

**24 SEPTEMBER 2024**

# **ASE 367K: FLIGHT DYNAMICS**

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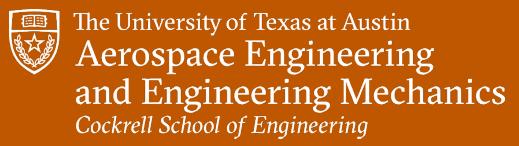
TTH 09:30-11:00  
CMA 2.306

**JOHN-PAUL CLARKE**

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# **Topics for Today**

- Topic(s):
  - Straight and Level Flight
  - Cruise Range



# STRAIGHT AND LEVEL FLIGHT

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Power = Watts  
= Force x Velo.

increase speed  
cause Federal  
in & for propellers  
causes & in lift for  
propeller which is  
max

# Typical Effects of Altitude and Velocity on Power and Thrust

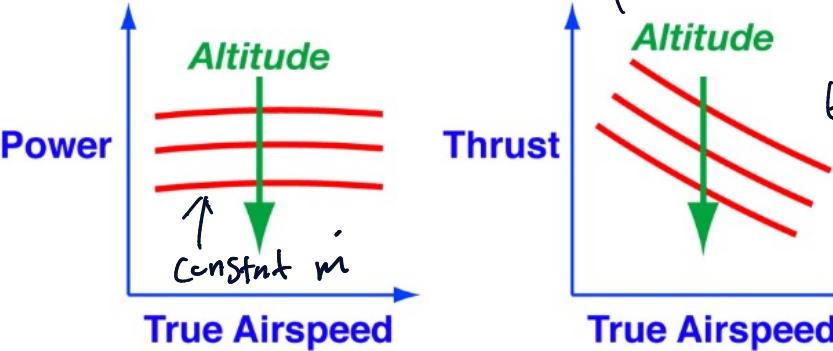
\* Propeller:  
in effects how  
much power is  
available, not thrust.  
because fuel is  
supplied to an engine  
that rotates  
the propeller.

It doesn't directly  
create thrust. Thrust  
depends on power.

Jet: The in  
directly influence  
thrust by

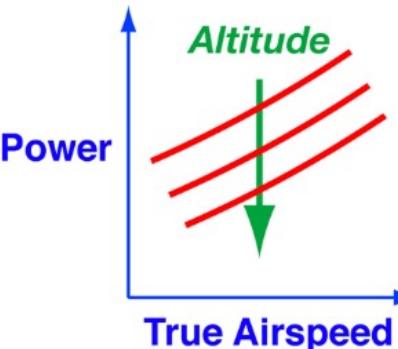
bringing in more  
air. Power depends  
on thrust

- **Propeller**  
[Air-breathing engine]

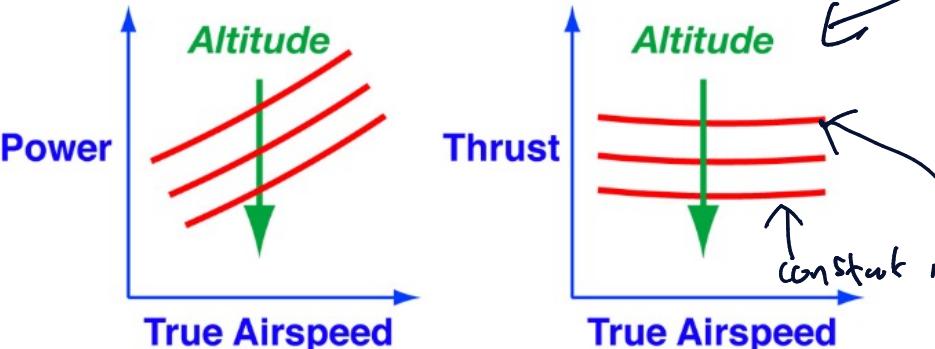


- **Turbofan**

### [In between]



- **Turbojet**



- **Battery**

### [Independent of altitude and airspeed]

This means  
propeller: in related  
to power, P  
Jet: in related to  
thrust.

