RoVi1

Final Project

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Project Description

1 Tracking points using image Jacobian

We have implemented algorithm for visual servoing in this part. For this part we selected specific marker points as described in problem statement and use mathematical camera model to get image pixel coordinates of the points. Image recognition thus wasn't used in this part.

To compute joint updates it was first needed to compose matrix Z_{image} as described in Robotics Notes:

$$Z_{image}(q) = J_{image}S(q)J(q)$$
 (1)

where J(q) is manipulator Jacobian. For its computation we used function from Rob-Work library. J_{image} is image Jacobian matrix. We implemented function for its computation called calculateImageJ which can be found in the file inverseKinematics.cpp. We used fixed value for z coordinate. Since we used frame cameraSim to model the camera we set z=-0.5 for every function call. Finally matrix S(q) was composed by inserting transpose of the rotational matrix R_{base}^{tool} twice to its diagonal.

The next information necessary to compute joints updates is difference or move of target points $\overrightarrow{dU}_{image}$. We have programmed function calculate_dUImage to solve for $\overrightarrow{dU}_{image}$.

Having matrix Z_{image} and $\overrightarrow{dU}_{image}$ it was possible to solve for joint positional update dq using method of Linear Least Squares.

We adapted two equations from robotics notes into single expression for dq computation:

$$dq = \mathbf{Z}^T \left(\mathbf{Z} \mathbf{Z}^T \right)^{-1} \overrightarrow{dU}_{image}$$
 (2)

In this equation we used Z to denote Z_{image} . For this solving of this LSM problem we have implemented function compute_dQ_LSM which can be found in inverseKinematics.cpp.

algorithm2 is the function, where are all of described functions organized together to compute joint updates dq base on the manipulator state and the error in image coordinates $\overrightarrow{dU}_{image}$.

We have implemented J_{image} and $\overrightarrow{dU}_{image}$ composition in a scalable way, so the same functions can be used to track one or multiple target points.

Model of the robot manipulator has velocity limits on joint movements, so it was necessary to check if the limits were satisfied before joint updates. We did so by measuring time for update computations, subtracting this time from workcell update period specified by \mathtt{deltaT} and finally we divided update dq by the result of subtraction. Velocity of joint movement is the result of the operation. By comparing the actual velocity with manipulator limits it was possible to find out if the limits are satisfied. If they aren't algorithm simply saturate joint movement in order to hold all conditions. For comparison and saturation, function $\mathtt{saturateDQ}$ was implemented.

In the following section we provide simulation results from tests of inverse kinematics.

1.1 Simulation Tests

During simulations, we recorded joint configurations, tool/camera frame position and orientation for $\mathtt{deltaT} = 1000ms$ and finally we performed tests for different values for $\overrightarrow{\mathtt{deltaT}}$ in the range $50\,ms < \mathtt{deltaT} < 1000\,ms$ and plotted maximum errors of $\overrightarrow{\mathtt{dU}}_{image}$

Slow Marker Sequence

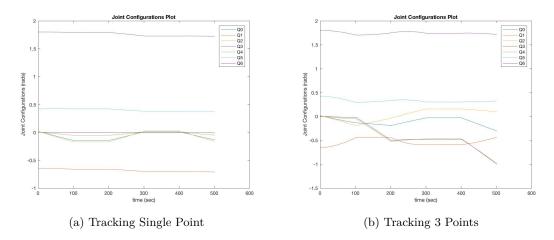


Figure 1: Joint configurations

There are differences between joint coordinates for tracking single and 3 target points in the graphs 1a and 1b. The reason behind this is following. When the manipulator is tracking single point, it just follow its position. There is no orientation information about the marker when using single tracking point. Whereas during following of 3 target points, orientation of the marker gains important role, as the manipulator is trying to rotate its tool/camera frame to align its position and orientation with the marker.

In figure 2a and 2b are apparent jumps in roll angle around z axis. This however doesn't imply jumps in tool orientation. Abrupt jumps in the graphs were caused because of switching between $-\pi$ and π rad angle. In the real world, change in orientation is small. Implementation of Robwork transformations probably keeps all orientation angles in the interval $\langle -\pi, \pi \rangle$.

Simulation for different ΔT s

There are plotted maximum pixel errors on the figure 3. When looking to the Tracking of 3 points figure, there should be du and dv line for all of the 3 tracked points. However, because they were very close to each other, we ommitted the another two lines in the graph for better clarity.

For timing purposes we used C++ Chrono library, for taking time instant of start of the computation of updates and the end instant. For differentiation of joint updates and

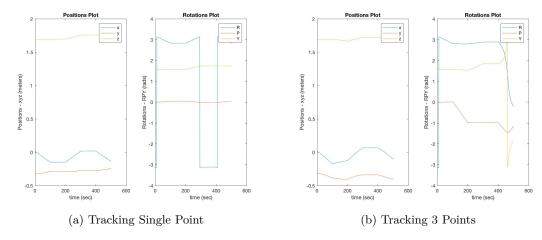


Figure 2: Tool pose transformations

subsequently getting of velocity, we used difference of these two time stamps. Due to non-real time OS, results might be different for each simulation and doesn't offer precise information. However for the purpose of the school exercise, we were able to limit joints speed velocities according to problem statement.

