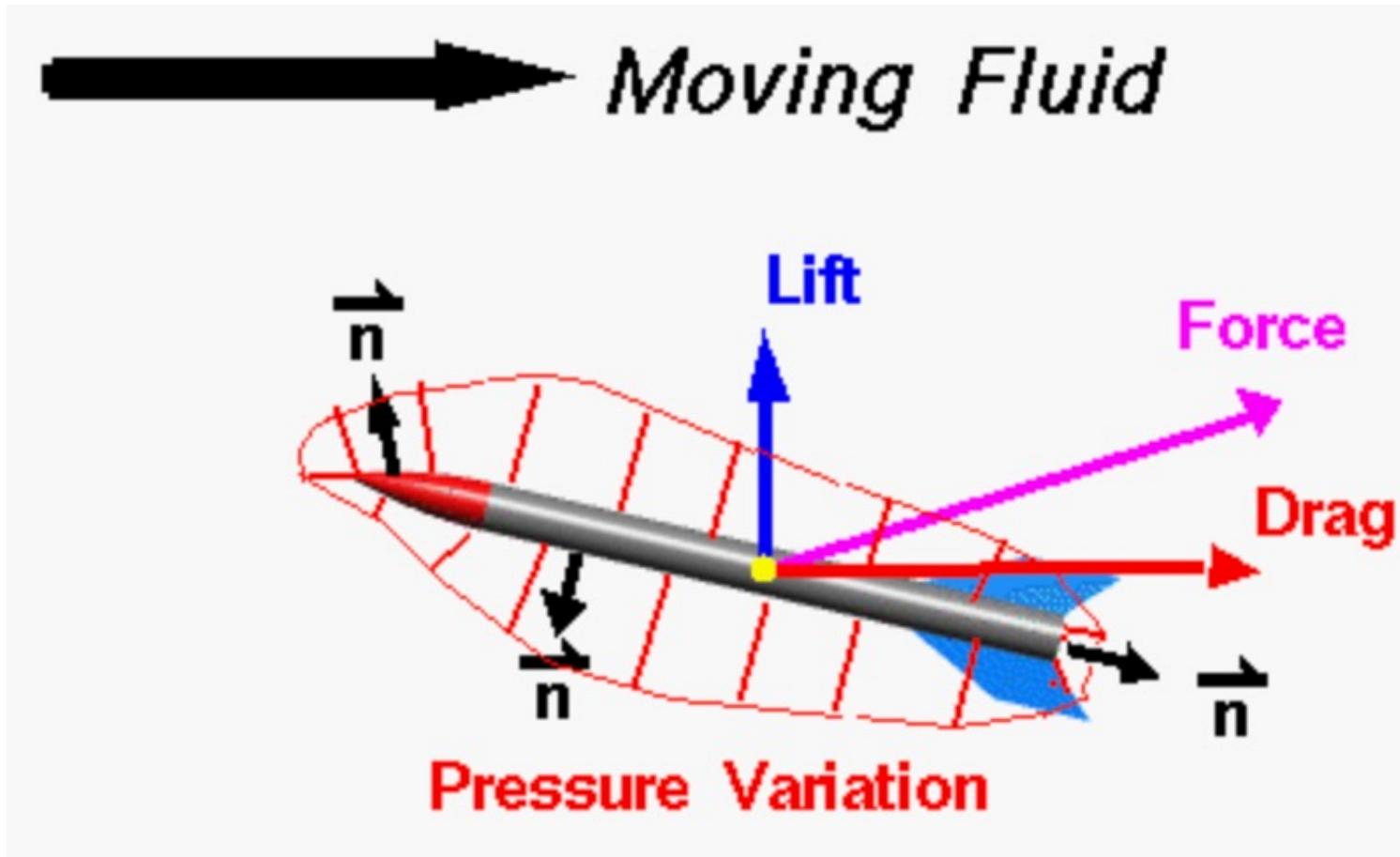
**3:1**

**1:1**

# Drag Coefficient v. Mach Number



# Aerodynamic Forces



L = Lift, net force normal to air flow  
D = Drag, net force parallel to air flow

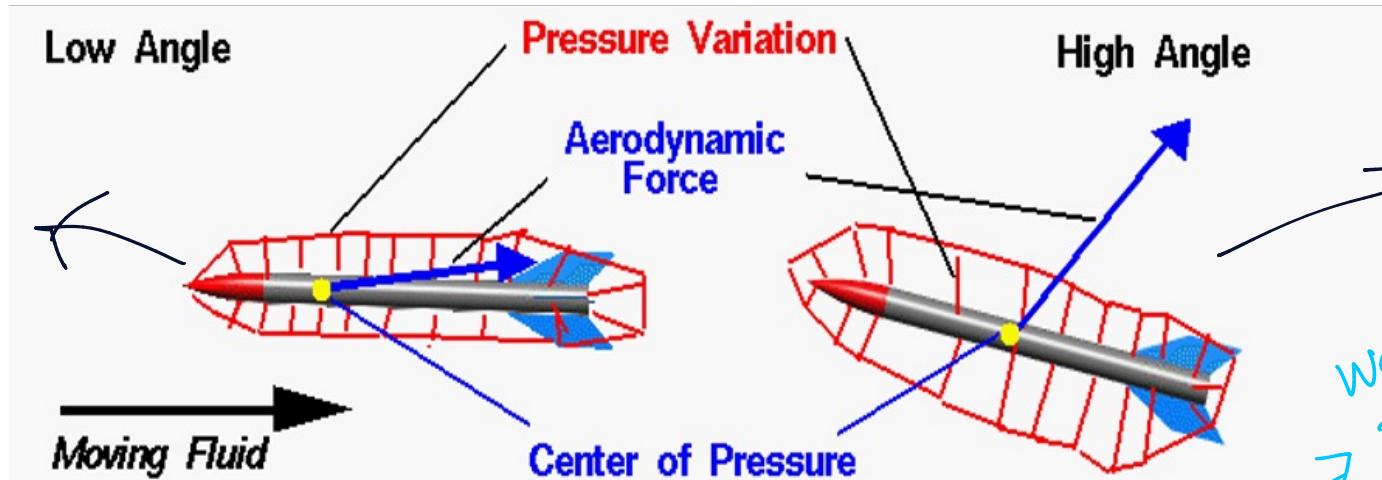
*Symmetrical Rackets*

*Surface integral*

$$\vec{F}_{Aero} = \sum_{\text{Surface}} p \cdot \vec{n} \cdot \vec{A} = \oint p \cdot \vec{n} \cdot d\vec{A}$$

# Center of Pressure

$C_P$  = Weighted sum of pressure.



Center of Pressure is the average location of the pressure.  
Pressure varies around the surface of an object.  $P = P(x)$

$$C_P = \frac{\int x \cdot p(x) \cdot dx}{\int p(x) \cdot dx}$$

Aerodynamic force acts through the center of pressure.

Center of pressure moves with angle of attack.