Propeller  
becomes less efficient

In  
keep P  
constant  
thrust  
and power  
just depends  
on thrust.

this line  
indicates max  
thrust & can  
exist.

# Performance Parameters

$L$ : lift  
~ how much work lift is doing

## Lift-to-Drag Ratio

$$L/D = C_L / C_D$$

## Load Factor

$$n = L/W = L/mg, "g"s$$

## Thrust-to-Weight Ratio

$$T/W = T/mg, "g"s$$

must be larger than 1 for rocket and fighters

how much

## Wing Loading



$$W/S, \text{ } N/m^2 \text{ or } lb/ft^2$$

# Trimmed Lift Coefficient, $C_L$

- Trimmed lift coefficient,  $C_L$

- Proportional to weight and wing loading factor,  $W/S$
- Decreases with  $V^2$
- At constant true airspeed, increases with altitude

$$W = C_{L_{trim}} \left( \frac{1}{2} \rho V^2 \right) S = C_{L_{trim}} \bar{q} S$$

$$C_{L_{trim}} = \frac{1}{\bar{q}} (W/S) = \frac{2}{\rho V^2} (W/S)$$

The faster you go, the lower you can get. This goes down as you go up in altitude.

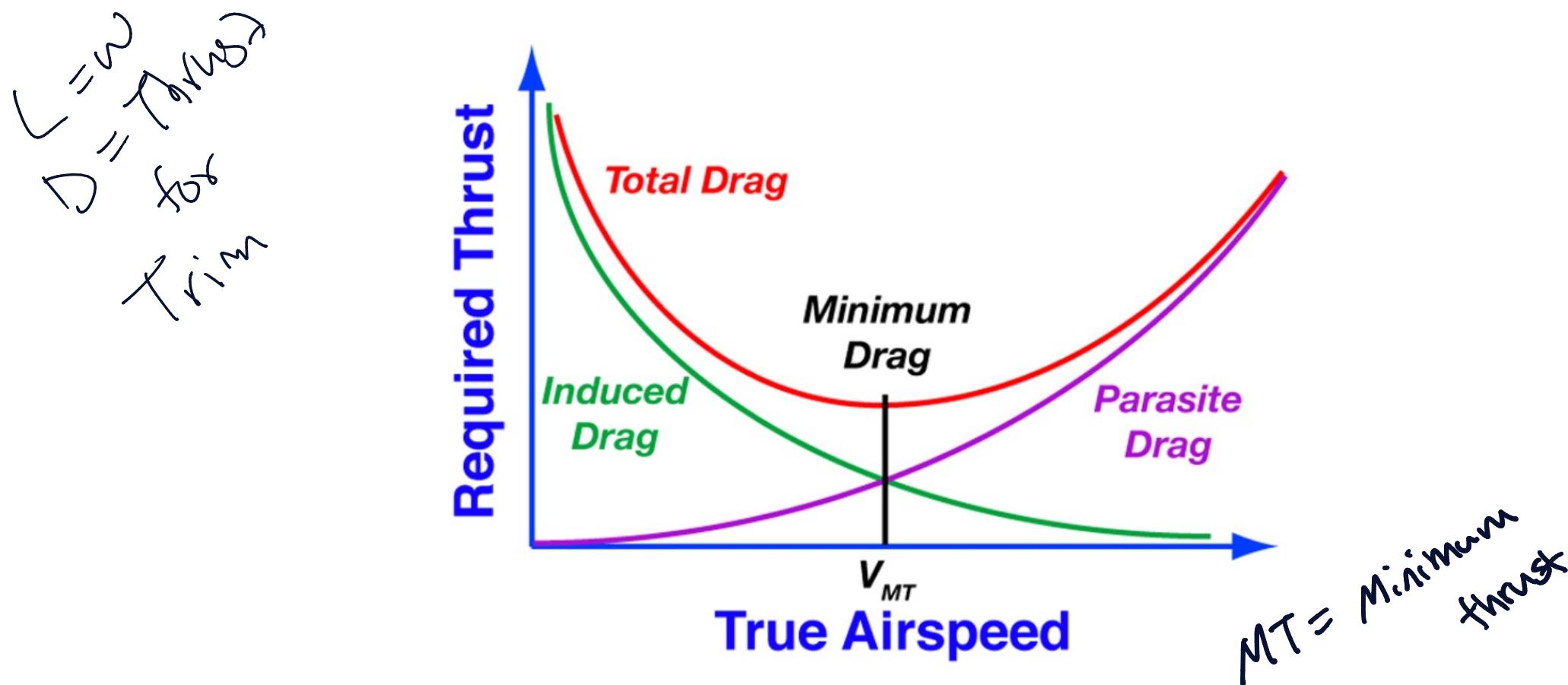
*Heavy aircraft* → You need more lift by increasing  $\alpha$ .

