

# P R O J E C T

Development of low-order shock-capturing scheme for  
discontinuous Galerkin method

Sana Amri  
*Research Master Student*

## MIDTERM PUBLIC PRESENTATION

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**von Karman Institute for Fluid Dynamics**  
Aeronautics & Aerospace department

### Supervisors & Advisors:

Thierry Magin<sup>+</sup>

Fabio Pinna<sup>★</sup>

Pierre Schrooyen<sup>▲</sup>

Alessandro Turchi<sup>★</sup>

<sup>+</sup> Associate Professor in the Aeronautics and Aerospace Department, VKI

<sup>★</sup> Senior Research Engineer in the Aeronautics and Aerospace Department, VKI

<sup>▲</sup> Senior Research Engineer in the Computational Multi-physics Software Development Team, Cenaero

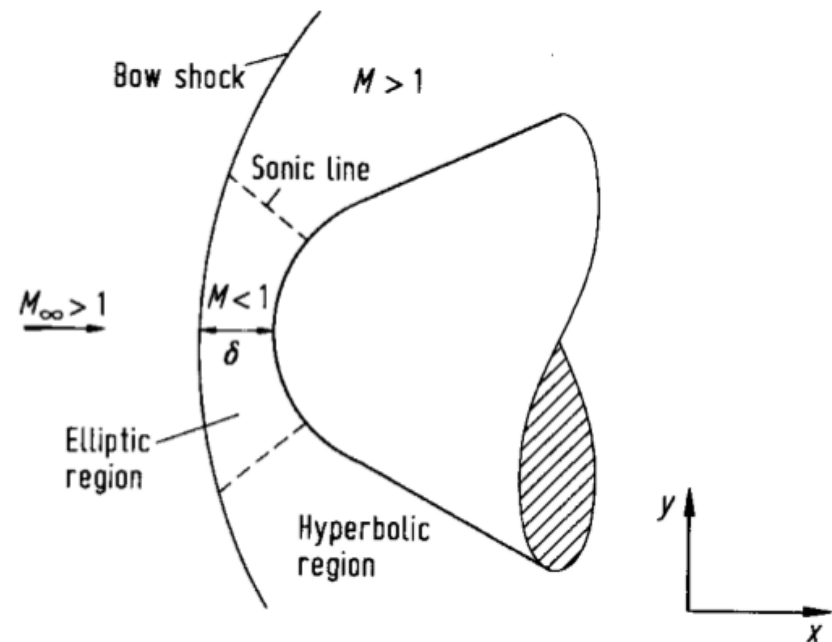
# OUTLINE

- 1 Motivation
- 2 State of the art
- 3 Aim of the project
- 4 Progress up to today
- 5 Conclusion & future work

## CHALLENGES

- Measure the aerodynamic forces and heat flux on a body:
  - Experiments in wind tunnels
  - Simulation by means of CFD
- Hypersonic flow: → Multi-physics phenomena
  - High temperature and compressible effects

*“The role of CFD in engineering predictions has become so strong that today it can be viewed as a new ‘third dimension’ in fluid dynamics, the other two dimensions being the classical cases of pure experiment and pure theory.”*  
[J.D. Anderson]

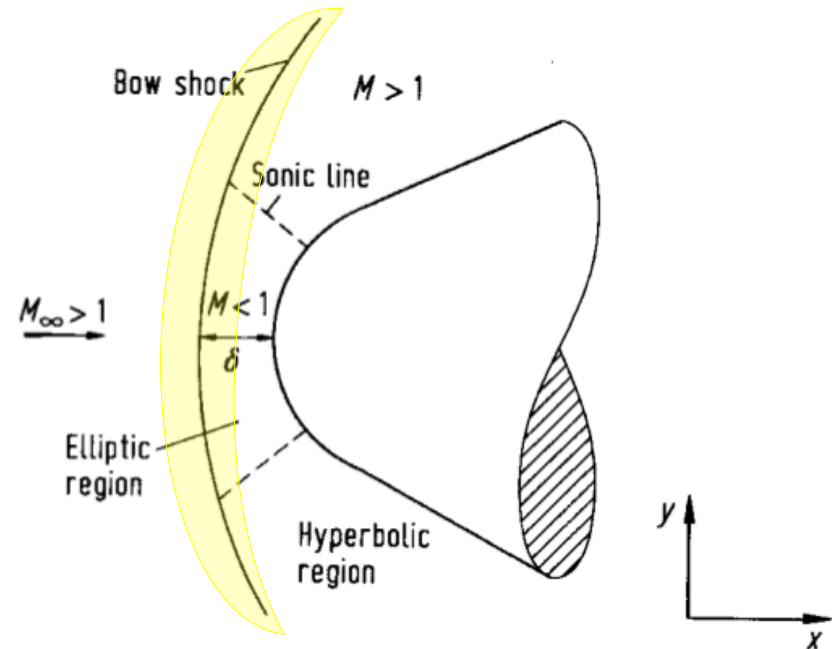


## CHALLENGES

- **Measure the aerodynamic forces and heat flux on a body:**
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**The shock Capturing** method consist in letting appear naturally within the computational space the shock region without any specific treatment of the shocks themselves.

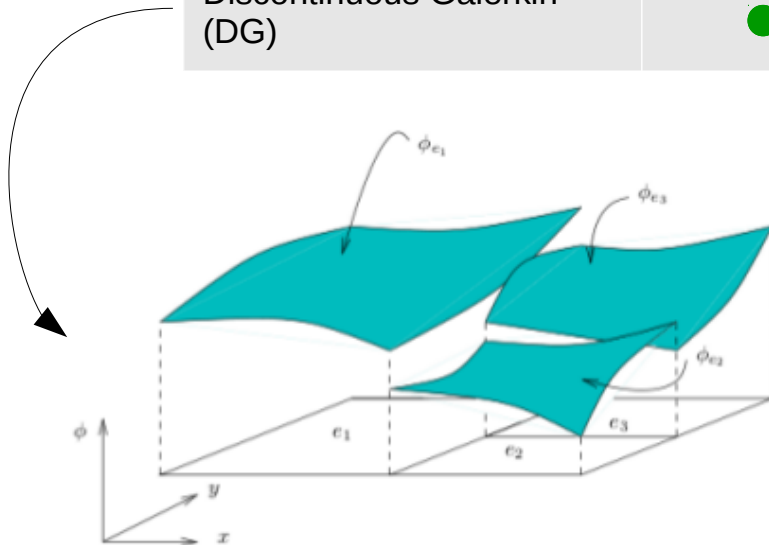
**The shock fitting** method treats the shock region independently from the flowfield by treating the shock as an internal boundary condition.



## Going high order with the discontinuous Galerkin method

### Criteria for high order scheme

	Compact stencil	hp- adaptability	Unstructured grid approach	Parallel implementation	Shock capturing at high Mach number
Finite Difference (FD)	●	●	●	●	●
Finite Volume (FV)	●	●	●	●	●
Finite Element (FE)	●	●	●	●	●
Discontinuous Galerkin (DG)	●	●	●	●	?



- Well adapted
- Can be adapted with some constraints
- Not adapted

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## Shock detector and artificial viscosity

**Shock detector:** identify the location of discontinuities in the computational domain

**Artificial viscosity:** makes shocks broader


Solution:

$$u = \sum_{i=1}^{N(p)} u_i \psi_i$$

Approximation of the solution:

$$\hat{u} = \sum_{i=1}^{N(p-1)} u_i \psi_i$$

Cell e



**IF**(the polynomials shapes are similar)  
**Then** the solution on the cell e is smooth  
**Else** the solution contains discontinuities

**Sensor of the discontinuity** on the cell e:

$$S_e = \frac{(u - \hat{u}, u - \hat{u})_e}{(u, u)_e}$$

$(\cdot, \cdot)_e$  inner product in  $L_2(\Omega_e)$

**Artificial viscosity for each cell e:**

$$\varepsilon_e = \begin{cases} 0 & \text{if } s_e < s_0 - \kappa \\ \frac{\varepsilon_0}{2} \left( 1 + \sin \frac{\pi(s_e - s_0)}{2\kappa} \right) & \text{if } s_0 - \kappa \leq s_e \leq s_0 + \kappa \\ \varepsilon_0 & \text{if } s_e > s_0 + \kappa \end{cases}$$

with  $s_e = \log_{10} S_e$

**Input defined by the user:**

- The threshold  $s_0 \sim 1/p^4$
- The interval  $\kappa$
- The amount of artificial viscosity  $\varepsilon_0 \sim h/p$

## Conservative form of the NS equations in 2D for a calorically and thermally perfect gas

**Let**  $\Omega_{adm} = \{\mathbf{w} \in \mathbb{R}^4 : \rho > 0, \mathbf{u} \in \mathbb{R}^2, e > 0\}$

**Find**  $\mathbf{w} = \begin{pmatrix} \rho \\ \rho \mathbf{u} \\ \rho E \end{pmatrix} \in \Omega_{adm}$  **such that:**

$$\partial_t \mathbf{w} + \nabla \cdot \mathbb{F}_c(\mathbf{w}) - \nabla \cdot \mathbb{F}_v(\mathbf{w}, \nabla \mathbf{w}) = 0, \quad \forall (\mathbf{x}, t) \in \Omega \times ]0; +\infty[$$

$$\mathbf{w}(\mathbf{x}, 0) = \mathbf{w}_{t=0}(\mathbf{x}), \quad \forall \mathbf{x} \in \Omega$$

$$p = \rho R T$$

+ **Boundary conditions** on  $\Gamma = \Gamma_{in} \cup \Gamma_{out} \cup \Gamma_{wall}$

$$\mathbb{F}_c(\mathbf{w}) = \begin{pmatrix} \rho \mathbf{u}^T \\ \rho \mathbf{u} \otimes \mathbf{u} + p \mathbb{I} \\ (\rho E + p) \mathbf{u}^T \end{pmatrix}_{4 \times 2}$$

$$\mathbb{F}_v(\mathbf{w}) = \begin{pmatrix} \mathbf{0}_{\mathbb{R}^2}^T \\ \boldsymbol{\tau} \\ \mathbf{u}^T \cdot \boldsymbol{\tau} - \mathbf{q}^T \end{pmatrix}_{4 \times 2}$$



## Generic Form of the Variational Formulation

$$\sum_{K \in \Omega_h} \int_K \phi_i^K \partial_t \mathbf{w}_h dV + \mathcal{L}_c(\mathbf{w}_h, \phi^K) + \mathcal{L}_v(\mathbf{w}_h, \nabla \mathbf{w}_h, \phi^K) = 0$$