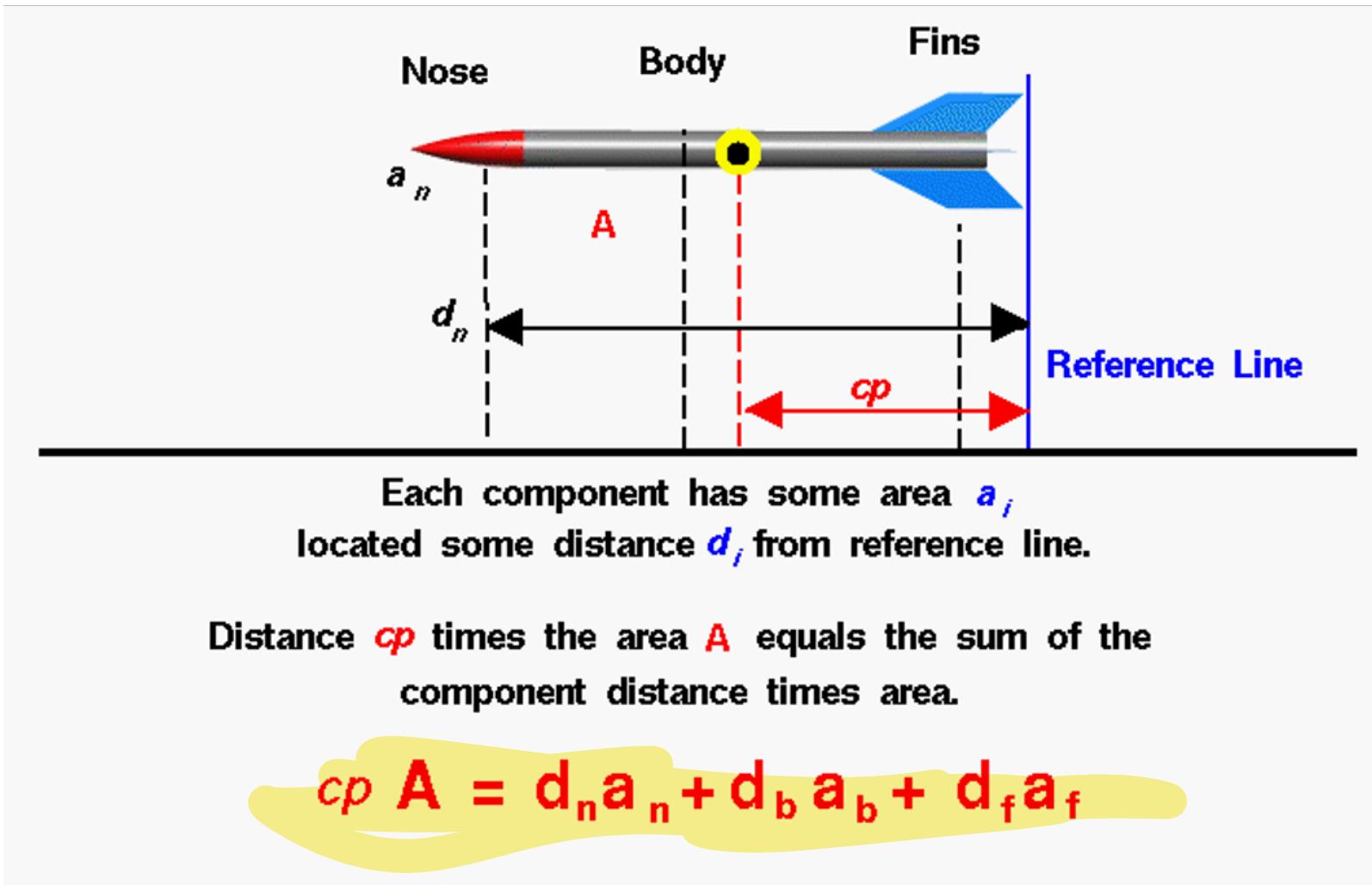
Assuming pressures are distributed evenly over the area over the surface

Sockets are symmetric so we can dismiss it out of page

$C_P$  back  
We are looking at thin foil just to find location of CP. also assuming the airfoil is symmetric about its full axis (x)  
"Moment" =  $(\text{pressure} \times \text{Area}) \times \text{distance}(x)$   
"Force" = pressure  $\times$  "Area" Form  
Normalization by net pressure

Not aerodynamic center

# Center of Pressure

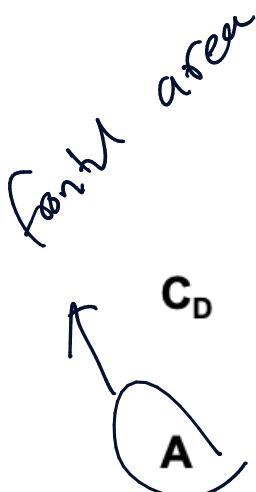


Taken from ref.: <http://exploration.grc.nasa.gov/education/rocket/cp.html>

# Rocket Drag Equation

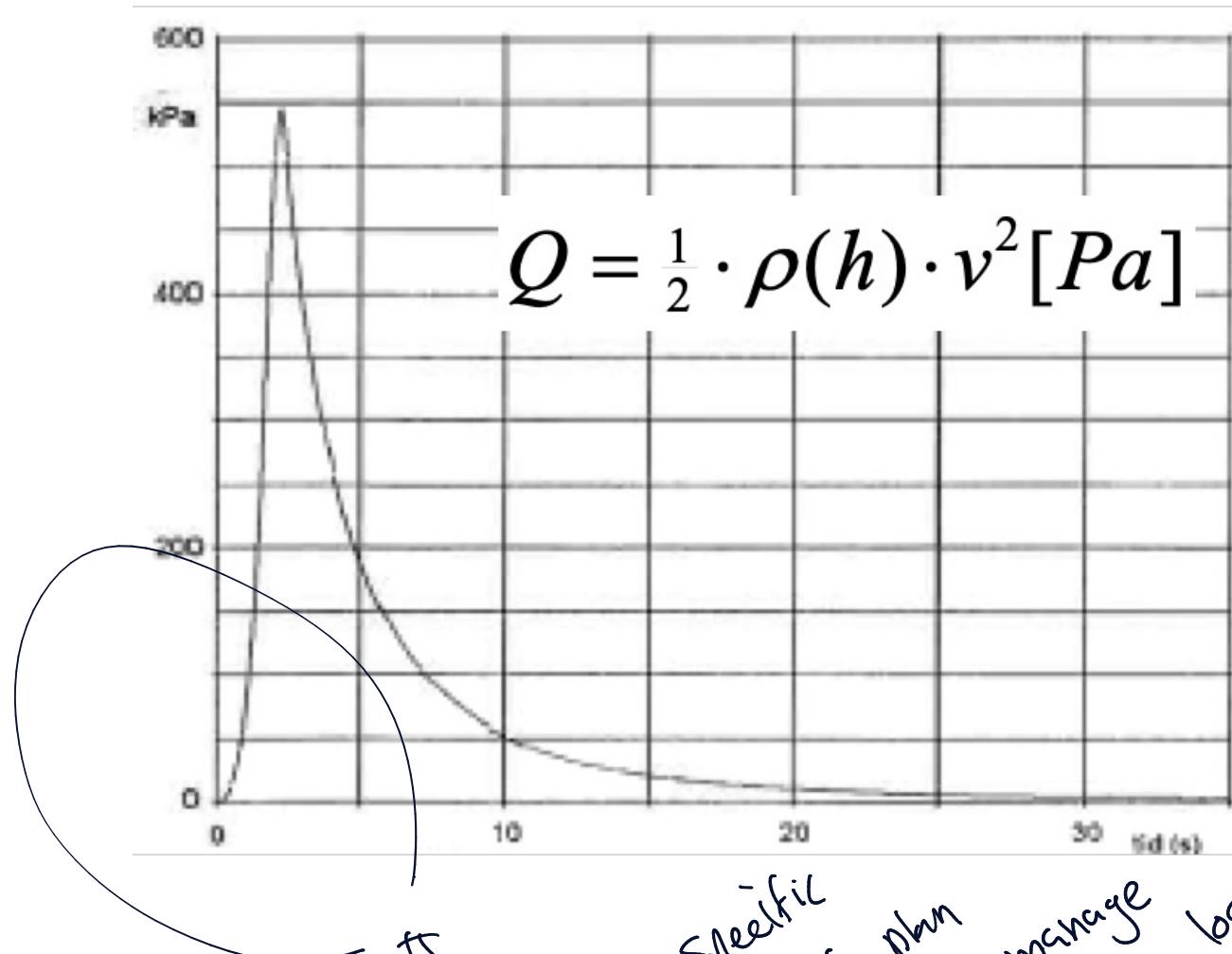
$$D = C_D(M, \alpha) \cdot A \cdot \frac{\rho \cdot v^2}{2} [N]$$

→ Dynamic Pressure



- : Drag coefficient. Contains all complex dependencies like air compressibility, viscosity, body shape and angle-of-attack.
- : Reference area, typically the base diameter of the nose. Different A, affect the value of C<sub>D</sub>.
- : Density of the atmosphere of consideration (typically 1.23kg/m<sup>3</sup> for air at sea-level).
- : Rocket speed

# Dynamic Load

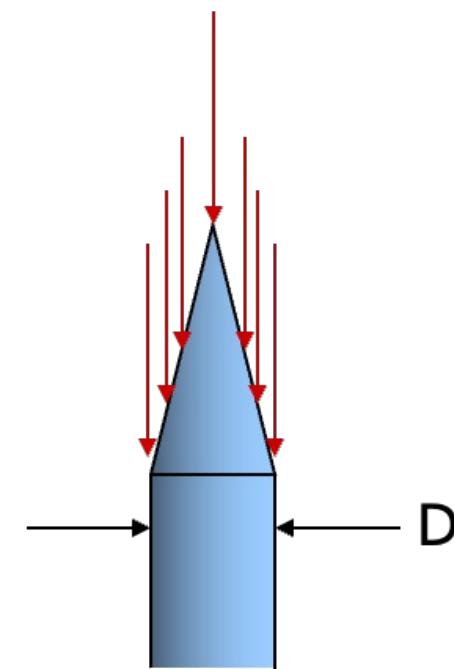


Plan acceler

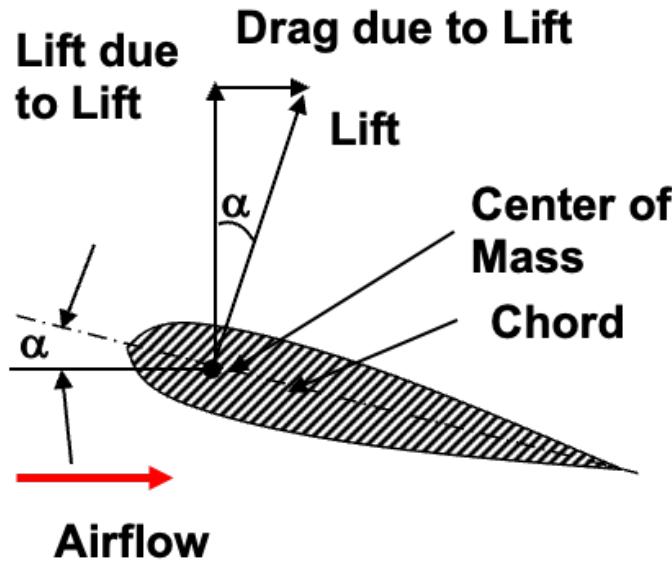
Student Rocket: dynamic load affect heat load,

