

THE UNIVERSITY OF TEXAS AT AUSTIN  
Department of Aerospace Engineering and Engineering Mechanics

ASE 367K FLIGHT DYNAMICS  
Fall 2024

HOMework 3  
Due: 2024-09-20 at 11:59pm via Canvas

Problem 1

The vertical tail volume of an aircraft is defined by

$$V_F = \frac{S_f(x_{ac_f} - x_{cg})}{Sb},$$

where  $S_f$  and  $S$  are the fin and wing planform area, respectively,  $b$  is the wing span, and  $x_{ac_f} - x_{cg}$  is the distance between the aerodynamic center of the fin and the CG of the aircraft. For an airplane with  $C_{L_{\alpha_f}} = 5.5$ , assuming negligible sidewash effects, what tail volume is required to achieve a weathercock stability derivative of  $C_{n_{\beta}} = 0.16$ ?

Problem 2

For the airplane below, assume the right engine fails when the aircraft is in level flight at 130 knots, creating a yawing moment of 100000 [ft-lb]. Neglect the fuselage effect, determine:

- The resulting sideslip angle in degrees if no rudder deflection is input.
- The rudder input  $\delta_r$  required to maintain the direction of flight prior to the engine failure.

Assume sea level, standard conditions:  $\rho = 0.002378$  [slugs/ft<sup>3</sup>]. Also,  
1 [knot] = 1.6878 [ft/s].

Wing		Horizontal Tail		Vertical Fin	
$b$	= 80 [ft]	$S$	= 250 [ft <sup>2</sup> ]	$S$	= 125 [ft <sup>2</sup> ]
$\bar{c}$	= 10 [ft]	$\bar{c}$	= 5 [ft]	$\bar{c}$	= 5 [ft]
$i$	= 0 [deg]	$i$	= -1.6 [deg]		
$C_{L_{\alpha}}$	= 5.2 [rad <sup>-1</sup> ]	$C_{L_{\alpha}}$	= 4.5 [rad <sup>-1</sup> ]	$C_{L_{\alpha}}$	= 5.5 [rad <sup>-1</sup> ]
$C_{L_0}$	= 0.1	$C_{L_0}$	= 0.0	$C_{L_0}$	= 0.0
$C_{M_{ac}}$	= -0.1	$C_{M_{ac}}$	= 0.0	$C_{M_{ac}}$	= 0.0
		$C_{L_{\delta_e}}$	= 1.5 [rad <sup>-1</sup> ]	$C_{L_{\delta_r}}$	= 1.5 [rad <sup>-1</sup> ]
$x_{ac}$	= 13 [ft]	$x_{ac}$	= 40 [ft]	$x_{ac}$	= 40 [ft]
		$\epsilon_0$	= 1.0 [deg]	$\sigma_0$	= 0.0 [deg]
		$\epsilon_{\alpha}$	= 0.3	$\sigma_{\beta}$	= 0.0
		$\eta$	= 0.95	$\eta$	= 1.0

The cg of the aircraft is at  $x_{cg} = 14$  [ft], the weight of the aircraft is 20,000 [lb], and

$$C_{M_{0p}} = 0.0, \quad C_{M_{0f}} = 0.0, \quad C_{M_{\alpha_p}} = 0.0 \text{ [rad}^{-1}\text{]}, \quad \text{and} \quad C_{M_{\alpha_f}} = 0.0 \text{ [rad}^{-1}\text{]}.$$

9/20/24

1)

$$V_v = \frac{S_f (x_{ac_f} - x_{cg})}{S_b}$$

$$C_{L\alpha_f} = 5.5$$

$$C_{n\beta} = 0.16$$

$$C_{L\alpha_f} = \frac{dC_L}{d\alpha_f}$$

$$\frac{\partial \phi}{\partial \beta} = 0$$

$$\alpha_F = -\beta + \phi$$

$$C_{n_F} = -V_v \left( \frac{V_F}{V} \right)^2 C_{L_F}$$

$$\frac{\partial C_{n_F}}{\partial \alpha_F} = -V_v \left( \frac{V_F}{V} \right)^2 \frac{\partial C_{L_F}}{\partial \alpha_F}$$

$$\frac{\partial C_{n_F}}{\partial \beta} = -V_v \left( \frac{V_F}{V} \right)^2 C_{L\alpha_F}$$

$$C_{n\beta} = 0.16 = -V_v \left( \frac{V_F}{V} \right)^2 (5.5)$$

$$\frac{-0.16}{5.5} = -V_v (1)^2$$

$$V_v = +0.029$$

Assume fin  
is not in  
slipstream

$$C_{n_F} = -V_v \left( \frac{V_F}{V} \right)^2 C_{L_F}$$

$$\frac{\partial C_{n_F}}{\partial \beta} = -V_v \left( \frac{V_F}{V} \right)^2 \frac{\partial C_{L_F}}{\partial \beta}$$

$$C_{L_F} = a_F (-\beta + \phi) + a_\delta \delta_r$$

$$C_{L_F} = -\beta a_F + a_F \alpha$$

$$\frac{\partial C_{L_F}}{\partial \beta} = -a_F$$

$$\frac{\partial C_{n_F}}{\partial \beta} = a_F V_v \left( \frac{V_F}{V} \right)^2$$

$$0.16 = 5.5 V_v \left( \frac{V_F}{V} \right)^2$$

$$V_v = 0.029$$

2)

$$130 \text{ knots} = 219.415 \text{ ft/s}$$

$$N_{\text{engine}} = 100,000 \text{ ft-lb.}$$

$$a) \quad C_n = C_{n\beta} \beta + C_{n\delta_r} \delta_r \quad 0, \text{ since } \delta_r = 0$$

$$C_n = \frac{N}{\frac{1}{2} \rho V^2 S_b}$$

$$C_{n\beta} \beta = \frac{N}{\frac{1}{2} \rho V^2 S_b}$$

$$\beta = \frac{2N}{\rho V^2 S_b} \frac{1}{C_{n\beta}}$$

assume  $\frac{V_F}{V} = 1$  for free stream.

$$C_{n\beta} = -V_v \left( \frac{V_F}{V} \right)^2 \frac{\partial C_{LF}}{\partial \beta} = a_F V_v \left( \frac{V_F}{V} \right)^2 \left( 1 - \frac{\partial \beta}{\partial \beta} \right)$$

0, no sideslash

$$a_F = C_L \alpha_F$$

$$V_v = \frac{S_F l_F}{S_b} = \frac{125(40-14)}{1200(80)} = 0.03385$$

$$C_{n\beta} = 5.5(0.03385)(1)(1) = 0.1862$$

$$\beta = \frac{2(100,000)}{0.002378(219.415)^2 1200 \cdot 80 \cdot 0.1862}$$

$$= 0.09773 \text{ rad} \quad \approx 5.60^\circ$$

b)

$$C_n = \overset{0}{C_{n\beta}} + C_{n\delta_r} \delta_r$$

$$= C_{n\delta_r} \delta_r$$

$$C_{n\delta_r} = -a_r V_v \left( \frac{V_v}{V} \right)^2$$

$$a_r = C_{n\delta_{rF}} = 1.5$$

$$V_v = 0.03385$$

$$C_{n\delta_r} = -1.5 (0.03385) = -0.050775$$

$$C_n = \frac{N}{\frac{1}{2} \rho V^2 S_b}$$

$$= \frac{100,000}{\frac{1}{2} (0.002378) (29.415)^2 (1200) (80)}$$

$$= 0.0181976$$

$$0.0181976 = -0.050775 \delta_r$$

$$\delta_r = -0.3584$$

$$= -20.5346^\circ$$