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Lax Friedrich Riemann Solver

$$\hat{\mathbb{F}}_c(\mathbf{w}_h^+, \mathbf{w}_h^-, \mathbf{n}) = \{\mathbb{F}_c(\mathbf{w}_h)\} \mathbf{n} + \frac{a}{2} \llbracket \mathbf{w}_h \rrbracket$$

$$a = \max \left\{ \left| \frac{\partial \mathbb{F}_c \mathbf{n}}{\partial \mathbf{w}} \right| : \mathbf{w} = \mathbf{w}_h^\pm \right\}$$

$$z^\pm(x_e) = \lim_{y \rightarrow x_e, y \in K^\pm} z(y)$$

$$\llbracket z \rrbracket = \begin{cases} z^+ - z^- & \text{if } e \in \epsilon_i \\ z^+ - z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases}$$

$$\{z\} = \begin{cases} \frac{z_+ + z_-}{2} & \text{if } e \in \epsilon_i \\ z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases}$$

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Internal penalty  
method

$$z^\pm(x_e) = \lim_{y \rightarrow x_e, y \in K^\pm} z(y) \quad \llbracket z \rrbracket = \begin{cases} z^+ - z^- & \text{if } e \in \epsilon_i \\ z^+ - z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases} \quad \{z\} = \begin{cases} \frac{z_+ + z_-}{2} & \text{if } e \in \epsilon_i \\ z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases}$$

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Internal penalty  
method

Inconsistent at  $p=0$

$$z^\pm(x_e) = \lim_{y \rightarrow x_e, y \in K^\pm} z(y)$$

$$[[z]] = \begin{cases} z^+ - z^- & \text{if } e \in \epsilon_i \\ z^+ - z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases}$$

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The second scheme  
of Bassi Rebay

Introduce a new equation  
in the initial problem  
To solve

$$\begin{cases} \gamma_h = \nabla \mathbf{w}_h \\ \partial_t \mathbf{w} + \nabla \cdot \mathbb{F}_c(\mathbf{w}) - \nabla \cdot \mathbb{F}_v(\mathbf{w}, \nabla \mathbf{w}) = 0 \end{cases}$$

$$z^\pm(x_e) = \lim_{y \rightarrow x_e, y \in K^\pm} z(y) \quad \llbracket z \rrbracket = \begin{cases} z^+ - z^- & \text{if } e \in \epsilon_i \\ z^+ - z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases} \quad \{z\} = \begin{cases} \frac{z_+ + z_-}{2} & \text{if } e \in \epsilon_i \\ z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases}$$

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New  
Variational  
Formulation

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$$z^\pm(x_e) = \lim_{y \rightarrow x_e, y \in K^\pm} z(y)$$

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## Generic Form of the Variational Formulation

$$\begin{cases} \mathcal{L}_{aux}(\mathbf{w}_h, \Upsilon_h, \alpha^K) = 0 \\ \sum_{K \in \Omega_h} \int_K \phi_i^K \partial_t \mathbf{w}_h dV + \mathcal{L}_c(\mathbf{w}_h, \phi^K) + \mathcal{L}_v(\mathbf{w}_h, \Upsilon_h, \phi^K) = 0 \end{cases}$$

The second scheme  
of Bassi Rebay is  
consistent in p0

$$z^\pm(x_e) = \lim_{y \rightarrow x_e, y \in K^\pm} z(y) \quad \llbracket z \rrbracket = \begin{cases} z^+ - z^- & \text{if } e \in \epsilon_i \\ z^+ - z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases} \quad \{z\} = \begin{cases} \frac{z_+ + z_-}{2} & \text{if } e \in \epsilon_i \\ z_{wall} & \text{if } e \in \epsilon_{wall} \end{cases}$$

## Shock capturing methods

Low order approach

1. Compute in P0 in all the domain
2. Localize the shock with a sensor
3. Restrain the shock region to P0 and run in a higher order everywhere else on the domain

High order approach

Run in high order in all the domain & use the AV to reduce the spurious oscillations in the shock region



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## Aim of the project

Develop a robust shock capturing scheme for the DG method

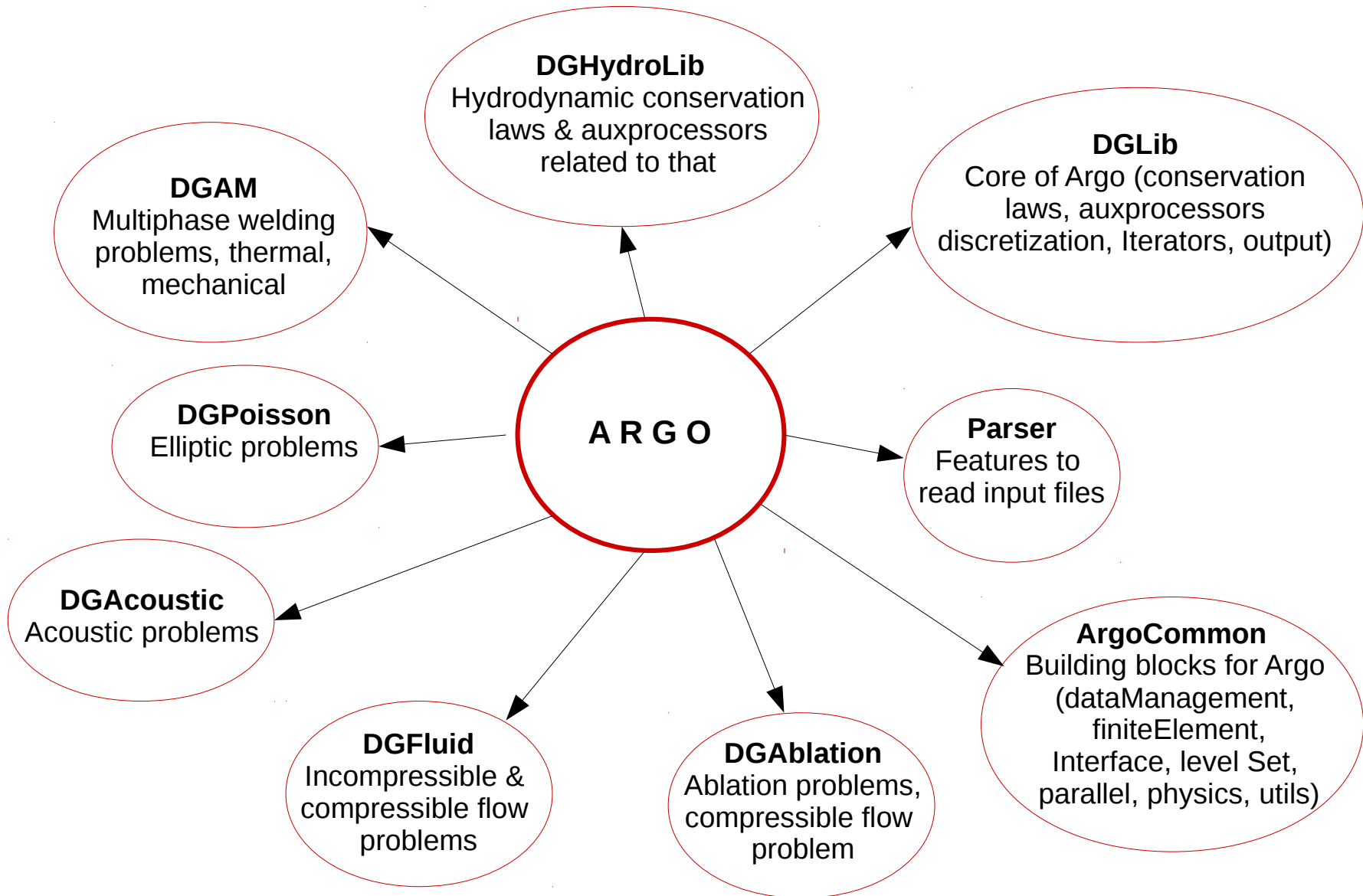
### Main tasks

1. Review the hypersonic flow challenges for **high order numerical simulation** ✓
2. Identify the limit of the **artificial viscosity** into the Argo platform ✓
3. Optimize and adapt a hybrid solver for hypersonic applications which uses a **degraded order scheme** (DG(P0)) with LF-BR2) in the shock region and a high order method (DG(P>1) with LF-BR2) everywhere else ⌘
4. Validation on a specific test case ✗