$D = \emptyset 70\text{mm} \rightarrow 0.07\text{m}$

$$A = \frac{\pi \cdot D^2}{4} \Rightarrow 0.00385\text{m}^2$$
$$F_{\max} = Q_{\max} \cdot A \Rightarrow 550000 \cdot 0.00385 = 2117.5\text{N} \approx 216.0\text{kg}$$



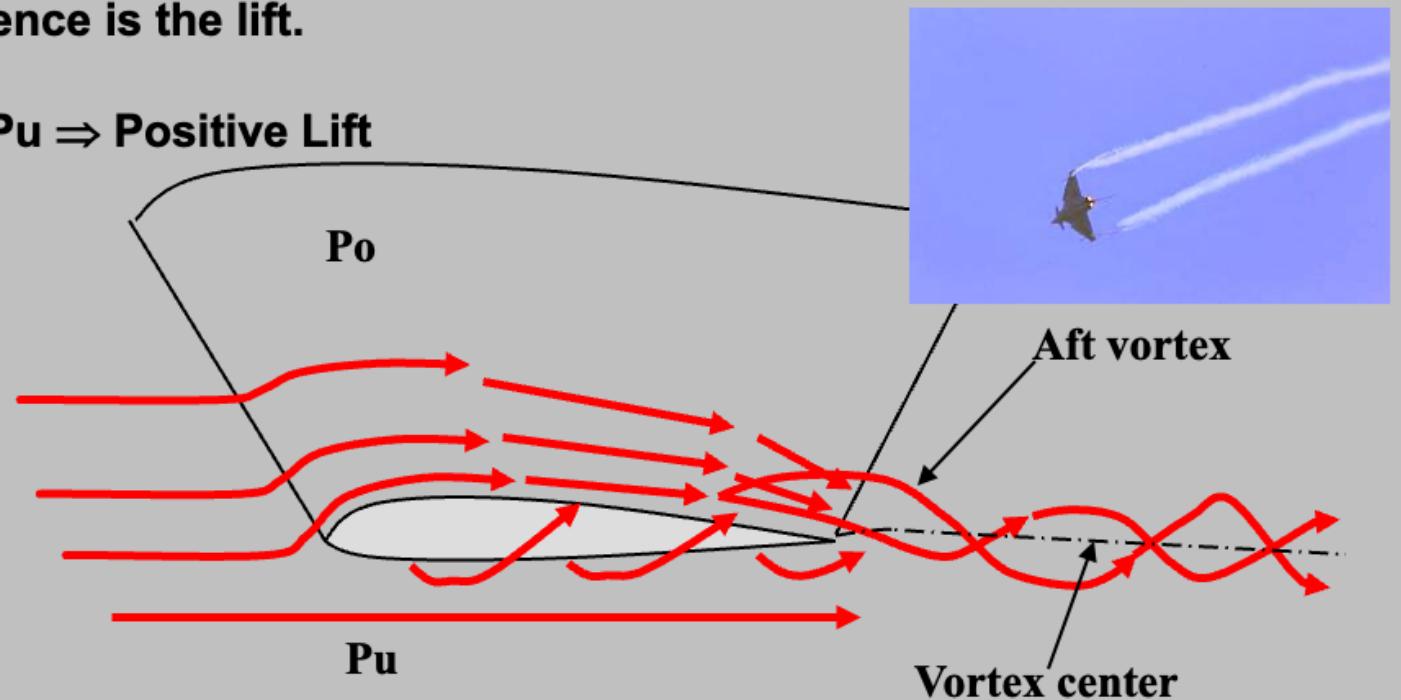
# Induced Drag



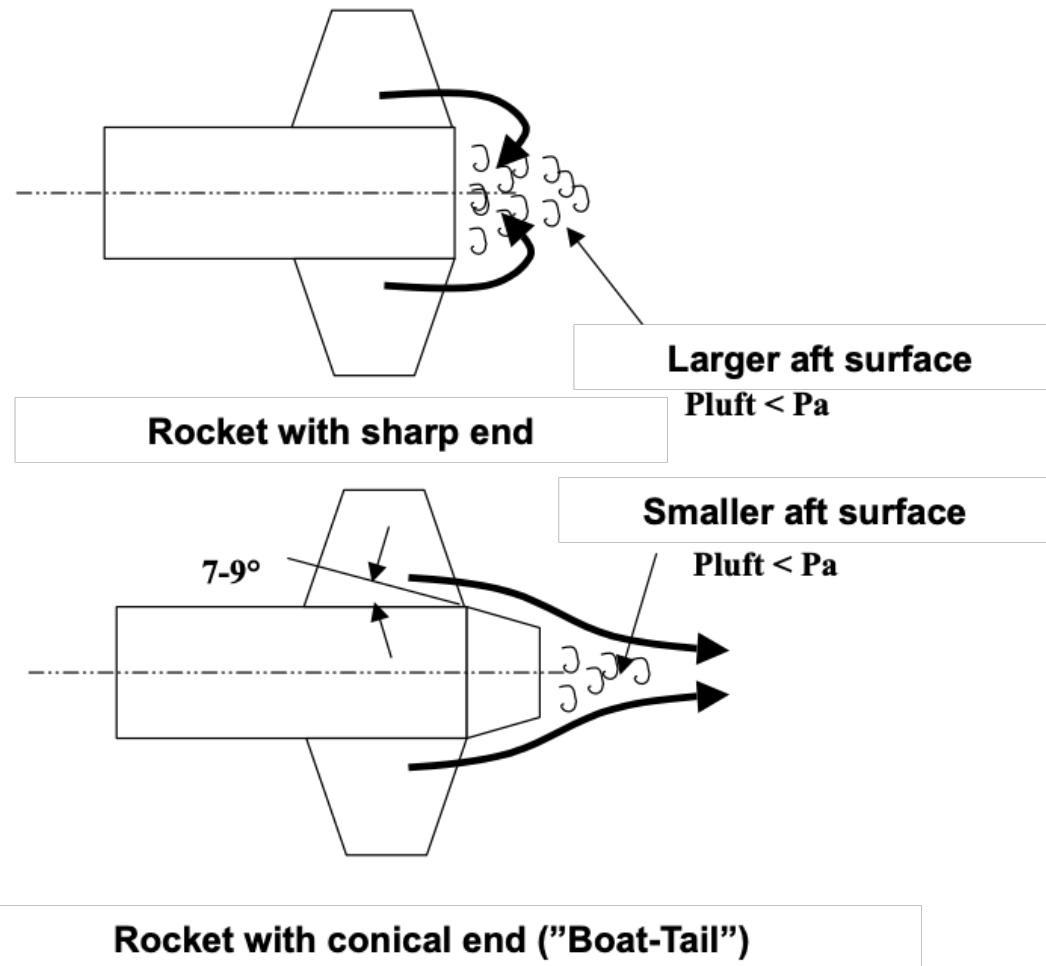
A symmetrical wing/fin will generate lift when  $| \alpha | > 0^\circ |$

A unsymmetrical fin / wing in an airflow will have excess pressure on the face with least surface (often on the side facing down) and low pressure on the opposite face with largest surface. The pressure difference is the lift.