## Trimmed Angle of Attack, $\alpha$

- Trimmed angle of attack,  $\alpha$ 
  - Constant if dynamic pressure and weight are constant
  - If dynamic pressure decreases, angle of attack must increase

$$\alpha_{trim} = \frac{2W/\rho V^2 S - C_{L_o}}{C_{L_\alpha}} = \frac{\frac{1}{\bar{q}}(W/S) - C_{L_o}}{C_{L_\alpha}}$$

# Thrust Required for Steady, Level Flight



# Thrust Required for Steady, Level Flight

Trimmed thrust

Parasitic Drag

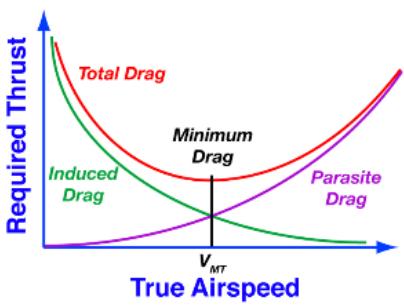
Induced Drag

$$T_{trim} = D_{cruise} = C_{D_o} \left( \frac{1}{2} \rho V^2 S \right) + \epsilon \frac{2W^2}{\rho V^2 S}$$

Minimum required thrust conditions

$$\frac{\partial T_{trim}}{\partial V} = C_{D_o} (\rho V S) - \frac{4\epsilon W^2}{\rho V^3 S} = 0$$

Necessary Condition:  
Slope = 0



## Necessary and Sufficient Conditions for Minimum Required Thrust

**Necessary Condition = Zero Slope**

$$C_{D_o}(\rho VS) = \frac{4\varepsilon W^2}{\rho V^3 S}$$

$$\Rightarrow V^4 = \frac{4\varepsilon W^2}{\rho^2 S^2 C_D} \\ = \frac{4\varepsilon}{\rho^2 C_D} (W/S)^2$$

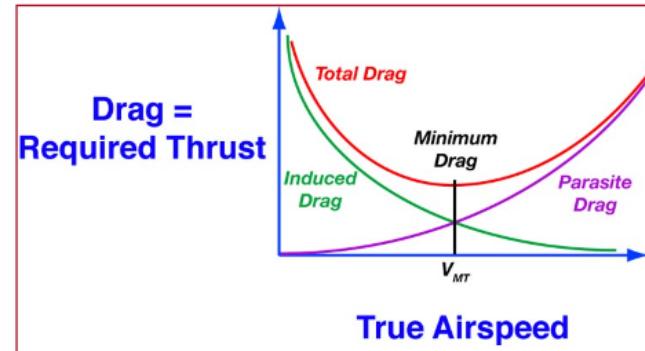
**Sufficient Condition for a Minimum = Positive Curvature when slope = 0**

$$\frac{\partial^2 T_{trim}}{\partial V^2} = C_{D_o}(\rho S) + \frac{12\varepsilon W^2}{\rho V^4 S} > 0$$

(+)

(+)