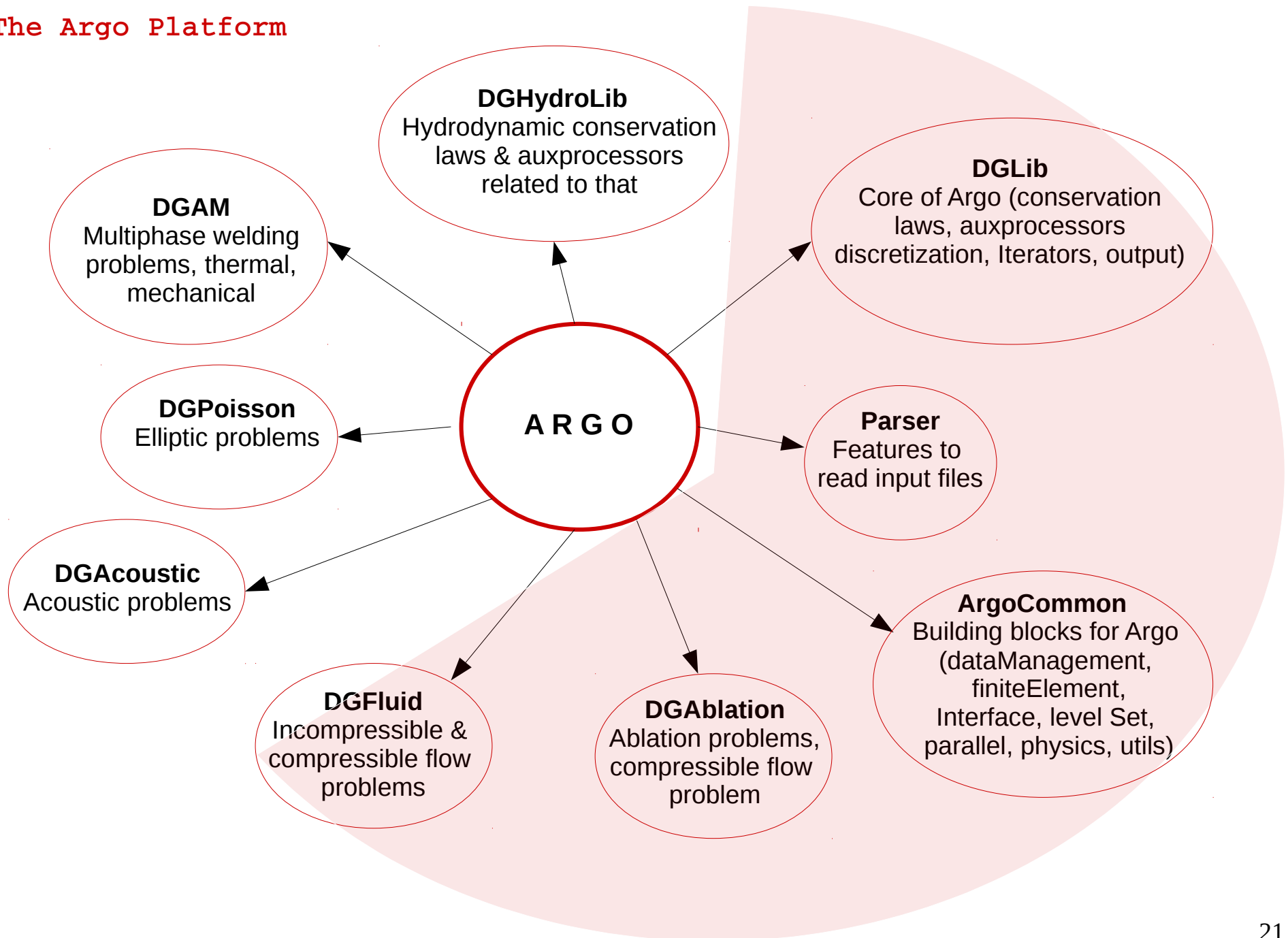
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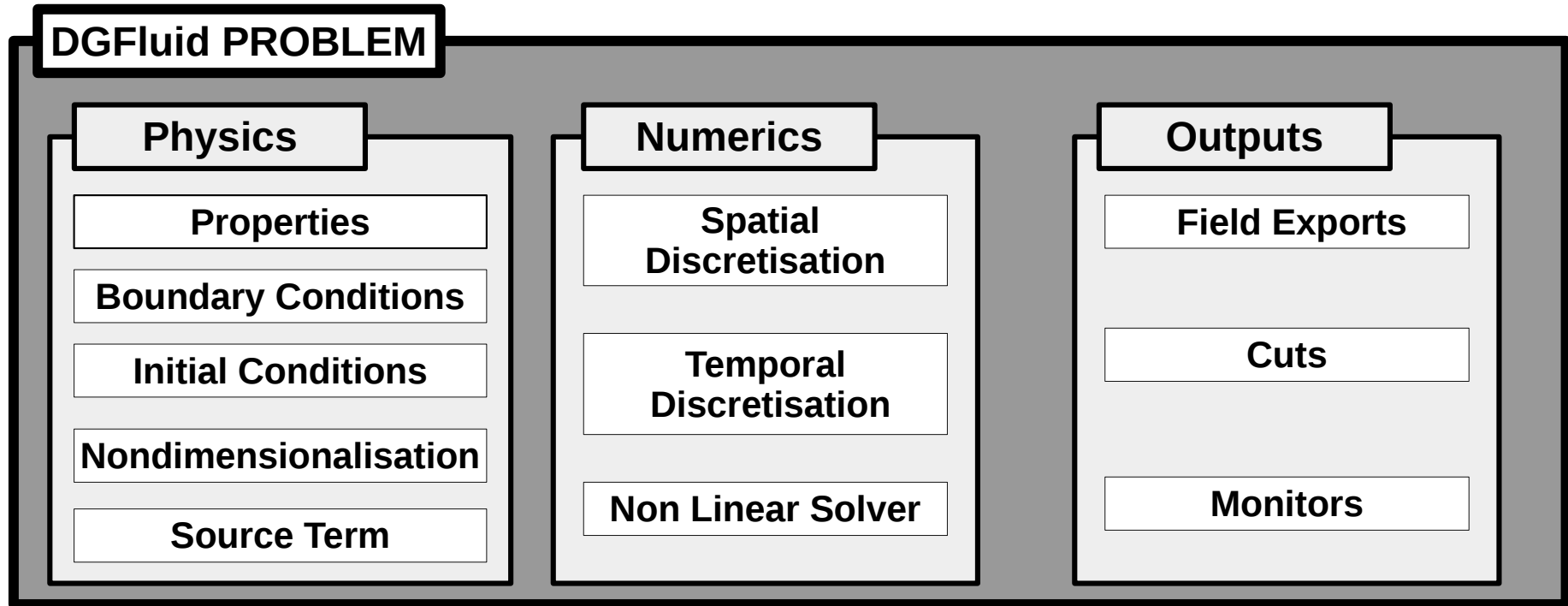
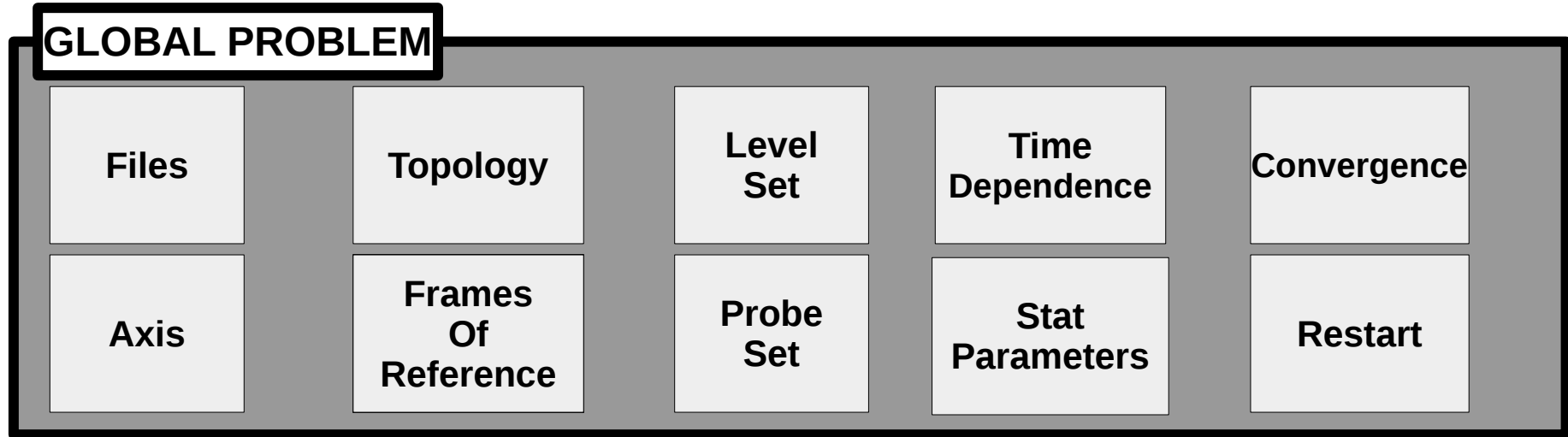
## The Argo Platform