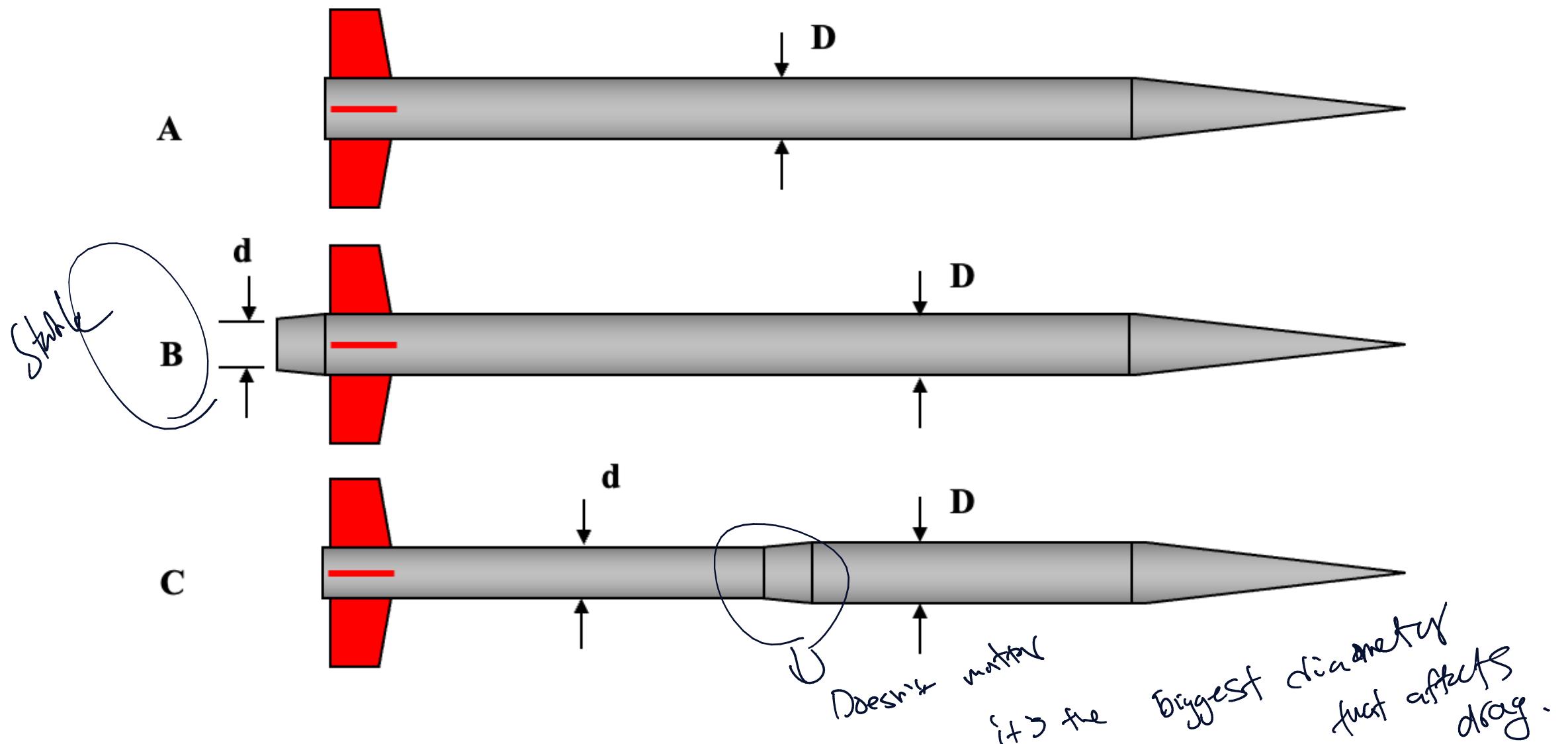
$P_o > P_u \Rightarrow \text{Positive Lift}$