# Airspeed for Minimum Thrust in Steady, Level Flight



Drag = Required Thrust

$$\frac{1}{2} \rho V^3 S$$

Satisfy necessary condition

$$V^4 = \left( \frac{4\varepsilon}{C_{D_o} \rho^2} \right) (W/S)^2$$

Fourth-order equation for velocity  
Choose the positive root

$$V_{MT} = \sqrt{\frac{2}{\rho} \left( \frac{W}{S} \right) \sqrt{\frac{\varepsilon}{C_{D_o}}}}$$

*Continued from  $\frac{\partial T_{thrust}}{\partial V} = 0$*

# Lift, Drag, and Thrust Coefficients in Minimum-Thrust Cruising Flight

## Lift coefficient

$$C_{L_{MT}} = \frac{2}{\rho V_{MT}^2} \left( \frac{W}{S} \right)$$
$$= \sqrt{\frac{C_{D_o}}{\epsilon}} = (C_L)_{(L/D)_{\max}}$$

Plug in  $V_{MT}$  from previous slide

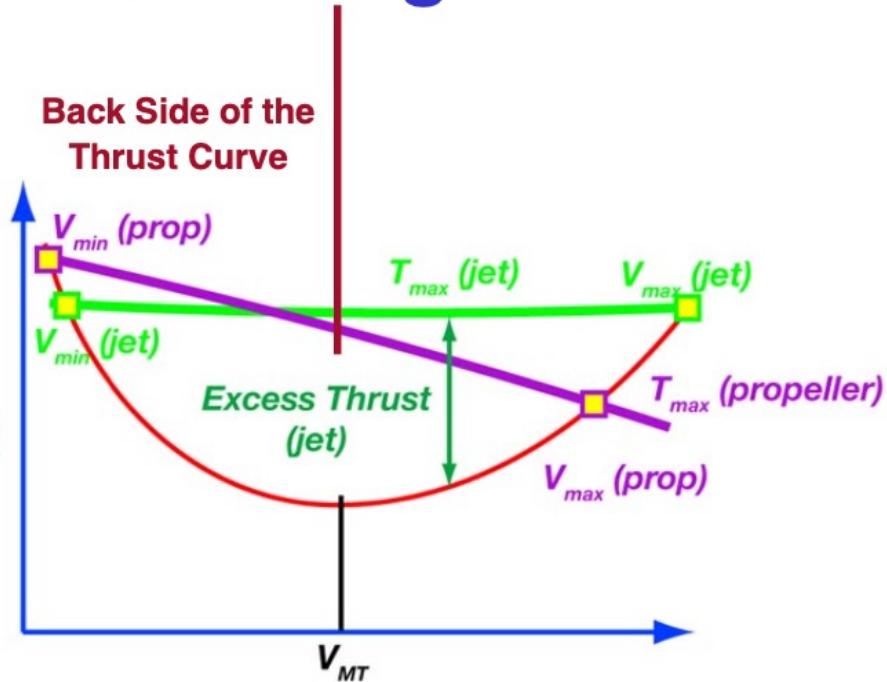
## Drag and thrust coefficients

$$C_{D_{MT}} = C_{D_o} + \epsilon C_{L_{MT}}^2 = C_{D_o} + \epsilon \frac{C_{D_o}}{\epsilon}$$
$$= 2C_{D_o} \equiv C_{T_{MT}}$$

↑  
thrust, minimum  
thrust coeff.