## The Argo Platform

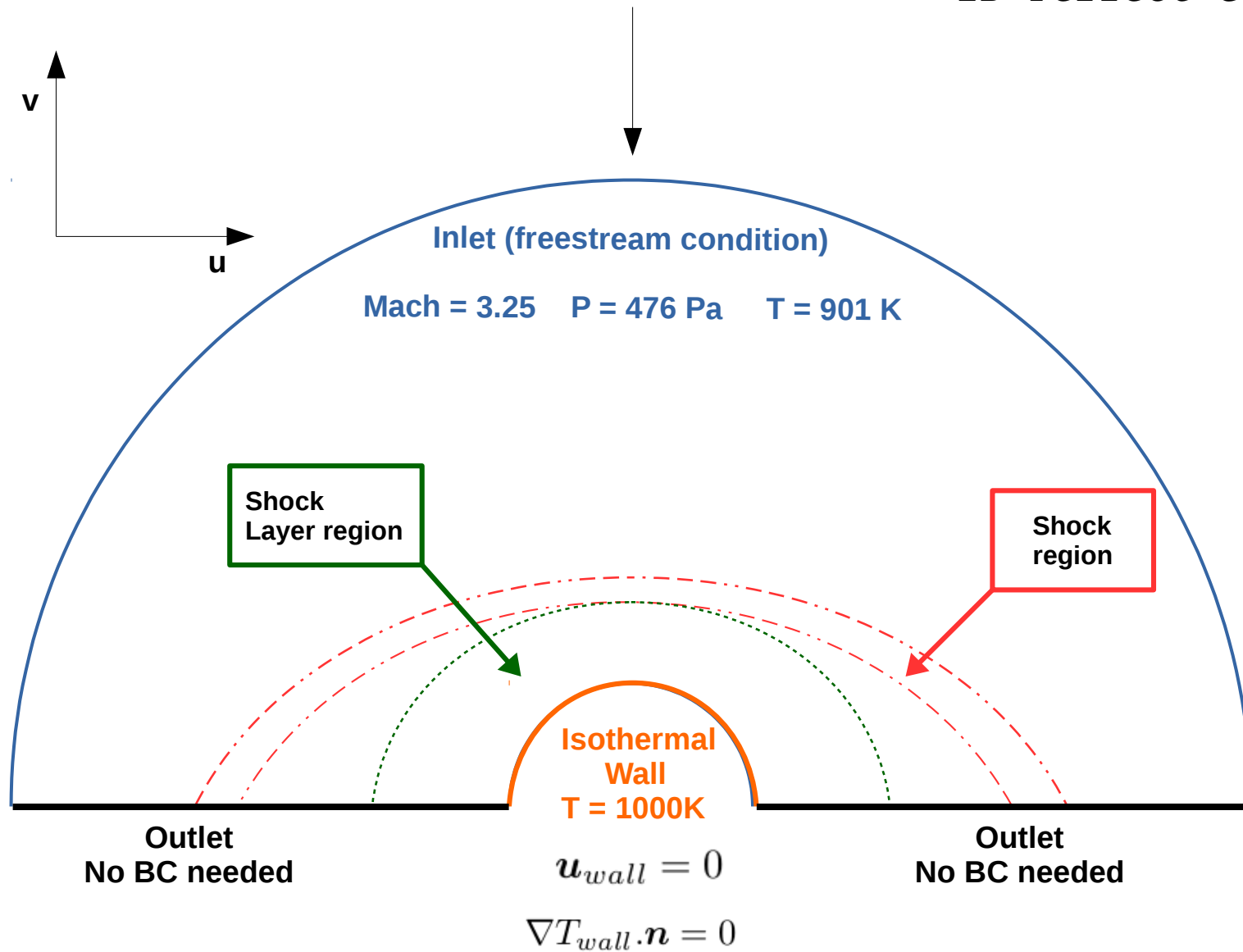


## Structure of the input file



## Test case configuration

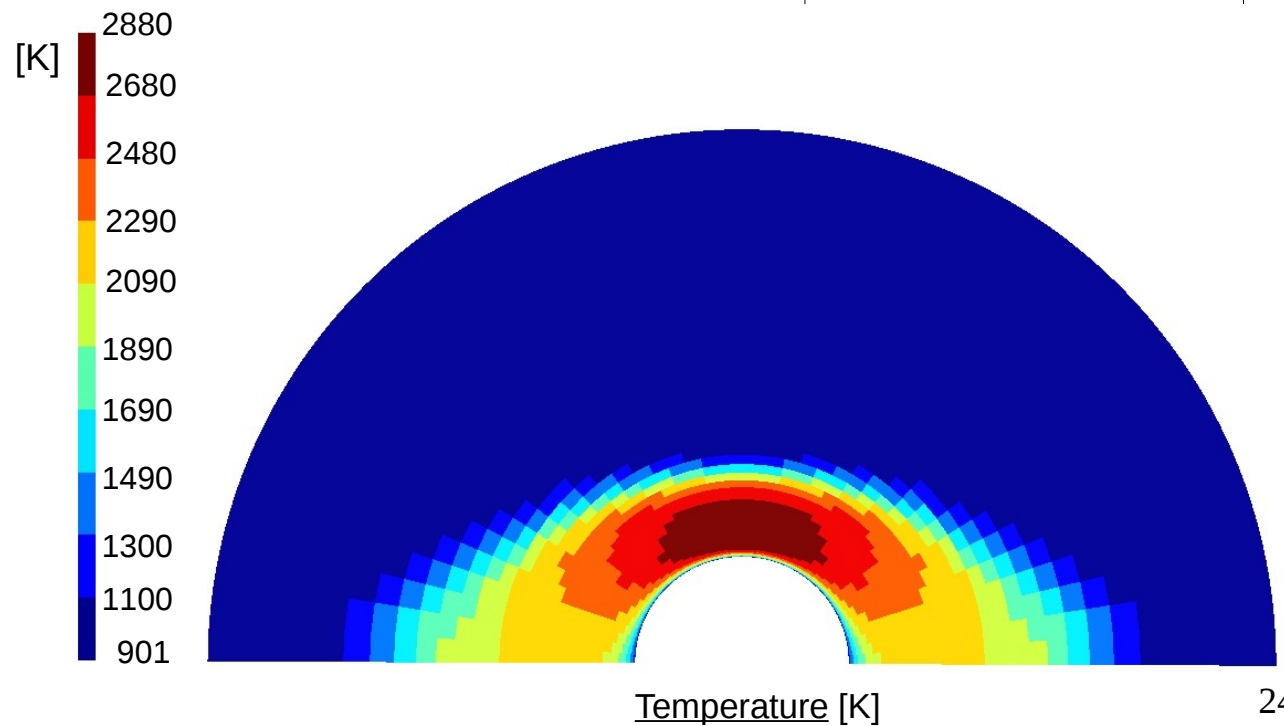
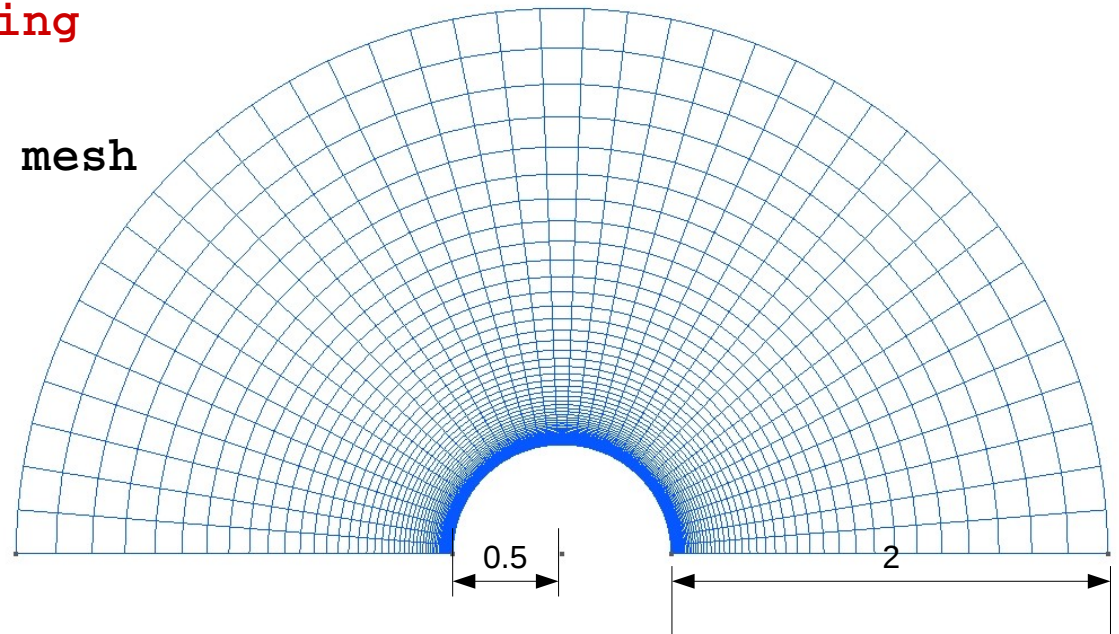
2D Perfect Gas