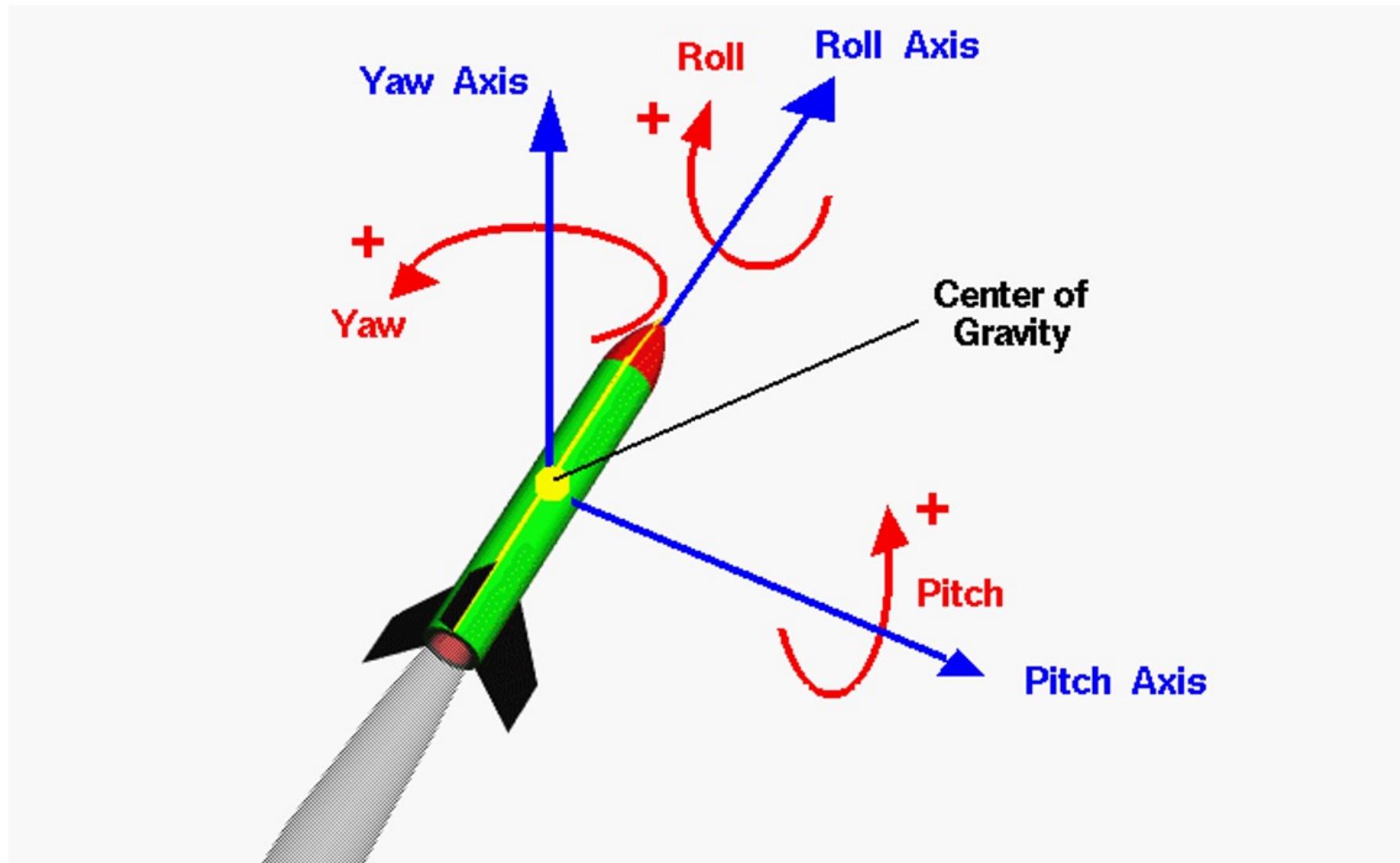
# Drag Reduction



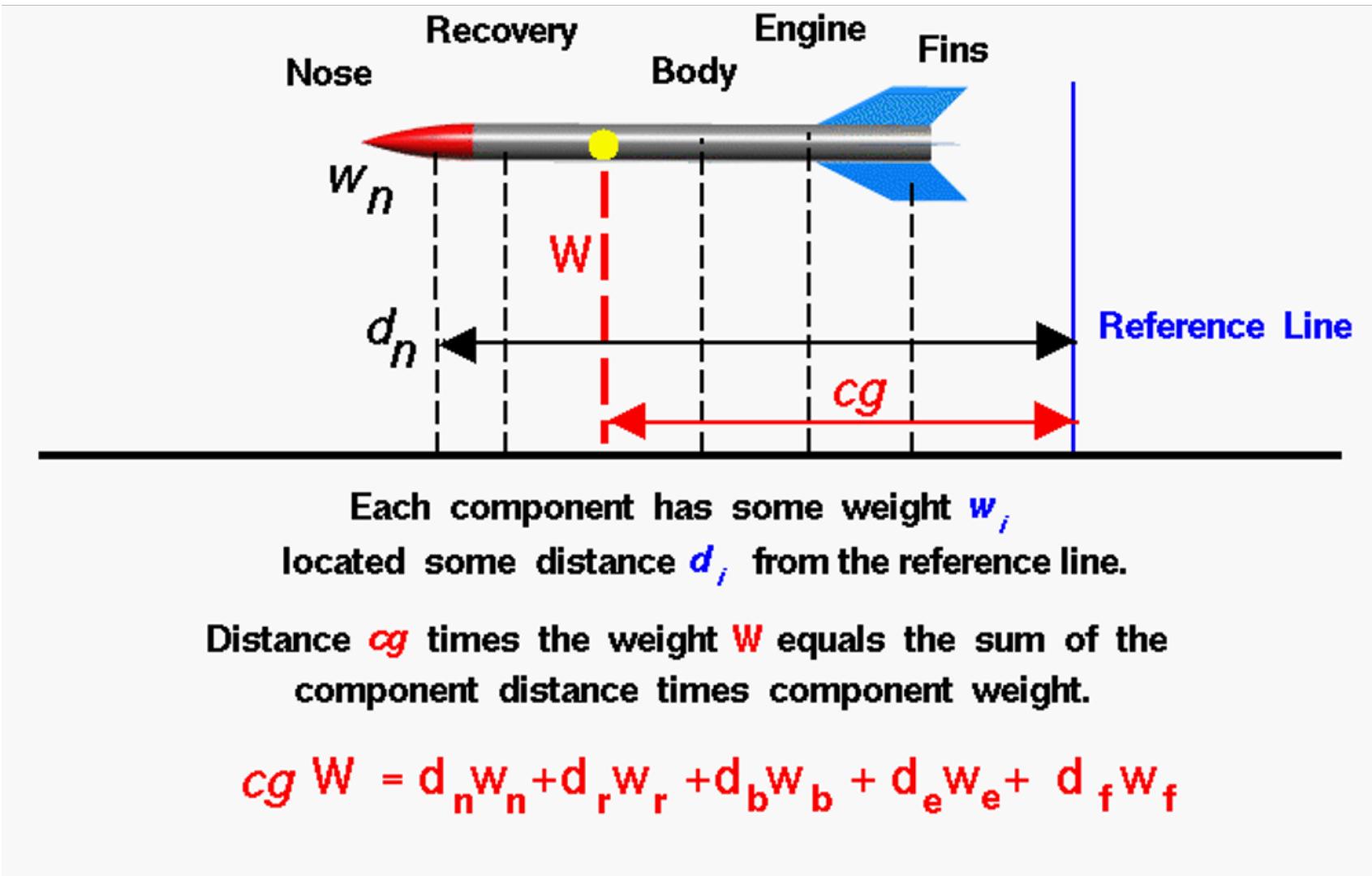
# What Rocket Shape has the Highest Drag?