# Achievable Airspeeds in Constant-Altitude Flight

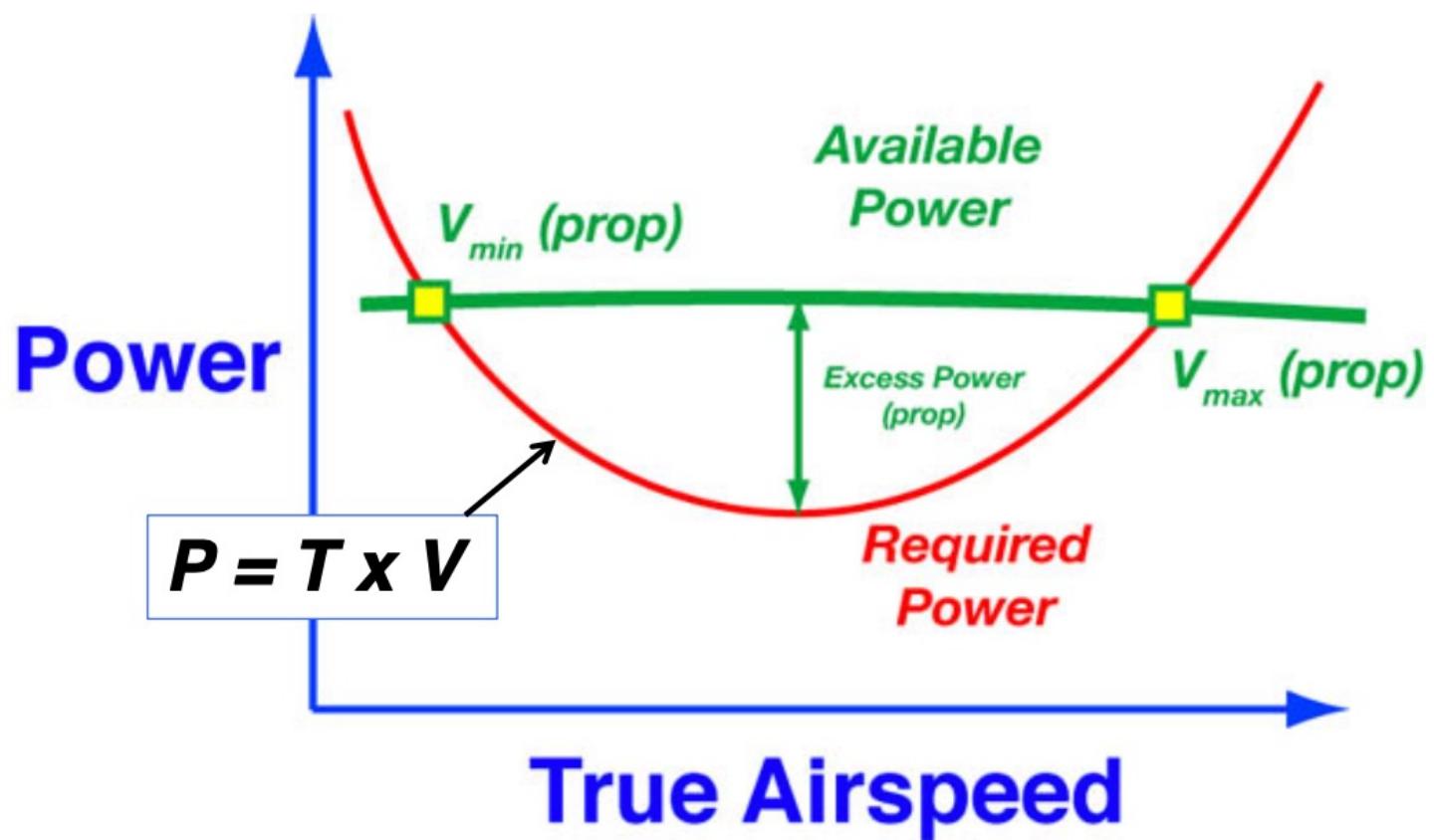
Drag =  
Required Thrust

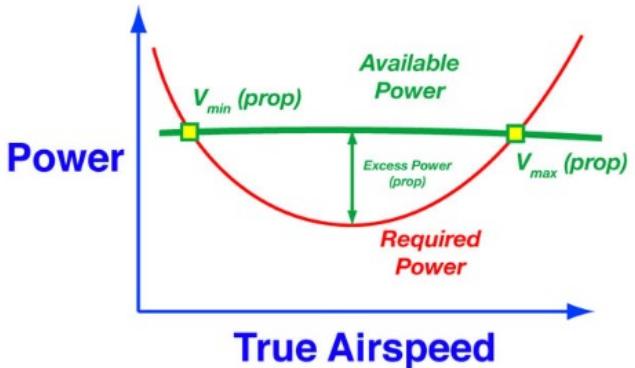


## True Airspeed

- Two equilibrium airspeeds for a given thrust or power setting
  - Low speed, high  $C_L$ , high  $\alpha$
  - High speed, low  $C_L$ , low  $\alpha$
- Achievable airspeeds between minimum and maximum values with maximum thrust or power