## First Test P0 (shock capturing method)

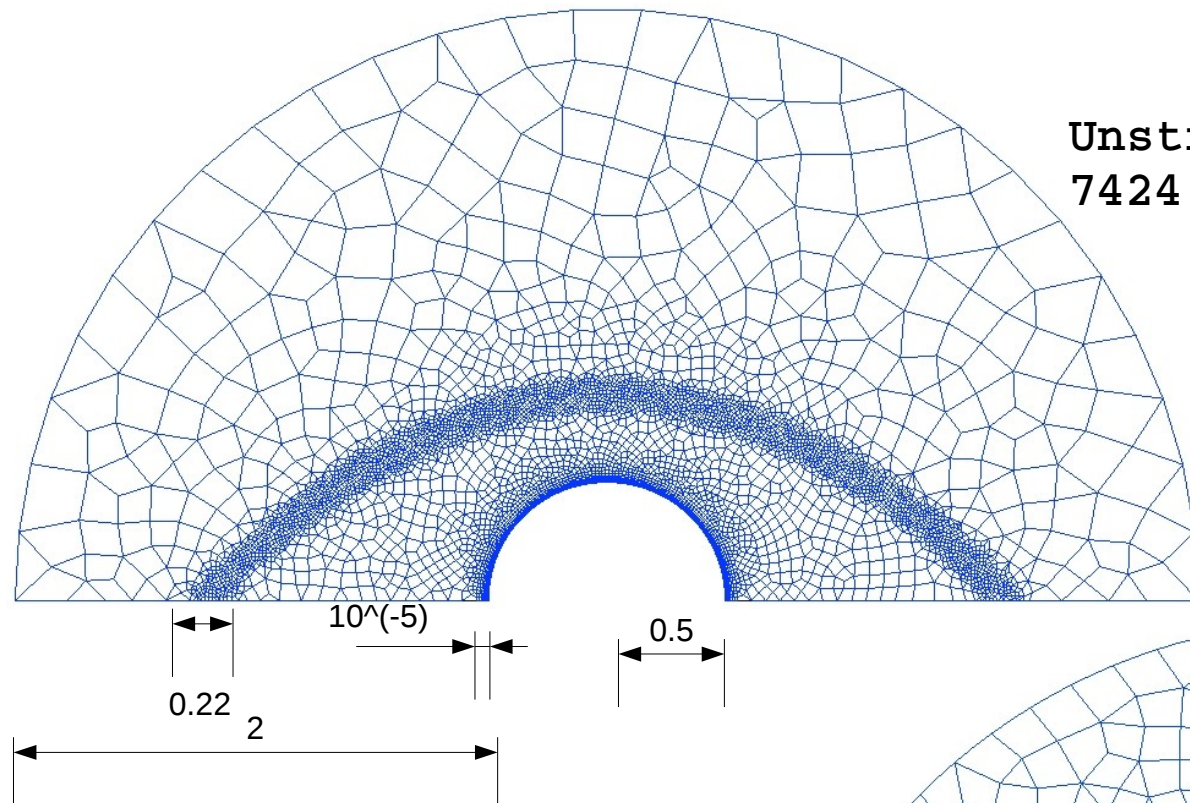
Coarse structured mesh

Method	DG(P=0)
Diffusive flux	BR2
Mesh	3323 elements

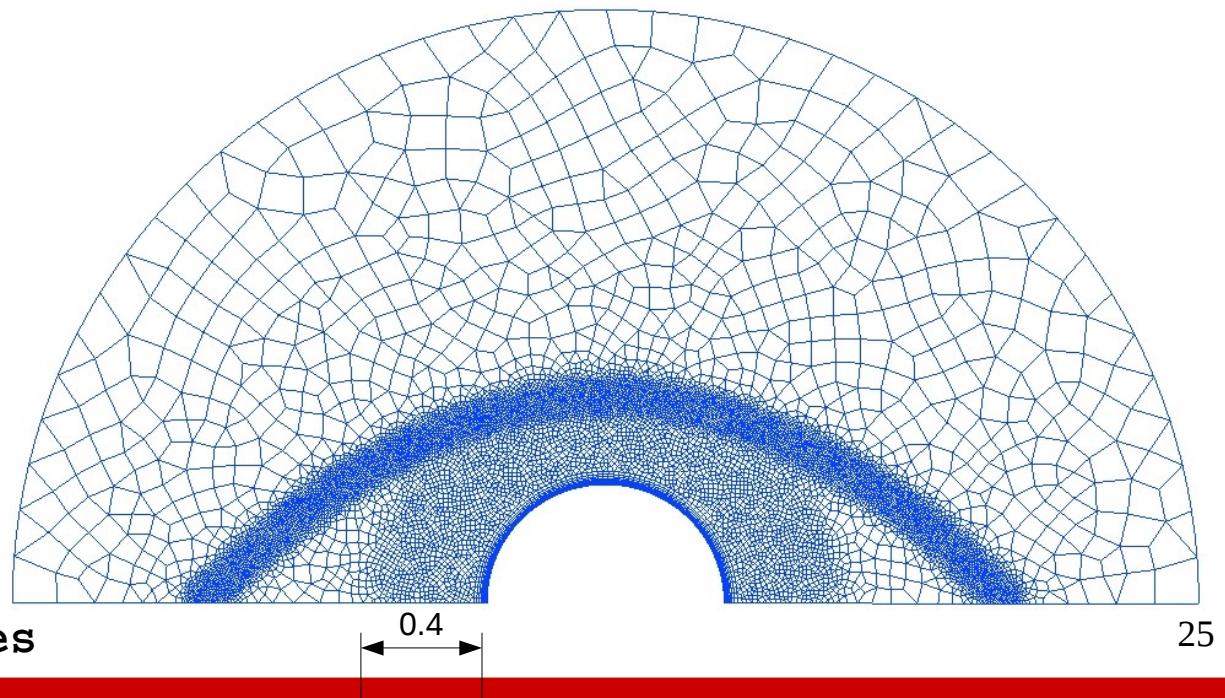




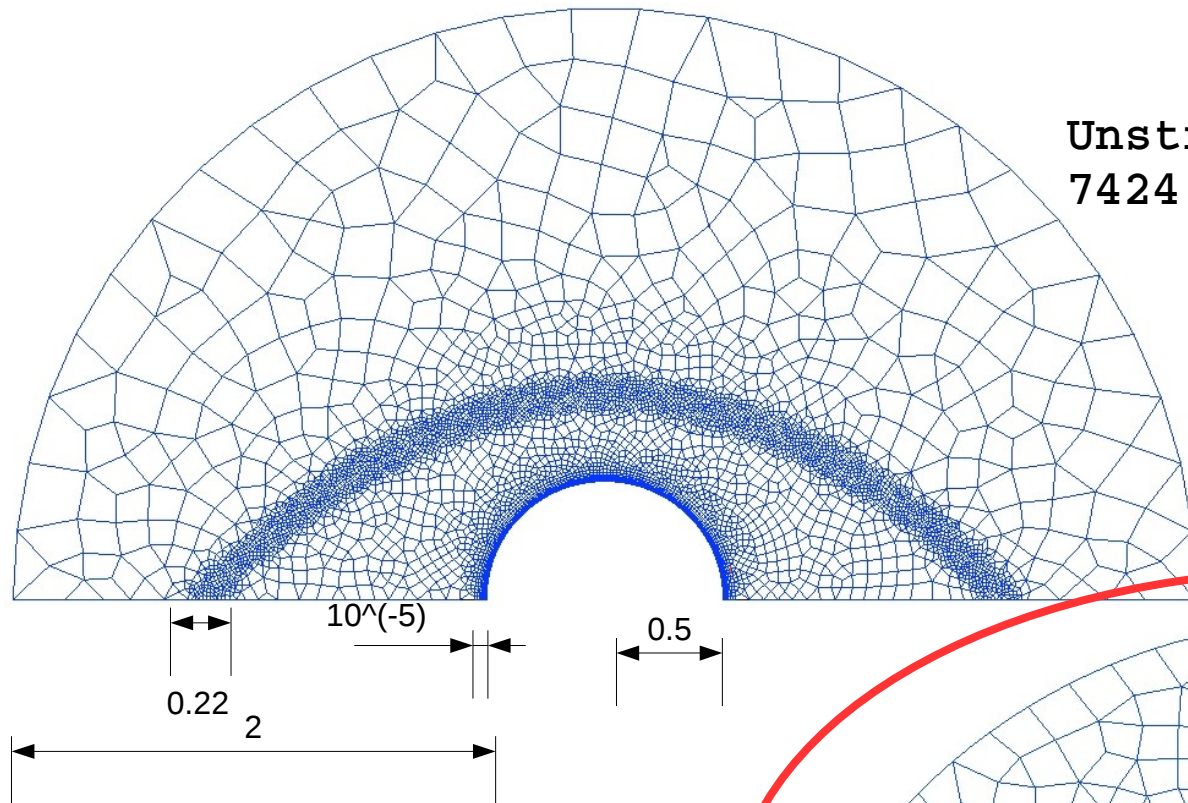
## Refined Meshes (Gmsh)



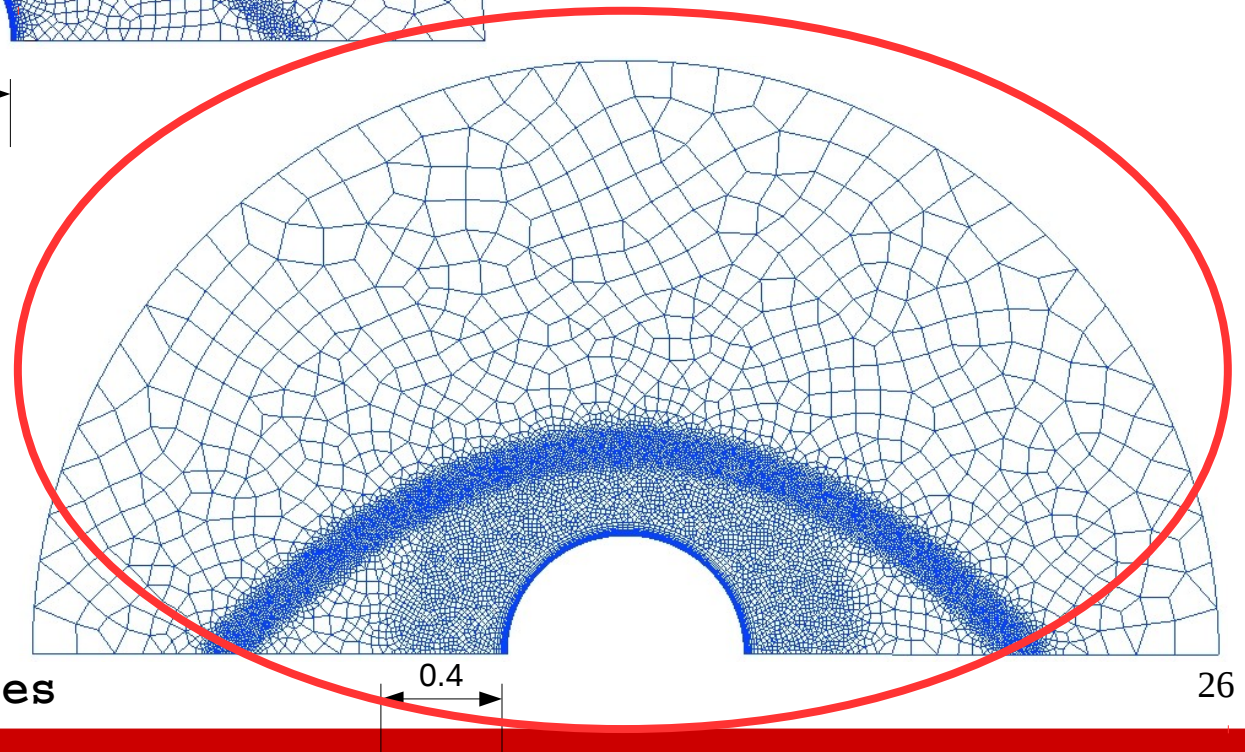
Unstructured mesh  
15 606 elements  
- 2865 triangles  
- 11652 quadrangles



## Refined Meshes (Gmsh)



Unstructured mesh  
7424 elements  
- 1154 triangles  
- 5764 quadrangles

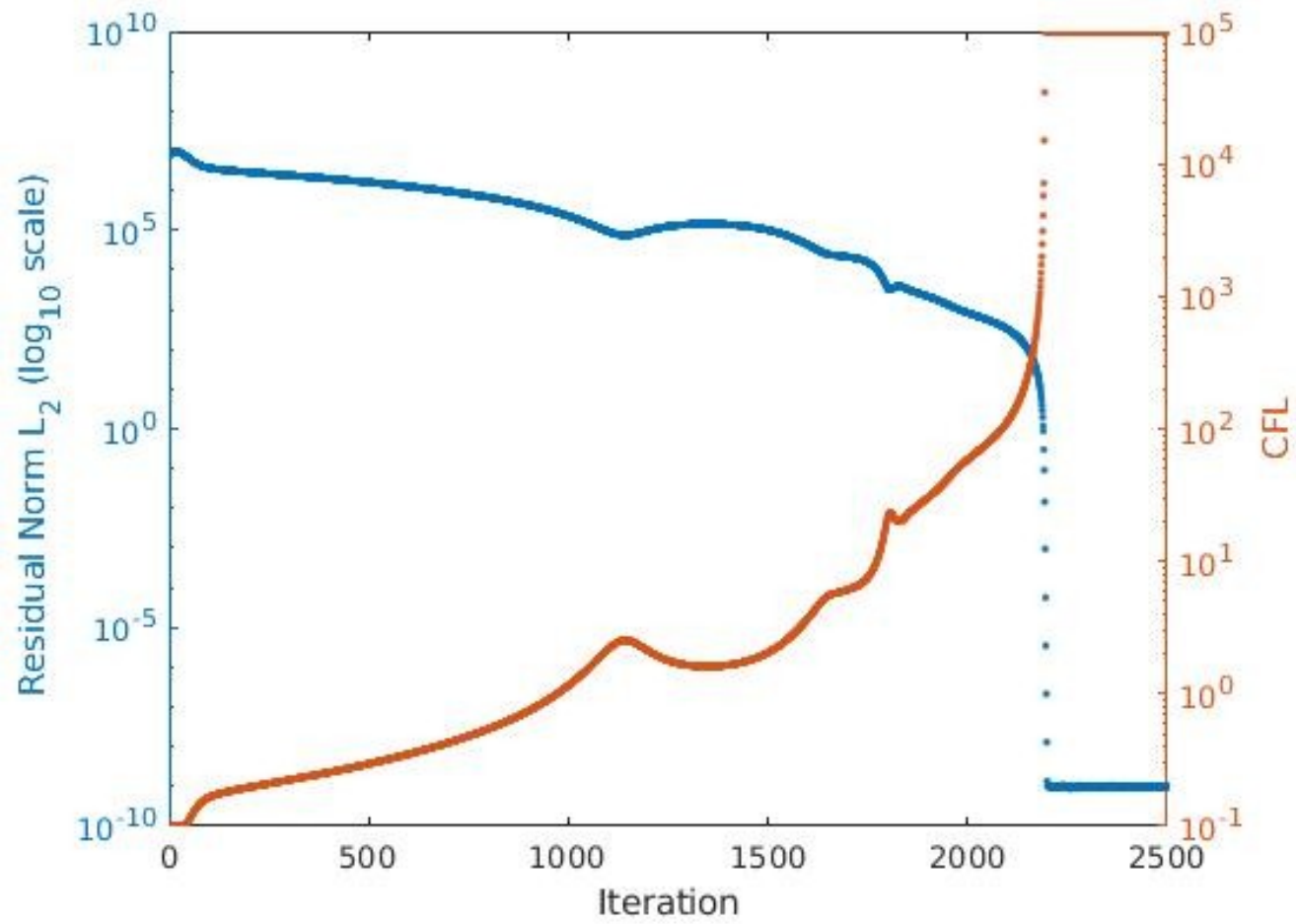


Unstructured mesh  
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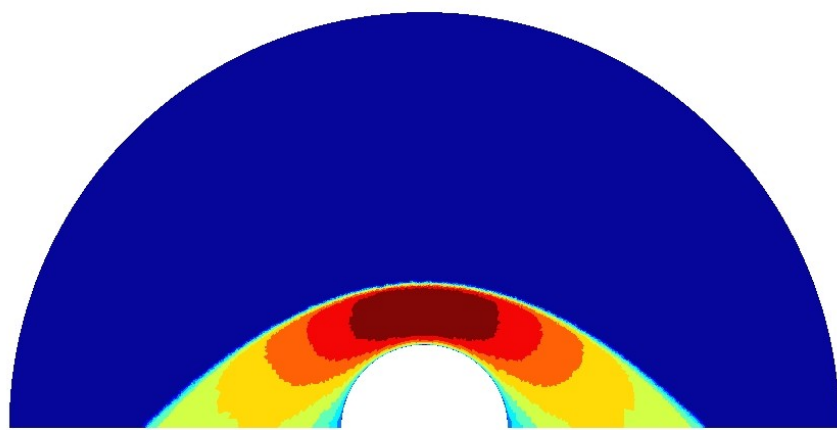