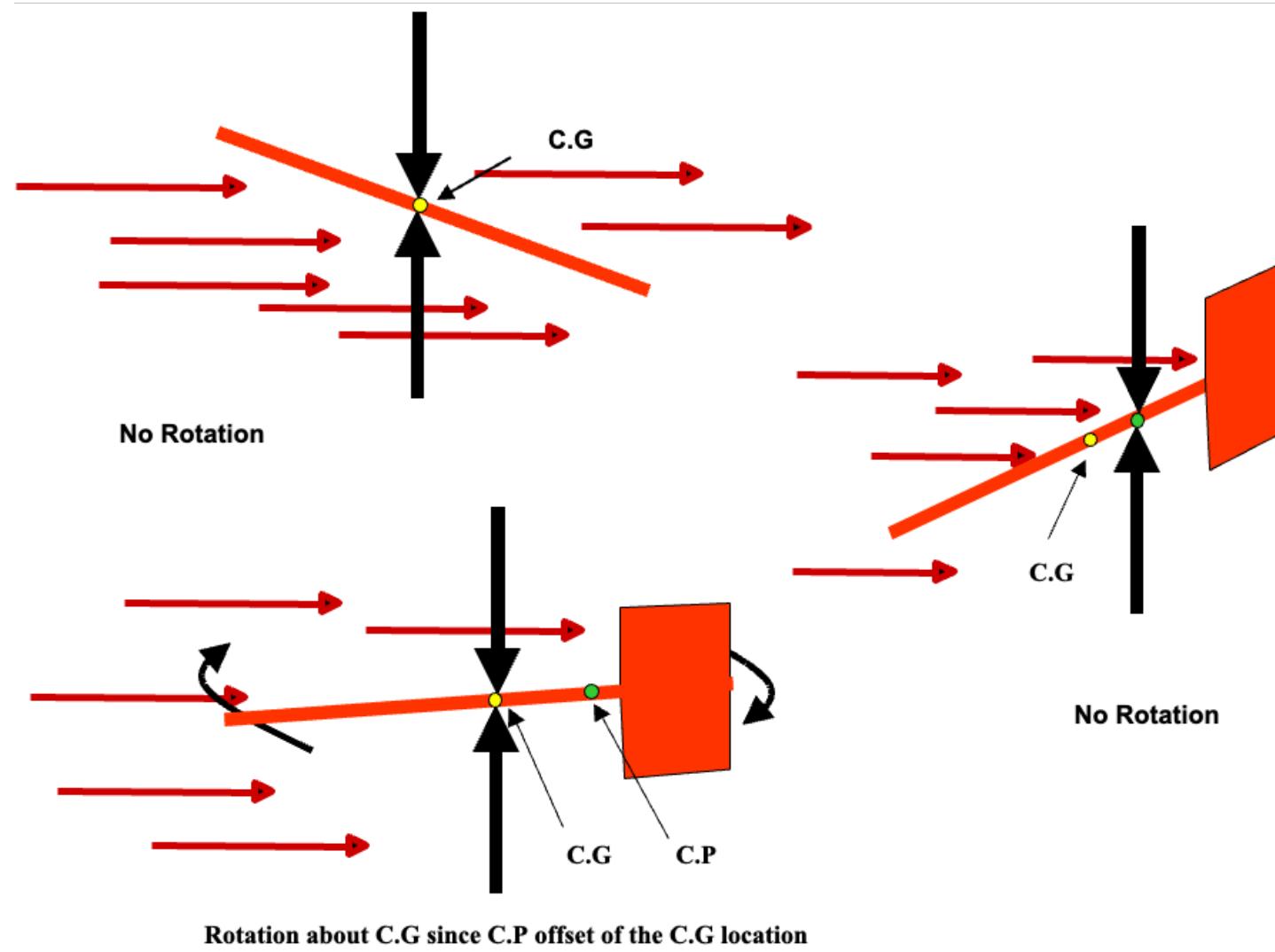
# Axes



# Center of Gravity

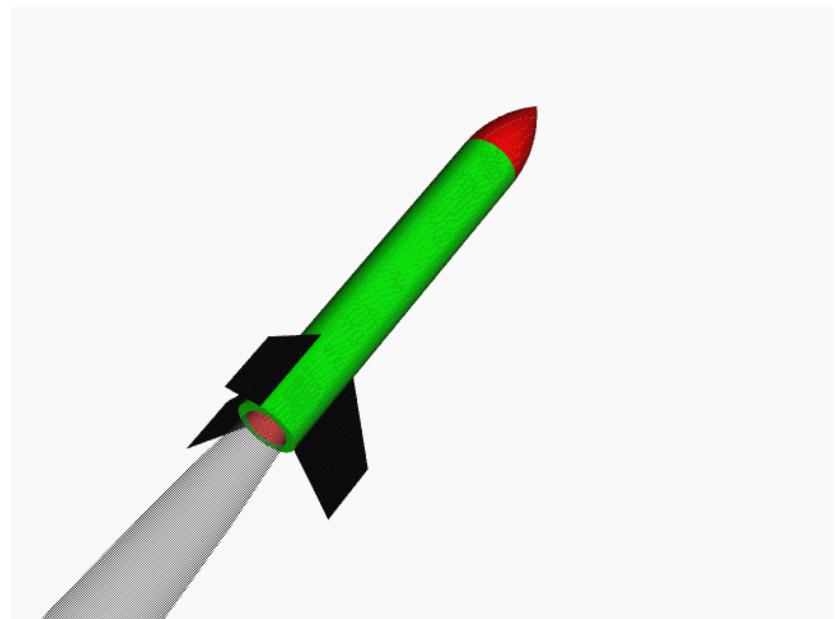


# Weathercock (Passive) Stability



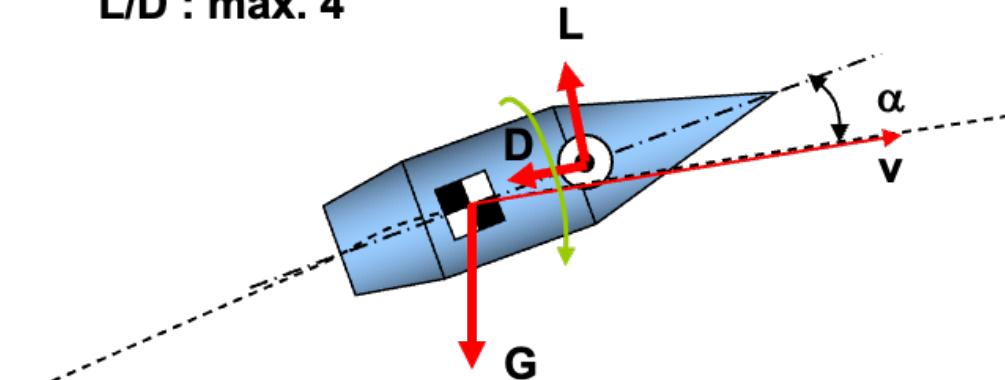
fins to provide Weathercock stability -

# Spin Stabilization

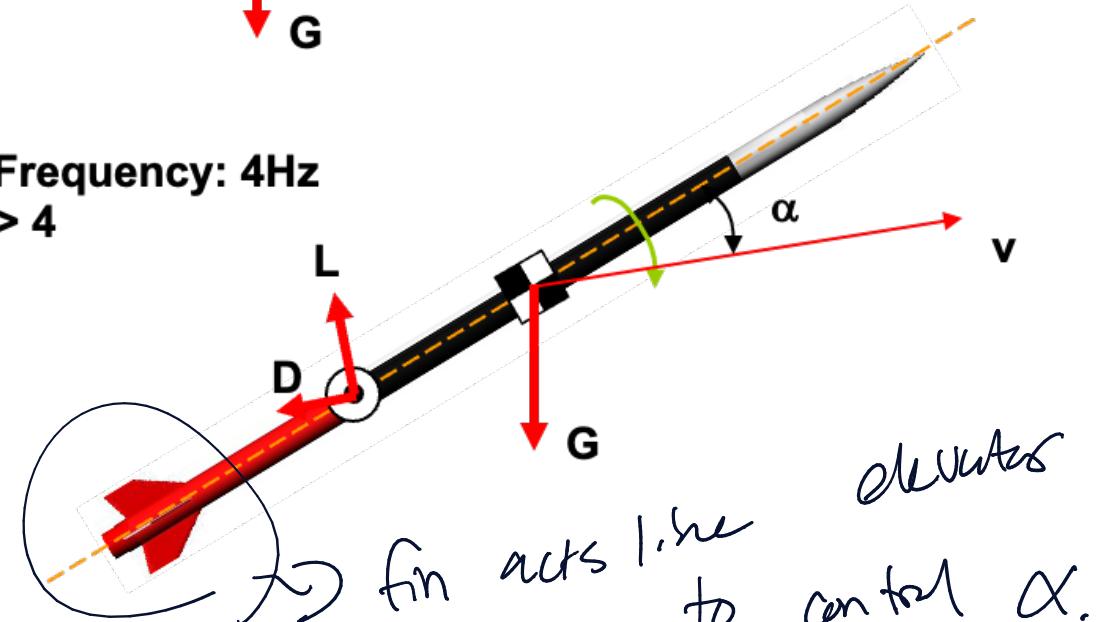


*h is constant  
w/r inertial space*

**Spin Frequency: 2000Hz**  
**L/D : max. 4**



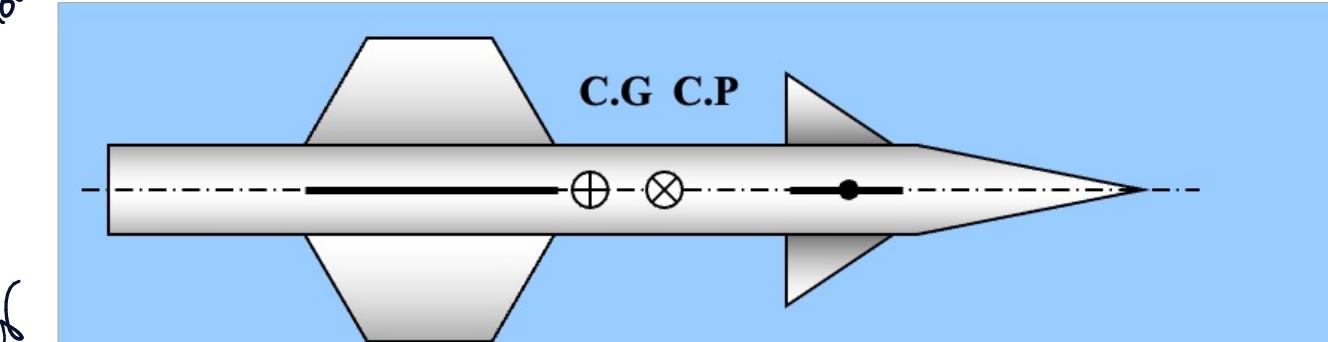
**Spin Frequency: 4Hz**  
**L/D : > 4**



*Rocket body symmetry helps*

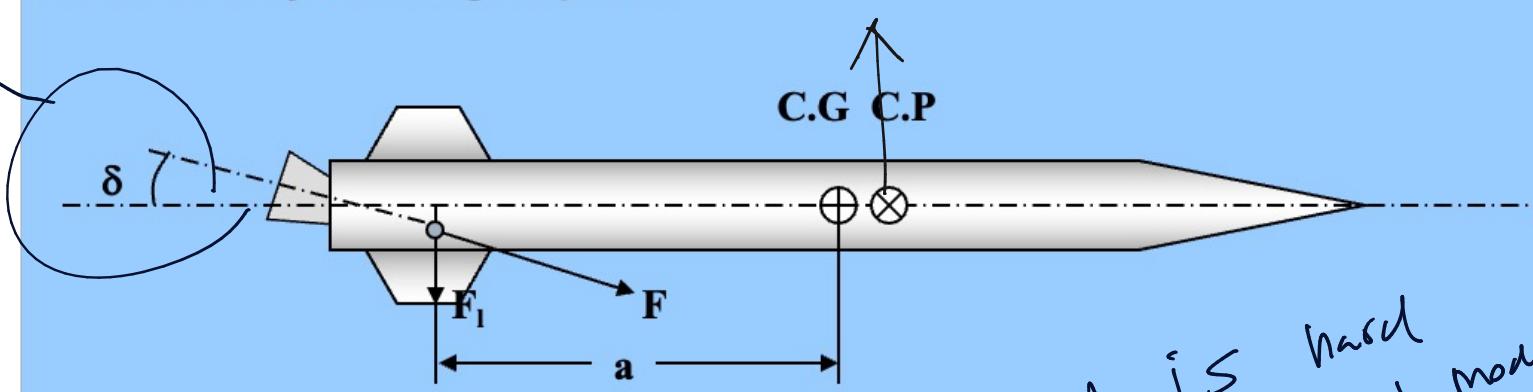
# Active Stabilization

(Ans-1)  
How Sait is  
my model?  
How fast is



gyroscopic  
moment

C.G  
(can be moved  
back and forth  
during flight)



symbol is hard  
you need good  
it is a nonminimum  
phase system.



Naturally dynamic unstable, but maintained stable due to an automatic attitude system. Trajectory and stability can be maintained by moving servo controlled fins or by use of side thrusters. A thrust vectoring system (TVC) can also be used. A TVC system is a device that can change the thrust vector by changing the orientation of the nozzle or by deflecting the plume.



What control scheme do you use?  
to keep CG in front of CP for concave  
non minimum phase problem with rockets