Medium Marker Sequence

The same problems and explanation apply for the Medium marker sequence. Joint coordinates and tool positions are plotted on the graphs 4 and 5. Only difference from Slow sequence is in the time axis. Due to faster and larger movements time span is shorter.

Simulation for different ΔT s

There are plotted maximum pixel errors on the figure 6. Again, when looking to the Tracking of 3 points figure, there should be du and dv line for all of the 3 tracked points. However, because they were very close to each other, we ommitted the another two lines in the graph for better clarity.

From the graphs it is apparent that the manipulator wasn't able to track the sequence when deltaT was lower than $200\,ms$. There were experienced some difficulties with tracking even for higher deltaT. You can see peaks in errors at about $0.8\,s$ for single point tracking.

We have to state the same as for the preceding test. All timing tests were performed on the regular laptop PC, running non-real time operating system. So results from another tests can differ.

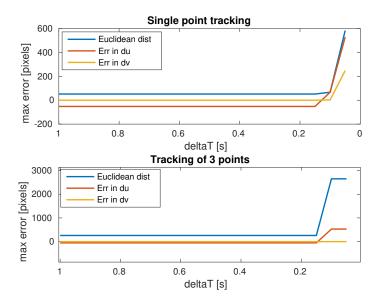


Figure 3: Maximum errors during Slow Sequence Marker following

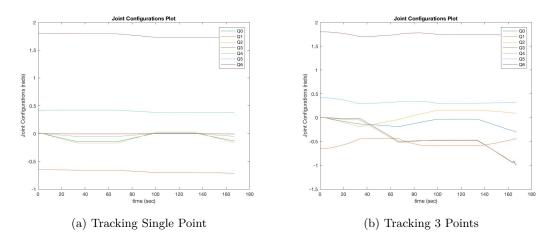


Figure 4: Joint configurations

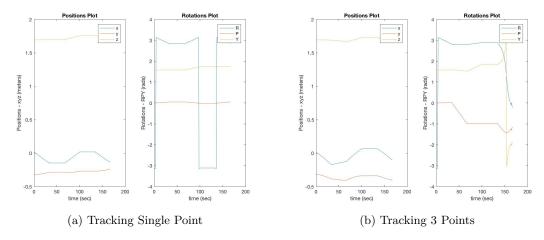


Figure 5: Tool pose transformations

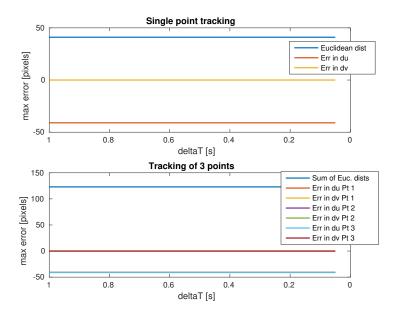


Figure 6: Maximum errors during Medium Sequence Marker following

Fast Marker Sequence

Joint coordinates and tool positions are plotted on the graphs 7 and 8. Span of time axis is again shorter.

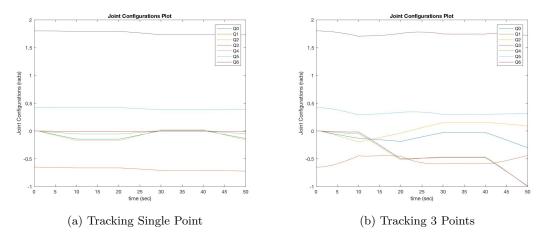


Figure 7: Joint configurations

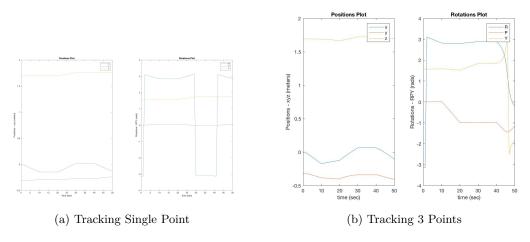


Figure 8: Tool pose transformations

Simulation for different ΔTs

There are plotted maximum pixel errors on the figure 9. Again, when looking to the Tracking of 3 points figure, there should be du and dv line for all of the 3 tracked points. However, because they were very close to each other, we ommitted the another two lines in the graph for better clarity.

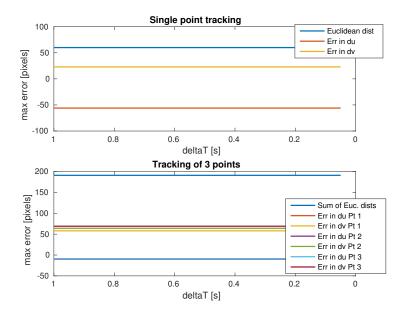


Figure 9: Maximum errors during Fast Sequence Marker following

From the graphs it is apparent that the manipulator wasn't able to track the sequence when \mathtt{deltaT} was lower than $200\,ms$. There were experience some difficulties with tracking even for higher \mathtt{deltaT} . You can see peaks in errors at about $0.4\,s$ for single point tracking and around $0.7\,s$ for tracking of 3 points.

We have to state the same as for 2 preceding tests. All timing tests were performed on the regular laptop PC, running non-real time operating system.

Conclusion for different speed sequences

Even though timing and velocity computation during test simulations wasn't precise due to non-realtime of the OS, we can conclude some final facts. Manipulator was able to follow the marker for each sequence with $\mathtt{deltaT} > 200\,ms$. However in the faster sequences, the maximal pixel errors were larger. This is reasonable result for common sense.