Solution on refined 15606 elements mesh P0

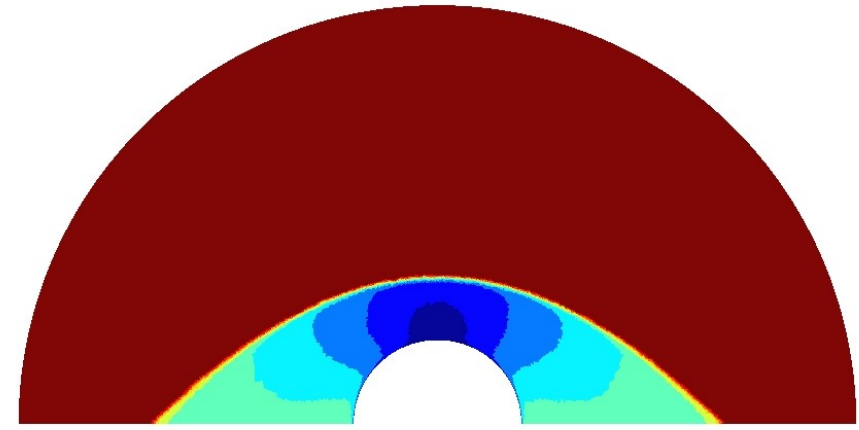
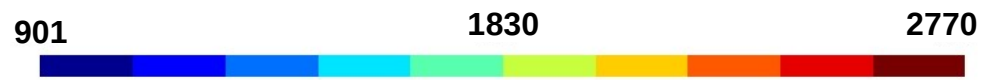
Method	DG(P=0)
Diffusive flux	BR2
Mesh	Refined 15606 elements



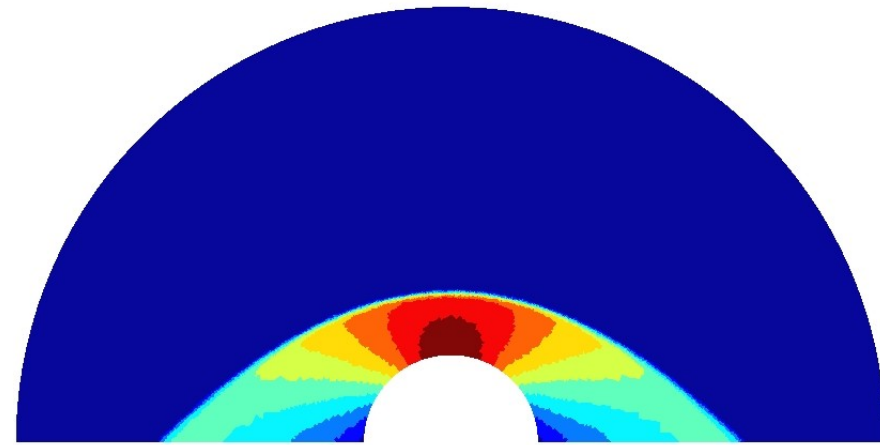
Solution on refined 15606 elements mesh P0



Temperature [K]



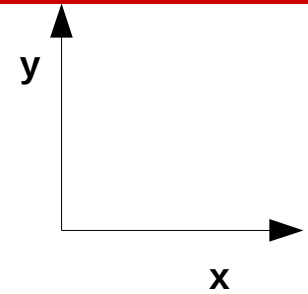
Mach Number



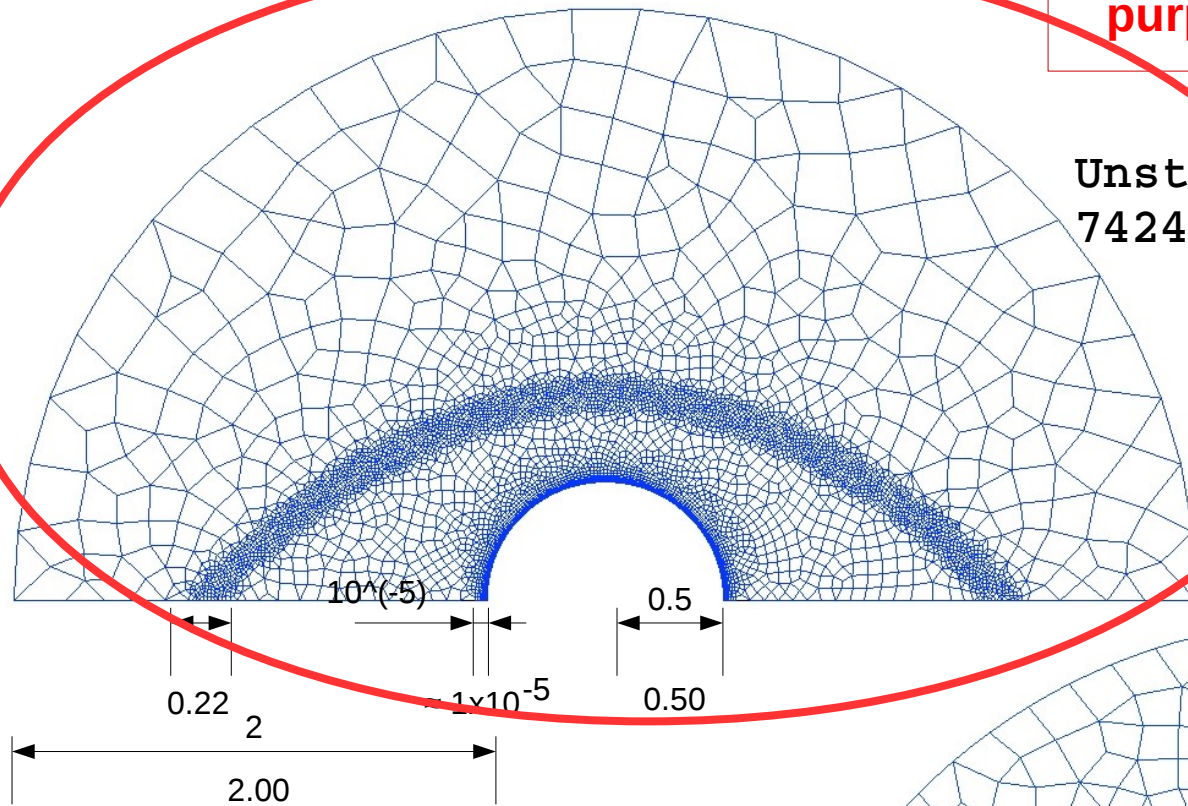
Pressure [Pa]