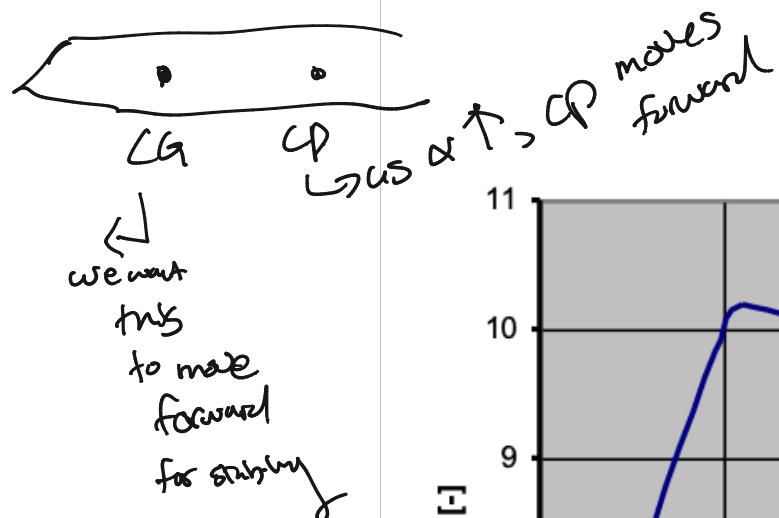
# Thrust Vectoring



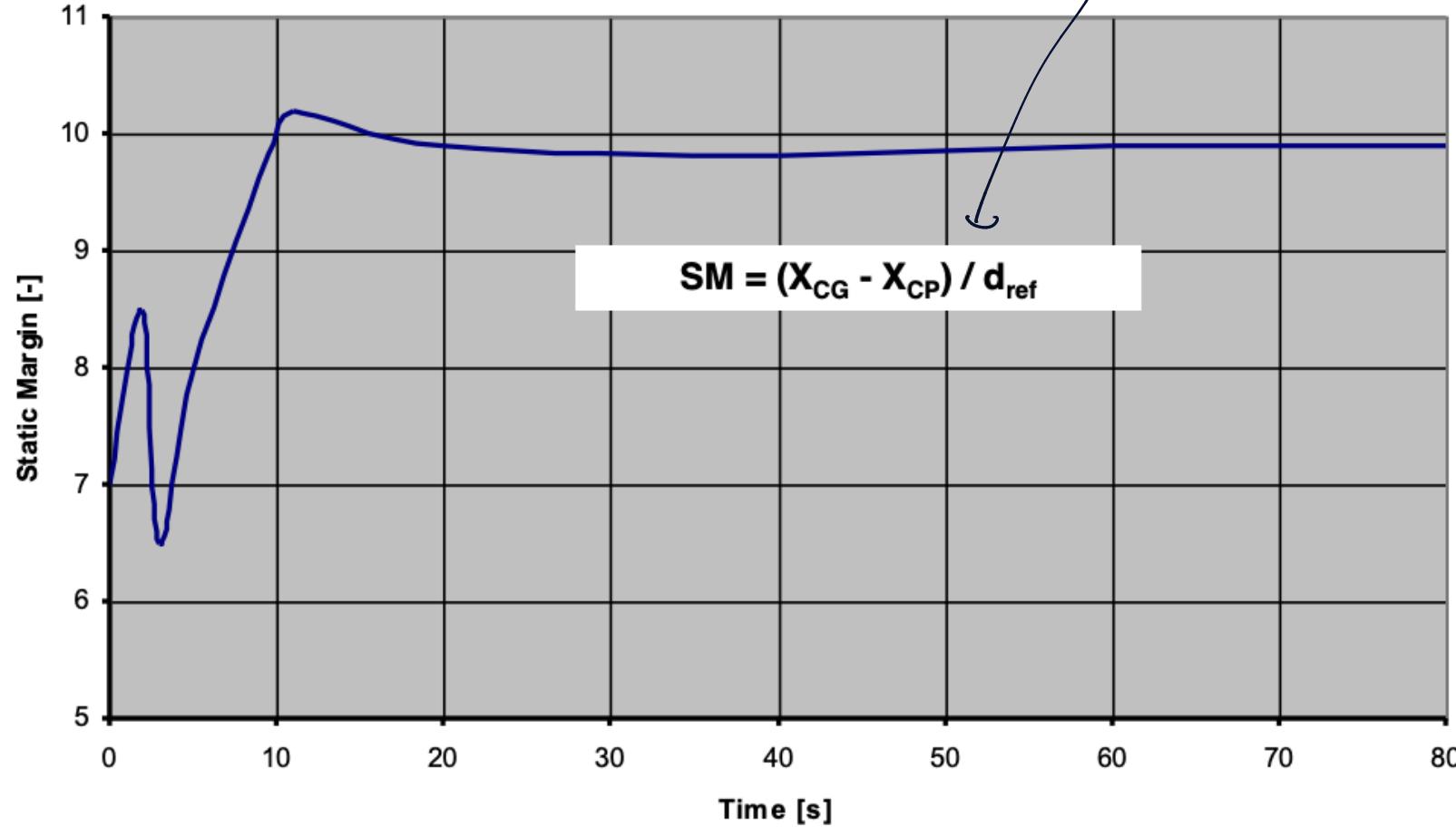
**IRIS-T Air-To-Air Jet Vane TVC System**

$\uparrow SM$   
= more stability

**Static Margin** = distance btwn CG and C.P.



Static Margin vs. Time  
SCA2005 Rocket



for this case

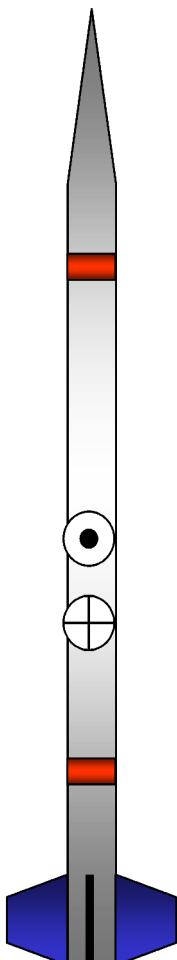
Neutral point: Aerodynamic center  
the pitch moment  
due to  $\alpha$  stays  
constant

\* This is showing  
how SM changes  
throughout its flight

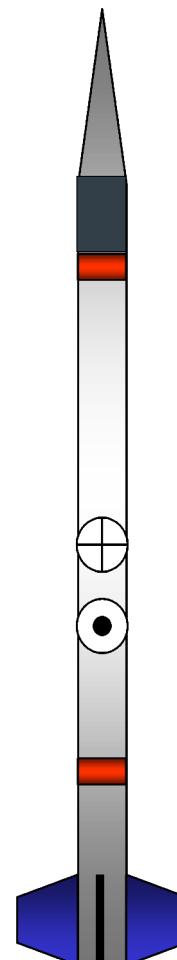
a.c. is used  
for longitudinal  
stability.

# Which of these are stable? And why?

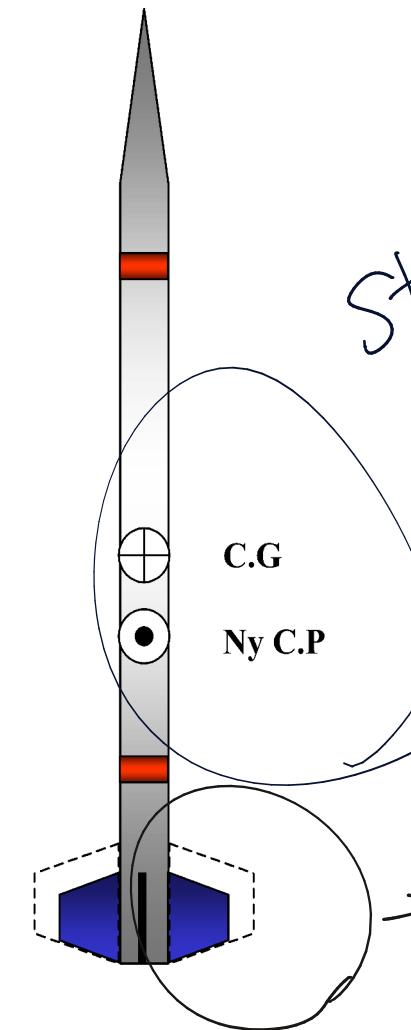
More water resistance means ↑ drag.



C.P  
C.G

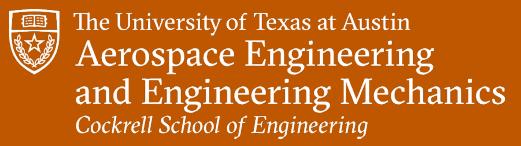


Ny C.G  
C.P



Stable

bigger fin  
shifts C.P.  
towards the  
tail  
this ↑ S.M.