# Power Required for Steady, Level Flight





## Airspeed for Minimum Power in Steady, Level Flight

we looked at minimum thrust in the previous slides

- Satisfy necessary condition
- Fourth-order equation for velocity
  - Choose the positive root
- Corresponding lift and drag coefficients

$$C_{D_o} \frac{3}{2} (\rho V^2 S) = \frac{2 \varepsilon W^2}{\rho V^2 S}$$

$$V_{MP} = \sqrt{\frac{2}{\rho} \left( \frac{W}{S} \right)} \sqrt{\frac{\varepsilon}{3C_{D_o}}}$$

$$C_{L_{MP}} = \sqrt{\frac{3C_{D_o}}{\varepsilon}}$$

$$C_{D_{MP}} = 4C_{D_o}$$

# Achievable Airspeeds for Jet in Cruising Flight

**Thrust = constant**

$$T_{avail} = C_D \bar{q} S = C_{D_o} \left( \frac{1}{2} \rho V^2 S \right) + \frac{2 \varepsilon W^2}{\rho V^2 S}$$

$$C_{D_o} \left( \frac{1}{2} \rho V^4 S \right) - T_{avail} V^2 + \frac{2 \varepsilon W^2}{\rho S} = 0$$

$$V^4 - \frac{2 T_{avail}}{C_{D_o} \rho S} V^2 + \frac{4 \varepsilon W^2}{C_{D_o} (\rho S)^2} = 0$$

4<sup>th</sup>-order algebraic equation for  $V$

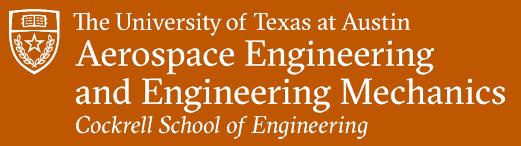
## Achievable Airspeeds for Jet in Cruising Flight

Solutions for  $V^2$  can be put in quadratic form and solved easily

$$V^2 \triangleq x; \quad V = \pm\sqrt{x}$$

$$V^4 - \frac{2T_{avail}}{C_{D_o}\rho S}V^2 + \frac{4\varepsilon W^2}{C_{D_o}(\rho S)^2} = 0$$
$$x^2 + bx + c = 0$$

$$x = -\frac{b}{2} \pm \sqrt{\left(\frac{b}{2}\right)^2 - c} = V^2$$



# CRUISE RANGE

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# Cruising Range and Specific Fuel Consumption



- **Thrust = Drag**

$$0 = (C_T - C_D) \frac{1}{2} \rho V^2 S / m$$

- **Lift = Weight**

$$0 = \left( C_L \frac{1}{2} \rho V^2 S - mg \right) / mV$$

- **Level flight**

$$\begin{aligned}\dot{h} &= 0 \\ \dot{r} &= V\end{aligned}$$

- **Thrust specific fuel consumption,  $TSFC = c_T$** 
  - Fuel mass burned per sec per unit of thrust

$$c_T : \frac{kg/s}{kN}$$

$$\dot{m}_f = -c_T T$$

- **Power specific fuel consumption,  $PSFC = c_P$** 
  - Fuel mass burned per sec per unit of power

$$c_P : \frac{kg/s}{kW}$$

$$\dot{m}_f = -c_P P$$

incomplete fuel eff.  
By J.S.