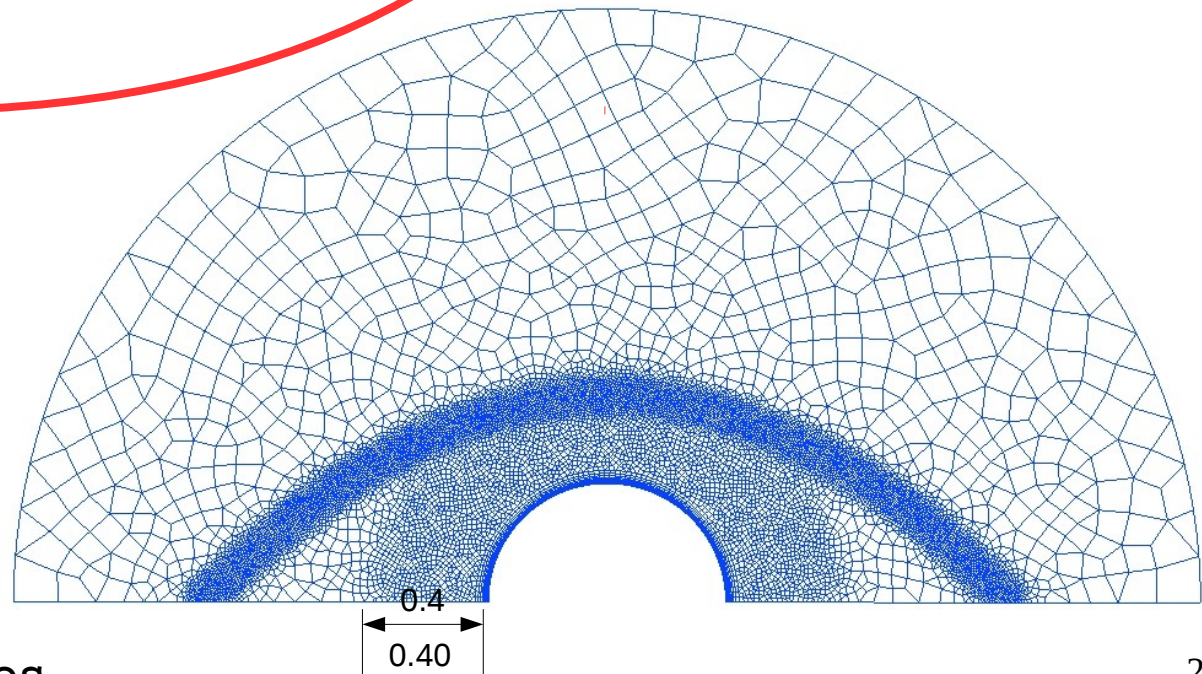
For testing  
purposes



Unstructured mesh  
7424 elements  
- 1154 triangles  
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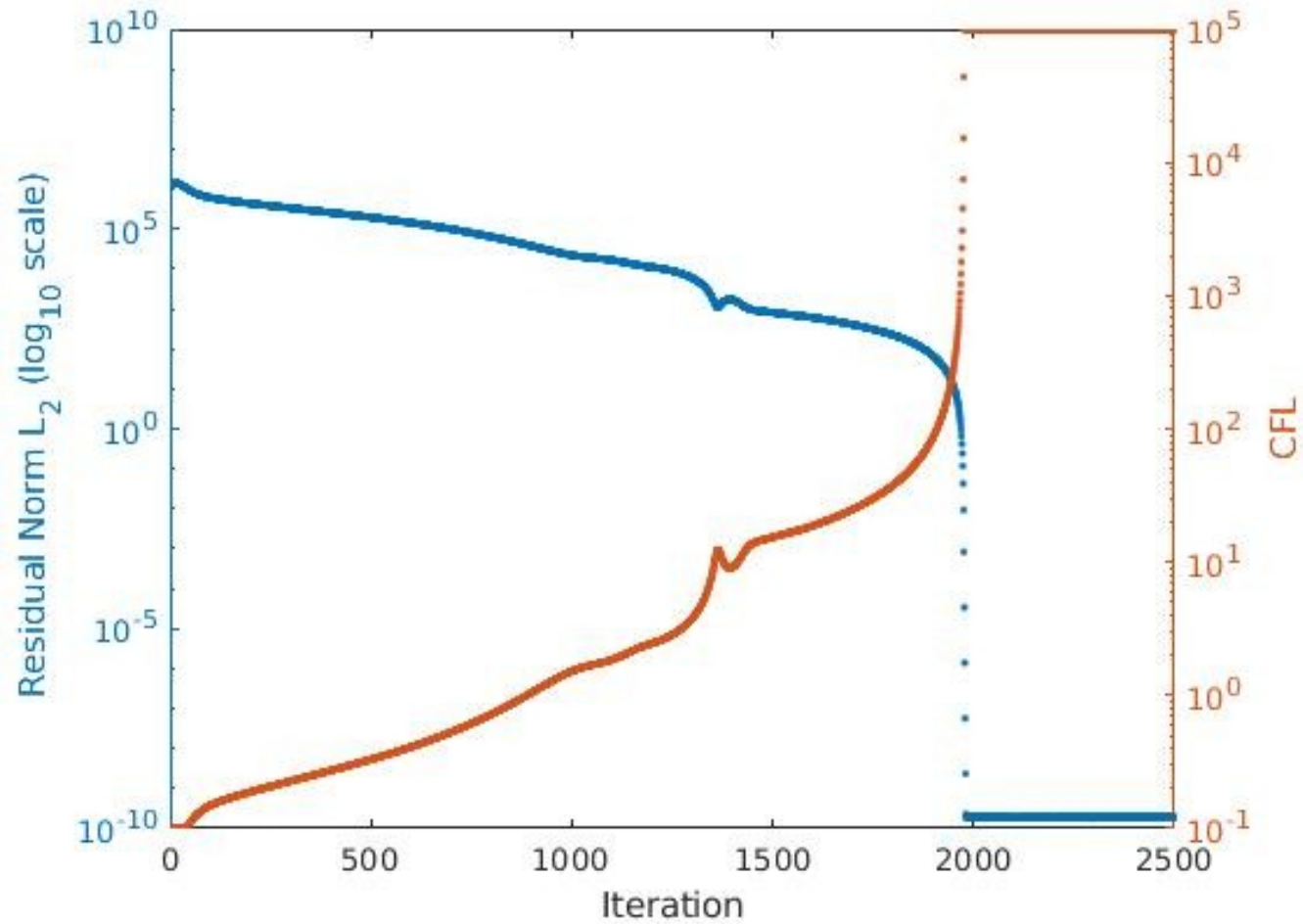


Unstructured mesh  
15 606 elements  
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## Residual on refined 7424 elements mesh P0

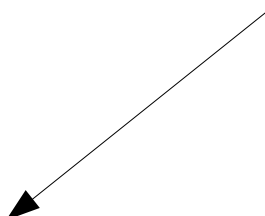
Method	DG(P=0)
Diffusive flux	BR2
Mesh	Refined 7424 elements



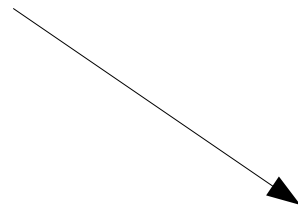
Comparison of the results obtained for the temperature  
And the Mach number with those obtained by Marc Cruellas  
Bordes (using IP+AV in DG(P=1))

### Test case configuration

Parameter	Freestream	Wall	Outlet
Velocity [m/s]	1956	No-slip	NA
Static pressure [Pa]	476	NA	NA
Static temperature [K]	901	1000	NA

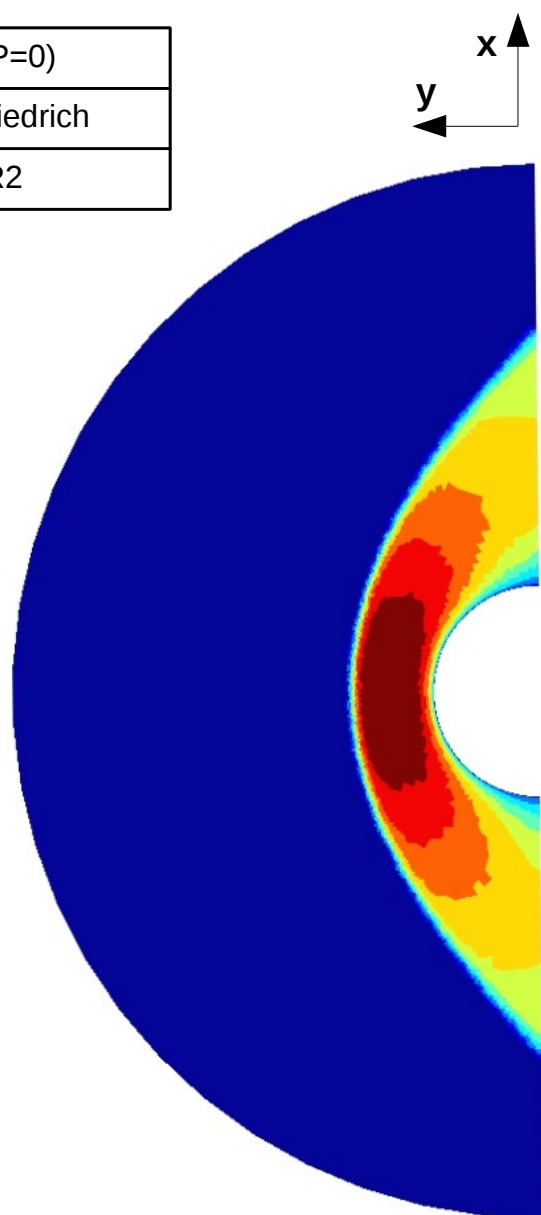
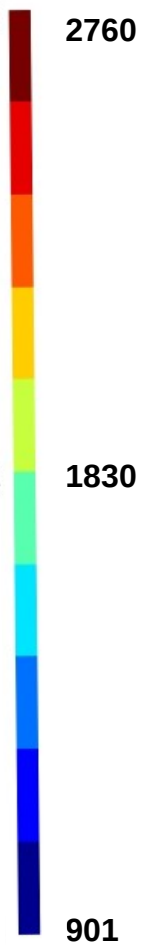


Method	DG(P=0)
Convective flux	Lax Friedrich
Diffusive flux	<b>BR2</b>
Mesh	Refined 7424 elements

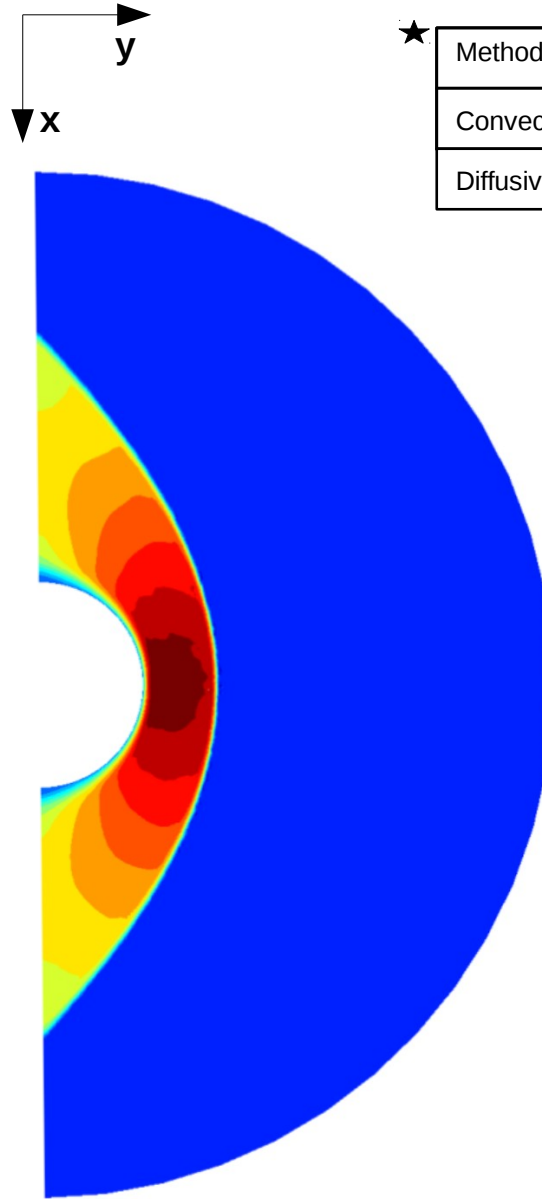
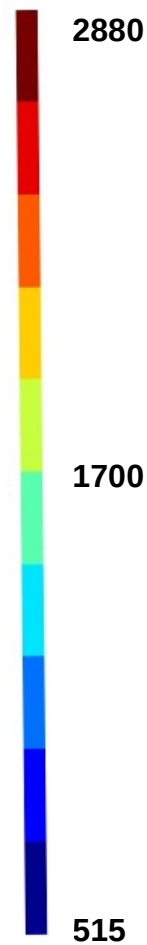


Method	DG(P=1)
Convective flux	Lax Friedrich
Diffusive flux	<b>IP + AV</b>
Mesh	Refined 7424 elements