# COMPUTING LOCATION OF THE CENTER OF PRESSURE

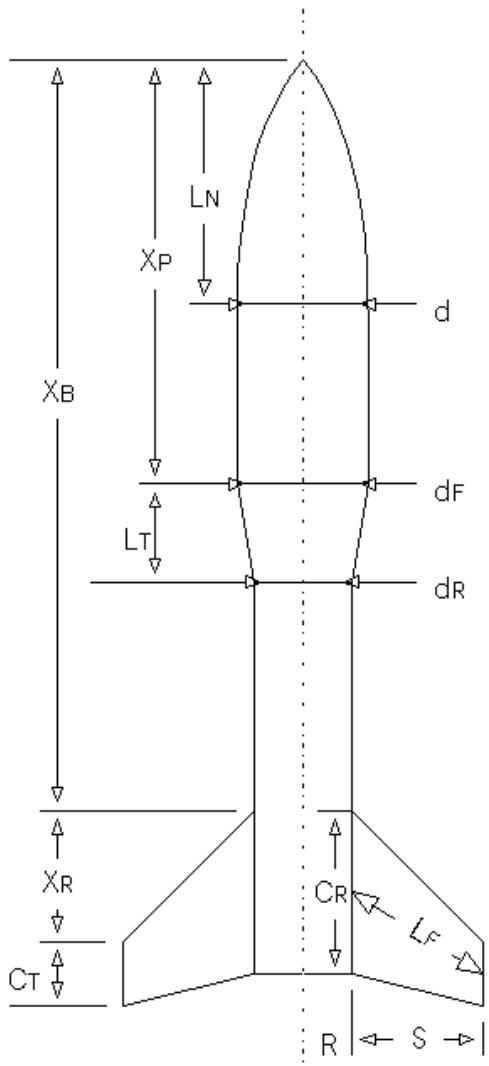
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# Barrowman Equations

useful for  
 $C_p$



$L_N$  = length of nose

$d$  = diameter at base of nose

$d_F$  = diameter at front of transition

$d_R$  = diameter at rear of transition

$L_T$  = length of transition

$X_P$  = distance from tip of nose to front of transition

$C_R$  = fin root chord

$C_T$  = fin tip chord

$S$  = fin semispan

$L_F$  = length of fin mid-chord line

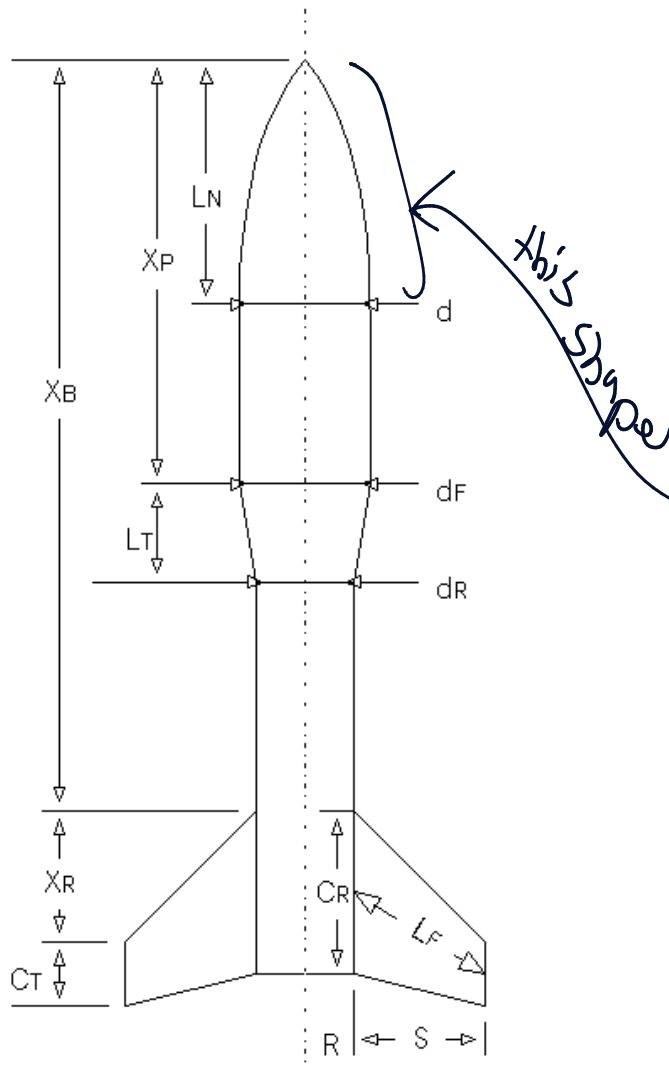
$R$  = radius of body at aft end

$X_R$  = distance between fin root leading edge and fin tip leading edge parallel to body

$X_B$  = distance from nose tip to fin root chord leading edge

$N$  = number of fins

# Barrowman Equations



$$\bar{X} = \frac{(C_N)_N X_N + (C_N)_T X_T + (C_N)_F X_F}{(C_N)_R}$$

## NOSE

$$(C_N)_N = 2$$

$$\text{For Cone: } X_N = 0.666L_N$$

$$\text{For Ogive: } X_N = 0.466L_N$$

## TRANSITION

$$(C_N)_T = 2 \left[ \left( \frac{d_R}{d} \right)^2 - \left( \frac{d_F}{d} \right)^2 \right]$$

$$X_T = X_P + \frac{L_T}{3} \left[ 1 + \frac{1 - \frac{d_F}{d_R}}{1 - \left( \frac{d_F}{d_R} \right)^2} \right]$$

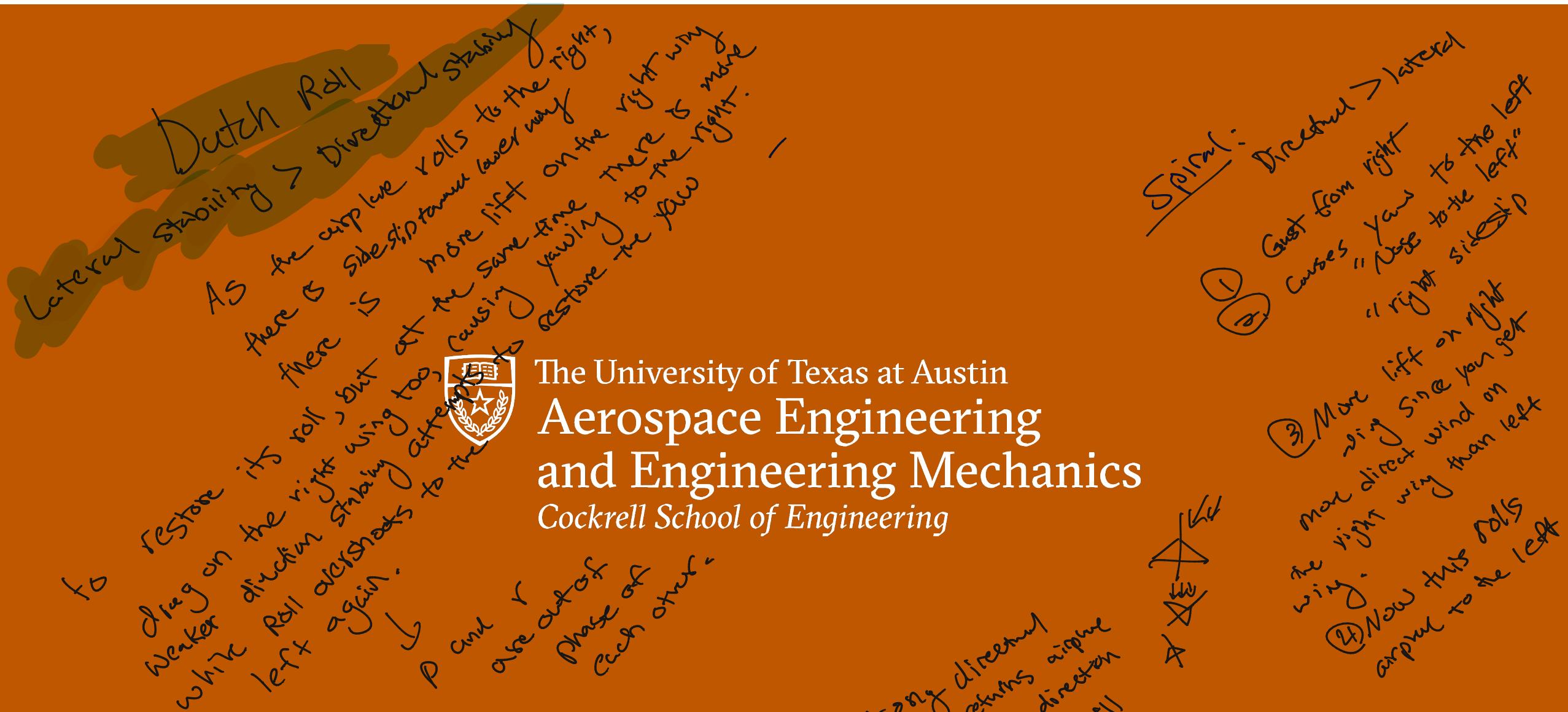
## FIN

$$(C_N)_F = \left[ 1 + \frac{R}{S+R} \right] \left[ \frac{4N \left( \frac{S}{d} \right)^2}{1 + \sqrt{1 + \left( \frac{2L_F}{C_R + C_T} \right)^2}} \right]$$

$$X_F = X_B + \frac{X_R}{3} \frac{(C_R + 2C_T)}{(C_R + C_T)} + \frac{1}{6} \left[ (C_R + C_T) - \frac{(C_R C_T)}{(C_R + C_T)} \right]$$

↳ Good estimate of CP

OML  
Outer Moll line



# The University of Texas at Austin Aerospace Engineering and Engineering Mechanics

## Cockrell School of Engineering

- Strong directional stability returns airplane to its original direction
- Airplane is still rolled to the left.
- Weak lateral stability doesn't allow the airplane to recover its roll.
- Yawing back to its original direction