## Breguet Range Equation for Jet Aircraft

Rate of change of range with respect to weight of fuel burned

$$\frac{dr}{dm} = \frac{dr/dt}{dm/dt} = \frac{\dot{r}}{\dot{m}} = \frac{V}{(-c_T T)} = -\frac{V}{c_T D} = -\left(\frac{L}{D}\right) \frac{V}{c_T mg}$$

$$dr = -\left(\frac{L}{D}\right) \frac{V}{c_T mg} dm$$

Range traveled

$$Range = R = \int_0^R dr = - \int_{W_i}^{W_f} \left(\frac{L}{D}\right) \left(\frac{V}{c_T g}\right) \frac{dm}{m}$$



## Maximum Range of a Jet Aircraft Flying at Constant Altitude

At constant altitude and SFC

$$V_{cruise}(t) = \sqrt{2W(t)/C_L\rho(h_{fixed})S}$$

$$\begin{aligned} Range &= - \int_{W_i}^{W_f} \left( \frac{C_L}{C_D} \right) \left( \frac{1}{c_T g} \right) \sqrt{\frac{2}{C_L \rho S}} \frac{dm}{m^{1/2}} \\ &= \left( \frac{\sqrt{C_L}}{C_D} \right) \left( \frac{2}{c_T g} \right) \sqrt{\frac{2}{\rho S}} \left( m_i^{1/2} - m_f^{1/2} \right) \end{aligned}$$

Range is maximized when

$$\left( \frac{\sqrt{C_L}}{C_D} \right) = \text{maximum}$$

be selected  
C depends on  
Vcruise  
in this equation  
Cent' Specific Power  
in this case  
Minimum thrust or  
Power

# Breguet Range Equation for Jet Aircraft at Constant Airspeed



For constant true airspeed,  $V = V_{cruise}$ , and  $SFC$

$$\begin{aligned} R &= -\left(\frac{L}{D}\right)\left(\frac{V_{cruise}}{c_T g}\right) \ln\left(\frac{m_i}{m_f}\right)^{m_f} \\ &= \left(\frac{L}{D}\right)\left(\frac{V_{cruise}}{c_T g}\right) \ln\left(\frac{m_i}{m_f}\right) \\ &= \left(V_{cruise} \frac{C_L}{C_D}\right) \left(\frac{1}{c_T g}\right) \ln\left(\frac{m_i}{m_f}\right) \end{aligned}$$

- $V_{cruise}(C_L/C_D)$  as large as possible
- $M \rightarrow M_{crit}$
- $\rho$  as small as possible
- $h$  as high as possible

*Keep it constant*

# Maximize Jet Aircraft Range Using Optimal Cruise-Climb

$$\frac{\partial R}{\partial C_L} \propto \frac{\partial \left( V_{cruise} \frac{C_L}{C_D} \right)}{\partial C_L} = \frac{\partial \left[ V_{cruise} \frac{C_L}{(C_{D_0} + \epsilon C_L^2)} \right]}{\partial C_L} = 0$$

$$V_{cruise} = \sqrt{2W/C_L \rho S}$$

- speed ↑
- As we fly fuel is spent, then less lift is required

What does  
cruising flight  
have diff from  
trimming flight?  
man? How diff  
we trim

Assume  $\sqrt{2W(t)/\rho(h)S} = \text{constant}$   
i.e., airplane **climbs at constant TAS** as fuel is burned

Is there a difference between TAS and V<sub>cruise</sub>?  
just saying W(t) and ρ(h)  
are changing at the same  
rate?

Why did we assume this?

Is this

## Description

Cruise climb is the most fuel efficient cruising technique. It allows the aircraft to constantly operate at its optimal performance.

As fuel is burnt, the aircraft gradually becomes lighter. Therefore, less lift is required to balance the weight. This means that either speed will increase, or altitude will increase, or thrust will be reduced. Increasing the speed will also increase drag, hence fuel consumption. Reducing thrust means the engine would run in a sub-optimal mode. Increasing the altitude, on the other hand, will keep the engine setting and reduce drag due to air density reduction.

The downside of cruise climb is that it is often incompatible with ATS procedures and traffic demand. In busier airspaces (e.g. Europe, USA, etc.) traffic levels are such that clearing a flight to perform a cruise climb will deny several others the opportunity to fly at or near their optimal levels.