Method	DG(P=0)
Convective flux	Lax Friedrich
Diffusive flux	BR2



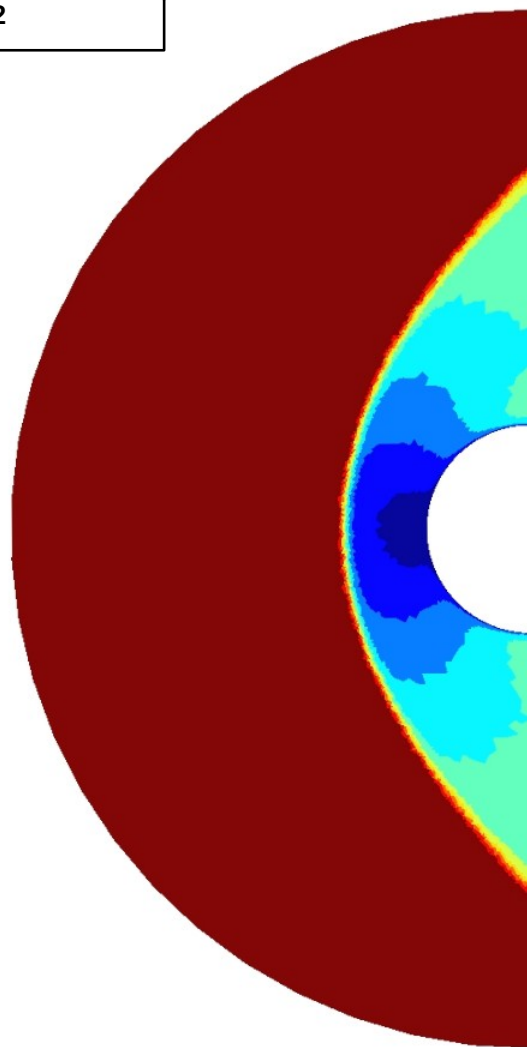
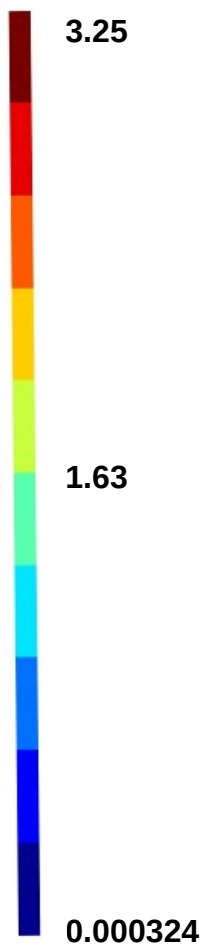
★ Method	DG(P=1)
Convective flux	Lax Friedrich
Diffusive flux	IP + AV



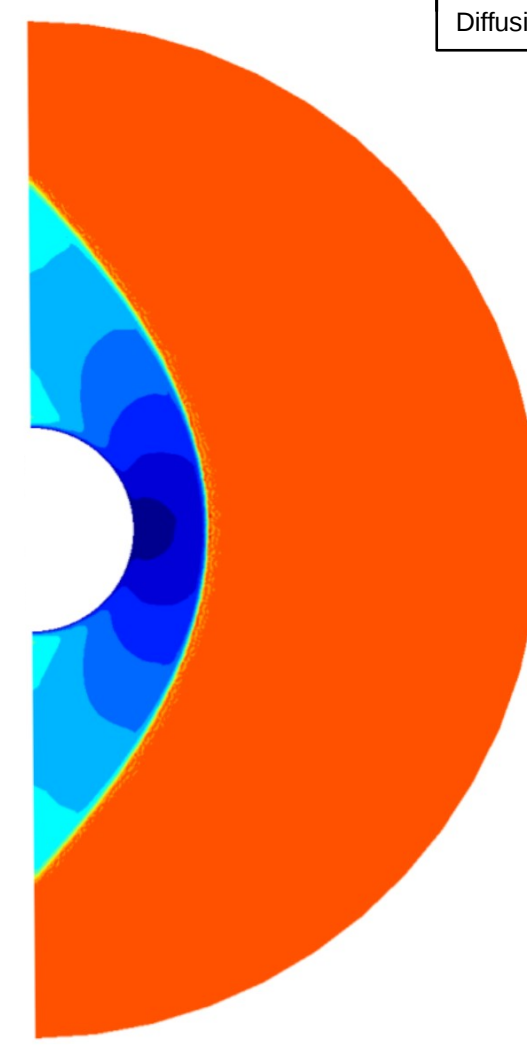
Temperature [K] on refined 7424 elements mesh P0



Method	DG(P=0)
Convective flux	Lax Friedrich
Diffusive flux	BR2



★ Method	DG(P=1)
Convective flux	Lax Friedrich
Diffusive flux	IP + AV



Mach number on refined 7424 elements mesh P0

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## Conclusion & Futur Work

- The BR2 method showed promising results compared to the internal penalty method
- The artificial viscosity requires the tuning of three parameters
- Suggestion of future work :
  - Assess the BR2 method on coarse mesh with different Mach number

## Planning

January	February	March	April	May	June
Installation of the Argo platform + Running some test cases					
	Bibliographic Study				
	Identify the limit of the artificial viscosity				
		Assess the BR2 method in p0 for different hypersonic cases			
			Writing of the Report		

A repository on Github has been created. It contains all the current test cases and results.

[SanaAmri/Argo\\_TestCases](https://github.com/SanaAmri/Argo_TestCases)

# BACKUP SLIDES

## Variational Formulation

Each cell  $K$  is approximate by a polynomial that results from a linear combination of  $N_p$  basis functions  $\phi_i^K$  that are polynomial in the cell  $K$  and equal to zero in  $\Omega_h \setminus K$ .

Find  $w_h \in (v_h^p)^4$  such that  $\forall \phi_i^K, i \in \llbracket 1, N_p \rrbracket, w_h$  is solution of

$$\sum_{K \in \Omega_h} \int_K \phi_i^K \partial_t w_h dV - \sum_{K \in \Omega_h} \int_K (\mathbb{F}_c(w_h) - \mathbb{F}_v(w_h, \Upsilon_h)) \nabla \phi_i^K dv \\ + \sum_{K \in \Omega_h} \oint_{\partial K} \phi_i^K (\hat{\mathbb{F}}_c - \hat{\mathbb{F}}_v) dS = 0$$

$\Upsilon_h$  is an auxiliary variable that represents the gradient  $\nabla w_h$  in the space of discretization

$$v_h^p = \{f \in L^2(\Omega_h) : \phi|_K \in \mathcal{P}^p(K), \forall K \in \Omega_h\}$$

$\mathcal{P}^p(K)$ : Polynomial of degree inferior or equal to  $p$  on  $K$

$$\dim(v_h^p) := N \times N_p$$

$$\dim(\mathcal{P}^p) := \prod_{i=1}^d \frac{(p+i)}{i} = N_p$$

$$\mathbb{F}_v(\mathbf{w}_h, \nabla \mathbf{w}_h) := (G(\mathbf{w}_h) \Upsilon_h)$$

Global lifting operator:

$$\Upsilon_h := \nabla \mathbf{w}_h + R_h(\llbracket \mathbf{w}_h \rrbracket)$$

Local lifting operator:

$$\{G\Upsilon_h\} = \{G\nabla \mathbf{w}_h\} + \{Gr_h^e\}$$

$\eta_r$  : Stabilization parameter

$$\begin{aligned} \mathcal{L}_c(\mathbf{w}_h, \phi^K) = & - \sum_{K \in \Omega_h} \int_K \nabla(\phi^K) \mathbb{F}_c(\mathbf{w}_h) \\ & + \sum_{e \in \epsilon_i} \int_e \llbracket \phi^K \rrbracket \hat{\mathbb{F}}_c(\mathbf{w}_h^+, \mathbf{w}_h^-, \mathbf{n}) \\ & + \sum_{e \in \epsilon_{wall}} \int_e \phi^+ \mathbb{F}_c(\mathbf{w}_{wall}) \end{aligned}$$

$$\begin{aligned} \mathcal{L}_c(\mathbf{w}_h, \phi^K) = & - \sum_{K \in \Omega_h} \int_K \nabla(\phi^K) \mathbb{F}_c(\mathbf{w}_h) \\ & + \sum_{e \in \epsilon_i} \int_e \llbracket \phi^K \rrbracket \hat{\mathbb{F}}_c(\mathbf{w}_h^+, \mathbf{w}_h^-, \mathbf{n}) \\ & + \sum_{e \in \epsilon_{wall}} \int_e \phi^+ \mathbb{F}_c(\mathbf{w}_{wall}) \end{aligned}$$

## Local lifting

$$\int_{K^L \cup K^R} \phi^K r_h^e ([\![\mathbf{w}_h]\!]) dV = \begin{cases} - \int_e \{ \phi^K \} [\![\mathbf{w}_h]\!] \otimes \mathbf{n} dS & \text{if } e \in \epsilon_i \\ - \int_e \phi^{K,+} [\![\mathbf{w}_h]\!] \otimes \mathbf{n} dS & \text{if } e \in \epsilon_{wall} \end{cases}$$

## Global Lifting

$$\sum_{K \in \Omega_h} \int_K \phi^K R_h ([\![\mathbf{w}_h]\!]) dV = - \sum_{e \in \epsilon_i} \int_e \{ \phi^K \} [\![\mathbf{w}_K]\!] \otimes \mathbf{n} ds + \sum_{e \in \epsilon_{wall}} \int_e \phi^{K,+} [\![\mathbf{w}_K]\!] \otimes \mathbf{n} ds$$



Discretisation of the **diffusive term** : The Interior penalty method limitation

Gouverning PDE's expressed in conservative and hypervectorial form:

$$\frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot \mathbf{F}(\mathbf{U}) = \nabla \cdot \mathbf{F}_v(\mathbf{U}, \nabla \mathbf{U}) + \mathbf{S}(\mathbf{U}, \nabla \mathbf{U})$$

Weak form of the equation (DG method):

$$\sum_{\Omega_e} \int_{\Omega_e} v \frac{\partial u}{\partial t} d\Omega_e + \sum_{\Omega_e} \int_{\Omega_e} v \frac{\partial F(u)}{\partial x} d\Omega_e = \sum_{\Omega_e} \int_{\Omega_e} v \frac{\partial}{\partial x} \left( D \frac{\partial u}{\partial x} \right) d\Omega_e$$

$$[v] = v^- n^- + v^+ n^+$$

$$\langle \bullet \rangle = \frac{1}{2} (\bullet^- + \bullet^+)$$

Rewritting the diffusive term as:

$$\begin{aligned} \sum_{\Omega_e} \int_{\Omega_e} v \frac{\partial}{\partial x} \left( D \frac{\partial u}{\partial x} \right) d\Omega_e &= \sum_{\Omega_e} \int_{\Omega_e} \frac{\partial v}{\partial x} \left( D \frac{\partial u}{\partial x} \right) d\Omega_e \\ &\quad - \sum_{\partial\Omega_e} \int_{\partial\Omega_e} \left\langle D(u) \frac{\partial u}{\partial x} \right\rangle [v] dS - \theta \sum_{\partial\Omega_e} \int_{\partial\Omega_e} \left\langle D(u) \frac{\partial v}{\partial x} \right\rangle [u] dS + \alpha \sum_{\partial\Omega_e} \int_{\partial\Omega_e} [v][u] dS \end{aligned}$$

The **interior penalty coefficient**  $\theta$  can take the value -1, 0 or 1.