Another issue with clearing an aircraft to perform a cruise climb is that the vertical speed is much lower than the usual 1000-2000 feet per minute. This results in a situation where the

# Maximize Jet Aircraft Range Using Optimal Cruise-Climb

$$\frac{\partial \left[ V_{cruise} C_L / (C_{D_o} + \epsilon C_L^2) \right]}{\partial C_L} = \sqrt{\frac{2w}{\rho S}} \frac{\partial \left[ C_L^{1/2} / (C_{D_o} + \epsilon C_L^2) \right]}{\partial C_L} = 0$$

$\sqrt{\frac{2w}{\rho S}}$  = Constant; let  $C_L^{1/2} = x$ ,  $C_L = x^2$

$$\frac{\partial}{\partial x} \left[ \frac{x}{(C_{D_o} + \epsilon x^4)} \right] = \frac{(C_{D_o} + \epsilon x^4) - x(4\epsilon x^3)}{(C_{D_o} + \epsilon x^4)^2} = \frac{(C_{D_o} - 3\epsilon x^4)}{(C_{D_o} + \epsilon x^4)^2}$$

Optimal values:

$$C_{L_{MR}} = \sqrt{\frac{C_{D_o}}{3\epsilon}} : C_{D_{MR}} = C_{D_o} + \frac{C_{D_o}}{3} = \frac{4}{3}C_{D_o}$$

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$R = \max$   
 $\frac{\partial R}{\partial C_L} = 0$   
@

Max Range  
You stay at a certain  
mach #.

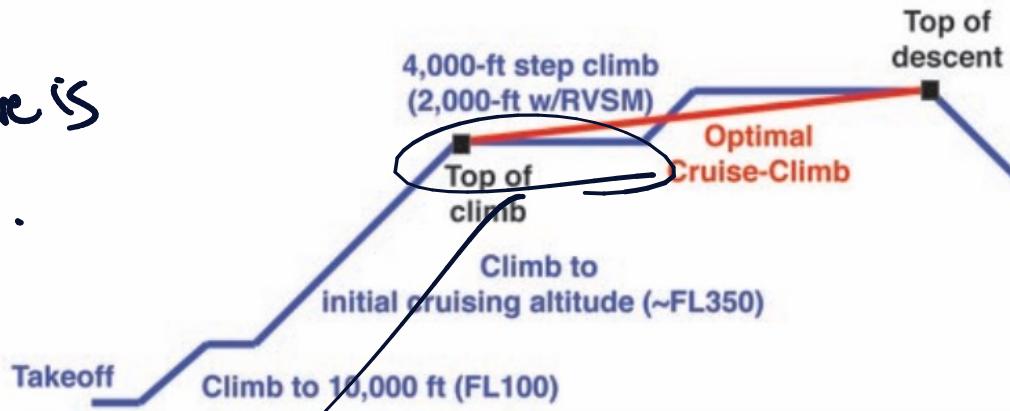
$$V_{cruise-climb} = \sqrt{2W(t)/C_{L_{MR}}\rho(h)S} = a(h)M_{cruise-climb}$$

$a(h)$ : Speed of sound;  $M_{cruise-climb}$  : Mach number

# Step-Climb Approximates Optimal Cruise-Climb

- **Cruise-climb** usually violates air traffic control rules
- Constant-altitude cruise does not
- **Compromise: Step climb from one allowed altitude to the next as fuel is burned**

If we want to climb so there is less drag, less thrust required



You pitch down as you burn fuel but keep altitude. At some point you get right enough to reach an equilibrium at a higher altitude

① We learned we can maximize range by cruise-climbing. To do that we set  $\frac{\sqrt{2W(E)}}{C(h)S}$

Constant

• How would we have known to do that?  
Why not increase alt. in the first place and fly at the altitude?  
• How does air flow work  
optimal vs step. Does the pilot put in thrust or constant thrust for optimal?  
what about step P2.



The University of Texas at Austin  
**Aerospace Engineering**  
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